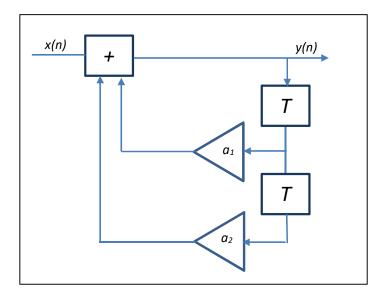
Bandpass IIR pole zero + resonant frequency

The applications of digital bandpass filters include:

- Transmitters and receivers
- · Graphic equalizers (Filter banks)
- Speech recognition systems
- Noise rejection
- Mains frequency rejection

We will examine the design of a 2nd order system as shown below. For higher order systems, numerical methods are the normal method of design.



This filter would be classified as a 2nd order IIR type.

$$y(n) = x(n) + a_1 y(n-1) + a_2 y(n-2)$$

$$Y(z) = X(z) + a_1 Y(z) z^{-1} + a_2 Y(z) z^{-2}$$

$$H(z) = \frac{Y(z)}{X(z)} = \frac{1}{1 - a_1 z^{-1} - a_2 z^{-2}} = \frac{z^2}{z^2 - a_1 z - a_2}$$

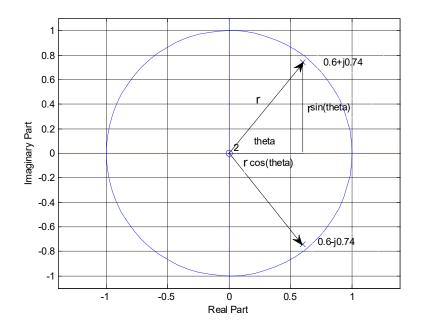
$$Roots \ of \ z^2 - a_1 z - a_2 \ are \quad z = \frac{a_1}{2} \pm \frac{\sqrt{a_1^2 + 4a_2}}{2} = \frac{a_1}{2} \pm j \frac{\sqrt{-(4a_2 + a_1^2)}}{2}$$

$$H(z) = \frac{z^2}{\left(z - \frac{a_1}{2} - j \frac{\sqrt{-(4a_2 + a_1^2)}}{2}\right) \left(z - \frac{a_1}{2} + j \frac{\sqrt{-(4a_2 + a_1^2)}}{2}\right)}$$

Let
$$a_1 = 1.2$$
 $a_2 = -0.91$

Poles are $z = \frac{a_1}{2} \pm j \frac{\sqrt{-(4a_2 + a_1^2)}}{2} = \frac{1.2}{2} \pm j \frac{\sqrt{-(4 \times (-0.91) + (1.2)^2)}}{2}$

$$= 0.6 \pm j \frac{\sqrt{-(-3.64 + 1.44)}}{2} = 0.6 \pm j \frac{\sqrt{2.2}}{2} = 0.6 \pm j 0.74$$



The poles are inside the unit circle. This results in a stable system. If the poles were outside the unit circle, the system becomes unstable and if they are on the unit circle the system is marginally stable.

$$\begin{split} r\cos(\theta_0) &= \frac{a_1}{2} \quad r\sin(\theta_0) = \frac{\sqrt{-\left(4a_2 + a_1^2\right)}}{2} \quad \frac{r\sin(\theta_0)}{r\cos(\theta_0)} = \tan(\theta_0) = \frac{\sqrt{-\left(4a_2 + a_1^2\right)}}{a_1} \\ &\Rightarrow \theta_0 = \tan^{-1}\!\left(\frac{\sqrt{-\left(4a_2 + a_1^2\right)}}{a_1}\right) \quad f_0 = \frac{f_s}{2\pi}\tan^{-1}\!\left(\frac{\sqrt{-\left(4a_2 + a_1^2\right)}}{a_1}\right) \\ a_1 &= 1.2 \quad a_2 = -0.91 \quad f_0 = 1133 \, Hz \quad f_s = 8000 \, Hz \\ y(n) &= x(n) + 1.2 y(n-1) - 0.91 y(n-2) \\ H(z) &= \frac{1}{1 - a_1 z^{-1} - a_2 z^{-2}} \quad H(\theta_0) = \frac{1}{1 - a_1 e^{-j\theta_0} - a_2 z^{-j2\theta_0}} \\ H(\theta_0) &= \frac{1}{1 - a_1 \left\{\cos(\theta_0) - j\sin(\theta_0)\right\} - a_2 \left\{\cos(2\theta_0) - j\sin(2\theta_0)\right\}} \\ \left|H(\theta_0)\right|^2 &= \frac{1}{\left\{1 - a_1\cos(\theta_0) - a_2\cos(2\theta_0)\right\}^2 + \left\{a_1\sin(\theta_0) + a_2\sin(2\theta_0)\right\}^2} \\ \left|H(\theta_0)\right|_{dB} &= -10\log\left(\left\{1 - a_1\cos(\theta_0) - a_2\cos(2\theta_0)\right\}^2 + \left\{a_1\sin(\theta_0) + a_2\sin(2\theta_0)\right\}^2\right) = 23 \, dB \end{split}$$



 f_0 is the resonant (centre) frequency of the band-pass filter. Simulating and plotting the FFT gives:

Problem

See if you can adjust the values of a_1 and a_2 so that the centre frequency of the BPF is exactly 1 kHz.

$$\theta_{0} = \tan^{-1} \left(\frac{\sqrt{-(4a_{2} + a_{1}^{2})}}{a_{1}} \right) \implies \tan(\theta_{0}) = \frac{\sqrt{-(4a_{2} + a_{1}^{2})}}{a_{1}}$$

$$\theta_{0} = \frac{2\pi f_{0}}{f_{s}} = \frac{2\pi (1)}{8} = \frac{\pi}{4} \implies \tan\left(\frac{\pi}{4}\right) = \frac{\sqrt{-(4a_{2} + a_{1}^{2})}}{a_{1}} = 1$$

$$\sqrt{-(4a_{2} + a_{1}^{2})} = a_{1} \implies -(4a_{2} + a_{1}^{2}) = a_{1}^{2}$$

$$-4a_{2} = 2a_{1}^{2} \implies -2a_{2} = a_{1}^{2}$$

If you look at the pole/zero diagram, any value along the line from 0 to 1 with the 45° angle will result in the correct centre frequency. The closer to 1 you put it though will result in a higher Q-factor. So you could arbitrarily choose:

$$r = 0.9$$

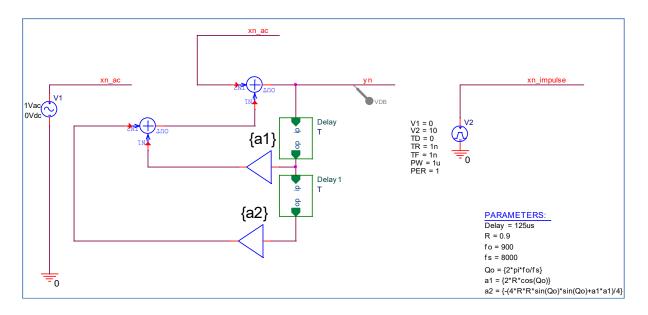
$$r\cos(\theta_0) = \frac{a_1}{2} \Rightarrow a_1 = 2r\cos(\theta_0) = \frac{2r}{\sqrt{2}} = r\sqrt{2}$$

$$a_1 = 0.9\sqrt{2} = 1.27$$

$$a_2 = -\frac{a_1^2}{2} = -\frac{(0.9)^2 2}{2} = -(0.9)^2 = -0.81$$

Draw the block diagram of an IIR BPF with a_2 =-1.5 and a_1 =1.8. What is the centre frequency of the filter if the sampling frequency is 16 kHz?

Using Pspice to Design a Filter



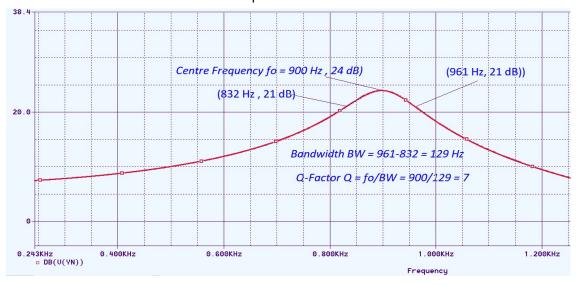
Note:

$$r\cos(\theta_{0}) = \frac{a_{1}}{2} \implies a_{1} = 2r\cos(\theta_{0}) = \frac{a_{1}}{2}$$

$$r\sin(\theta_{0}) = \frac{\sqrt{-(4a_{2} + a_{1}^{2})}}{2} \implies 2r\sin(\theta_{0}) = \sqrt{-(4a_{2} + a_{1}^{2})}$$

$$\implies 4r^{2}\sin^{2}(\theta_{0}) = -(4a_{2} + a_{1}^{2}) \implies -4r^{2}\sin^{2}(\theta_{0}) - a_{1}^{2} = 4a_{2}$$

$$\implies a_{2} = -\frac{4r^{2}\sin^{2}(\theta_{0}) + a_{1}^{2}}{4}$$



DSP3108 DSP Applications

r IIR BPF D	esign							
fs	a2	a1	fs/2*pi	sqrt(-(4a2+a1^2))	sqrt(-(4a2+a1^2))/a1	invtan()=Q0	atan()*fs/2	*pi
8000	-0.91	1.2	1273.2395	1.483239697	1.236033081	0.89056755	1133.906	
a1cos(Q0)	a2cos(2Q0)	a1sin(Q0)	a2sin(Q0)	(1-a1cos(Q0)-a2cos(2Q0))^2	(a1sin(Q0)+a2sin(2Q0))^2	G(f0)		
0.75476508	0.19	0.9329146	-0.8899438	0.003050896	0.001846489	23.1003575		
fs	a2	a1	fs/2*pi	sqrt(-(4a2+a1^2))	sqrt(-(4a2+a1^2))/a1	invtan()=Q0	atan()*fs/2	*pi
16000	-1.5	1.8	2546.4791	1.661324773	0.922958207	0.74535537	1898.032	
a1cos(Q0)	a2cos(2Q0)	a1sin(Q0)	a2sin(Q0)	(1-a1cos(Q0)-a2cos(2Q0))^2	(a1sin(Q0)+a2sin(2Q0))^2	G(f0)		
1.32272446	-0.12	1.2208194	-1.4951923	0.041097207	0.075280487	9.34130251		