

代数式碰撞模型

2023.5.30

1 2d hopper

1.1 动力学方程

$$m\ddot{l} = m\dot{\theta}^2 - k(l - l_0) - mg \cos \theta + f \quad (1a)$$

$$ml^2\ddot{\theta} = mgl \sin \theta - 2ml\dot{l}\dot{\theta} + \tau \quad (1b)$$

如果考虑弹簧的阻尼系数，那么动力学方程如下：

$$m\ddot{l} = m\dot{\theta}^2 - k(l - l_0) - c\dot{l} - mg \cos \theta + f$$

$$ml^2\ddot{\theta} = mgl \sin \theta - 2ml\dot{l}\dot{\theta} + \tau$$

如果简化系统，忽视重力以及驱动器的作用：

$$m\ddot{l} = m\dot{\theta}^2 - k(l - l_0)$$

$$ml^2\ddot{\theta} = -2ml\dot{l}\dot{\theta}$$

$$m\ddot{l} - m\dot{\theta}^2 + k(l - l_0) = 0$$

$$\frac{d}{dt}(ml^2\dot{\theta}) = 0$$

$$m\ddot{l} + k(l - l_0) = 0$$

$$\frac{d}{dt}(ml^2\dot{\theta}) = 0$$

1.2 微分平坦推导

1.2.1 平坦输出

取直角坐标系中的 x 和 z 分别作为平坦输出，且有：

$$x = l \sin \theta \quad (2a)$$

$$z = l \cos \theta \quad (2b)$$

1.2.2 平坦输出 x 多阶导数

相应的存在 x 和 z 的多阶导数：

$$\dot{x} = l \dot{\sin \theta} \quad (3a)$$

$$\dot{z} = l \dot{\cos \theta} \quad (3b)$$

$$\ddot{x} = \ddot{l} \sin \theta + 2\dot{l}\dot{\theta} \cos \theta + l\ddot{\theta} \cos \theta - l\dot{\theta}^2 \sin \theta \quad (3c)$$

注意到对动力学方程 1a 两边乘上 $\sin \theta$ ，对 1b 两边乘上 $\cos \theta$ 改写有：

$$T1 : m\ddot{l} \sin \theta = m l \dot{\theta}^2 \sin \theta - k(l - l_0) \sin \theta - mgl \sin \theta \cos \theta + f \sin \theta$$

$$T2 : m l^2 \ddot{\theta} \cos \theta = mg \sin \theta \cos \theta - 2ml\dot{\theta} \cos \theta + \tau \cos \theta$$

继续改写， $T1$ 移项，除以 m ； $T2$ 移项，除以 ml ：

$$T1 : \ddot{l} \sin \theta - l\dot{\theta}^2 \sin \theta = -\frac{k(l - l_0) \sin \theta}{m} - g \sin \theta \cos \theta + \frac{f \sin \theta}{m}$$

$$T2 : l\ddot{\theta} \cos \theta + 2\dot{l}\dot{\theta} \cos \theta = g \sin \theta \cos \theta + \frac{\tau \cos \theta}{ml}$$

$T1$ 加上 $T2$ 项，得到

$$\begin{aligned} T1 + T2 &= \ddot{l} \sin \theta - l\dot{\theta}^2 \sin \theta + l\ddot{\theta} \cos \theta + 2\dot{l}\dot{\theta} \cos \theta \\ &= -\frac{k(l - l_0) \sin \theta}{m} - g \sin \theta \cos \theta + \frac{f \sin \theta}{m} + g \sin \theta \cos \theta + \frac{\tau \cos \theta}{ml} \\ &= -\frac{k(l - l_0) \sin \theta}{m} + \frac{f \sin \theta}{m} + \frac{\tau \cos \theta}{ml} \end{aligned}$$

因此还有

$$\ddot{x} = \ddot{l} \sin \theta - l\dot{\theta}^2 \sin \theta + l\ddot{\theta} \cos \theta + 2\dot{l}\dot{\theta} \cos \theta \quad (4a)$$

$$\ddot{x} = -\frac{k(l - l_0) \sin \theta}{m} + \frac{f \sin \theta}{m} + \frac{\tau \cos \theta}{ml} \quad (4b)$$

1.2.3 平坦输出 z 多阶导数

同理继续推导 z 的多阶导数:

$$z = l \cos \theta \quad (5a)$$

$$\dot{z} = \dot{l} \cos \theta - l \dot{\theta} \sin \theta \quad (5b)$$

$$\ddot{z} = \ddot{l} \cos \theta - 2\dot{l}\dot{\theta} \sin \theta - l\ddot{\theta} \sin \theta - l\dot{\theta}^2 \cos \theta \quad (5c)$$

对动力学方程 1a 两边乘上 $\cos \theta$, 对 1b 两边乘上 $\sin \theta$ 改写有:

$$T3 : m\ddot{l} \cos \theta = m l \dot{\theta}^2 \cos \theta - k(l - l_0) \cos \theta - mg \cos^2 \theta + f \cos \theta$$

$$T4 : m l^2 \ddot{\theta} \sin \theta = m g l \sin^2 \theta - 2 m l \dot{l} \dot{\theta} \sin \theta + \tau \sin \theta$$

继续改写, $T3$ 移项, 除以 m ; $T4$ 移项, 除以 ml :

$$T3 : \ddot{l} \cos \theta - l \dot{\theta}^2 \cos \theta = -\frac{k(l - l_0) \cos \theta}{m} - g \cos^2 \theta + \frac{f \cos \theta}{m}$$

$$T4 : l \ddot{\theta} \sin \theta + 2 \dot{l} \dot{\theta} \sin \theta = g \sin^2 \theta + \frac{\tau \sin \theta}{ml}$$

$T3$ 减去 $T4$ 项, 得到

$$\begin{aligned} T3 - T4 &= \ddot{l} \cos \theta - l \dot{\theta}^2 \cos \theta - l \ddot{\theta} \sin \theta - 2 \dot{l} \dot{\theta} \sin \theta \\ &= -\frac{k(l - l_0) \cos \theta}{m} - g \cos^2 \theta + \frac{f \cos \theta}{m} - g \sin^2 \theta - \frac{\tau \sin \theta}{ml} \\ &= -\frac{k(l - l_0) \cos \theta}{m} - g + \frac{f \cos \theta}{m} - \frac{\tau \sin \theta}{ml} \end{aligned}$$

因此还有

$$\ddot{z} = \ddot{l} \cos \theta - l \dot{\theta}^2 \cos \theta - l \ddot{\theta} \sin \theta - 2 \dot{l} \dot{\theta} \sin \theta \quad (6a)$$

$$\ddot{z} = -\frac{k(l - l_0) \cos \theta}{m} - g + \frac{f \cos \theta}{m} - \frac{\tau \sin \theta}{ml} \quad (6b)$$

1.2.4 平坦输出表示状态变量

首先是对 θ 及其一阶导的表示:

$$\begin{aligned} \tan \theta &= \frac{l \sin \theta}{l \cos \theta} = \frac{x}{z} \\ \theta &= \arctan \frac{x}{z} \end{aligned}$$

对式 (3b) 乘以 $z = l \cos \theta$, 对式 (5b) 乘 $x = l \sin \theta$:

$$\dot{x}z = \dot{l} \sin \theta \cos \theta + l^2 \dot{\theta} \cos^2 \theta$$

$$\dot{z}x = \dot{l} \sin \theta \cos \theta - l^2 \dot{\theta} \sin^2 \theta$$

以上两式相减则有那么则有:

$$l^2\dot{\theta} = \dot{x}z - \dot{z}x$$

$$\dot{\theta} = \frac{\dot{x}z - \dot{z}x}{l^2} = \frac{\dot{x}z - \dot{z}x}{x^2 + z^2}$$

综上有 θ 及其一阶导数关于平坦输出的表示:

$$\theta = \arctan \frac{x}{z}$$

$$\dot{\theta} = \frac{\dot{x}z - \dot{z}x}{x^2 + z^2}$$

再继续求对 l 及其一阶导的表示:

$$l = x^2 + z^2$$

对式 (3b) 乘以 $x = l \sin \theta$, 对式 (5b) 乘以 $z = l \cos \theta$:

$$\dot{x}x = \dot{l}l \sin^2 \theta + l^2 \dot{\theta} \sin \theta \cos \theta$$

$$\dot{z}z = \dot{l}l \cos^2 \theta - l^2 \dot{\theta} \sin \theta \cos \theta$$

以上两式相加那么则有:

$$\dot{l}l = \dot{x}x + \dot{z}z$$

$$\dot{l} = \frac{\dot{x}x + \dot{z}z}{l} = \frac{\dot{x}x + \dot{z}z}{\sqrt{x^2 + z^2}}$$

最后有:

$$\theta = \arctan \frac{x}{z} \quad (7a)$$

$$\dot{\theta} = \frac{z\dot{x} - x\dot{z}}{x^2 + z^2} \quad (7b)$$

$$l = x^2 + z^2 \quad (7c)$$

$$\dot{l} = \frac{x\dot{x} + z\dot{z}}{\sqrt{x^2 + z^2}} \quad (7d)$$

1.2.5 平坦输出表示控制变量

将式 (4b) 乘以 $x = l \sin \theta$; 式 (6b) 乘以 $z = l \cos \theta$

$$x\ddot{x} = -\frac{kl(l-l_0)\sin^2 \theta}{m} + \frac{lf\sin^2 \theta}{m} + \frac{\tau \sin \theta \cos \theta}{ml}$$

$$z\ddot{z} = -\frac{kl(l-l_0)\cos^2 \theta}{m} - gz + \frac{lf\cos^2 \theta}{m} - \frac{\tau \sin \theta \cos \theta}{ml}$$

以上两式相加:

$$\begin{aligned}
x\ddot{x} + z\ddot{z} &= -\frac{kl(l-l_0)}{m} - gz + \frac{lf}{m} \\
f &= \frac{mx\ddot{x} + mz\ddot{z} + kl(l-l_0) + mgz}{l} \\
&= k(\sqrt{x^2 + z^2} - l_0) + \frac{mx\ddot{x} + mz\ddot{z} + mgz}{l}
\end{aligned}$$

再将式 (4b) 乘以 $z = l \cos \theta$; 式 (6b) 乘以 $x = l \sin \theta$:

$$\begin{aligned}
z\ddot{x} &= -\frac{kl(l-l_0)\sin\theta\cos\theta}{m} + \frac{lf\sin\theta\cos\theta}{m} + \frac{\tau\cos^2\theta}{m} \\
x\ddot{z} &= -\frac{kl(l-l_0)\sin\theta\cos\theta}{m} - gx + \frac{lf\sin\theta\cos\theta}{m} - \frac{\tau\sin^2\theta}{m}
\end{aligned}$$

以上两式相减:

$$\begin{aligned}
z\ddot{x} - x\ddot{z} &= gx + \frac{\tau}{m} \\
\tau &= mz\ddot{x} - mx\ddot{z} - mgx
\end{aligned}$$

最后有:

$$f = k(\sqrt{x^2 + z^2} - l_0) + \frac{mx\ddot{x} + mz\ddot{z} + mgz}{\sqrt{x^2 + z^2}} \quad (8a)$$

$$\tau = mz\ddot{x} - mx\ddot{z} - mgx \quad (8b)$$

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反馈线性化

$$\begin{aligned}
f &= m(\ddot{x}_d \sin \theta + \ddot{z}_d \cos \theta + g) + k(l - l_0) - k_1(\dot{x} - \dot{x}_d) - k_2(x - x_d) \\
\tau &= ml(\ddot{x}_d \cos \theta - \ddot{z}_d \sin \theta) - k_3(\dot{z} - \dot{z}_d) - k_4(z - z_d)
\end{aligned}$$

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$$\begin{aligned}
\frac{d}{dt}(l \sin \theta \cos \phi) &= \dot{l} \sin \theta \cos \phi + l \dot{\theta} \cos \theta \cos \phi - l \sin \theta \sin \phi \dot{\phi} \\
\frac{d^2}{dt^2}(l \sin \theta \cos \phi) &= \ddot{l} \sin \theta \cos \phi + 2\dot{l}\dot{\theta} \cos \theta \cos \phi - 2\dot{l} \sin \theta \sin \phi \dot{\phi} + l\ddot{\theta} \cos \theta \cos \phi \\
&\quad - l\dot{\theta}^2 \sin \theta \cos \phi - 2l\dot{\theta} \sin \theta \sin \phi \dot{\phi} - l \cos \theta \sin \phi \ddot{\phi} - l \sin \theta \cos \phi \dot{\phi}^2 \\
\frac{d}{dt}(l \sin \theta \sin \phi) &= \dot{l} \sin \theta \sin \phi + l \dot{\theta} \cos \theta \sin \phi + l \sin \theta \cos \phi \dot{\phi} \\
\frac{d^2}{dt^2}(l \sin \theta \sin \phi) &= \ddot{l} \sin \theta \sin \phi + 2\dot{l}\dot{\theta} \cos \theta \sin \phi + 2\dot{l} \sin \theta \cos \phi \dot{\phi} + l\ddot{\theta} \cos \theta \sin \phi \\
&\quad - l\dot{\theta}^2 \sin \theta \sin \phi + 2l\dot{\theta} \sin \theta \cos \phi \dot{\phi} + l \sin \theta \cos \phi \ddot{\phi} - l \sin \theta \sin \phi \dot{\phi}^2 \\
\frac{d}{dt}(l \cos \theta) &= \dot{l} \cos \theta - l \dot{\theta} \sin \theta \\
\frac{d^2}{dt^2}(l \cos \theta) &= \ddot{l} \cos \theta - 2\dot{l}\dot{\theta} \sin \theta - l\ddot{\theta} \sin \theta - l\dot{\theta}^2 \cos \theta
\end{aligned}$$

$$\begin{aligned}
Q &= 288P_{\text{seg0},4}^2 + 360P_{\text{seg0},4}P_{\text{seg0},5} + 360P_{\text{seg0},4}P_{\text{seg0},6} + 315P_{\text{seg0},4}P_{\text{seg0},7} \\
&\quad + 360P_{\text{seg0},5}P_{\text{seg0},4} + 600P_{\text{seg0},5}^2 + 675P_{\text{seg0},5}P_{\text{seg0},6} + 630P_{\text{seg0},5}P_{\text{seg0},7} \\
&\quad + 360P_{\text{seg0},6}P_{\text{seg0},4} + 675P_{\text{seg0},6}P_{\text{seg0},5} + 787.5P_{\text{seg0},6}^2 + 787.5P_{\text{seg0},6}P_{\text{seg0},7} \\
&\quad + 315P_{\text{seg0},7}P_{\text{seg0},4} + 630P_{\text{seg0},7}P_{\text{seg0},5} + 787.5P_{\text{seg0},7}P_{\text{seg0},6} + 787.5P_{\text{seg0},7}^2 \\
&\quad + 288P_{\text{seg1},4}^2 + 360P_{\text{seg1},4}P_{\text{seg1},5} + 360P_{\text{seg1},4}P_{\text{seg1},6} + 315P_{\text{seg1},4}P_{\text{seg1},7} \\
&\quad + 360P_{\text{seg1},5}P_{\text{seg1},4} + 600P_{\text{seg1},5}^2 + 675P_{\text{seg1},5}P_{\text{seg1},6} + 630P_{\text{seg1},5}P_{\text{seg1},7} \\
&\quad + 360P_{\text{seg1},6}P_{\text{seg1},4} + 675P_{\text{seg1},6}P_{\text{seg1},5} + 787.5P_{\text{seg1},6}^2 + 787.5P_{\text{seg1},6}P_{\text{seg1},7} \\
&\quad + 315P_{\text{seg1},7}P_{\text{seg1},4} + 630P_{\text{seg1},7}P_{\text{seg1},5} + 787.5P_{\text{seg1},7}P_{\text{seg1},6} + 787.5P_{\text{seg1},7}^2
\end{aligned}$$

$$(@1 * P_{\text{seg0},4}) + (@2 * P_{\text{seg0},5}) + (@2 * P_{\text{seg0},6}) + (@3 * P_{\text{seg0},7})$$

$$\begin{aligned}
&@1=576, @2=1440, @3=2880, @4=5040, @5=4800, @6=10800, @7=20160, @8=25920, \\
&@9=50400, @10=100800 @1=288, @2=360, @3=315, @4=600, @5=675, @6=630, @7=810, \\
&@8=787.5 ((@1 * P_{\text{seg0},4}) + (@2 * P_{\text{seg0},5}) + (@2 * P_{\text{seg0},6}) + (@3 * P_{\text{seg0},7}) * P_{\text{seg0},4}) + ((@2 * \\
&P_{\text{seg0},4}) + (@4 * P_{\text{seg0},5}) + (@5 * P_{\text{seg0},6}) + (@6 * P_{\text{seg0},7}) * P_{\text{seg0},5}) + ((@2 * P_{\text{seg0},4}) + (@5 * \\
&P_{\text{seg0},5}) + (@7 * P_{\text{seg0},6}) + (@8 * P_{\text{seg0},7}) * P_{\text{seg0},6}) + ((@3 * P_{\text{seg0},4}) + (@6 * P_{\text{seg0},5}) + (@8 * \\
&P_{\text{seg0},6}) + (@8 * P_{\text{seg0},7}) * P_{\text{seg0},7}) +
\end{aligned}$$

$$\begin{aligned}
&((@1 * P_{\text{seg1},4}) + (@2 * P_{\text{seg1},5}) + (@2 * P_{\text{seg1},6}) + (@3 * P_{\text{seg1},7}) * P_{\text{seg1},4}) + ((@2 * \\
&P_{\text{seg1},4}) + (@4 * P_{\text{seg1},5}) + (@5 * P_{\text{seg1},6}) + (@6 * P_{\text{seg1},7}) * P_{\text{seg1},5}) + ((@2 * P_{\text{seg1},4}) + (@5 * \\
&P_{\text{seg1},5}) + (@7 * P_{\text{seg1},6}) + (@8 * P_{\text{seg1},7}) * P_{\text{seg1},6}) + ((@3 * P_{\text{seg1},4}) + (@6 * P_{\text{seg1},5}) + (@8 * \\
&P_{\text{seg1},6}) + (@8 * P_{\text{seg1},7}) * P_{\text{seg1},7})
\end{aligned}$$