

# Chapter 9

## Finite element method

### 9.1 An introduction to the Finite Element Method

- Finite difference (FD) method is an approximation to the differential equation.
- Finite element method (FEM) is an approximation to its solution.
- FD methods are usually based on the assumption of regular domains eg line in 1-D, rectangle in 2-D with regular elements
- FEM is better for irregular regions as the domain can be partitioned into any simple subregion such as triangles or rectangles in 2-D or bricks and tetrahedra in 3-D. Figure 9.1 shows a finite element mesh with triangles for an irregular domain.

#### Example: Solving Poisson's equation in 1-D using FEM

$$-U_{xx} = q, \quad 0 \leq x \leq L \quad (9.1)$$

We consider Dirichlet boundary conditions:  $U(0) = U(L) = 0$ . A weak solution of (9.1) considers the variational form of (9.1):

$$\int_0^L U_{xx}(x)\phi(x)dx + \int_0^L q(x)\phi(x) = 0, \quad (9.2)$$

where  $\phi(x)$  satisfy the boundary conditions:  $\phi(0) = \phi(L) = 0$ .

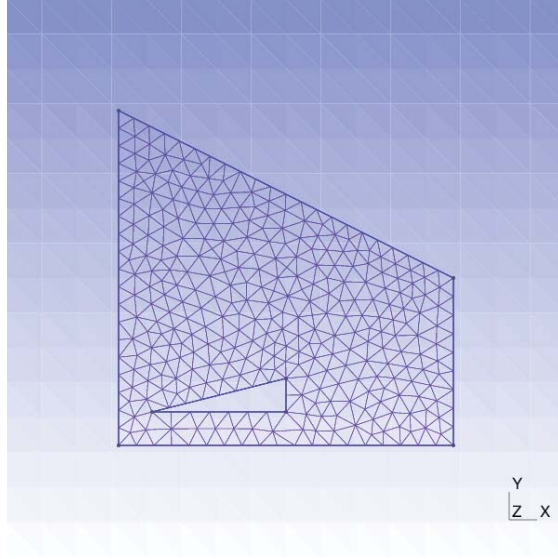


Figure 9.1: FEM mesh with triangles

We can integrate the first term by parts:

$$\begin{aligned} \int_0^L U_{xx}(x)\phi(x)dx &= U_x(x)\phi(x)]_{x=0}^{x=L} - \int_0^L U_x(x)\phi_x(x)dx \\ &= - \int_0^L U_x(x)\phi_x(x)dx \end{aligned}$$

using  $\phi(0) = \phi(L) = 0$ .

Then (9.2) becomes:

$$\int_0^L U_x(x)\phi_x(x)dx = \int_0^L q(x)\phi(x)dx \quad (9.3)$$

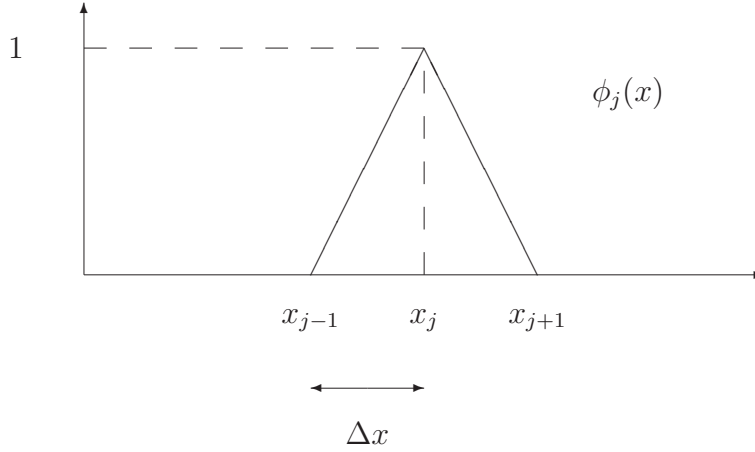
Equation (9.3) holds for all functions  $\phi(x)$  which are piece-wise continuous and satisfy the bc:  $\phi(0) = \phi(L) = 0$ .

To solve equation (9.3) using the FEM we again introduce a mesh (as in FD) on the interval  $[0, L]$  with mesh points  $x_j = j\Delta x$ ,  $j = 0, \dots, n+1$  where  $\Delta x = \frac{L}{n+1}$ . To complete the discretisation we must choose a basis for  $\phi(x)$ . The most common basis chosen for  $\phi(x)$  are the “hat” functions,  $\phi_j(x)$ . We solve (9.3) using these:

$$\phi(x) = \sum_{j=1}^n a_j \phi_j(x)$$

where

$$\phi_j(x) = \begin{cases} 0, & \text{for } 0 \leq x \leq x_{j-1} \\ \frac{1}{\Delta x}(x - x_{j-1}), & \text{for } x_{j-1} \leq x \leq x_j \\ 1 - \frac{1}{\Delta x}(x - x_j), & \text{for } x_j \leq x \leq x_{j+1} \\ 0, & \text{for } x \geq x_{j+1} \end{cases}$$



with this construction:  $\phi_j(x_i) = \delta_{ij}$  and:

$$\phi_j'(x) = \frac{\partial \phi_j}{\partial x} = \begin{cases} 0, & \text{for } 0 < x < x_{j-1} \\ \frac{1}{\Delta x}, & \text{for } x_{j-1} < x < x_j \\ -\frac{1}{\Delta x}, & \text{for } x_j < x < x_{j+1} \\ 0, & \text{for } x > x_{j+1} \end{cases}$$

We let  $\phi(x) = \sum_{j=1}^n a_j \phi_j(x)$  and  $\phi(x_i) = a_i$  for  $i = 1, \dots, n$ , and  $\phi(0) = \phi_1(0) = 0$  and  $\phi(L) = \phi_n(L) = 0$  so that  $\phi(x)$  satisfies boundary conditions.

The hat functions are advantageous as a basis as they are nearly “orthonormal”, ie.  $\int_0^L \phi_j(x) \phi_k(x) dx = 0$  when  $|j - k| > 1$ .

Using FEM we seek an **approximate** solution to (9.3) which is satisfied for all basis functions,  $\phi_i(x)$ , for  $i = 1, \dots, n$ :

$$\int_0^L U_x(x) \phi_x(x) dx = \int_0^L q(x) \phi(x) dx$$

and require that 9.3 be satisfied for  $\phi = \phi_i$ ,  $i = 1, \dots, n$ . We also expand the solution  $U(x)$  using the hat functions  $\phi_i$  as a basis:

$$U(x) \approx U_h(x) = \sum_{j=1}^n b_j \phi_j(x)$$

This simplifies equation 9.3 and we solve for  $\phi = \phi_i$ ,  $i = 1, \dots, n$ :  
ie.

$$\int_0^L U'_h(x) \phi'_i(x) dx = \int_0^L q(x) \phi_i(x) dx, \quad \text{for } i = 1, \dots, n$$

where  $f'(x) = \frac{\partial f}{\partial x}$ .

$$\begin{aligned} LHS &= \int_0^L U'_h(x) \phi'_i(x) dx \\ &= \int_0^L \sum_{j=1}^n b_j \phi'_j(x) \phi'_i(x) dx \\ &= \sum_{j=1}^n C_{i,j} b_j \end{aligned}$$

where  $C_{i,j} = \int_0^L \phi'_j(x) \phi'_i(x) dx$ .  $C_{i,j}$  is known as the stiffness matrix in mechanics.

To find the coefficients  $b_j$  which define our solution  $U(x)$  we must solve  $n$  linear equations:

$$LHS = \sum_{j=1}^n C_{i,j} b_j = RHS = \int_0^L q(x) \phi_i(x) dx = q_i \quad (9.4)$$

for  $i = 1, \dots, n$  with  $q_i = \int_0^L q(x) \phi_i(x) dx$ .

We approximate the solution by expanding in the basis of “hat” functions:  $U(x) \approx \sum_{j=1}^n b_j \phi_j(x)$ . Thus we only need to know the coefficients  $b_j$  to define our solution  $U(x)$  and FEM solves the following equation for vector  $\vec{b} = (b_1, \dots, b_n)$ :

$$\begin{aligned} \sum_{j=1}^n b_j \int_0^L \phi_{j,x}(x) \phi_{i,x}(x) dx &= \int_0^L q(x) \phi_i(x) dx, \\ \text{or } \sum_{j=1}^n b_j C_{i,j} &= q_i \end{aligned}$$

for  $i = 1, \dots, n$ .

We will show that the stiffness matrix  $C$  is tridiagonal for this example. We are solving the above system for coefficients  $b_j$ , thus we are solving  $C\vec{b} = \vec{q}$  and can use iterative methods in FEM solutions too.

We can show that the stiffness matrix is tridiagonal:

$$C_{ij} = \int_0^L \phi_{j,x}(x) \phi_{i,x}(x) dx = \begin{cases} \frac{-1}{\Delta x}, & i = j - 1 \\ \frac{2}{\Delta x}, & i = j \\ \frac{-1}{\Delta x}, & i = j + 1 \\ 0, & \text{elsewhere} \end{cases}$$

We approximate  $q_i$  using:

$$\begin{aligned}
q_i &= \int_0^L q(x)\phi_i(x)dx \approx q(x_i) \int_0^L \phi_i(x)dx \\
&= q(x_i) \left( \int_{x_{j-1}}^{x_j} \frac{1}{\Delta x}(x - x_{j-1})dx + \int_{x_j}^{x_{j+1}} 1 - \frac{1}{\Delta x}(x - x_j)dx \right) \\
&= \Delta x q(x_i)
\end{aligned}$$

We can substitute the above simplifications into equation 9.4 and arrive at  $C\vec{b} = \Delta x \vec{q}$  or  $\frac{1}{\Delta x}C\vec{b} = \vec{q}$ :

$$\begin{pmatrix} \frac{2}{\Delta x^2} & \frac{-1}{\Delta x^2} & 0 & \cdots \\ \frac{-1}{\Delta x^2} & \frac{2}{\Delta x^2} & \frac{-1}{\Delta x^2} & \ddots \\ 0 & \ddots & \ddots & \ddots \\ \vdots & \ddots & \frac{-1}{\Delta x^2} & \frac{2}{\Delta x^2} \end{pmatrix} \begin{pmatrix} b_1 \\ b_2 \\ \vdots \\ b_n \end{pmatrix} = \begin{pmatrix} q_1 \\ q_2 \\ \vdots \\ q_n \end{pmatrix}$$

Thus the matrix system to solve is the same as FD solution in this example and the solution involves inverting the stiffness matrix  $C$ :

$$\vec{b} = C^{-1}\Delta x \vec{q}$$

Iterative methods are useful in FEM too as it involves inverting large, sparse matrices.

Once  $\vec{b}$  is known, the solution  $U$  to the PDE is given by:

$$U(x) \approx \sum_{j=1}^n b_j \phi_j(x)$$

This is a weak solution of the PDE  $-U_{xx} = q$ .

## 9.2 Comparing FEM solution to FD solution for our example

$$-U_{xx} = q, \quad 0 \leq x \leq L, \quad U(0) = U(L) = 0$$

### 9.2.1 FD solution

Discretise using  $x_j = j\Delta x$ ,  $j = 0, 1, \dots, n+1$  where  $\Delta x = \frac{L}{n+1}$ ,  $U_0 = 0 = U_{n+1}$  (using boundary conditions).

We let  $U(x_j) = U_j$ ,  $q(x_j) = q_j$ . The central difference approximation to the PDE is:

$$U_{xx} = \frac{U_{j+1} - 2U_j + U_{j-1}}{\Delta x^2}$$

and  $-U_{xx} = q$  becomes

$$-\frac{U_{j+1} + 2U_j - U_{j-1}}{\Delta x^2} = q_j$$

We solve for  $U_1, \dots, n$  since  $U_0$  and  $U_{n+1}$  given from boundary conditions and we can rewrite in matrix form:

$$\underbrace{\begin{pmatrix} \frac{2}{\Delta x^2} & \frac{-1}{\Delta x^2} & 0 & \cdots \\ \frac{-1}{\Delta x^2} & \frac{2}{\Delta x^2} & \frac{-1}{\Delta x^2} & \ddots \\ 0 & \ddots & \ddots & \ddots \\ \vdots & \ddots & \frac{-1}{\Delta x^2} & \frac{2}{\Delta x^2} \end{pmatrix}}_{\text{same coefficient matrix for FD as FEM}} \begin{pmatrix} U_1 \\ U_2 \\ \vdots \\ U_n \end{pmatrix} + \begin{pmatrix} -\frac{U_0(=0)}{\Delta x^2} \\ 0 \\ \vdots \\ -\frac{U_{n+1}=0}{\Delta x^2} \end{pmatrix} = \begin{pmatrix} q_1 \\ q_2 \\ \vdots \\ q_n \end{pmatrix}$$

same coefficient matrix for FD as FEM

In this example FEM and FD methods solve the same matrix system.

### 9.3 2-D Finite Element Method

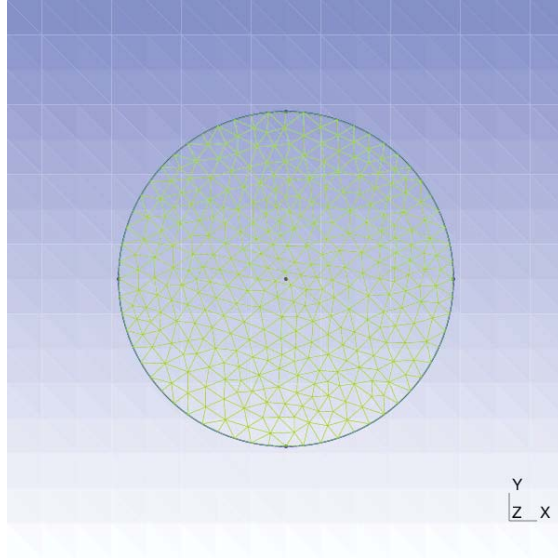


Figure 9.2: FEM mesh with triangles

We consider a triangular mesh (could also be rectangular) shown in figure 9.2 where  $G$  is the domain inside the circle and  $\partial G$  is the domain's boundary.

We are solving:

$$-\nabla^2 U = q \text{ in } G \quad (9.5)$$

with boundary conditions,  $U = 0$  on  $\partial G$ .

The weak solution for  $U$  satisfies the variational form for Equation 9.5:

$$-\int \int_G \nabla^2 U(x, y) \phi(x, y) dx dy = \int \int_G q(x, y) \phi(x, y) dx dy \quad (9.6)$$

where  $\phi(x, y) = 0$  on  $\partial G$  (satisfies boundary conditions).

Using Green's first identity:

$$\begin{aligned} \int \int_G (\phi \nabla^2 U) dx dy &= \underbrace{\oint_{\partial G} \phi (\nabla U \cdot \hat{n}) dS}_{=0 \text{ since } \phi=0 \text{ on } \partial G} - \int \int_G (\nabla \phi \cdot \nabla U) dx dy \\ &= - \int \int_G (\nabla \phi \cdot \nabla U) dx dy \end{aligned}$$

Thus equation 9.6 becomes:

$$\int \int_G (\nabla \phi \cdot \nabla U) dx dy = \int \int_G q \phi dx dy \quad (9.7)$$

which holds  $\forall \phi \in G$  where  $\phi = 0$  on  $\partial G$ .

Similarly to the 1-D case we seek an approximate solution to equation 9.7 by expanding  $U(x, y)$  in a basis of 2-D “hat” functions:

$$U(x, y) \approx U_h(x, y) = \sum_{j=1}^n b_j \phi_j(x, y)$$

where  $U_h(x_i, y_i) = b_i$  and  $U_h = 0$  on  $\partial G$ .

### 9.3.1 2-D “hat functions”

The 2-D hat functions satisfy  $\phi_j(x_j, y_j) = 1$ ,  $\phi_j(x_i, y_l) = 0$  if  $i \neq j$  and  $j \neq l$  at all other vertices. The 2D hat function is plotted in figure 9.3.

We require that equation 9.7 holds for all  $\phi(x, y)$  and solve for  $\phi = \phi_1, \phi_2, \dots, \phi_n$ :

$$\int \int_G \nabla U_h \cdot \nabla \phi_i dx dy = \int \int_G q \phi_i dx dy, \text{ for } i = 1, \dots, n \quad (9.8)$$

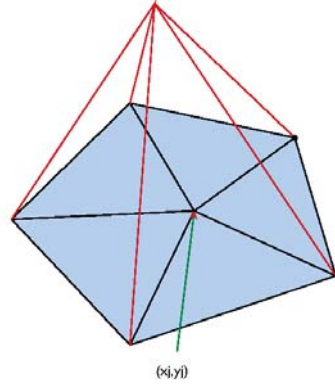


Figure 9.3: 2D hat function ( $\phi_j(x_j, y_j) = 1$ ,  $\phi_j(x_i, y_l) = 0$  if  $i \neq j$  and  $j \neq l$ )

$$LHS = \int \int_G \nabla U_h \cdot \nabla \phi_i dx dy = \sum_{j=1}^n C_{i,j} b_j$$

where  $C_{i,j} = \int \int_G \nabla \phi_j \cdot \nabla \phi_i dx dy$  is called the “stiffness matrix”. Equation 9.8 becomes:

$$\sum_{j=1}^n C_{i,j} b_j = q_i, \text{ for } i = 1, \dots, n \text{ where } q_i = \int \int_G q \phi_i dx dy.$$

If  $C$  is symmetric and positive definite then the system has a unique solution.

### 9.3.2 Example: 2-D Finite Element Method using eScript for elastic wave propagation from a point source.

- eScript is a general PDE solver which implements the finite element method written in python  
(see <https://launchpad.net/escript-finley>)
- eScript can be applied to any problem of the form:

$$-(A_{jl}a_{,l} + B_j a)_{,j} + C_l a_{,l} + D a = -X_{j,j} + Y$$

where  $a$  is the *scalar* we are solving for in this example.  
(eScript can also solve for a *vector*  $\vec{a}$ )



We are using *Einstein notation* and according to this convention if an index appears *twice* in a single term it implies we are summing over all possible values:

$$a_i f_{,ii} = a_i \frac{\partial^2 f_i}{\partial x_i^2} = a_1 \frac{\partial^2 f_1}{\partial x_1^2} + a_2 \frac{\partial^2 f_2}{\partial x_2^2}$$

We will see that the FEM takes care of *spatial* derivative in the problem below. However we still need to approximate *time* derivatives.

We want to solve the 2-D wave equation for a point source:

$$\Psi_{tt} = V_p^2(\Psi_{xx} + \Psi_{yy}) + F_{\text{PS}}$$

where  $p$  is the wave speed,  $\Psi$  is the wave-field and  $F_{\text{PS}}$  is the force due to the point source.

In eScript this becomes:

$$\begin{aligned} D_a &= -X_{j,j} + Y \\ \text{where } a &= \Psi_{tt} \\ D &= 1 \\ X_j &= -V_p^2 \Psi_{,j} \\ Y &= F_{\text{PS}} \end{aligned}$$

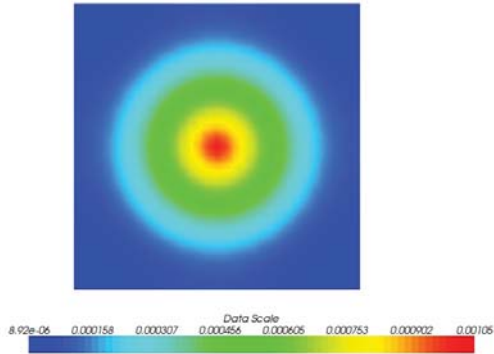


Figure 9.4: Plot of Euclidean normal of the displacement at  $t > 0$  for a point source using eScript.

We solve for  $a^k$  at each time step  $t^k$ . Once  $a^k$  is known we use it to calculate the solution at the next time step,  $\Psi^{k+1}$  using the central difference

formula:

$$a^k = \frac{\partial^2 \Psi^k}{\partial t^2} \approx \frac{\Psi^{k+1} - 2\Psi^k + \Psi^{k-1}}{\Delta t^2}$$

or

$$\Psi^{k+1} = 2\Psi^k - \Psi^{k-1} - \Delta t^2 a^k$$

The eScript python code is **2Dpointsource.py** and the output from this code is shown in figure 9.4.