```
clear;clc;close all

% note: these dynamics are valid only for regular waves, since I haven't
% implemented the convolution integral (memory effect).

plot_hydro = false;
RM5_spring_string = false; % whether RM5 uses a string-spring PTO

disp('Running RM5')
run_wec(5,RM5_spring_string,plot_hydro) % RM5
disp('Running RM3')
run_wec(3,RM5_spring_string,plot_hydro) % RM3
```

Running RM5

```
function run_wec(dof,RM5_spring_string,plot_hydro)
   [gear_ratio, spring_size, omega_test, lambda, T_amp, H, p] = get_numerical_inputs(dof, RM5_spring_string);
   powered = true:
   inner_loop_qty = H;
   run sweep(powered,gear ratio,spring size,omega test,inner loop qty,lambda,plot hydro,p);
   powered = false;
   inner_loop_qty = T_amp;
   run_sweep(powered,gear_ratio,spring_size,omega_test,inner_loop_qty,lambda,plot_hydro,p);
function [gear_ratio, spring_size, omega_test, lambda, T_amp, H, p] = get_numerical_inputs(dof, RM5_spring_string)
   lambda = 50;
   H = [0.02, 0.06, 0.10, 0.136]; % wave heights - from Olivia slack message 8/1/24
   T_{amp} = .2 : .2 : .6; \%1:4; \% torque amplitude for radiation tests (Nm)
   m_{rotor} = .354;
   r_rotor = .087/2;
   I_g = 1/2 * m_rotor * r_rotor^2; % moment of inertia of generator/powertrain
   % parameters
   p = struct('Ig',I_g,...
               'H',H,...
               'tau_max_Nm',4, 'motor_max_rpm',3000,... % motor max torque and speed
               \dots"T_s',0.05, T_d',0.05, b',.1,... % static and dynamic friction torques and viscous friction coefficient
                T_s',0,'T_d',0,'b',0,...
               'dof',dof,'string_spring',RM5_spring_string);
   % set gear ratios and springs to sweep over
   if dof==5
       gear ratio = 1 : 2 : 9; % gear ratio range
   elseif dof==3
       pinion radius = 0.010 : .005 : 0.025; % m
       gear_ratio = 1./pinion_radius; % 1/m
   end
   if dof == 3 || ~RM5_spring_string
       spring_size = 0;
    elseif dof == 5 && RM5_spring_string
       spring_size = 1:1:10; % constant force spring size [N-m]
   \% set frequencies to sweep over
   % g = 9.8;
   % depth = 1.36; % Oregon tank depth [m]
   % w_min_deepwater = sqrt(2*g./depth);
   % w_max = 10; % rad/s
   % omega_idx_min = find(w_scaled > w_min_deepwater,1,'first');
   % omega_idx_max = find(w_scaled < w_max,</pre>
   % omega_idxs = omega_idx_min : omega_idx_max;
   omega_test = [7.07, 8.49, 9.83]; % override with actual test values
function [] = run_sweep(powered,gear_ratio,spring_size,omega_test,inner_loop_qty,lambda,plot_hydro,p)
   [w_scaled, A_scaled, B_scaled, K_scaled, gamma_scaled] = coeffs(p.dof,lambda,plot_hydro);
   if p.dof == 5
       K_scaled = 0.8580; % override since K_scaled is somehow negative
        I_scaled = 0.0372; % override to match actual ptype moment of inertia
       mI_A_scaled = A_scaled + I_scaled;
   elseif p.dof == 3
       m scaled = 1.208;
       mI_A_scaled = A_scaled + m_scaled;
   w_diff = abs(w_scaled - omega_test');
   [~,omega_idxs] = find(w_diff == min(w_diff,[],2));
   omegas = w_scaled(omega_idxs);
   if powered
        powered_label = 'powered';
        inner_loop_label = 'H - regular wave height (m)';
   else
```

```
powered_label = 'forced oscillation';
    inner_loop_label = 'Generator torque amplitude (Nm)';
end
RM_label = [', RM' num2str(p.dof)];
non_slack_combo = zeros(length(gear_ratio),length(spring_size),length(omega_idxs),length(inner_loop_qty));
max_motor_torque = zeros(length(gear_ratio),length(spring_size),length(omega_idxs),length(inner_loop_qty));
                 = zeros(length(gear_ratio),length(spring_size),length(omega_idxs),length(inner_loop_qty));
amplitude
                 = zeros(length(gear_ratio),length(spring_size),length(omega_idxs),length(inner_loop_qty));
plot_timeseries = false;
[spring_mesh, omega_mesh] = meshgrid(spring_size,omegas);
p.Kh = K_scaled; % hydrodynamic stiffness
fig_start_number = numel(findobj('Type', 'figure'));
for i = 1:length(gear_ratio)
    p.GR = gear_ratio(i); % gear ratio
    if p.dof == 5
        GR_label = ['GR=' num2str(gear_ratio(i))];
        GR_label = ['Pinion radius = ' num2str(1000/gear_ratio(i)) ' mm'];
    for j = 1:length(spring size)
        p.T_spring = spring_size(j); % spring torque
if p.dof == 5 && p.string_spring
    spring_label = [', spring = ' num2str(spring_size(j)) ' Nm'];
        else
            spring_label = '';
        end
        for k = 1:length(omega_idxs)
            omega_idx = omega_idxs(k);
            p.Bh = B_scaled(1,omega_idx); % hydrodynamic damping
            p.I = mI_A_scaled(1,omega_idx); % moment of inertia of flap
            p.w = w_scaled(1,omega_idx); % wave frequency
            for inner_idx = 1:length(inner_loop_qty)
                if powered
                    % impedance matching
                    p.Kp = p.I * p.w^2 - p.Kh;
                    p.Bp = p.Bh;
                    H = inner_loop_qty(inner_idx);
                    p.Fh = H/2 * gamma_scaled(1,omega_idx); % exciting force amplitude
                    odefun = @(t,y,yp)dynamics_power(t,y,yp,p);
                    p.T_gen_amplitude = inner_loop_qty(inner_idx);
                    odefun = @(t,y,yp)dynamics_radiation(t,y,yp,p);
                [non_slack_combo(i,j,k,inner_idx), ...
                    max_motor_torque(i,j,k,inner_idx),...
                    amplitude(i,j,k,inner_idx),...
                    power(i,j,k,inner_idx) ] = run_sim(odefun,p,plot_timeseries);
            end
        end
        \ensuremath{\mathrm{\%}} results for this GR and spring, over each frequency and amplitude
        each_test_non_slack = squeeze(non_slack_combo(i,j,:,:))';
        each_test_torque = squeeze(max_motor_torque(i,j,:,:))';
        each_test_amplitude = squeeze(amplitude(i,j,:,:))';
        each_test_power
                           = squeeze(power(i,j,:,:))';
        % titles
        GR_spring_title = [GR_label spring_label];
        omegas_label = 'Frequency rad/s';
        \ensuremath{\mathrm{\%}} plots for this GR and spring, over each frequency and amplitude
        subplot_number = i + (j-1)*(length(gear_ratio));
        f1 = figure(fig_start_number + 1);
        subplot(length(spring_size),length(gear_ratio),subplot_number)
        sgtitle(['Max Motor Torque (Nm), ' powered_label RM_label])
        plot_results(omegas,omegas_label, inner_loop_qty,inner_loop_label, each_test_torque, GR_spring_title,[0 p.tau_max_Nm])
        f2 = figure(fig_start_number + 2);
        f2.WindowState = 'maximized';
        subplot(length(spring_size),length(gear_ratio),subplot_number)
        sgtitle(['WEC amplitude, ' powered_label RM_label])
        plot_results(omegas,omegas_label, inner_loop_qty,inner_loop_label, each_test_amplitude,GR_spring_title,[0 max(each_test_amplitude,[], 'all')])
        f3 = figure(fig_start_number + 3);
        f3.WindowState = 'maximized':
        subplot(length(spring_size),length(gear_ratio),subplot_number)
        sgtitle(['WEC power (W), ' powered_label RM_label])
        plot_results(omegas_nomegas_label, inner_loop_qty,inner_loop_label, each_test_power, GR_spring_title,[0 max(each_test_power,[],'all')])
        if p.dof == 5 && p.string_spring
```

```
f4 = figure(fig_start_number + 4);
               f4.WindowState = 'maximized':
               subplot(length(spring_size),length(gear_ratio),subplot_number)
               sgtitle(['Acceptable combinations for preventing slackness, ' powered_label RM_label])
               plot_results(omegas,omegas_label, inner_loop_qty,inner_loop_label, each_test_non_slack,GR_spring_title,[0 1])
           each_test_non_slack(isnan(each_test_non_slack)) = 0;
           each_test_torque(isnan(each_test_torque)) = 0;
           all_tests_ok = all(each_test_non_slack & each_test_torque<=p.tau_max_Nm,'all');</pre>
   % overall comparison of which GRs and springs work for every test
       GR_label = 'Pinion radius (mm)';
       x_GR = 1000./gear_ratio;
   elseif p.dof == 5
       GR_label = 'GR (-)';
       x_GR = gear_ratio;
   end
   figure
   \verb|plot_results|(x\_GR,GR_label,spring_size,'spring_torque_(Nm)',all_tests_ok,...|
       ['Acceptable for all tests - ' powered_label RM_label],[0 1])
function plot_results(x,x_label,y,y_label,z,z_title,z_lim)
   h = imagesc(x, y, z);
   colorbar
   xlabel(x_label)
   ylabel(y_label)
   title(z_title)
   if z_lim(1) ~= z_lim(2) && all(~isnan(z_lim))
       clim(z_lim)
   end
   draw_lines(x,y)
   set(h, 'AlphaData', ~isnan(z))
function [non_slack, max_motor_torque, amplitude, power] = run_sim(odefun,p,plot_timeseries)
   % ode inputs
   T = 2*pi/p.w;
   y0 = [0;0];
   yp0 = [0;0];
   tspan = [0 5*T];
   % ode solve
   options = odeset('MaxStep',T/20);
   %[y0,yp0] = decic(odefun, 0, y0, [1,1], yp0, [0,0]);
   sol = ode15i(odefun,tspan,y0,yp0,options);
   t = linspace(tspan(1),tspan(end));
   try
       [v,vp] = deval(sol,t);
       [err,P,T_gen,T_fric,T_string] = odefun(t,y,yp);
       if p.dof == 5 && p.string_spring && any(T_string <= 0)</pre>
           non_slack = false;
           max motor torque = NaN;
           %fprintf('UNACCEPTABLE GR %f and Spring Force %f and Frequency %f\n',gear_ratio(i),spring_size(j),w_scaled(1,omega_idx))
       else
           non_slack = true;
           max_motor_torque = max(abs(T_gen));
           %fprintf(' ACCEPTABLE GR %f and Spring Force %f and Frequency %f\n',gear_ratio(i),spring_size(j),w_scaled(1,omega_idx))
           if plot_timeseries
               % plot solution
               figure
               plot(t,y, t,T_gen, t,T_fric, t,T_string, t,P)
               xlabel('Time (s)')
               legend('$\theta$','$\dot{\theta}$','$T_{gen}$','$T_{fric}$','$T_{string}$', ...
                   'P', 'interpreter', 'latex', 'FontSize', 14)
               figure
               xlabel('Time (s)')
               ylabel('Integration Error')
               plot(t,err(1,:),t,err(2,:))
               legend('err_T (Nm)','err_v (m/s)')
           end
       power = max(P);
       amplitude = max(y(1,:)) - min(y(1,:));
   catch exception
       non_slack = NaN;
           max_motor_torque = NaN;
```

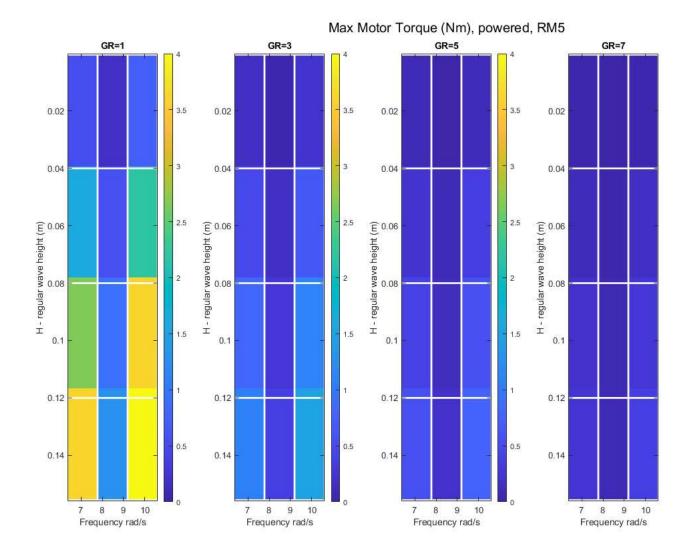
```
power = NaN;
               amplitude = NaN;
          else
               rethrow(exception);
          end
     end
end
function draw_lines(x,y)
     hold on
     if length(x)>1
         d_x = diff(x(1:2))/2;
         d_x = .5;
     if length(y)>1
         d_y = diff(y(1:2))/2;
          d_y = .5;
     end
    for xi = x
         \verb|plot(d_x+[xi\ xi],[min(y)-d_y\ max(y)+d_y],'w','LineWidth',2) \% \ vert \ line \\
    xlim([min(x)-d_x, max(x)+d_x])
     for yi = y
         plot([min(x)-d\_x\ max(x)+d\_x],d\_y+[yi\ yi],'w','LineWidth',2)\ \%\ horz\ line
    ylim([min(y)-d_y, max(y)+d_y])
\ensuremath{\text{\%}} dynamics for forced oscillation radiation test
function [err,P,T_gen,T_fric,T_string] = dynamics_radiation(t,y,yp,p)
     T_gen_cmd = p.T_gen_amplitude * sin(p.w * t);
     T_exc = 0;
     [\texttt{err}, \texttt{P}, \texttt{T}\_\texttt{gen}, \texttt{T}\_\texttt{fric}, \texttt{T}\_\texttt{string}] = \texttt{dynamics}(\texttt{T}\_\texttt{exc}, \texttt{T}\_\texttt{gen}\_\texttt{cmd}, \texttt{t}, \texttt{y}, \texttt{yp}, \texttt{p});
\ensuremath{\mathrm{\%}} dynamics for impedance controlled power generation
function [err,P,T_gen,T_fric,T_string] = dynamics_power(t,y,yp,p)
    th = y(1,:);
    th_dot = y(2,:);
    % effective gear ratio
    alpha = 0; % fixme - should be a function of theta
    GR_eff = p.GR * cos(alpha);
    T_gen_cmd = -(p.Kp * th + p.Bp * th_dot) / GR_eff; % fixme
    % hydro excitaton torques on flap
    T_{exc} = p.Fh * sin(p.w * t);
     [\texttt{err}, \texttt{P}, \texttt{T}\_\texttt{gen}, \texttt{T}\_\texttt{fric}, \texttt{T}\_\texttt{string}] = \texttt{dynamics}(\texttt{T}\_\texttt{exc}, \texttt{T}\_\texttt{gen}\_\texttt{cmd}, \texttt{t}, \texttt{y}, \texttt{yp}, \texttt{p});
end
\ensuremath{\text{\%}} shared dynamics function - equation of motion
function [err,P,T_gen,T_fric,T_string] = dynamics(T_exc,T_gen_cmd,t,y,yp,p)
    % states
     th = y(1,:);
     th_dot = y(2,:);
    th_dot_next = yp(1,:);
    th_ddot = yp(2,:);
     % effective gear ratio
    alpha = 0; % fixme - should be a function of theta
    GR_eff = p.GR * cos(alpha);
     % hydro and interial torques
     T_hydro = p.Kh * th + p.Bh * th_dot;
     T_inertia = p.I * th_ddot;
     % string torque on drivetrain
     T_string = (T_inertia + T_hydro - T_exc) / GR_eff;
     if p.dof == 5 && p.string_spring
         T_string(T_string < 0) = 0;
    end
    % generator torque limiting
     \label{eq:T_gen} T\_gen = min(max(T\_gen\_cmd/p.tau\_max_Nm, -1), 1) * p.tau\_max_Nm; \\ motor\_rpm = GR\_eff * th\_dot * 60/(2*pi); 
     T_gen(abs(motor_rpm) > p.motor_max_rpm) = 0;
    % friction
```

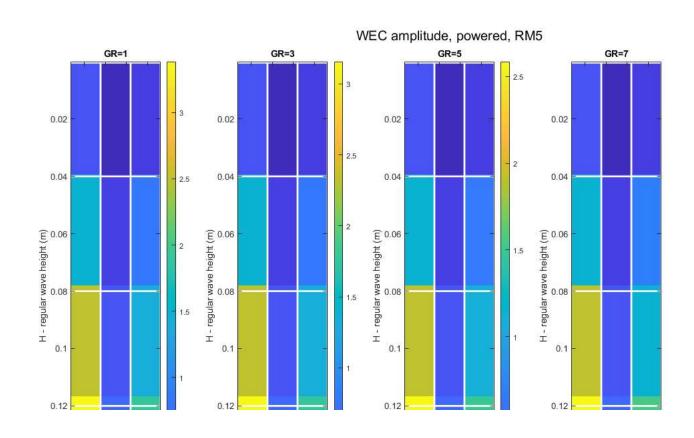
```
zero_speed_idxs = ismembertol(th_dot,0);
net_trq_without_fric = T_gen - T_string + p.T_spring;
T_static = min(p.T_s,abs(net_trq_without_fric)) .* sign(net_trq_without_fric);
T_dynamic = p.T_d * sign(th_dot) + p.b * GR_eff * th_dot;
T_fric = zeros(size(T_gen));
T_fric(zero_speed_idxs) = T_static(zero_speed_idxs);
T_fric(~zero_speed_idxs) = T_dynamic(~zero_speed_idxs);

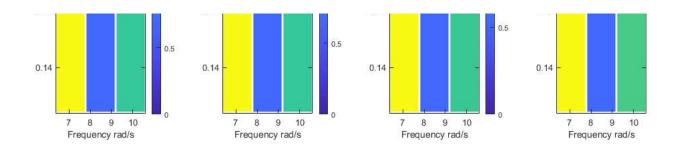
% unbalanced torque on drivetrain
T_unb = p.Ig * GR_eff * th_ddot - T_gen + T_fric + T_string - p.T_spring;
err = [T_unb; th_dot - th_dot_next];

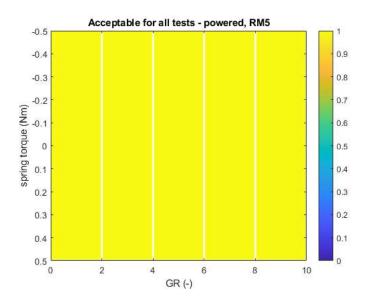
% power
P = T_gen .* th_dot * GR_eff;
end
```

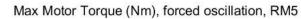
Running RM3

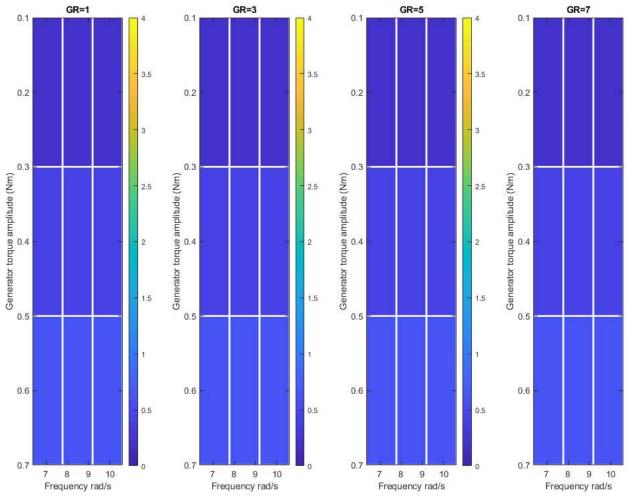


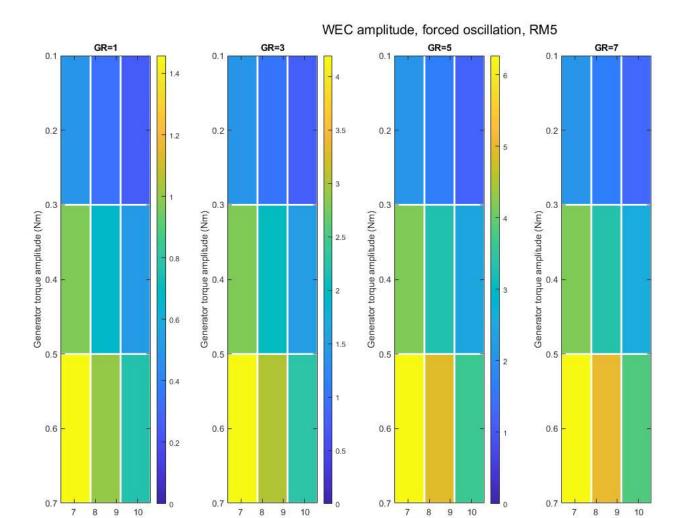










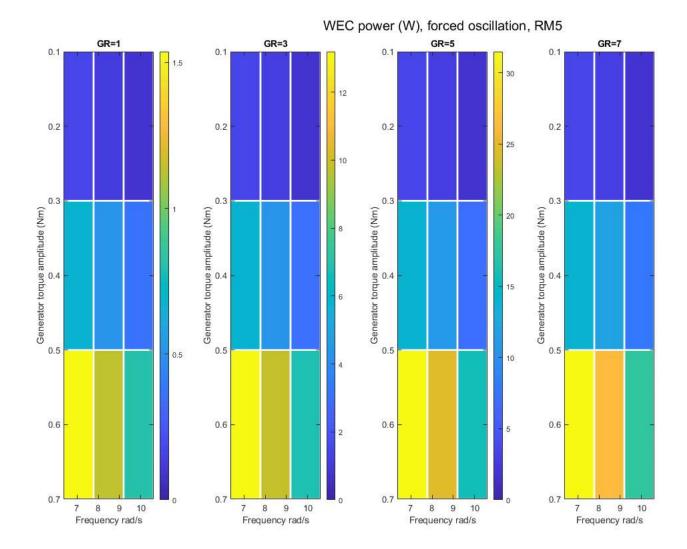


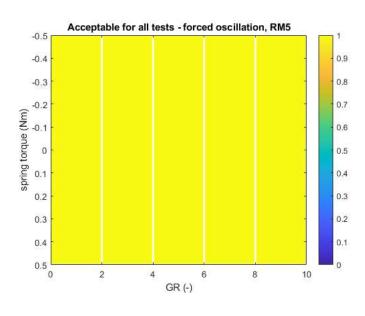
Frequency rad/s

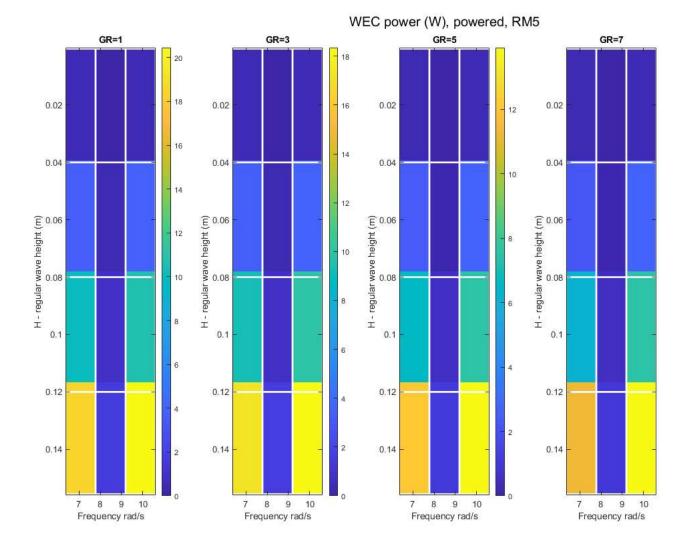
Frequency rad/s

Frequency rad/s

Frequency rad/s







Max Motor Torque (Nm), powered, RM3 Pinion radius = 10 mm Pinion radius = 15 mm Pinion radius = 20 mm 3.5 3.5 3.5 0.02 0.02 0.02 3 3 3 0.04 0.04 0.04 H - regular wave height (m) 2.5 H - regular wave height (m) 2.5 H - regular wave height (m) 2.5 1.5 1.5 1.5 0.1 0.1 0.1 0.12 0.12 0.12 0.5 0.5 0.5

8

Frequency rad/s

10

0.14

8

9

Frequency rad/s

10

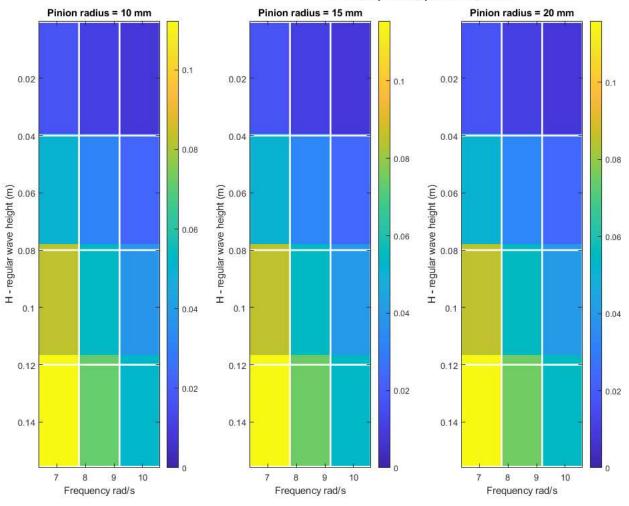
0.14

10

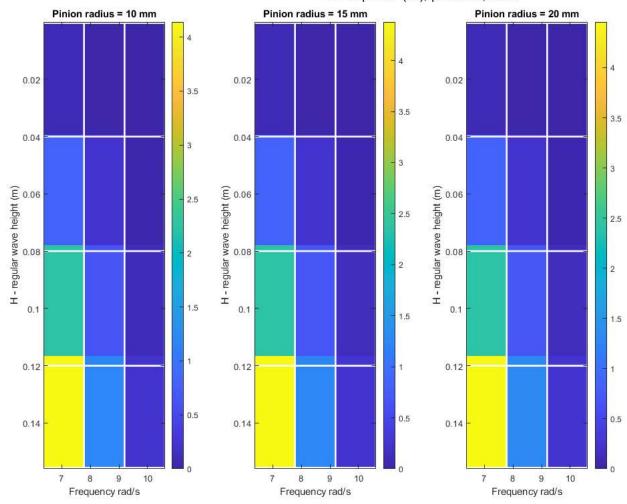
8 9 Frequency rad/s

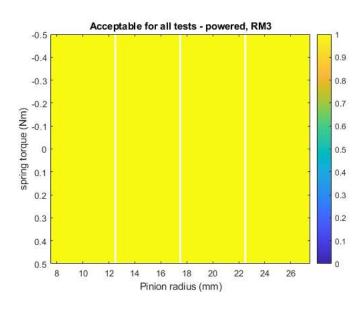
0.14

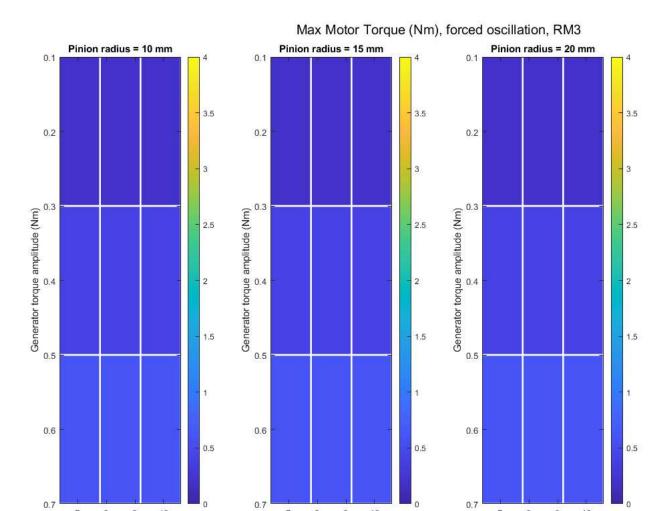
WEC amplitude, powered, RM3



WEC power (W), powered, RM3





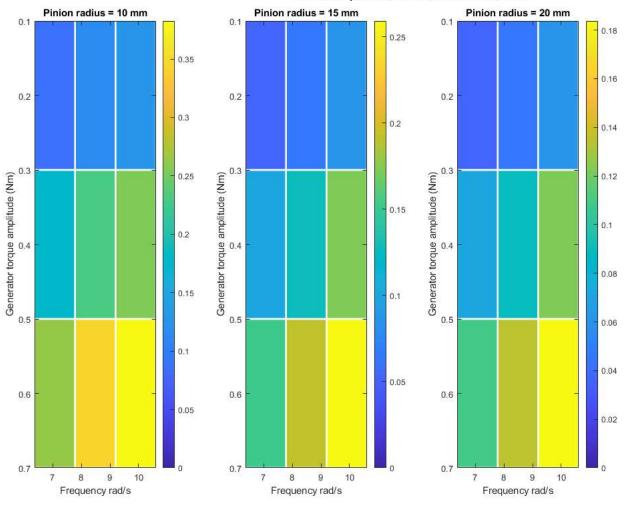


Frequency rad/s

Frequency rad/s

Frequency rad/s

WEC amplitude, forced oscillation, RM3



WEC power (W), forced oscillation, RM3

