

Landauer Experiment

Recent results and discussions 2

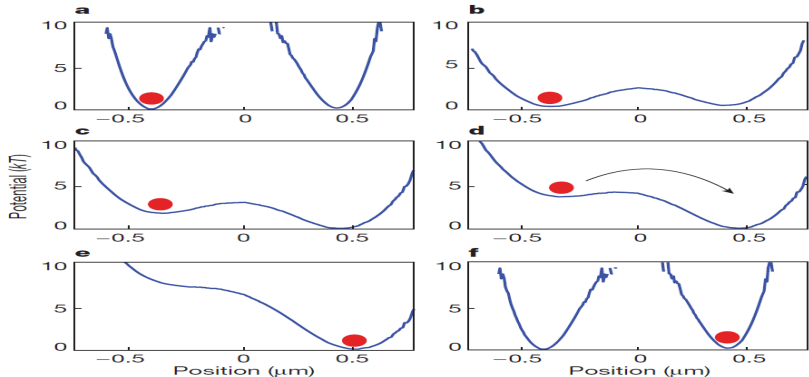
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July 29, 2015

Outline

- 1 Understanding approach in the Nature paper
- 2 Tilting wells - Multiple transfers
- 3 Work Done - Existing Literature
 - Work done in Nature Paper
 - Work done in EPL Paper
- 4 Preliminary calculations
 - Using drag force on the bead
 - Using total force on the bead

What has been done in Nature paper-1



What has been done in Nature paper-2

For fig. a,b and f the plots are found using experimental data as:

- Well potential calculated using pdf is used via.

$$U_0(x, l_L) = -K_B T \ln[(P(x, l_L)]$$

- According to paper, the measured $U_0(x, l_L)$ is plotted in fig.a,b,f and can be fitted by 8th order polynomial as :

$$U_0(x, l_L) = \sum_{n=0}^8 u_n(l_L, d_f) x^n$$

where d_f is the distance between the two points over which laser is switched (1450 nm here)

What has been done in Nature paper-3

For fig. c,d and e the plots are found using following calculations :

- Total time of erasure = Time of stage motion with increasing velocity = τ
- Amplitude of viscous force is increased linearly during time τ : $F(t) = \pm F_{max} t / \tau$
- Intermediate plots during transfer is calculated at three different values of time t :

$$U(x, t) = U_0(x, l_L) - F_{max}(t/\tau).x$$

- *I suspect, the plot in fig.b is also an 8th order fit, since the contours in the plots from b to e are the same*

Our approach-1

Points of discussion last time :

- How did they obtain good curve for saddle points ?
- Their is not only a polynomial fit, but involves calculation using the 8th order fitted curve $U_0(x, I_L)$ as :

$$U(x, t) = U_0(x, I_L) - F(t)$$

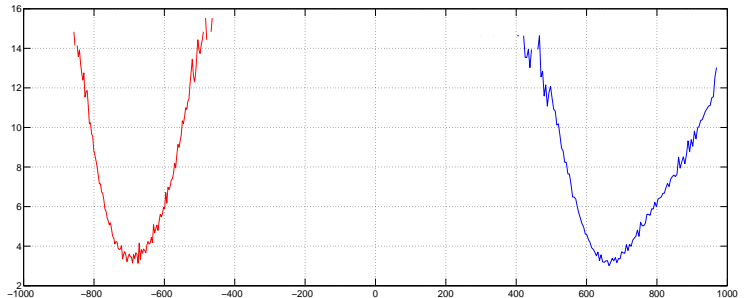
- This is why they obtain such good curve at the saddle point

Our approach to match their plots :

- Obtain fig. a and f using the photodiode data as they have done
- Obtain the fig. d **which is the exact point of transfer** using actual data and fitted curve

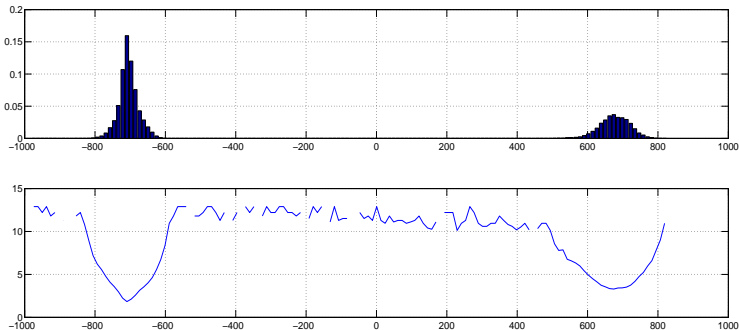
Our approach-2

Replicated fig.a and f with $R=3.2 K_B T$, $SD = 48.3$ nm, $L = 3.4 K_B T$, $SD = 37.1$ nm



Our approach-3

Replicated fig.d at exact point of transfer with blinks $L=7$, $R=1$
; $L = 2 K_B T$, $R = 3.3 K_B T$, Height = $12.5 K_B T$



Our approach-4

To obtain good curve at saddle points, following is done :

- Several datasets depicting the exact points of transfer are obtained
- Each individual potential well calculated using pdf is used via.

$$U_0(x, l_L) = -K_B T \ln[(P(x, l_L)]$$

- Several datasets averaged to depict actual wells
- Polynomial fitted for comparison

Outline

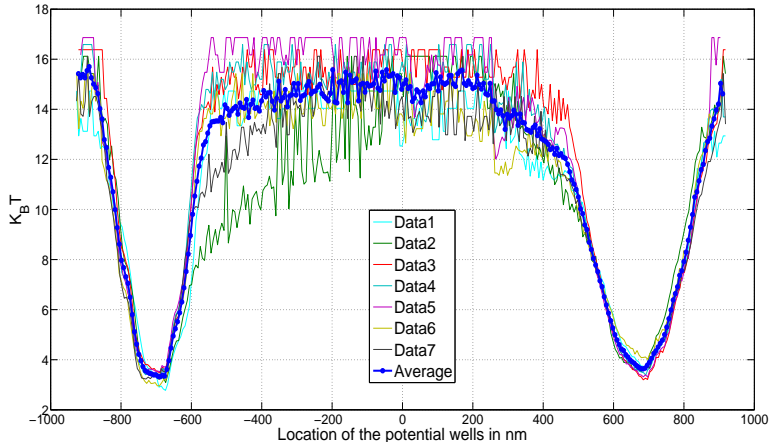
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Multiple Transfers - Several examples

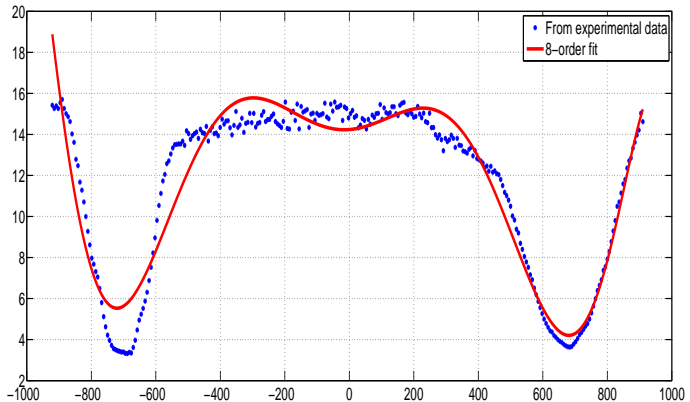
- Trap bead at +700; potential well formed at +700
- Total 12 blinks fixed : for equal potential, 6 blinks for each well, each blink for $20 \mu s$
- R \rightarrow L transition seen from 8,4 onwards i.e. 8,4...9,3...10,2 and 11,1
- To see the minimum tilt needed for this transition, 8,4 is fixed
- Modulate the on times as :

Total	Left	Right
12	6	6
12	7	5
12	8	4
12	6	6

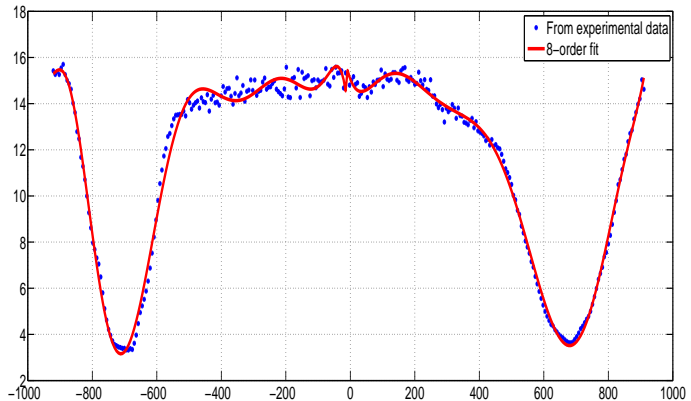
Averaging 7 instances of $R \rightarrow L$ transfer at 8,4 blinks



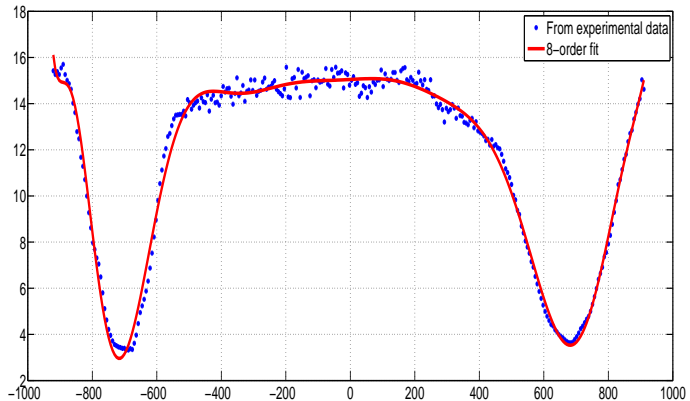
Polynomial fit- 8 th order, both wells together



Polynomial fit- 8 th order,R and L separately



Polynomial fit- 15 th order,both wells together



Inference

- Averaging multiple transfers gives good graphical representation of the 'saddle point'
- Fitting polynomial to both wells together needs higher order fit (at least 15th order here)
- Separately fitting R and L wells can be accomplished with lower order polynomials

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Idea

Directly using calculated work done :

- Calculate work done $W = \int_{t_1}^{t_2} F \cdot dx$; Heat dissipated
 $Q = - \int_{t_1}^{t_2} F \cdot dx$
- $\langle Q \rangle$ over several iterations should approach Landauer's limit $K_B T \ln(2)$

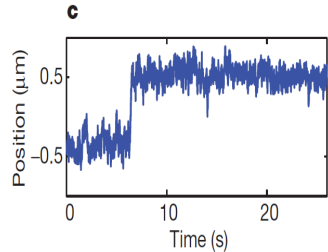
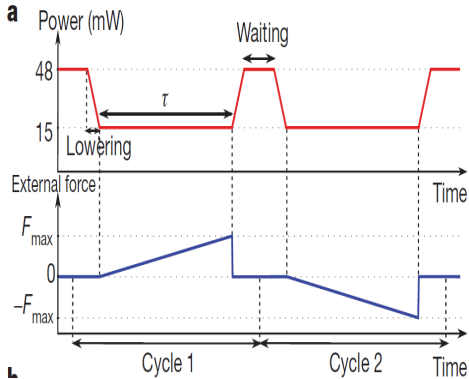
Using Jarzynski's equality :

- For a quasi-static process $\langle W \rangle \approx \Delta F$
- Using $\langle e^{-\beta W} \rangle = e^{-\beta \Delta F}$, find ΔF , the free energy difference
- The value $\Delta F_{eff} = -\ln(\langle e^{-\beta W} \rangle)$ is always close to the Landauer's limit $K_B T \ln(2)$, *independent of the maximal force or procedure duration**

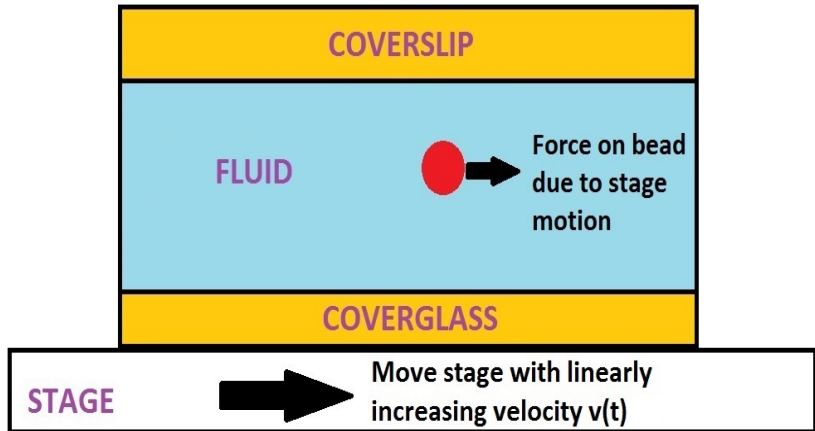
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Work done in the Nature paper



Work done in the Nature paper



Work done in the Nature paper

- Stage velocity v , viscous force on the bead $F = -\gamma v$
- During erasure, magnitude of force increased linearly during time τ as $F(t) = \pm F_{max} \cdot (t/\tau)$
- Heat dissipated during tilt :

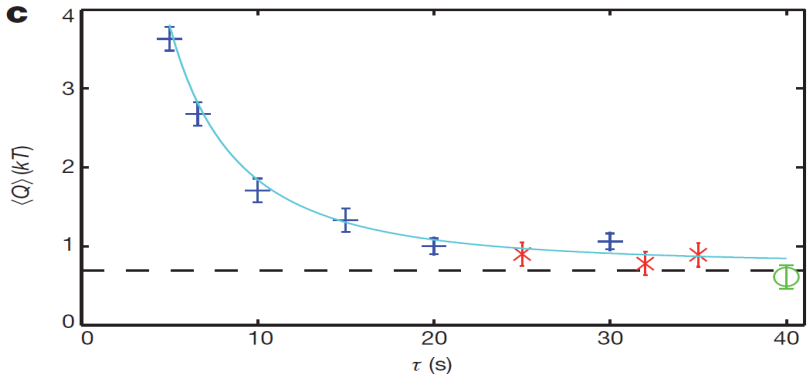
$$Q = - \int_0^{\tau_{cycle}} F(t) \dot{x}(t) dt = \pm \int_0^{\tau} F_{max}(t/\tau) \dot{x}(t) dt$$

- Velocity is calculated using the discretization

$$\dot{x}(t + \Delta t/2) \approx [x(t + \Delta t) - x(t)]/\Delta t$$

- For ideal quasi static erasure process ($\tau \rightarrow \infty$) the dissipated heat equals Landauer's value

Work done in the Nature paper



plus sign $r \geq 90\%$; cross sign $r \geq 85\%$; circle sign $r \geq 75\%$
where r is the success rate of the erasure protocol

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Free energy using Jarzynski

When $r \rightarrow 1$ we have $\langle e^{-\beta W} \rangle = 1/2$, then $\Delta F_{\text{eff}} \approx K_B T \ln(2)$
 All we need is the **work done**

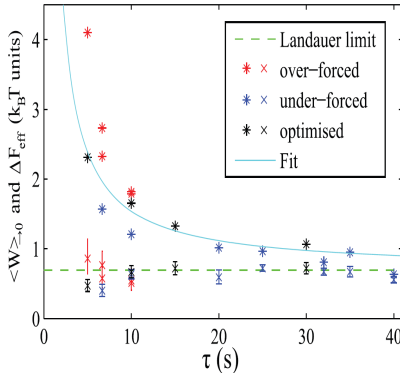


Fig. 3: (Colour on-line) Mean of the work (*) and effective free energy difference (x) for different procedures. The over-forced procedures (red) have a proportion of success $P_S \sim 95\%$, the optimized procedures (black) have $P_S > 91\%$, the under-forced procedures have $P_S > 83\%$ (except the last point, that has $P_S \approx 75\%$). The fit (blue line) is $\langle W(\tau) \rangle_{\tau \rightarrow 0} = k_B T \ln(2) + B/\tau$ with B a constant. For reader's convenience the error-bars on the mean work (*) are not shown but were estimated to be $\pm 0.15 k_B T$.

Inference

- 1 Work done calculated using $\int F \cdot dx$ and averaged over several cycles should approach Landauer's limit
- 2 This work done is the **work done by external agency on the bead during the tilting of the wells**
- 3 The free energy difference calculated using Jarzynski equality converges to the limit independent of the value of the maximal force or procedure duration, so **from experimental viewpoint, Jarzynski equality enables us to perform experiments over a shorter duration**
- 4 *Bottom-line* : We need to calculate work done in our case where tilting of wells is done by modulating the dwell times of the laser

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Using drag force on the bead

- Force on bead due to viscous drag

$$F_{drag} = -\gamma v = -6\pi\eta Rv$$

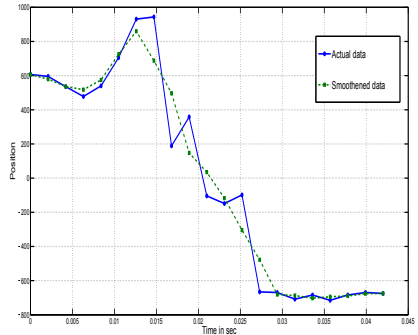
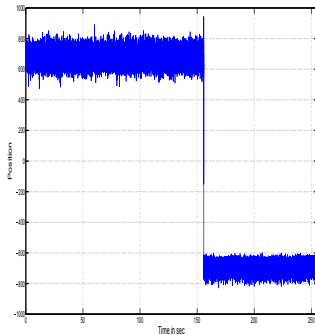
where η is viscosity coefficient for water, R is bead radius and v is relative velocity between bead and medium

- Work done = $\int_0^T F_{drag} dx = \int_0^T -(\gamma v) dx$
- Two calculations are done : (1) Using unfiltered data and (2) Using filtered data with a 3-point MA filter*
- Question : How to decide τ ? We first considered total time, then time just around the transfer

* In the nature paper, they've processed the images to increase precision before using them

Using drag force on the bead

Illustration on sample dataset



Calculations-1

$\eta = 8.9 \times 10^{-4} \text{ Pa.s}$ for distilled water at 25°C

$R = 500 \text{ nm}$ and $v = \text{velocity of bead} = dx/dt$

$dt = 0.002 \text{ sec}$ ($500 H_z$)

Dataset	Total data ($K_B T$)		Data around transfer ($K_B T$)	
	Unfiltered	Filtered	Unfiltered	Filtered
1	-111850	-17956	-2963.2	-814.87
2	-204420	-33144	-1502	-568.5
3	-169840	-32520	-12470	-382.8
4	-265370	-38830	-689.3	-251.93
5	-352990	-70021	-2351.3	-600.51
6	-112830	-19527	-34864	-590.9
7	-161950	-29409	-168937	-579.40

Clearly these are very high values !

Analysis

Issue I:

- The work done by drag force is dissipative
- Motion of bead in either + or - direction will add to the dissipative work
- Also, the more data points are considered, higher is be the work done calculated by this method
- Bead position detected has some noisy component as well, which gets captured. It is clearly evident that filtering helps, but still not significantly enough

Analysis

Issue II:

- Coefficient of friction used by Nature Paper is $\gamma = 1.89 \times 10^{-10} \text{Ns/m}$ for $2\mu\text{m}$ diameter bead, which translates to $\eta = 1.003 \times 10^{-5} \text{Pa.s}$ for our $1\mu\text{m}$ bead
- It is about **an order lower** than the η we use, which is the standard coefficient for distilled water
- To see its effect, I recalculated the work done using this lower η

Calculations-2

$\eta = 1.003 \times 10^{-5} \text{Pa.s}$ for distilled water at 25°C

$R = 500 \text{ nm}$ and $v = \text{velocity of bead} = dx/dt$

Dataset	Total data ($K_B T$)		Data around transfer ($K_B T$)	
	Unfiltered	Filtered	Unfiltered	Filtered
1	-1253.5	-201.22	-33.2	-9.131
2	-2290.8	-371.42	-16.83	-6.37
3	-1903.3	-364.42	-13.97	-4.289
4	-2301.5	-435.13	-7.724	-2.823
5	-3955.7	-784.68	-26.416	-6.729
6	-1264.4	-218.82	-39.06	-6.622
7	-1814.8	-329.56	-18.93	-6.4931

Analysis

- Clearly, the lower value of η has significant effect
- When combined with filtering and using data around transfer, work done values seem practical

Several questions arise, which have been listed next

Questions-1

- 1 Is this approach using drag forces (dissipative work) correct ? In that case, it makes sense to **use only the data around transfer**.
- 2 Perhaps truncating the data around transfer might help even more ?*
- 3 For calculating the drag force F_{drag} we use $F_{drag} = -\gamma v$ where v is the velocity of bead.
According to Stokes law, v is the relative velocity between fluid and bead; so our assumption here is that the fluid is stationary(as we're not moving the stage). Is that correct ?

Refer to rightmost column of table in the calculations-2 slide

Questions-2

- 1 The coefficient of viscosity η used in Nature paper (bidistilled water) is an order lower than ours (de-ionized water). *Deionization produces a high purity water that is generally similar to distilled water.* Which to use ?
- 2 Filtering (3-point MA filter, the smallest one possible) has significant effect. How to decide which one to use ?
- 3 In our case where tilting is done due to different dwell times of blinking, what is the external parameter ?
- 4 How do we calculate **work done on the bead** due to the variation of this external parameter ?

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Using total force on the bead

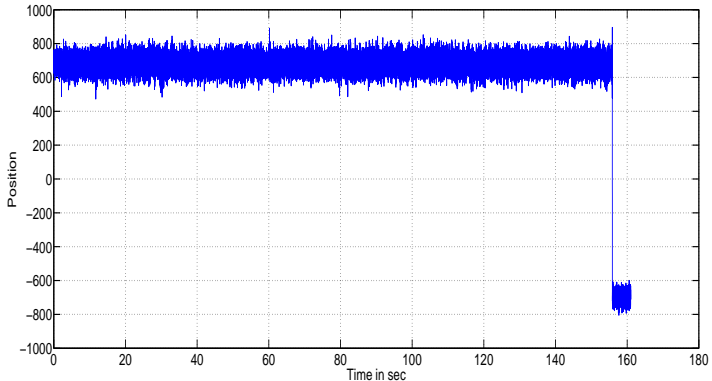
- Total force on bead at given instant:

$$F_{net} = m\ddot{x} = \frac{-\partial U}{\partial x} - \gamma v + noise$$

- For given polystyrene bead with diameter $1\mu m$ bead density $= 1.8189 \times 10^{12} beads/gm$; so individual bead mass $= 5.4978 \times 10^{-16} kg$
- Work done $= \int_0^\tau F_{net} dx$ where τ is *time until just after the bead transfer* and $F_{net} = m\ddot{x}$
- Work is calculated using unfiltered and MA filtered(window=3) bead position data

Using total force on the bead

Illustration on sample dataset. Transfer at 156 s, data till $\tau = 161$ s



Using total force $\rightarrow \tau$ just after transfer

τ is till just after transfer

Dataset	Work Done ($K_B T$)		Well Potential ($K_B T$)		ΔU
	Unfiltered	Filtered	U_2 (Left well)	U_1 (Right well)	$U_2 - U_1$ ($K_B T$)
1	-0.767	-0.075	2.8	3.68	-0.83
2	-3.21	-0.289	3.2	3.55	-0.35
3	-4.402	-0.4246	3.5	3.25	0.25
4	-4.4706	-0.4336	3.35	3.45	-0.10
5	-7.1814	-0.7003	3.55	3.35	0.20
6	-1.0911	-0.1037	3.0	4.05	-1.05
7	-2.855	-0.269	3.25	3.65	-0.40

Using total force $\rightarrow \tau$ is entire dataset

τ is entire dataset

Dataset	Work Done ($K_B T$)		Well Potential ($K_B T$)		ΔU
	Unfiltered	Filtered	U_2 (Left well)	U_1 (Right well)	$U_2 - U_1$ ($K_B T$)
1	-1.3901	-0.1303	2.8	3.68	-0.83
2	-7.8841	-0.6667	3.2	3.55	-0.35
3	-7.015	-0.6507	3.5	3.25	0.25
4	-8.5449	-0.7862	3.35	3.45	-0.10
5	-11.6882	-1.091	3.55	3.35	0.20
6	-2.8291	-0.2251	3.0	4.05	-1.05
7	-6.034	-0.5412	3.25	3.65	-0.40

Mean heat dissipated

Using work done : Heat dissipated $Q = - \int_0^T F dx$

	Unfiltered	Filtered
Data around transfer	3.4253	0.3279
Total data	6.4836	0.5845

Using Jarzynski: $\Delta F_{eff} = -\ln \langle e^{-\beta W} \rangle$

	Unfiltered	Filtered
Data around transfer	2.0265	0.3087
Total data	3.1107	0.5386