

Last time, we found that the vector potential is given by  $\vec{A} = \frac{\mu_0}{4\pi} \int \frac{\vec{J} dv}{r}$ .

In theory this gives  $\vec{A}$  for any setup, but in some cases you get an infinite result.

For example, this  $\vec{A}$  is infinite for an infinite straight wire (but see Problem 6.5 for a way to get around this problem). However, there are many  $\vec{A}$ 's that get the  $\vec{B} = \nabla \times \vec{A}$  job done, for example:

Example: Show that  $\vec{A} = -\hat{z} \frac{\mu_0 I}{2\pi} \ln(r)$  is a valid vector potential for a straight wire: ln(r/R)...but ln(r) - ln(R) and the second term goes out when you take derivative

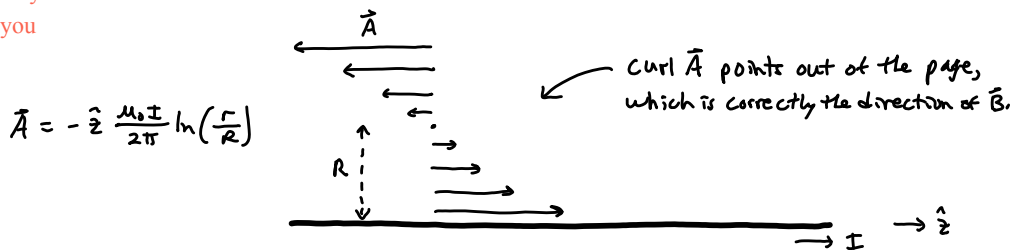
For this  $\vec{A}$ , only one term in the curl in cylindrical coordinates survives. We obtain:

$$\nabla \times \vec{A} = -\frac{dA_z}{dr} \hat{\phi} = \frac{\mu_0 I}{2\pi} \cdot \frac{1}{r} \hat{\phi} \quad \checkmark \quad \leftarrow \text{the correct } \vec{B}$$

We could add on any vector field with zero curl, and we would still have a valid  $\vec{A}$ .

Actually, the above expression for  $\vec{A}$  makes no sense, because it makes no sense to take the log of a dimensionful quantity. So we should write  $\ln(r/R)$ , where  $R$  is any arbitrary length. We then have:

why can't  
you



It turns out that  $\vec{A}$  isn't that useful for what we'll do in this course. (It's useful in Phys 153 and Phys 232). Instead what we will make frequent use of is the...

### Biot-Savart law

We'll derive this law with the help of  $\vec{A}$ , and then we'll pretty much forget about  $\vec{A}$ .

We'll restrict the current flow to wires, so  $\vec{J} = \frac{I}{a} \hat{z}$  and  $dv = a d\ell \Rightarrow \vec{J} dv = I d\ell$

So we can replace  $\vec{J} dv$  with  $I d\ell \Rightarrow$

$$\vec{A} = \frac{\mu_0 I}{4\pi} \int \frac{d\vec{\ell}}{r} \Rightarrow d\vec{A} = \frac{\mu_0 I}{4\pi} \frac{d\vec{\ell}}{r}$$

The long way to get  $\vec{B}$ : Integrate  $d\vec{A}$  to get  $\vec{A}$ , then take the curl to get  $\vec{B}$ .

Shorter way: Take the curl of  $d\vec{A}$  to get  $d\vec{B}$ , then integrate to get  $\vec{B}$ . need  $\vec{A}$  as a function of position (that is, need to know  $\vec{A}$  at nearby points)

only need to know  $\vec{B}$  at one point.

Purcell works out  $\nabla \times d\vec{A}$  in Cartesian coordinates. Let's do it in a quicker vector-calculus way:

$$d\vec{B} = \nabla \times d\vec{A} = \nabla \times \left( \frac{\mu_0 I}{4\pi} \frac{d\vec{\ell}}{r} \right) = \frac{\mu_0 I}{4\pi} \nabla \left( \frac{1}{r} \right) \times d\vec{\ell} \quad \leftarrow \text{from the identity } \nabla \times (f \vec{F}) = f \nabla \times \vec{F} + (\nabla f) \times \vec{F}$$

Here,  $\vec{F} = d\vec{\ell}$ , which is constant.

But  $\nabla \left( \frac{1}{r} \right) = -\frac{\hat{r}}{r^2}$  because we know that  $\frac{\vec{E}}{4\pi\epsilon_0 r^2} \hat{r} = -\nabla \left( \frac{q}{4\pi\epsilon_0 r} \right)$  Coulomb  $\vec{E} = -\nabla \phi$

Therefore,  $d\vec{B} = \frac{\mu_0 I}{4\pi} \left( \frac{-\hat{r}}{r^2} \times d\vec{\ell} \right) \Rightarrow \boxed{d\vec{B} = \frac{\mu_0 I}{4\pi} \frac{d\vec{\ell} \times \hat{r}}{r^2}} = \frac{\mu_0 I}{4\pi} \frac{d\vec{\ell} \times \vec{r}}{r^3}$

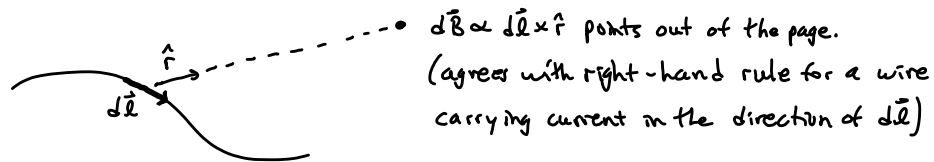
(Biot-Savart law)

switched  $\hat{r}, d\vec{\ell}$  order

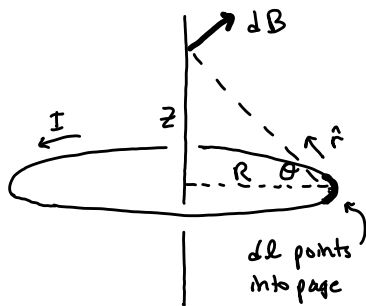
$\hat{r}$ -hat  $\swarrow$   $\vec{r}$ -vector  $\nwarrow$

This law is valid for steady currents (but they can be arbitrarily fast).

The  $\hat{r}$  vector goes from the element  $d\vec{\ell}$  to the point where you're finding  $\vec{B}$ .



Example: Find the magnetic field due to a ring of current, on the axis.



Only the  $z$  component of  $\vec{B}$  survives, by symmetry.

$d\vec{\ell}$  is perp to  $\hat{r}$ .  $\swarrow$  from vertical component

$$dB_z = \frac{\mu_0 I}{4\pi} \frac{d\ell}{r^2} \cos\theta = \frac{\mu_0 I}{4\pi} \frac{d\ell}{R^2 + z^2} \frac{R}{\sqrt{R^2 + z^2}}$$

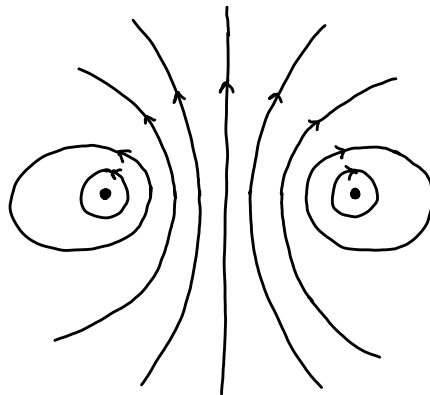
The  $d\ell$  simply integrates to  $2\pi R \Rightarrow \boxed{B = \frac{\mu_0 I R^2}{2(R^2 + z^2)^{3/2}}}$  on axis

$$= \frac{\mu_0 I R^2}{2r^3}$$

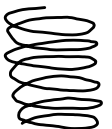
At the center, we have  $B = \frac{\mu_0 I}{2R}$ .

This field points upward everywhere on the axis, even below the ring.

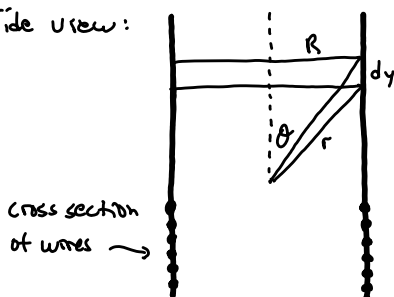
At locations off the axis, a side view of the field looks something like this:



Solenoids: A solenoid is a coil of wire - effectively many rings stacked on top of each other:



Side view:

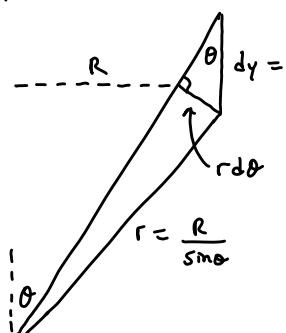


Let there be  $n$  windings per unit length (essentially continuous).

The current is  $I \Rightarrow$  current per unit length is  $nI$ .

Having found above the  $B$  from a ring, we must integrate over the rings with height  $dy$ .

Expanded view:



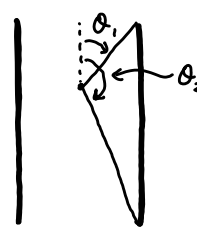
$$dy = \frac{r d\theta}{\sin\theta} = \frac{R d\theta}{\sin^2\theta} \Rightarrow \text{current in ring of height } dy \text{ is } nI dy = \frac{nIR d\theta}{\sin^2\theta}$$

$$\Rightarrow dB = \frac{\mu_0 (dI) R^2}{2r^3} = \frac{\mu_0 R^2}{2r^3} \frac{nIR d\theta}{\sin^2\theta}$$

Using  $R/r = \sin\theta$ , this becomes  $dB = \frac{\mu_0 n I}{2} \sin\theta d\theta$

$$\Rightarrow B = \int_{\theta_1}^{\theta_2} \frac{\mu_0 n I}{2} \sin\theta d\theta = \frac{\mu_0 n I}{2} (\cos\theta_1 - \cos\theta_2)$$

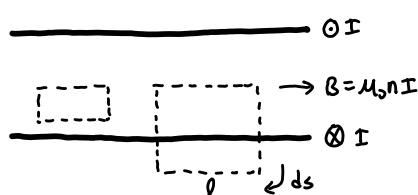
(direction from RH rule)



### Infinite solenoid

If we have an infinite solenoid, so that  $\theta_1 = 0$  and  $\theta_2 = \pi$ , then  $B = \mu_0 n I$

What about the field outside? Use Ampere's law:

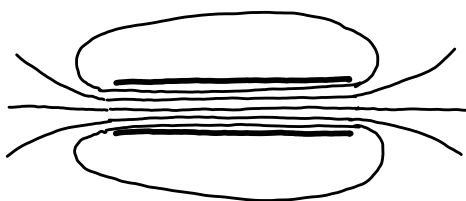


In the left Amperian loop, there is no current enclosed, so  $\oint \vec{B} \cdot d\vec{s} = \mu_0 I_{\text{encl}}$  tells us that  $\vec{B}$  is the same on the two long sides of the rectangle  $\Rightarrow \vec{B} = \mu_0 n I$  everywhere inside the solenoid.

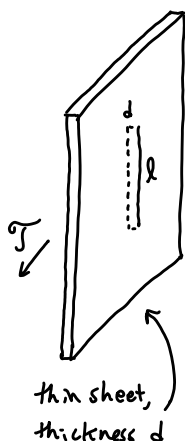
In the right Amperian loop, we have  $\oint \vec{B} \cdot d\vec{s} = \mu_0 I_{\text{encl}} \Rightarrow B_{\text{in}} l - B_{\text{out}} l = \mu_0 (n I l)$   
 $\Rightarrow B_{\text{in}} - B_{\text{out}} = \mu_0 n I \Rightarrow B_{\text{out}} = 0$

So the field is zero everywhere outside the solenoid (or very small for a long but finite solenoid).

This makes sense, because the field lines outside are sparse!



### Change in B at a current sheet



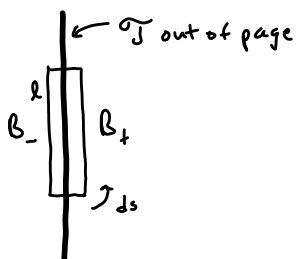
Recall that for the volume current density,  $J$ , we have  $J \cdot \text{area} = \text{current}$ .  
 Define the surface current density,  $\mathcal{J}$ , as follows:

the current through a height  $l$  is  $J(ld) = (\mathcal{J}l)d$

$\Rightarrow$  surface current density is  $\mathcal{J} \equiv Jd$ . So  $\mathcal{J} \cdot \text{length} = \text{current}$   
 units =  $\frac{C}{sm}$

$\mathcal{J}$  determines the change in  $B$  across a sheet, as follows

CHECK  
SOLUTION TO  
IN CLASS  
QUIZ.



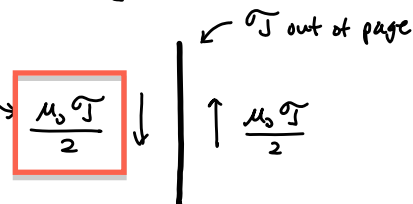
Ampere's law gives:

$$\oint \vec{B} \cdot d\vec{s} = \mu_0 I \Rightarrow B_+ l - B_- l = \mu_0 (\sigma l)$$

$$\Rightarrow B_+ - B_- = \mu_0 \sigma$$

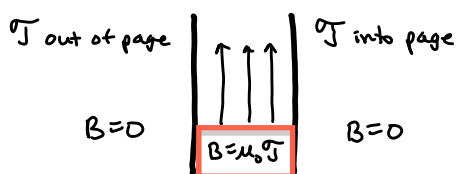
So the change across the sheet is  $\mu_0 \sigma$

If we have one sheet and nothing else, then the field is  
(You could also find this field by slicing the sheet up into thin wires and then integrating over these wires.)



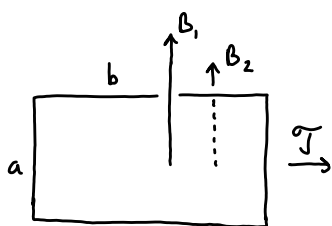
In general, we can superpose on this field any other field.

In the case of two opposite sheets of current, we have:



All statements here have analogous statements in the case of the  $E$  from a thin sheet of charge.

### Force on a sheet



What is the force on this sheet?

The current is  $I = \sigma a$

$\Rightarrow$  force on length  $b$  is  $F = I b B = (\sigma a) b \frac{B_1 + B_2}{2}$   $\swarrow$  avg field

But  $B_2 - B_1 = \mu_0 \sigma \Rightarrow \sigma = (B_2 - B_1) / \mu_0$

So the force per area is  $\frac{F}{ab} = \left( \frac{B_2 - B_1}{\mu_0} \right) \left( \frac{B_2 + B_1}{2} \right) = \frac{1}{2\mu_0} (B_2^2 - B_1^2)$  (use right-hand rule to get the direction)

Or we can just write this as  $\sigma \frac{B_1 + B_2}{2}$ , just like the electric formula  $\sigma \frac{E_1 + E_2}{2}$ .

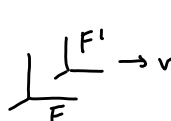
The force on each of the above sheets with opposite currents is outward.

$\nwarrow$  agrees with two-wire demo.

### Transformations of $\vec{E}$ , $\vec{B}$

If frame  $F'$  moves with velocity  $\vec{v}$  w.r.t. frame  $F$ , then the  $\vec{E}$  and  $\vec{B}$  components in the two frames are related by:

$$\begin{aligned} \vec{E}'_{\parallel} &= \vec{E}_{\parallel} & \vec{E}'_{\perp} &= \gamma (\vec{E}_{\perp} + \vec{v} \times \vec{B}_{\perp}) \\ \vec{B}'_{\parallel} &= \vec{B}_{\parallel} & \vec{B}'_{\perp} &= \gamma (\vec{B}_{\perp} - \frac{\vec{v}}{c^2} \times \vec{E}_{\perp}) \end{aligned}$$



(In Gaussian units, both  $\vec{v}$  and  $\vec{v}/c^2$  are replaced by  $\vec{\beta}$ .)

$\nwarrow$   $\vec{v}$  is the velocity of  $F'$  w.r.t.  $F$ .

The proofs of these are in the textbook. Let's just look at some special cases to help convince you that they're true.

Case 1

If the sources are at rest in  $F$ , then  $\vec{B}_{||} = \vec{B}_\perp = 0 \Rightarrow \vec{E}'_{||} = \vec{E}_{||}$  and  $\vec{E}'_\perp = \gamma \vec{E}_\perp$  ✓  
 Additionally, we have  $\vec{B}'_\perp = -\gamma \frac{\vec{v}}{c^2} \times \vec{E}_\perp$ , and this is indeed correct because consider the case of a single sheet:

Frame  $F$ :

$$\begin{array}{c} \uparrow E_\perp = \frac{\sigma}{2\epsilon_0} \\ \hline \leftarrow v \quad \textcircled{F'} \quad \sigma \end{array}$$

Frame  $F'$ :

$$\begin{array}{c} \uparrow E'_\perp = \frac{\gamma\sigma}{2\epsilon_0} \quad B'_\perp = ? \\ \hline \gamma\sigma \quad \vec{v} \end{array}$$

What is  $B'_\perp$ ? First note that a general expression for  $\mathcal{T}$  is  $\mathcal{T} = \sigma v$ , because

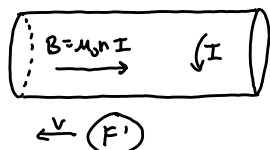
$$\mathcal{T} = \frac{dq}{dt} = \frac{\sigma(v dt)l}{dt} = (\sigma v)l \equiv \mathcal{T}l \quad (\text{arbitrary length in transverse direction})$$

$$\text{So } B'_\perp = \frac{\mu_0 \mathcal{T}}{2} = \frac{\mu_0 (\gamma\sigma)v}{2} = \frac{\gamma\sigma v}{2\epsilon_0 c^2} = \frac{\gamma v}{c^2} \frac{\sigma}{2\epsilon_0} = \frac{\gamma v}{c^2} E_\perp \quad \checkmark$$

And  $B'_\perp$  points out of the page, which is correctly the direction of  $-\vec{v} \times \vec{E}_\perp$  ✓  
 ↗ of  $F'$  w.r.t.  $F$

Case 2

To see why  $\vec{B}'_{||} = \vec{B}_{||}$ , consider a solenoid:

Frame  $F$ :Frame  $F'$ :

In  $F'$ ,  $n$  increases by  $\gamma$  (length contraction)  
 but  $I$  decreases by  $\gamma$  (time dilation)  
 $\Rightarrow B' = \mu_0 n' I' = \mu_0 n I = B$  ✓

Case 3:

If  $\vec{E}_\perp = 0$ , then  $\vec{B}'_\perp = \gamma \vec{B}_\perp$  and  $E'_\perp = \gamma \vec{v} \times \vec{B}_\perp$ . Consider this setup:

Frame  $F$ :

$$\begin{array}{c} \sigma \text{ (}\sigma/\gamma \text{ proper)} \\ \hline E_\perp = 0 \\ \otimes B_\perp = \frac{\mu_0 \sigma}{2} = \frac{\mu_0 \sigma v}{2} \\ \hline \sigma \quad \textcircled{F'} \quad \vec{v} \end{array}$$

Frame  $F'$ :

$$\begin{array}{c} \sigma/\gamma \\ \hline E'_\perp = ? \\ B'_\perp = ? \\ \hline \leftarrow v \quad \gamma\sigma \end{array}$$

$$B'_\perp = \frac{\mu_0 \sigma'}{2} = \frac{\mu_0 (\gamma\sigma)}{2} = \gamma B_\perp \quad \checkmark$$

$$E'_\perp = \frac{1}{2\epsilon_0} \left( \gamma\sigma - \frac{\sigma}{\gamma} \right) = \frac{1}{2\epsilon_0} \gamma\sigma \left( 1 - \frac{1}{\gamma^2} \right) = \frac{1}{2\epsilon_0} \gamma\sigma \cdot \beta^2 = \frac{\gamma\sigma v^2}{2\epsilon_0 c^2} = \frac{\mu_0 \gamma\sigma v^2}{2}$$

$$= \gamma v \left( \frac{\mu_0 \sigma v}{2} \right) = \gamma v B_\perp \quad (\text{upward}) \quad \leftarrow \text{the direction of } \vec{v} \times \vec{B} \quad \checkmark$$