

# Galileo Masterclass Brazil (GMB) 2022

## Lecture 2 - Spread Spectrum Ranging

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# Outline

Time-Delay Estimation

Signal Properties

Examples for Signal Design

# Maximum Likelihood Time-Delay Estimation (1)

For

$$\mathbf{x} = \mathbf{x}[0]$$

let us assume a random variable  $\mathbf{x}$  has a multivariate Gaussian probability density function (pdf) parameterized by the parameter  $\tau$  and thus we get

$$p_{\mathbf{x}}(\mathbf{x}; \tau) = \frac{1}{(2\pi\sigma_n^2)^{N/2}} \exp \left[ -\frac{\|\mathbf{x} - \sqrt{P}\mathbf{c}(\tau)\|_2^2}{2\sigma_n^2} \right]$$

The likelihood function with respect to the parameter  $\tau$  is given as

$$L(\mathbf{x}; \tau) = p_{\mathbf{x}}(\mathbf{x}; \tau)$$

- ▶  $L(\mathbf{x}; \tau)$  is a function of the parameter  $\tau$ , which is to be estimated at a given realization of the random variable  $\mathbf{x}$
- ▶ The pdf  $p_{\mathbf{x}}(\mathbf{x}; \tau)$  is a function of the realization of the random variable  $\mathbf{x}$  for a fixed value of the parameter  $\tau$

## Maximum Likelihood Time-Delay Estimation (2)

Now the maximum likelihood estimator (MLE) can be given as

$$\hat{\tau} = \arg \max_{\tau} \{L(\mathbf{x}; \tau)\} = \arg \max_{\tau} \{\log (L(\mathbf{x}; \tau))\}.$$

The MLE is asymptotically (large  $N$ ) unbiased and efficient.  
When further deriving the estimator we get

$$\begin{aligned}\hat{\tau} &= \arg \max_{\tau} \{\log (L(\mathbf{x}; \tau))\} \\ &= \arg \max_{\tau} \left\{ \log(1) - \log \left( (2\pi\sigma_n^2)^{N/2} \right) - \frac{1}{2\sigma_n^2} \|\mathbf{x} - \sqrt{P}\mathbf{c}(\tau)\|_2^2 \right\} \\ &= \arg \max_{\tau} \left\{ -\|\mathbf{x}\|_2^2 + 2\sqrt{P}\mathbf{x}^T\mathbf{c}(\tau) - P\|\mathbf{c}(\tau)\|_2^2 \right\}\end{aligned}$$

As the first term does not depend on  $\tau$  and the third term is constant with  $\|\mathbf{c}(\tau)\|_2^2 \approx N, \forall_{\tau}$  as well as dropping the constant factor  $2\sqrt{P}$  we can write

$$\hat{\tau} = \arg \max_{\tau} \{\mathbf{x}^T\mathbf{c}(\tau)\} = \arg \max_{\tau} \{J(\tau)\}$$

# Time-Delay Estimation with a Delay Locked Loop (DLL) (1)

In practice, time-delay estimation is performed using a DLL applying a gradient ascent method (step size  $\mu > 0$ ) where the  $k$ th iteration can be given as

$$\hat{\tau}[k] = \hat{\tau}[k-1] + \mu \frac{\partial J(\hat{\tau}[k-1])}{\partial \tau}$$

The derivative can be approximated using the central difference quotient of length  $2\Delta$ ,

$$\begin{aligned}\hat{\tau}[k] &= \hat{\tau}[k-1] + \frac{\mu}{2\Delta} (J(\hat{\tau}[k-1] + \Delta) - J(\hat{\tau}[k-1] - \Delta)) \\ &= \hat{\tau}[k-1] + \frac{\mu}{2\Delta} (\mathbf{x}^T \mathbf{c}(\hat{\tau}[k-1] + \Delta) - \mathbf{x}^T \mathbf{c}(\hat{\tau}[k-1] - \Delta))\end{aligned}$$

A stochastic version (considering successive periods  $k$ ) can be given as

$$\begin{aligned}\hat{\tau}[k] &= \hat{\tau}[k-1] + \frac{\mu}{2\Delta} (\mathbf{x}^T[k-1] \mathbf{c}(\hat{\tau}[k-1] + \Delta) \\ &\quad - \mathbf{x}^T[k-1] \mathbf{c}(\hat{\tau}[k-1] - \Delta))\end{aligned}$$

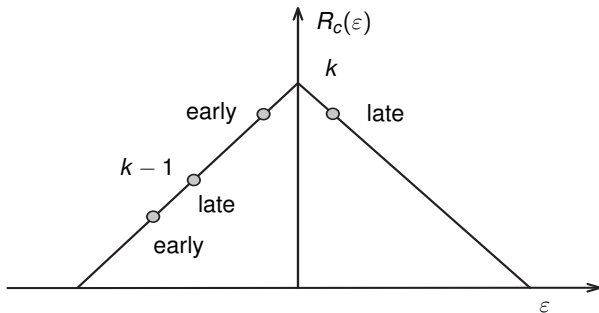
# Time-Delay Estimation with a Delay Locked Loop (DLL) (2)

Without noise, assuming that the receiver uses signal matched correlators, and the time-delay tracking error

$$\varepsilon = \tau - \hat{\tau}$$

the discriminator S-curve for a coherent early-late DLL is

$$S(\varepsilon) = R_c(\varepsilon - \Delta) - R_c(\varepsilon + \Delta)$$
$$S[k; \varepsilon[k]] = R_c[\varepsilon[k] - \Delta] - R_c[\varepsilon[k] + \Delta].$$



# Cramer-Rao Lower Bound (CRLB) (1)

If

$$\mathbb{E} \left[ \frac{\partial \log(L(\mathbf{x}; \tau))}{\partial \tau} \right] = 0$$

the variance of the time-delay estimation error  $\sigma_{\hat{\tau}}^2$  of any unbiased estimator is lower bounded by the Cramer Rao lower bound (CRLB)

$$\text{var}(\hat{\tau}) = \sigma_{\hat{\tau}}^2 \geq \frac{1}{-\mathbb{E} \left[ \frac{\partial^2 \log(L(\mathbf{x}; \tau))}{\partial \tau^2} \right]} = \frac{\frac{\sigma_n^2}{P}}{\frac{\partial \mathbf{c}^T(\tau)}{\partial \tau} \frac{\partial \mathbf{c}(\tau)}{\partial \tau}}$$

which leads to

$$\sigma_{\hat{\tau}}^2 \geq \frac{B_n}{\frac{P}{N_0}} \frac{1}{4\pi^2 \int_{-\infty}^{\infty} f^2 |P(f)|^2 df}$$

where  $B_n$  is the equivalent noise bandwidth of the generic estimator and

$$\int_{-\infty}^{\infty} |P(f)|^2 df = 1$$

## Cramer-Rao Lower Bound (CRLB) (2)

The term  $\int_{-\infty}^{\infty} f^2 |P(f)|^2 df$  is:

- ▶ Second moment of the power spectrum
- ▶ Root mean square (RMS) bandwidth
- ▶ Gabor bandwidth

It is equal to the curvature of  $R_c(\varepsilon)$  at  $\varepsilon = 0$

$$\int_{-\infty}^{\infty} f^2 |P(f)|^2 df = -\frac{1}{4\pi^2} \left. \frac{d^2 R_c(\varepsilon)}{d\varepsilon^2} \right|_{\varepsilon=0}$$

and if  $p(t)$  is band-limited to  $[-B, B]$  it is upper bounded by

$$\int_{-B}^B f^2 |P(f)|^2 df \leq \int_{-B}^B B^2 |P(f)|^2 df \leq B^2 \quad \text{s.t.} \quad \int_{-B}^B |P(f)|^2 df = 1$$

Thus,  $|P(f)|^2 = \frac{1}{2} (\delta(f - B) + \delta(f + B))$  maximizes the Gabor bandwidth and  $p(t) = \cos(2\pi Bt)$  or  $p(t) = \sin(2\pi Bt)$ .



# Outline

Time-Delay Estimation

Signal Properties

Examples for Signal Design

# Synchronization Accuracy

- ▶ The higher the Gabor bandwidth of the signal, the higher the synchronization accuracy that can be achieved in terms of the CRLB
- ▶ The second moment of the power spectrum of a signal with bandwidth  $B$  is upper bounded by  $B^2 \Rightarrow$  The higher the available signal bandwidth, the higher the possible synchronization accuracy
- ▶ A high processing gain  $G$  is desirable (large bandwidth  $B$ )  $\Rightarrow$  high synchronization accuracy, high interference robustness, and low MAI-A
- ▶ Minimizing the CRLB for  $\tau$  and maximizing time concentration are contradictory tasks

## We can state:

The lower the CRLB for  $\tau$  ( $\text{CRLB} \rightarrow \frac{1}{B^2}$ )  $\Rightarrow$  the lower time concentration of  $p(t)$  ( $p(t) \rightarrow \sin(2B\pi t)$  or  $\cos(2B\pi t)$ )

# Time Concentration (1)

Time and frequency concentration of  $p(t)$  can be given by the quantities:

$$\alpha = \frac{\int_{-T_c/2}^{T_c/2} |p(t)|^2 dt}{\int_{-\infty}^{\infty} |p(t)|^2 dt} \quad \beta = \frac{\int_{-B}^B |P(f)|^2 df}{\int_{-\infty}^{\infty} |P(f)|^2 df}$$

with

$$\int_{-\infty}^{\infty} |P(f)|^2 df = \int_{-\infty}^{\infty} |p(t)|^2 dt = 1$$

and  $p(t)$  being strictly band-limited to  $[-B, B] \Rightarrow \beta = 1$ , and (uncertainty principle of Fourier transform) we get

$$\int_{-T_c/2}^{T_c/2} |p(t)|^2 dt = \alpha < 1$$

## Time Concentration (2)

The maximum of the absolute value of the sidelobes of  $R_c(\varepsilon)$  is given as

$$\forall_{i \in \mathbb{N}} |\nu_i| \leq \kappa, \quad \kappa \in [0, 1]$$

$\nu_i$  denote the value of  $R_c(\varepsilon)$  at the sidelobes, besides the global maximum of  $R_c(\varepsilon)$  at  $\varepsilon = 0$ .

We can state:

1. The higher the sidelobes of  $R_c(\varepsilon) \Rightarrow$  the higher the sidelobes of  $p(t) \Rightarrow$  the lower time concentration of  $p(t)$
2. The higher the sidelobes of  $R_c(\varepsilon) \Rightarrow$  the higher  $\kappa \Rightarrow$  the less robust the estimation of  $\tau$  (likelihood has local maxima besides the global maximum)

# Multiple Access Interference (1)

- ▶ MAI-A and MAI-R can be considered as additional interference components with zero mean
- ▶ In general both MAI-A and MAI-R are dependent on the propagation characteristics of the transmitted signal
- ▶  $U$  users (*e.g.* visible GNSS satellites) with  $u = 1, \dots, U$  and power  $P_u$  causing MAI-A
- ▶  $V$  users of another system (*e.g.* visible satellites of a different GNSS) with  $v = 1, \dots, V$  and power  $P_v$  are causing MAI-R
- ▶ The received signal of another system (*e.g.* different GNSS) in the same frequency band has PSD  $\Phi_R(f)$
- ▶ The reference PR sequence generator is perfectly synchronized with the received desired signal with power  $P$ , so the time-delay  $\tau$  of the desired signal is known
- ▶ The receiver was able to perform down conversion, matched filtering with  $P^*(f)$ , and sampling at the chip duration

## Multiple Access Interference (2)

We can define the statistics of the matched filter output for a WSCS sequence  $\{d_m\} \in \{-1, 1\}$  with period  $T_d = N_d T_c$  as

$$\text{SINR} = \frac{P}{P_N + P_A + P_R}$$

where the noise power can be given as

$$P_N = \frac{1}{N_d T_c} \frac{N_0}{2} \int_{-\infty}^{\infty} |P(f)|^2 df = \frac{N_0}{2N_d T_c} = \frac{N_0}{2T_d}$$

the power of the MAI-A can be given as

$$P_A = \frac{1}{2N_d T_c} \sum_{u=1}^U P_u \int_{-\infty}^{\infty} |P(f)|^4 df$$

and the power of the MAI-R can be given as

$$P_R = \frac{1}{2N_d T_c} \sum_{v=1}^V P_v \int_{-\infty}^{\infty} |P(f)|^2 \Phi_R(f) df$$

## Multiple Access Interference (3)

- ▶ The background noise is assumed as white Gaussian noise with spectral density of  $N_0/2$
- ▶ The variance due to background noise can be considered as white noise of density  $N_0/2$  filtered by the transfer function of the receive filter  $P^*(f)$
- ▶ All  $u$  users (*e.g.* visible GNSS satellites) are assumed to be independent and unsynchronized with the desired signal
- ▶ It is assumed that their time-delays are independently uniformly distributed in  $[0, T_c]$  and their phases are independently uniformly distributed in  $[0, 2\pi]$
- ▶ The effect of the  $u$ -th user (*e.g.* GNSS satellite) on the matched filter output of the desired signal will be that of white noise passed through the tandem combination of two filters with the transfer functions  $|P(f)|^2 \Rightarrow \text{MAI-A}$
- ▶ Similar assumptions as for the  $u$  users above can be taken for the  $v$  users  $\Rightarrow \text{MAI-R}$

## Multiple Access Interference (4)

The ratio of the SNR to the SINR can be given as

$$\begin{aligned}\Delta\text{SNR} &= \frac{\text{SNR}}{\text{SINR}} = \frac{P/P_N}{P/(P_N + P_A + P_R)} = 1 + \frac{P_A + P_R}{P_N} \\ &= 1 + \sum_{u=1}^U \frac{P_u}{N_0} \int_{-B}^B |P(f)|^4 df + \sum_{v=1}^V \frac{P_v}{N_0} \int_{-\infty}^{\infty} |P(f)|^2 \Phi_R(f) df\end{aligned}$$

The variance of the MAI-A component can be lower bounded by

$$\int_{-B}^B |P(f)|^4 df \geq \frac{1}{2B}$$

with equality iff

$$|P(f)|^2 = \frac{1}{2B}, \quad -B \leq f \leq B, \quad p(t) = \sqrt{2B} \frac{\sin(2\pi Bt)}{2\pi Bt}$$



## Multiple Access Interference (5)

A proof can be given by using the Schwarz inequality:

$$\int_{-B}^B |X_1(f)|^2 df \int_{-B}^B |X_2(f)|^2 df \geq \left[ \int_{-B}^B X_1(f) X_2(f) df \right]^2$$

Suppose that  $X_1(f) = |P(f)|^2$ ,  $X_2(f) = 1$  and  $\int_{-B}^B |P(f)|^2 df = 1$ , it follows that

$$\int_{-B}^B |P(f)|^4 df \cdot 2B \geq \left[ \int_{-B}^B |P(f)|^2 df \right]^2 = 1$$

Thus we get,

$$\int_{-B}^B |P(f)|^4 df \geq \frac{1}{2B}$$

# Multiple Access Interference (6)

- ▶ Assumptions for MAI-A and MAI-R are derived following IS-95 and CDMA2000 standards
- ▶ In GNSS MAI-A and MAI-R are called spectral separation
- ▶ The term  $\int_{-\infty}^{\infty} |P(f)|^2 \Phi_R(f) df$  is called spectral separation coefficient (SSC)
- ▶ The term  $\int_{-\infty}^{\infty} |P(f)|^4 df$  is called self SSC
- ▶ MAI-A and MAI-R has to be considered in signal design (chip pulse shape design) or can be treated in the receiver (multi-user detection and mitigation)

We define the CRLB-I as the CRLB which considers noise plus interference (MAI-A, MAI-R):

$$\tilde{\sigma}_{\hat{\tau}}^2 \geq \sigma_{\hat{\tau}}^2 \cdot \Delta \text{SNR}$$

# Outline

Time-Delay Estimation

Signal Properties

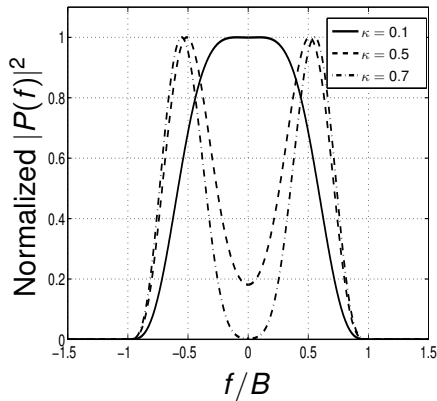
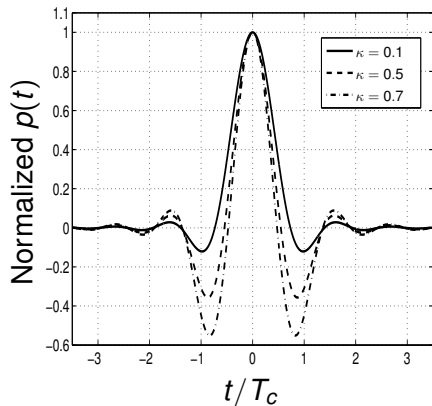
Examples for Signal Design

# Example Pulse Shapes

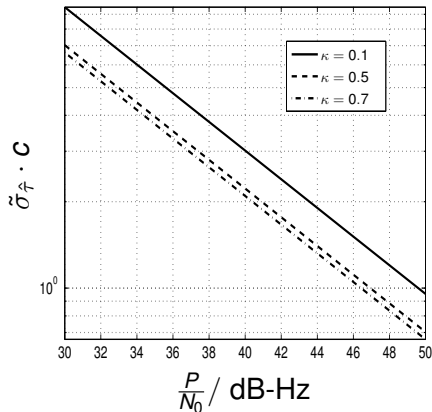
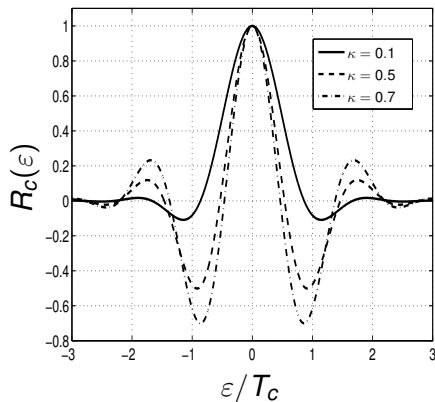
In order to illustrate the previously discussed signal or pulse shape properties we consider:

- ▶ Three example pulse shapes  $p(t)$  with  $\kappa = 0.1$ ,  $\kappa = 0.5$ ,  $\kappa = 0.7$ ,  $B = 1.023$  MHz, and  $BT_c = 1$
- ▶  $P_u = -154$  dBW with  $U = 11$
- ▶  $N_0 = -204$  dBW/Hz
- ▶  $c$  denotes the speed of light
- ▶ For this example we assume that no MAI-R is present
- ▶ The multipath error envelope gives the maximum bias of a DLL in case that in addition to the line-of-sight signal a single reflective multipath signal with signal-to-multipath ration of 6 dB is present
- ▶ The envelope is defined by the cases if the multipath signal has a relative phase of 0 or of  $\pi$  with respect to the line-of-sight signal

# Time and Frequency Domain

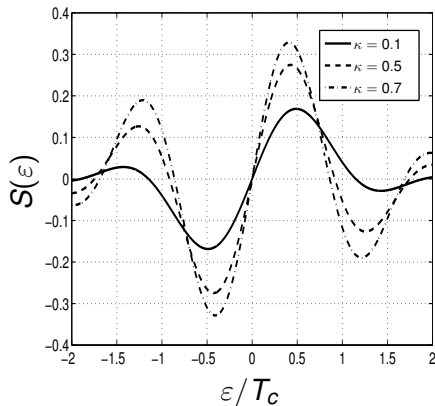
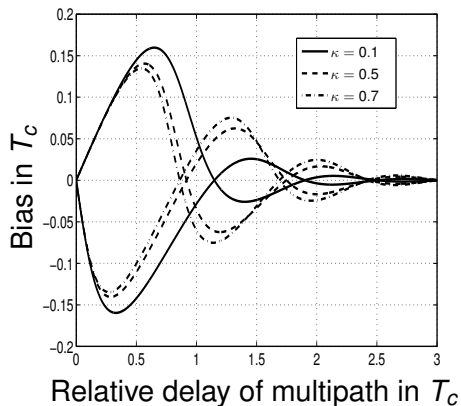


# Autocorrelation and CRLB-I



$p(t)$	$\kappa = 0.1$	$\kappa = 0.5$	$\kappa = 0.7$	Lower bound MAI-A
MAI-A	0.79	0.80	0.99	0.54
$\Delta$ SNR	1.79 (2.53 dB)	1.80 (2.55 dB)	1.99 (3.0 dB)	1.54 (1.87 dB)

# Multipath Error Envelope and S-Curve



## Signal properties for time-delay estimation and GNSS

1. The higher the Gabor bandwidth of the signal  $\Rightarrow$  the higher the synchronization accuracy that can be achieved in terms of the CRLB
2. Minimizing the CRLB for  $\tau$  and maximizing time concentration are contradictory tasks
3. The higher the processing gain  $G$  (large bandwidth  $B$ )  $\Rightarrow$  the higher synchronization accuracy and the higher interference robustness
4. The lower the CRLB for  $\tau$  ( $\text{CRLB} \rightarrow \frac{1}{B^2}$ )  $\Rightarrow$  the lower time concentration of  $p(t)$  ( $p(t) \rightarrow \sin(2B\pi t)$  or  $\cos(2B\pi t)$ )
5. The higher the sidelobes of  $R_c(\varepsilon) \Rightarrow$  the higher the sidelobes of  $p(t) \Rightarrow$  the lower time concentration of  $p(t)$
6. The higher the sidelobes of  $R_c(\varepsilon) \Rightarrow$  the higher  $\kappa \Rightarrow$  the less robust estimation of  $\tau$  (likelihood has local maxima besides the global maximum)
7. MAI-A and MAI-R have to be considered in the signal design (chip pulse shape design) or can be treated in the receiver (multi-user detection and mitigation)