

# Lecture 6

## MOS Current-Steering Circuits and Small Signal Operation of Current Mirror

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Taha Ahmed

## 1 MOS Current-Steering Circuits

Once a constant current has been generated, it can be replicated to provide dc bias or load currents for the various amplifier stages in an IC. Current mirrors can obviously be used to implement this current-steering function.

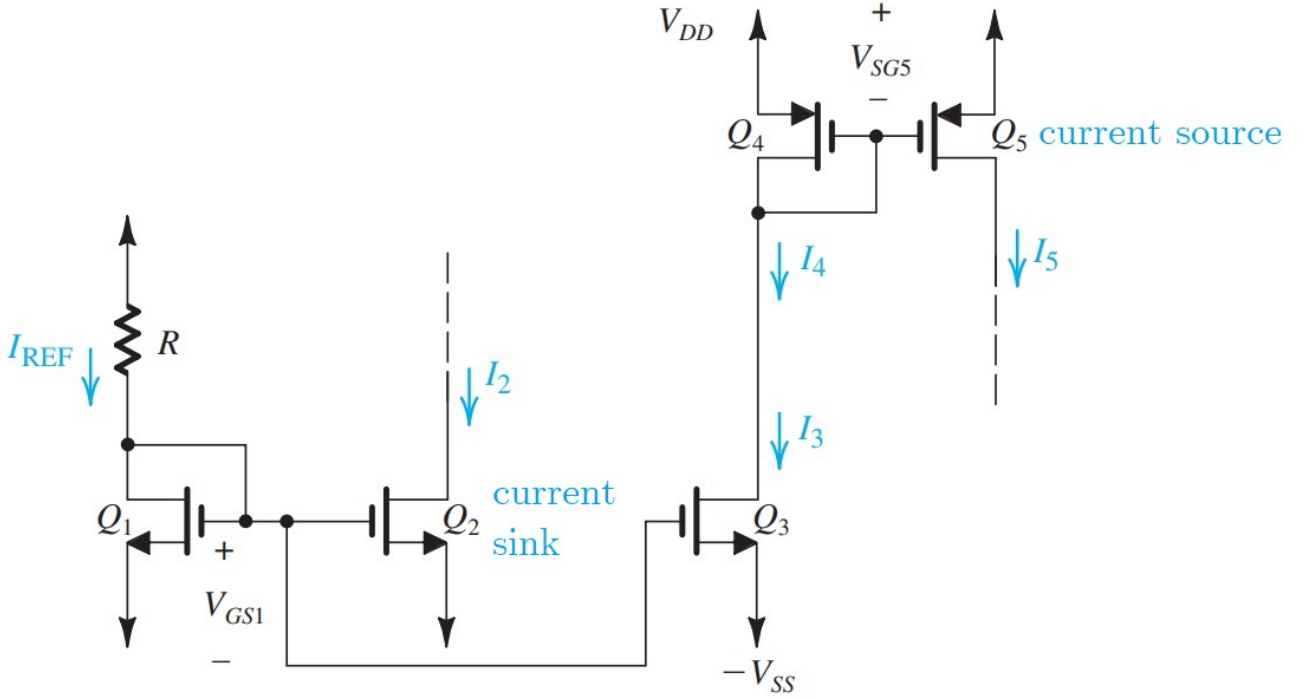


Figure 1: A current-steering circuit

$$I_2 = I_{\text{REF}} \frac{(W/L)_2}{(W/L)_1} \quad (1)$$

$$I_3 = I_{\text{REF}} \frac{(W/L)_3}{(W/L)_1} \quad (2)$$

To ensure operation in the saturation region, the voltages at the drains of  $Q_2$  and  $Q_3$  are constrained as follows:

$$V_{DS} \geq V_{OV} \quad (3)$$

Where :

$$V_{DS} = V_D - (-V_{SS}) \quad (4)$$

$$V_{OV} = V_{GS} - V_t \quad (5)$$

$$(6)$$

Therefore

$$V_{D2}, V_{D3} \geq -V_{SS} + V_{GS1} - V_{tn} \quad (7)$$

or, equivalently,

$$V_{D2}, V_{D3} \geq -V_{SS} + V_{OV1} \quad (8)$$

where  $V_{OV1}$  is the overdrive voltage at which  $Q_1$ ,  $Q_2$ , and  $Q_3$  are operating.

In other words, the drains of  $Q_2$  and  $Q_3$  will have to remain higher than  $-V_{SS}$  by at least the overdrive voltage.

$I_3$  is fed to the input side of a current mirror formed by PMOS transistors  $Q_4$  and  $Q_5$ . This mirror provides

$$I_5 = I_4 \frac{(W/L)_5}{(W/L)_4} \quad (9)$$

where  $I_4 = I_3$ . To keep  $Q_5$  in saturation (PMOS), its drain voltage should be

$$V_{DS5} \leq V_{DD} - |V_{OV5}| \quad (10)$$

where  $V_{OV5}$  is the overdrive voltage at which  $Q_5$  is operating.

Finally, an important point to note is that in the circuit of Fig 1, while  $Q_2$  pulls its current  $I_2$  from a circuit,  $Q_5$  pushes its current  $I_5$  into a circuit. Thus :

$Q_5$  is called a **current source**,

$Q_2$  is called a **current sink**

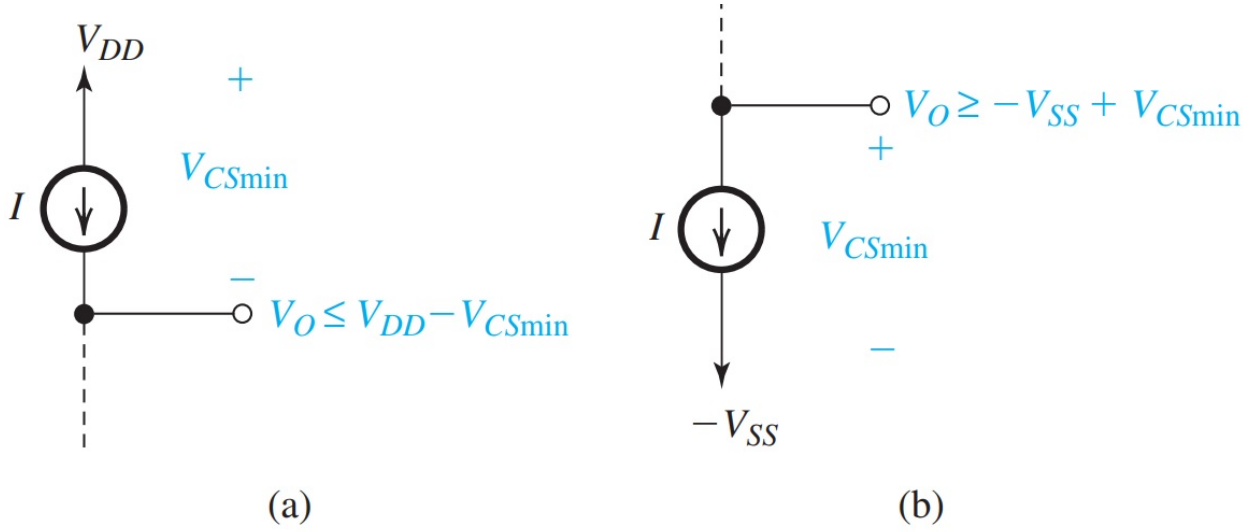


Figure 2: (a) A current source; and (b) a current sink.

## 2 Small-Signal Operation of Current Mirrors

In addition to their use in biasing, current mirrors are sometimes employed as current amplifiers. It is therefore useful to derive the small-signal parameters of the current mirror, that is, input resistance  $R_{in}$ , output resistance  $R_o$ , and short circuit current gain  $A_{is}$

Figure 3 (a) shows a MOS current mirror biased with a dc input current  $I_{D1}$  and fed with a small-signal input current  $i_i$ . Note that  $V_{GS}$  and  $I_{D2}$  are the resulting dc quantities, while  $v_{gs}$  and  $i_o$  are signal quantities.

Replacing  $Q_1$  and  $Q_2$  with their small-signal models results in the circuit in Figure 3 (b). Observe that the controlled current source  $g_{m1}v_{gs}$  appears across its control voltage  $v_{gs}$  and thus can be replaced by a resistance,  $1/g_{m1}$  (ohm's law), as shown in Figure 3 (c). For the latter circuit we can obtain

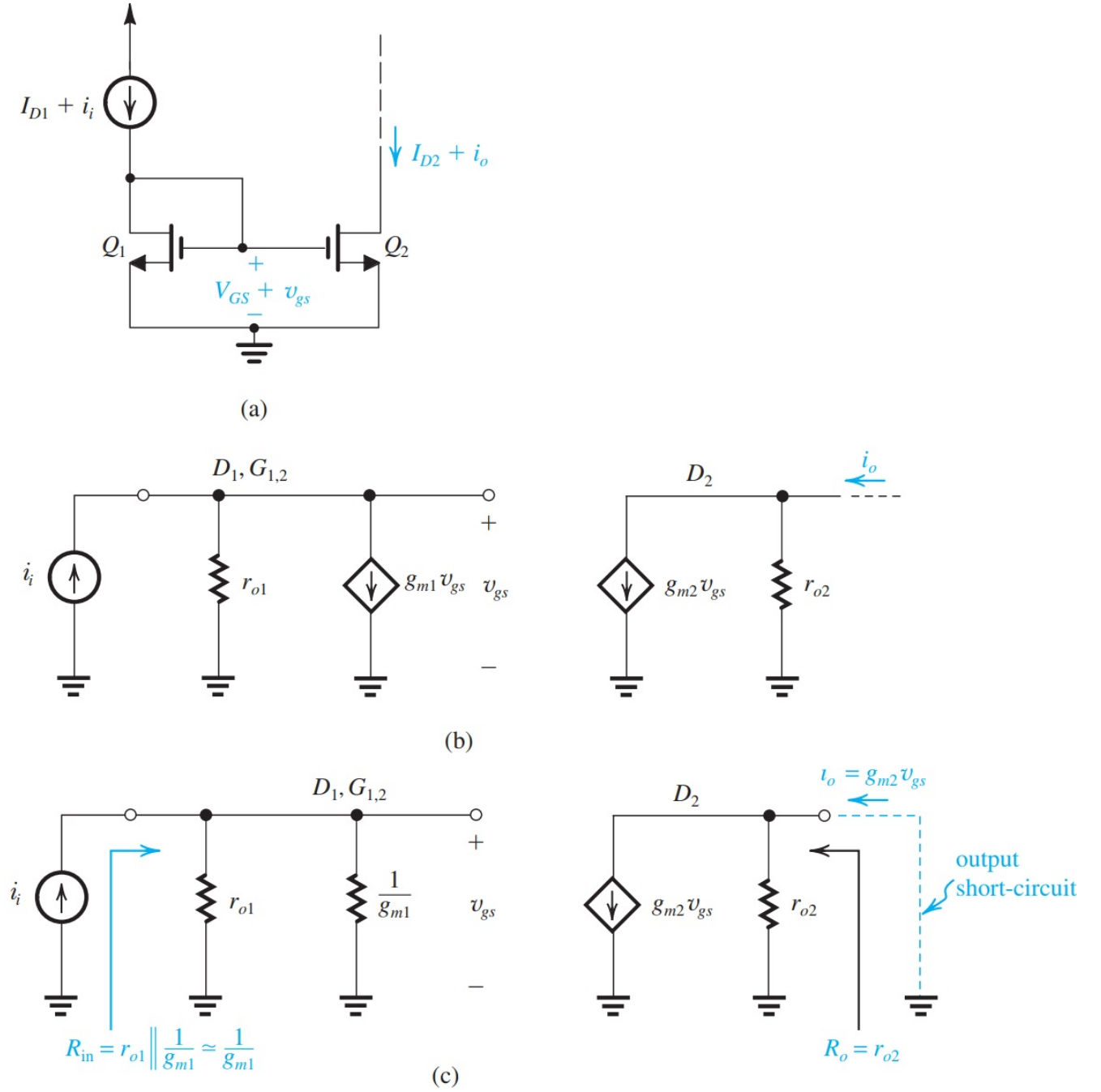


Figure 3: Obtaining the small-signal parameters of the MOS current mirror as a current amplifier.

**Input resistance**

$$R_{\text{in}} = r_{o1} \parallel \frac{1}{g_{m1}} \simeq \frac{1}{g_{m1}} \quad (11)$$

**Output resistance**

$$R_o = r_{o2} \quad (12)$$

Short circuit current gain

$$A_{is} = \left. \frac{i_o}{i_i} \right|_{v_{d2}=0} = \frac{g_{m2}v_{gs}}{i_i} \simeq \frac{g_{m2}i_i/g_{m1}}{i_i} \quad (13)$$

Thus :

$$A_{is} = \frac{g_{m1}}{g_{m2}} \quad (14)$$

Substituting for  $g_{m1,2} = \mu_n C_{ox}(W/L)_{1,2}V_{OV}$ , where  $V_{OV}$  is the overdrive voltage at which  $Q_1$  and  $Q_2$  are operating, yields for the short-circuit current gain

$$A_{is} = \frac{(W/L)_2}{(W/L)_1} \quad (15)$$

We conclude that the current mirror is an excellent current amplifier: It has a relatively low input resistance ( $1/g_{m1}$ ), a relatively high output resistance ( $r_{o2}$ ), and a gain determined by the aspect ratios of the MOSFETs.