Molecular Dynamics study of melting in 2D, inversetwelfth -power interaction

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1 Introduction

Recently there has been a great deal of experimental and theoretical effort devoted to the study of the melting transition in two dimensions (2D). Experimental systems studied include the melting of mono-layers of rare-gas atoms on graphite, 2 electrons on He films, polystyrene spheres on water, and thin liquid-crystal films. Other simulation work on hard disk and L-J potential suggested that 2-D melting is a first order phase transition. There are also different analytic method also to study the phase transition like **Renormalization Group** method etc. The geometric packing fraction idea plays an important rule in study of melting in 2D. The important question is that computer simulation is really capable to capture the physics of phase transition in 2D. It is true indeed that all such simulation even for long run computer simulation corresponds to small time in the time scale of real laboratory. There is an important reason to choose an inverse power r^{-n} . Because there is no characteristic length in potential ,inverse power systems have useful scaling property which allows the entire equation of state to be determined from that of the single isotherm. Yes it is true indeed that the hard-disc system($n \to \infty$) is believed to have first order phase transition. Here we have shown a MD simulation for n=12 system with particular attention near the melting point. We are able to observe the phase separation in the pressure vs density curve in the coexistence region.

2 Basic introduction for phase transition

If you have a homogeneous single molecular species which can exist atmost in 3 phases(let's assume). Generally this kind of system is characterised by thermodynamic variables (mainly intensive quantities) e.g volume(V), density(ρ) and pressure(P)(there could be other variables as well like specific heat, specific entropy but lets keep it simple). All these are connected by some kind of equation of state. The system is best described if you express the system in terms of any of the two variables and observe the change of one in terms of other. For the better purpose of illustration we are going to show the P-V diagram(isotherms). As you keep on decreasing the temperature ,local interaction starts appearing and these leads to the system from gaseous to liquid phase.

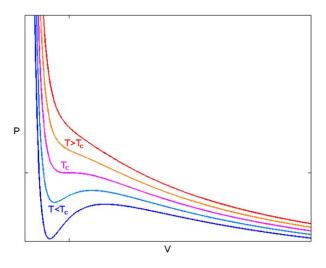


Figure 1: Phase Duagram of vanderwall gas

3 Algorithm for of pressure vs density with LJ potential

• Place the particles in triangular lattice initially, although they will move in continuum.

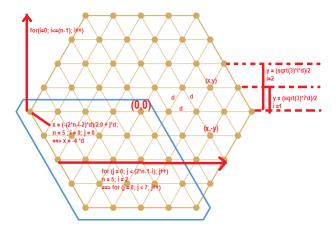


Figure 2: Placing the particle in a triangular lattice

- Calculate potential and force among neighboring particles.
- The update rule should be langevin equation in the overdamped limit i.e. with mass term zero and no change of velocity with time.
- Integration method used is modified euler update.

$$x_{t+1} = x_t + D\beta force_x \delta T + \eta_{aaussian} \sqrt{2D\delta T}$$
(1)

 δT is the time step which goes inside square root for dimensional consistency. D is the diffusion constant. $Force_x$ is the x-component of force, similarly there will be equation for y.

- Calculate the virial and from that calculate pressure
- variance of the pressure i.e. $\langle P^2 \rangle \langle P \rangle^2$.
- The formula for calculating virial pressure is given by,

$$p = \frac{k_B T N}{V} + \frac{1}{V d} \sum_{i < j} f(r_{ij}) r_{ij}. \tag{2}$$

where, V is the volume $f(r_{ij})$ is the force on particle i exerted by particle j, and r_{ij} is the vector going from i to j: $r_{ij} = r_j - r_i$, N is the total number of particles and d is the dimension of the system

• We have used **Langevin Thermostat** to keep the temperature of the system fixed. When we consider the motion of large particles through a continuum of smaller particles, Langevin equation

$$\frac{dp_i}{dt} = \left(\frac{\partial \phi(q)}{\partial q_i} - \gamma p_i + \delta p\right) \tag{3}$$

$$\frac{dq_i}{dt} = \frac{p_i}{m} \tag{4}$$

is taken into account. The smaller particles create a damping force to the momenta, $-\gamma p_i$, as the large particles push the smaller ones out of the way. The smaller(thermal) particles also move with kinetic energy and give random kicks to the large particles. σ , γ are connected by a fuctuation-dissipation relation $\sigma^2 = 2\gamma m_i k_B T$ in order to recover the canonical ensemble distribution.

At each time step Δt the Langevin thermostat changes the equation of motion so that the change in momenta is

$$\Delta p_i = \left(\frac{\partial \phi(q)}{\partial q_i} - \gamma p_i + \delta p\right) \Delta t \tag{5}$$

where γp_i damp the momenta and δp is a Gaussian distributed random number with probability

$$\rho(\delta p) = \frac{1}{\sqrt{2\pi}\sigma} exp(\frac{|\delta p|^2}{2\sigma^2})$$
 (6)

And standard deviation $\sigma^2 = 2\gamma m_i k_B T$. The random fluctuating force represents the thermal kicks from the small particles. The damping factor and the random force combine to give the correct canonical ensemble.

4 The System studied

We performed MD calculations for a system with 784 (26×30) particles of mass m interacting with the pair potential

$$u(r) = \epsilon (\sigma/r)^{12} \tag{7}$$

truncated at r =2.50 σ . Here σ has dimensions of length and ϵ energy. Assuming periodic-boundary conditions we confine the particles to a rectangular (very nearly square) unit cell whose ratio of height to width is (26/30) $(2/\sqrt{3}) = 1.00074$; this cell accommodates a section of a perfect unstrained hexagonal lattice. We generally used a time step $\Delta t = 0.00001 \times (\frac{\epsilon}{m\sigma^2})^{12}$ (In the following we use reduced units where a = e = m =1.) A typical (Einstein) vibrational period in the solid near the melting density is $(80-100)\Delta t$. Einstein assumed, for simplicity, that there was only one vibrational frequency, taking it to be an average if more than one frequency was present. This average frequency is now called the Einstein frequency E and one speaks of the Einstein single oscillator model.

5 The run time

Away from the phase-transition region only rela-tively short runs were required to achieve consistent results. We generally made an equilibration run of $25000\delta t$. Much shorter runs gave stable thermo-dynamic properties but some structural properties very sensitive to long-wavelength fluctuations such as the angular correlation function required the longer equilibration period. In the vicinity of the melting'transition $(0.97 \le p \le 1.02)$ much longer runs were made, particularly in the middle of this region where we attempted to distinguish between hexatic and two-phase behavior.

6 Programme

```
14 #define TIME 2.5
                             /*TOTAL TIME FOR EVOLUTION*/
15 #define TEMP 1.0
                                    /*TEMPERATURE OF THE HEAT BATH*/
16 #define Kb 1.0
                                   /*BOLTZMAN CONSTANT*/
17 #define deltaT 0.00001
                                     /*TIME steps*/
18 #define BETA 1/(Kb*TEMP)
                                   /*INVERSE OF ENERGY OF THE HEAT BATH*/
19 #define D 1/(BETA*GAMMA)
                                   /*DIFFUSION CONSTANT*/
20 #define T_START
                                         /*TIME FROM WHICH PRESSURE CALCULATION STARTED*/
21 #define R_CUT 2.5
22 #define DIMENSION 2.0
23
25 #define IM1 2147483563
26 #define IM2 2147483399
27 #define AM (1.0/IM1)
28 #define IMM1 (IM1-1)
29 #define IA1 40014
30 #define IA2 40692
31 #define IQ1 53668
32 #define IQ2 52774
33 #define IR1 12211
34 #define IR2 3791
35 #define NTAB 32
36 #define NDIV (1+IMM1/NTAB)
_{37} #define EPS 1.2e-7
38 #define RNMX (1.0-EPS)
39
   /* GAUSSIAN RANDOM NUMBER GENERATOR*/
41
42
  float ran2 (long idum)
43 {
     int j;
44
45
     long k;
     static long idum2=123456789;
46
47
     static long iy=0;
     static long iv [NTAB];
48
     float temp;
49
50
     \begin{array}{ll} \mbox{if } (\mbox{idum} <= 0) \ \{ \\ \mbox{if } (-(\mbox{idum}) < 1) \ \mbox{idum} = 1; \end{array}
51
       else idum = -(idum);
53
       idum2=(idum);
       for (j=NTAB+7; j>=0; j--) {
55
         k = (idum)/IQ1;
56
         idum{=}IA1*(idum{-}k*IQ1){-}k*IR1;\\
57
         if (idum < 0) idum += IM1;
58
         if (j < NTAB) iv [j] = idum;
59
60
       iy=iv[0];
61
62
63
     k = (idum)/IQ1;
     idum{=}IA1*(idum{-}k*IQ1){-}k*IR1;\\
64
     if (idum < 0) idum += IM1;
65
     k=idum2/IQ2;
66
     idum2=IA2*(idum2-k*IQ2)-k*IR2;
67
     if (idum2 < 0) idum2 += IM2;
68
69
     j=iy/NDIV;
     iy=iv[j]-idum2;
70
     iv[j] = idum;
71
     if (iy < 1) iy += IMM1;
72
73
     if ((temp=AM*iy) > RNMX) return RNMX;
74
     else return temp;
75 }
76 #undef IM1
77 #undef IM2
78 #undef AM
79 #undef IMM1
80 #undef IA1
81 #undef IA2
82 #undef IQ1
83 #undef IQ2
84 #undef IR1
```

```
85 #undef IR2
86 #undef NTAB
87 #undef NDIV
88 #undef EPS
89 #undef RNMX
90 float gasdev(long idum)
91 {
92
      float ran1(long idum);
      static int iset=0;
93
      static float gset;
94
      float fac, rsq, v1, v2;
95
96
      if (idum < 0) iset = 0;
97
98
         (iset = 0) {
99
       do {
          v1 = 2.0 * ran2 (idum) - 1.0;
100
          v2=2.0*ran2(idum)-1.0;
          rsq=v1*v1+v2*v2;
102
        \} while (rsq >= 1.0 || rsq == 0.0);
103
        fac = sqrt(-2.0*log(rsq)/rsq);
104
        gset=v1*fac;
105
        iset=1;
106
        \textcolor{return}{\texttt{return}} \ v2*fac \; ;
      } else {
108
109
        i s e t = 0;
        return gset;
110
111
112 }
113
114 struct particles
115 {
                                 /*X COORDINATES OF THE PARTICLES*/
116
        float x;
        float y;
                                 /*Y COORDINATES OF THE PARTICLES*/
                                 /*X COORDINATES USED DURING EULER UPDATES*/
        float x_euler;
118
        float y_euler;
                                 /*Y COORDINATEDS*/
119
        int n_number;
                                 /*NUMBER OF NEIGHBOR PARTICLES*/
120
                                 /*MAXIMUM DISPLACEMENT OF THE PARTICLES STARTING FROM A PARTICULAR
        float max_disp;
121
       TIME*/
float force1_x;
122
                                 /*FORCE ALONG THE X-DIRECTION BY THE NEIGHBORING PARTICLES BEFORE
       EULER UPDATE*/
        float force1_y;
                                 /*FORCE ALONG THE Y-DIRECTION BY THE NEIGHBORING PARTICLES BEFORE
123
       EULER UPDATE*/
                                 /*FORCE CALCULATED FROM COORDINATES OF EULER UPDATE*/
        float force2_x;
                                 /*FORCE CALCULATED FROM COORDINATES OF EULER UPDATE*/
        float force2_y;
   };
126
127
   /*....... Define the L-J potential......... as (4/r^12)*/
128
129 float WCAPOT(float r)
130
131 float f;
_{132} f=4.0/pow(r,12.0);
   return (f);
133
134
135
136
137 void main()
   {
138
139
140
141
        FILE *f5;
142
        f5=fopen("DENSITY_PRESSURE_VARIANCE.DAT", "w");
143
        long seed = 1;
144
        \begin{array}{ll} \textbf{float} & \max=0, \min=0, \; ENERGY=0.0\,, dr\,, t\,, a\,, h\,, Lx\,, Ly\,, dx\,, dy\,; \end{array}
145
        int i,j,counter=0,ensemble;
146
        struct particles arr[NOP];
147
        float VOLUME, PRESSURE=0.0, DENSITY, VIR=0.0, VAR=0.0, PRESSURESQUARED=0.0, force_x=0.0,
148
        force_y = 0.0, force = 0.0;
149
151 for (DENSITY=0.9; DENSITY<=.9; DENSITY+=0.01)
```

```
{
154
              a=sqrt(2/(sqrt(3)*DENSITY));
              h = sqrt(3) *a/2;
156
              a=floorf(a*100)/100;
157
              h=floorf(h*100)/100;
158
159
               Lx=sqrt (NOP) *a;
161
               Ly = sqrt(NOP) *h;
162
163
               VOLUME=Lx*Ly;
164
166
167
                * DISTRIBUTING THE PARTICLES IN A TRIANGULAR LATTICE*
168
169
          for (i=0; i < sqrt (NOP); i++)
170
171
           for (j=0; j < sqrt(NOP); j++)
172
173
               if (i%2==0)
174
175
               arr [counter]. x=j*a-Lx/2.0;
               arr[counter].y=h*i-Ly/2.0;
177
178
               arr \left[ \hspace{0.1cm} counter \hspace{0.1cm} \right]. \hspace{0.1cm} x\hspace{-0.1cm}=\hspace{-0.1cm} floorf \hspace{0.1cm} \left( \hspace{0.1cm} arr \hspace{0.1cm} \left[ \hspace{0.1cm} counter \hspace{0.1cm} \right]. \hspace{0.1cm} x\hspace{-0.1cm} *\hspace{-0.1cm} 100 \right) / 100;
179
               arr [counter].y=floorf(arr [counter].y*100)/100;
180
181
182
              else if (i %2!=0)
183
184
               arr [counter]. x=(j+0.5)*a-Lx/2.0;
               arr[counter].y=i*h-Ly/2.0;
186
               arr [counter].x=floorf(arr [counter].x*100)/100;
187
               arr [counter].y=floorf(arr [counter].y*100)/100;
188
189
190
               counter++;
192
    counter = 0:
193
194
195
               /*EVOLUTION OF THE SYSTEM THROUGH TIME*/
196
197
    counter = 0:
198
    for(t=0;t=TIME;t+=deltaT)
199
200
              /*INITIALIZATION*/
201
     for (i=0; i \triangleleft NOP; i++)
202
     {
203
           arr[i].force1_x=0;
204
           arr[i].force1_y=0;
205
           arr[i].force2_x=0;
206
207
           arr[i].force2_y=0;
     }
208
209
               /*FINDING THE FORCE ALONG THE X AND Y DIRECTION BY ALL THE PARTICLES—BEFORE EULER
210
          UPDATE*/
211
               /*
          for (i = 0; i < NOP-1; i++)
212
213
          for(j=i+1; j < NOP; j++)
214
215
               dx=arr[i].x-arr[j].x;
216
               dx=dx-Lx*rint(dx/Lx);
217
```

```
218
            dy=arr[i].y-arr[j].y;
219
220
            dy=dy-Ly*rint(dy/Ly);
221
             dr = sqrt(pow(dx,2) + pow(dy,2));
223
             force_x=dx*12/pow(dr,14);
224
225
             force_y=dy*12/pow(dr,14);
226
227
             if (dr<R_CUT)
228
229
             arr[i].force1_x+=force_x;
             arr[i].force1_y+=force_y;
230
231
232
             arr[j].force1_x+=-force_x;
             arr[j].force1_y+=-force_y;
233
234
235
        }
236
237
             /*EULER UPDATE OF COORDINATES*/
238
239
           for (i=0; i < NOP; i++)
240
241
242
             arr[i].x_euler=arr[i].x+D*BETA*arr[i].force1_x*deltaT+gasdev(seed)*sqrt(2*D*deltaT);
243
244
             arr[i].x_euler=arr[i].x_euler-Lx*rint(arr[i].x_euler/Lx);
245
             arr[i].y-euler=arr[i].y+D*BETA*arr[i].force1_y*deltaT+gasdev(seed)*sqrt(2*D*deltaT);
246
            arr[i].y_euler=arr[i].y_euler-Ly*rint(arr[i].y_euler/Ly);
247
248
249
250
             /*FINDING THE FORCE ALONG THE X AND Y DIRECTION BY THE NEIGHBORING PARTICLES—AFTER
251
       EULER UPDATE*/
252
        */
253
254
   for (i = 0; i < NOP - 1; i + +)
255
256
        for (j=i+1; j < NOP; j++)
257
            dx=arr[i].x_euler-arr[j].x_euler;
259
            dx=dx-Lx*rint(dx/Lx);
260
261
            dy=arr[i].y_euler-arr[j].y_euler;
262
263
            dy=dy-Ly*rint(dy/Ly);
264
             dr = sqrt(pow(dx,2) + pow(dy,2));
265
266
             force_x=dx*12/pow(dr,14);
267
268
             force_-y\!=\!\!dy\!*\!12/pow(dr\,,\!14)\;;
269
             if(dr < R_CUT)
271
272
             {
273
             arr[i].force2_x+=force_x;
274
275
             arr[i].force2_y+=force_y;
             arr[j].force2_x+=-force_x;
277
             arr[j].force2_y+=-force_y;
278
279
280
        }
281
282
283 }
```

```
284
285
   for (i = 0; i < NOP; i++)
286
287
             arr[i].x=arr[i].x+D*BETA*0.5*(arr[i].force1_x+arr[i].force2_x)*deltaT+gasdev(seed)*
289
        sqrt(2*D*deltaT);
290
             arr[i].x=arr[i].x-Lx*rint(arr[i].x/Lx);
291
             arr[i].y=arr[i].y+D*BETA*0.5*(arr[i].force1_y+arr[i].force2_y)*deltaT+gasdev(seed)*
        sqrt(2*D*deltaT);
293
             arr[i].y=arr[i].y-Ly*rint(arr[i].y/Ly);
294
295
297
298
299
   if (t>=T_START)
300
301
302
       /*CALCULATION OF VIRIAL*/
303
304
       for (i = 0; i < NOP - 1; i + +)
305
306
           for (j=i+1; j \le NOP; j++)
307
308
            dx=arr[i].x-arr[j].x;
309
310
            dx=dx-Lx*rint(dx/Lx);
311
            dy=arr[i].y-arr[j].y;
312
313
            dy=dy-Ly*rint(dy/Ly);
314
             dr = sqrt(pow(dx,2) + pow(dy,2));
315
316
             force = 12.0/pow(dr, 13.0);
317
318
             if (dr<R_CUT)
319
320
                VIR+=dr*force;
321
322
323
       /*PRESSURE CALCULATION*/
324
325
326
327
      PRESSURE+=(DENSITY/BETA)+VIR/(DIMENSION*VOLUME);
      PRESSURE_SQUARED+=pow((DENSITY/BETA)+VIR/(DIMENSION*VOLUME),2);
328
       VIR = 0.0;
329
330
   }//TIME LOOP
331
      VAR=sqrt (PRESSURE.SQUARED/((TIME-T.START)/deltaT)-pow(PRESSURE/((TIME-T.START)/deltaT), 2)
332
       fprintf(f5, "%f %f %f\n", DENSITY, PRESSURE/((TIME-T_START)/deltaT), VAR);
333
334
   VIR = 0.0;
335
336
   PRESSURE = 0.0;
   PRESSURE_SQUARED = 0.0;
337
338
339
340
        }//DENSITY LOOP
341
342 }//MAIN
```

7 Plot

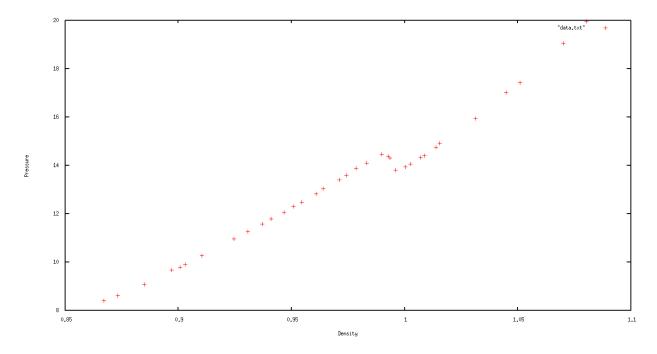


Figure 3: Density vs pressure data

8 The Explanation of our result

8.1 Equation of state

In this section we examine the behavior of the pressure along the T=1 isotherm to try to determine the nature of the phase transition. There are some practical advantages in analyzing thermodynamic functions along an isotherm rather than an isochore since distinctions between behavior expected for first and higherorder transitions are more apparent. In an infinite system the constant pressure in the two-phase region along an isotherm implies a very large change in slope of the P- ρ curve. This change is less noticeable along an isochore and is more easily confused with the behavior expected for a continuous transition. These advantages persist for finite systems. Mayer and Wood have analyzed the behavior to be expected along an isotherm at a first-order transition for a finite system at equilibrium with periodic-boundary conditions. They find there should be a symmetric loop in the P- ρ curve in the two-phase region. Because of the nonzero interface tension between the fluid and solid phases, the finite system initially overshoots the infinite system's coexistence pressure in the F traverse to avoid forming a "droplet" of the solid phase. Similar arguments apply to the S traverse. The size of the overshoot is an increasing function of $\frac{\tau}{N^{12}}$ where τ is the interface tension, and it vanishes in the limit $N \to \infty$. There can be regions in the loop where $\frac{\partial P}{\partial \rho_T} < 0$, which of course violates stability for an infinite system. Such a region in the P- ρ plane seems very hard to explain except by assuming a nonzero interface tension between two phases. The analysis of Mayer and Wood ignores fluctuations and hence probably overestimates the size of the overshoot and is by no means rigorous, but does give a reasonable first approximation to the behavior that might be expected at a classical first-order transition for a finite system.

8.2 The Experimental Evidence

Melting is considered to be one of the most fundamental problems in physical science. Generally, dimensionality plays an important role in melting. In three-dimension, it's well known that a crystal melts directly into a liquid via a first-order transition. In two-dimension (2D), however, the melting process has been widely debated whether it is a first-order transition or a two-step transition with an intermediate hexatic

phase. Experimentally 2D melting has been intensively studied in equilibrium systems such as molecular and colloidal crystals, but rarely been explored in non-equilibrium system such as granular materials. In this paper, people experimentally studied the 2D melting in a driven granular model system at single particle level using video recording and particle tracking techniques. Measurements of orientational/translational correlation functions show evidences that the melting is a two-step transition. A novel concept of orientational/translational susceptibilities enable us to clearly resolve the intermediate hexatic phase. Our results are in excellent agreement with the two-step melting scenario predicted by KTHNY theory, and demonstrate that the KTHNY melting scenario can be extended to non-equilibrium systems. The following plot confirm you there is phase transition from solid to liquid phase

The structure factor F_{hkl} is a mathematical function describing the amplitude and phase of a wave diffracted from crystal lattice planes characterised by Miller indices h,k,l.

The structure factor may be expressed as

$$F_{hkl} = F_{hkl} exp(i\alpha_{hkl})$$

$$= \sum_{j} f_{j} exp[2\pi i(hx_{j} + ky_{j} + lz_{j})]$$

$$= \sum_{j} f_{j} cos[2\pi (hx_{j} + ky_{j} + lz_{j})] + i \sum_{j} f_{j} sin[2\pi (hx_{j} + ky_{j} + lz_{j})$$

$$= A_{hkl} + iB_{hkl}$$
(8)

where the sum is over all atoms in the unit cell, x_j, y_j, z_j are the positional coordinates of the jth atom, f_j is the scattering factor of the jth atom, and α_{hkl} is the phase of the diffracted beam. Structure factor physically

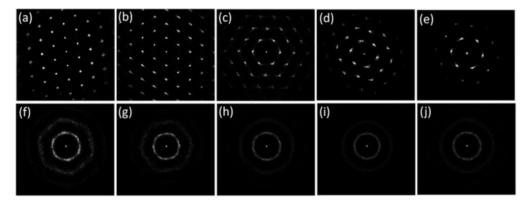


Figure 4: Change of structure factor from the solid to liquid transition

means that how closely the lattice is packed, the intensity in structure factor in solid phase is larger than liquid phase. The above diagram shows that intensity decrease with the decrease of density.

9 References

- Molecular Dynamics study of melting in two dimensions, inverse- twelfth -power interaction by Jeremy Q. Broughton, George H. Gilmer, and John D. Weeks
- Berezinskii–Kosterlitz–Thouless transition and two-dimensional melting* by V N Ryzhov, E E Tareyeva, Yu D Fomin and E N Tsiok