1000/B1600, leading jet 0.08 0.06 0.04 0.02 0.00 80 100 120 140 160 180 Mass [GeV]

1000/B1600, leading jet PR 0.12 Mean = -0.092Sigma = 0.067**PRCorr** 0.10 Mean = -0.029Sigma = 0.06980.0 AK8SD Mean = -0.074Sigma = 0.0790.06 AK8SDCorrThea Mean = 0.022Sigma = 0.1090.04 AK8SDHCorr Mean = 0.0310.02 0.00

0.0

0.1

0.3

(Mass-125)/125 [GeV]

-0.3

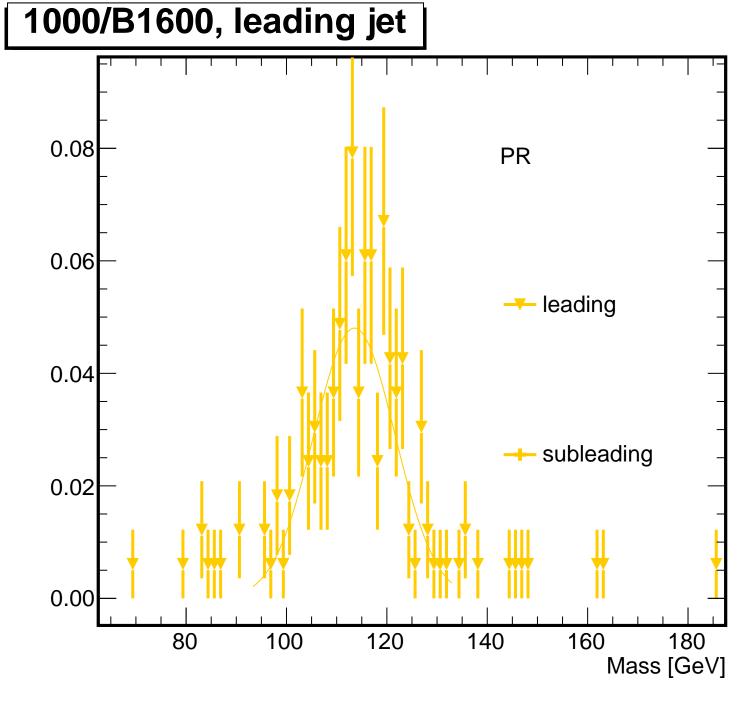
-0.2

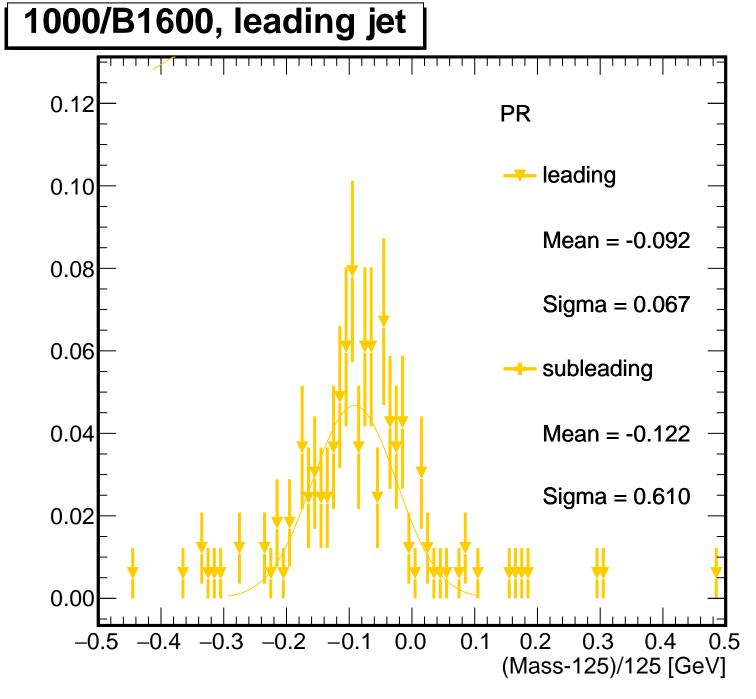
1000/B1600, subleading jet 0.35 **RCorr** 0.30 0.25 0.20 0.15 0.10 0.05 0.00 80 100 120 140 160 180 Mass [GeV]

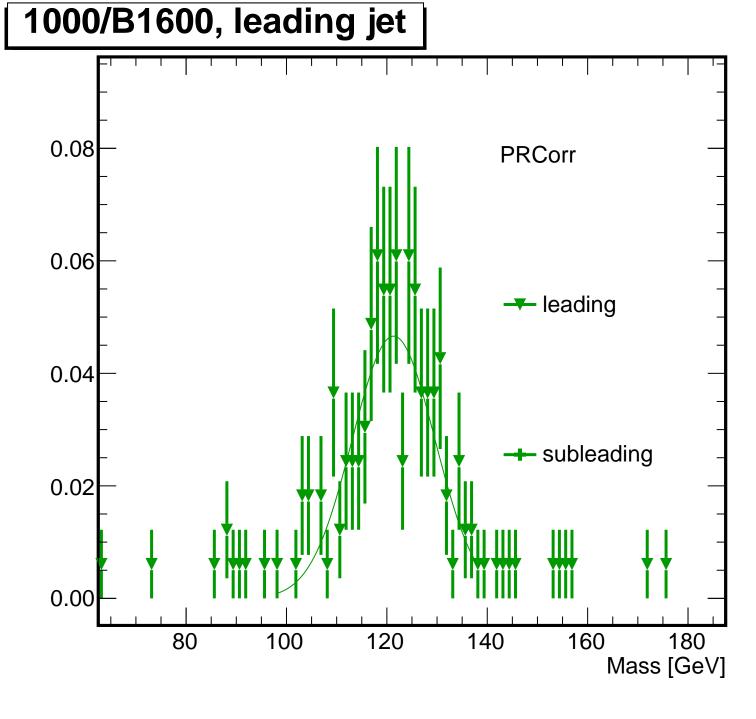
1000/B1600, subleading jet PR Mean = -0.122Sigma = 0.6100.4 **PRCorr** Mean = -0.049Sigma = 0.546AK8SD 0.3 Mean = 1.666Sigma **|** 0 748 AK8SDCorrThea $M_{ean} = 1.891$ 0.2 Sigma ⊨ 0.709 AK8SDHCorr $Mean = \{0.009\}$ Sigma | 0 102 0.1 -0.3-0.20.0 0.1 0.2 0.3 0.4 (Mass-125)/125 [GeV]

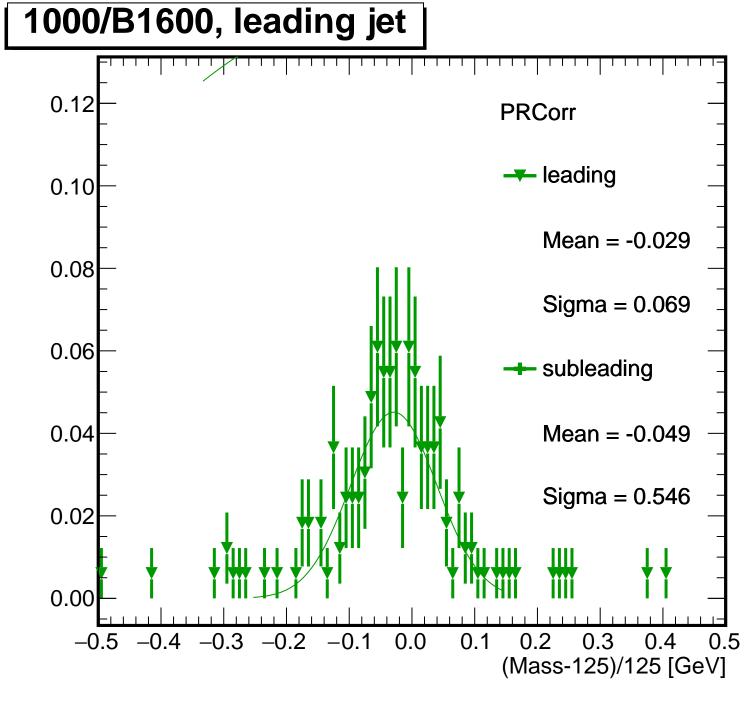
1000/B1600, both jets 0.09 80.0 0.07 0.06 0.05 0.04 0.03 0.02 0.01 120 160 80 100 140 180 Mass [GeV]

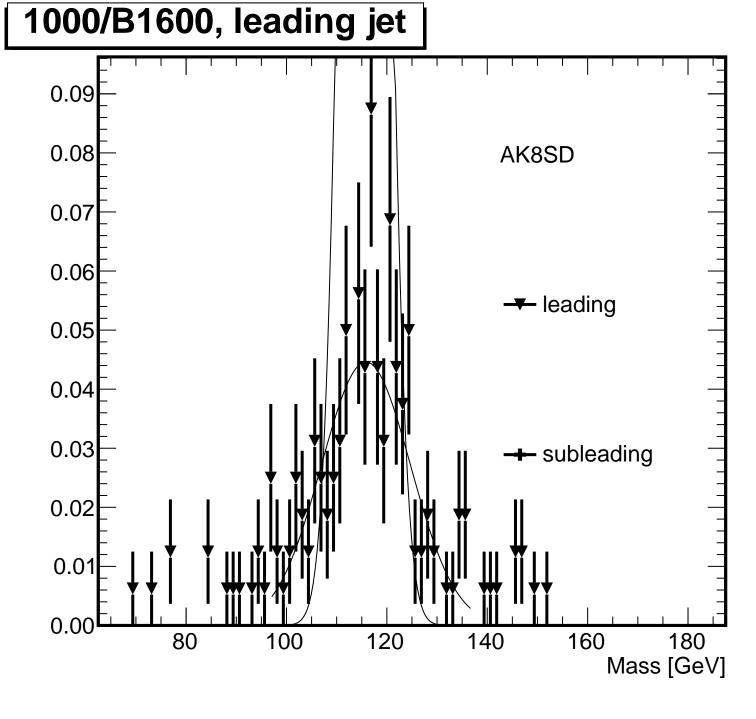
1000/B1600, both jets 0.12 PR Mean = -0.092Sigma = 0.0670.10 **PRCorr** Mean = -0.033Sigma = 0.07380.0 AK8SD Mean = -0.073Sigma = 0.0880.06 AK8SDCorrThea Mean = 0.016Sigma = 0.0850.04 AK8SDHCorr Mean = 0.029Sigma = 0.0880.02 A IT II THE THE CAN DATE 0.1(Mass-125)/125 [GeV]

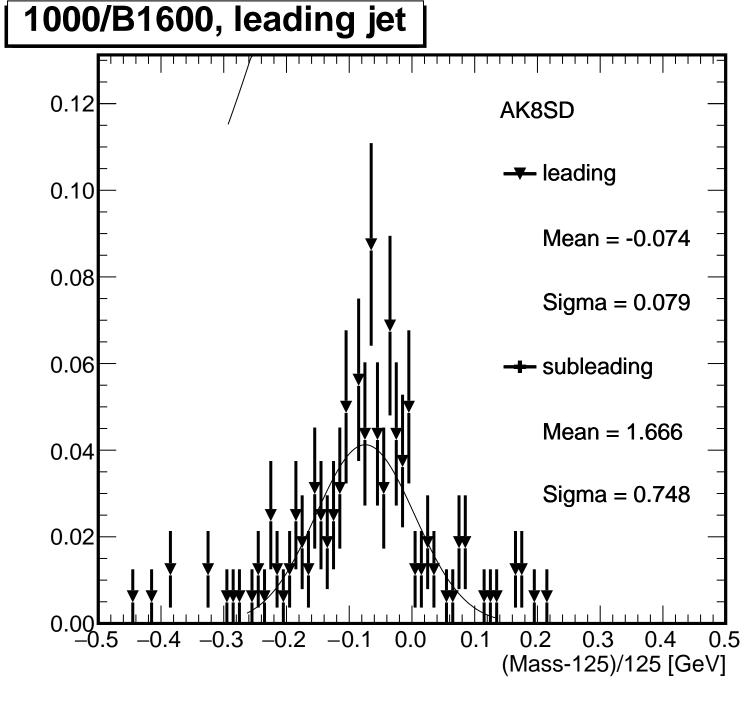


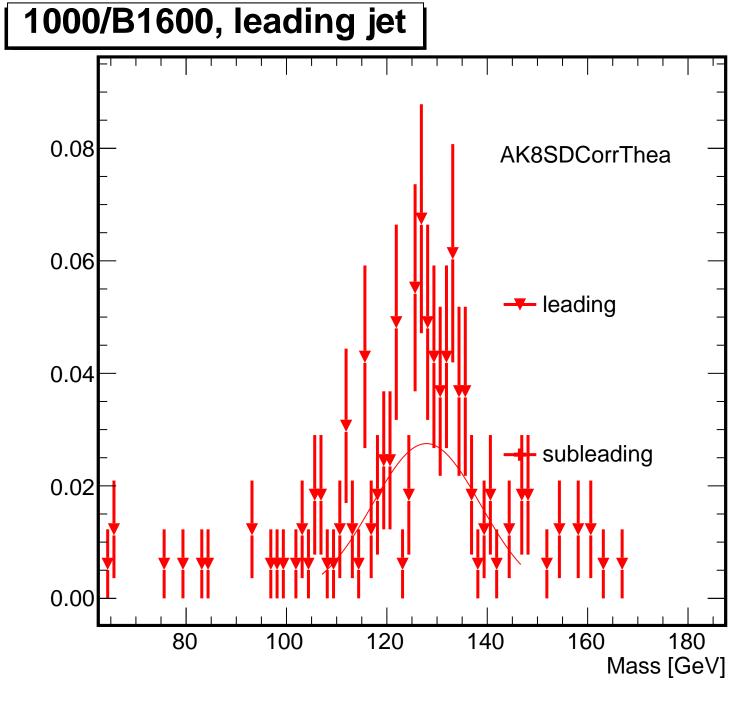












1000/B1600, leading jet 0.12 AK8SDCorrThea leading 0.10 Mean = 0.02280.0 Sigma = 0.1090.06 subleading 0.04 Mean = 1.891Sigma = 0.7090.02 0.00 -0.30.1 0.2 0.0 0.3 (Mass-125)/125 [GeV]

