

1           **SECOND-ORDER INVARIANT-DOMAIN PRESERVING**  
2           **APPROXIMATION TO THE MULTI-SPECIES EULER EQUATIONS\***

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4           **Abstract.** This work is concerned with constructing a second-order, invariant-domain preserving  
5 approximation of the compressible multi-species Euler equations where each species is modeled by  
6 an ideal gas equation of state. We give the full solution to the Riemann problem and derive its  
7 maximum wave speed. The maximum wave speed is used in constructing a first-order invariant-  
8 domain preserving approximation. We then extend the methodology to second-order accuracy and  
9 detail a convex limiting technique which is used for preserving the invariant domain. Finally, the  
10 numerical method is verified with analytical solutions and then validated with several benchmarks  
11 and laboratory experiments.

12           **Key words.** multi-species Euler, invariant-domain preserving, higher-order accuracy, convex  
13 limiting

14           **AMS subject classifications.** 65M60, 65M12, 35L50, 35L65, 76M10

15           **1. Introduction.** The understanding of fluid interactions between multiple mis-  
16 cible fluids remains a vital component of many engineering applications. For example,  
17 accurate modeling of multi-species fluid mixing is crucial in combustion research for  
18 predicting flame stability, ignition, and emissions characteristics, which directly affect  
19 engine efficiency and pollutant formation. Furthermore, in climate modeling, under-  
20 standing how different atmospheric gases and moisture interact and mix is essential  
21 for predicting weather patterns and climate change impacts. Such fluid mixing phe-  
22 nomena are also prevalent in fields like aerospace engineering, nuclear engineering,  
23 and materials science, where accurate modeling directly impacts system performance  
24 and safety.

25           Accurately simulating these complex flow phenomena has proven challenging for  
26 many numerical methods, particularly for applications involving high-speed flows  
27 where compressibility effects must be accounted for. Multi-species flows at high Mach  
28 numbers introduce additional challenges due to phenomena such as shock waves, con-  
29 tact discontinuities, rarefaction waves, and species interfaces. Developing robust and  
30 high-fidelity numerical techniques capable of effectively capturing this behavior re-  
31 mains an active area of research. A variety of numerical approaches have been pro-  
32 posed for modeling multiphase compressible flows, with methods typically falling into

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33 the categories of: i) mixture fraction models, where mixing is modeled by the evolution  
 34 of a scalar conserved field (i.e., the “mass/mixture fraction”) without resolving  
 35 individual species equations [31]; ii) multi-species (or multi-component) models, where  
 36 the evolution of individual species densities is modeled in addition to the momentum  
 37 and energy of the mixture [24]; and iii) multi-fluid models, where each species is  
 38 modeled as a separate fluid with individual conservation equations and interspecies  
 39 interaction terms [40].

40 The focus of this work is on the inviscid limit of the second approach – the  
 41 multi-species Euler equations. In particular, we are concerned with conservative ap-  
 42 proximations of the compressible multi-species Euler equations, where the equation of  
 43 state of each species is modeled as an ideal gas. In the context of numerical schemes  
 44 for hyperbolic conservation laws, namely gas dynamics, there has been growing in-  
 45 terest in the development of numerical schemes that are *provably robust* in the sense  
 46 that they guarantee the solution abides by known physical laws. For the multi-species  
 47 Euler equations, this corresponds to the preservation of physical invariants such as  
 48 positivity of species densities, positivity of internal energy (and consequently pres-  
 49 sure), and adherence to an entropy inequality. Early iterations of numerical schemes  
 50 which preserve positivity of species densities were shown in works such as that of Lar-  
 51 routurou [23]. To the authors’ knowledge, the first development of schemes which  
 52 *provably* preserve positivity of internal energy/pressure in multi-species flows was  
 53 shown in Shahbazi [36]. More recently, the minimum entropy principle for entropy sol-  
 54 utions of the multi-species Euler equations was proven in Gouasmi et al. [16], which  
 55 has led to the development of entropy-stable numerical schemes that adhere to an  
 56 entropy inequality for such equations [15, 33, 39, 5, 6].

57 The primary novelty of this work is the construction a second-order, invariant-  
 58 domain preserving approximation of the compressible multi-species Euler equations  
 59 which preserves physical invariants such as the positivity of the individual species  
 60 densities and internal energy/pressure as well as a local minimum principle on the  
 61 mixture entropy. We first give the full solution to the Riemann problem and derive  
 62 the local maximum wave speed – which, to the authors’ knowledge, has never been  
 63 explicitly derived before. We show that it is possible to estimate an upper bound  
 64 on the maximum wave speed of the one-dimensional Riemann problem in the multi-  
 65 species model, and then use this to construct a first-order invariant-domain preserving  
 66 approximation in the manner of Guermond and Popov [17]. We then describe a modi-  
 67 fied convex limiting technique [18] to blend a nominally second-order accurate scheme  
 68 with the first-order invariant-domain preserving approximation in such a way to re-  
 69 tain both the invariant-domain preserving properties and second-order accuracy. The  
 70 efficacy of the proposed scheme is shown in various numerical experiments involving  
 71 multi-species flows with strong shocks.

72 The remainder of this manuscript is organized as follows. We first describe the  
 73 multi-species model and thermodynamic assumptions in Section 2. We then give the  
 74 full solution to the Riemann problem and derive the maximum wave speed for the  
 75 Riemann problem in Section 3. The construction of a low-order invariant-domain  
 76 preserving approximation and a provisional high-order approximation is introduced  
 77 in Section 4, and the convex limiting technique is then described in Section 5. The  
 78 main result is given in Theorem 5.2. Finally, we present the results of numerical  
 79 experiments in Section 6.

80 **2. The model problem.** Let  $D \subset \mathbb{R}^d$  be a polygonal domain where  $d =$   
 81  $\{1, 2, 3\}$  is the spatial dimension. We consider a mixture of  $n_s \geq 2$  compress-

ible, inviscid species occupying  $D$ . We assume that at all times there exists at least one species in a subset of  $D$ . We further assume that all species are in thermal and mechanical equilibrium and ignore any effects due to molecular diffusion. We define the conserved variable of the mixture system in question by:  $\mathbf{u}(\mathbf{x}, t) := ((\alpha_1 \rho_1, \dots, \alpha_{n_s} \rho_{n_s}), \mathbf{m}, E)^\top(\mathbf{x}, t)$ . Here,  $\alpha_k \rho_k$  is the conserved partial density for each species where  $k \in \{1, \dots, n_s\}$ ,  $\mathbf{m}$  is the mixture momentum and  $E$  is the total mechanical energy of the mixture. We further define the following mixture quantities: density  $\rho(\mathbf{u}) := \sum_{k=1}^{n_s} \alpha_k \rho_k$ ; velocity  $\mathbf{v}(\mathbf{u}) := \mathbf{m}/\rho$ ; internal energy  $\varepsilon(\mathbf{u}) := E - \frac{1}{2\rho} \|\mathbf{m}\|_{\ell^2}^2$ ; and specific internal energy  $e(\mathbf{u}) := \varepsilon(\mathbf{u})/\rho(\mathbf{u})$ . The goal of this work is as follows. Given some initial data  $\mathbf{u}_0(\mathbf{x}) := ((\alpha_1 \rho_1, \dots, \alpha_{n_s} \rho_{n_s})_0, \mathbf{m}_0, E_0)(\mathbf{x})$  at time  $t_0$ , we seek solutions that solve the following system in some weak sense:

$$(2.1a) \quad \partial_t(\alpha_k \rho_k) + \nabla \cdot (\mathbf{v} \alpha_k \rho_k) = 0, \quad k \in \{1, \dots, n_s\},$$

$$(2.1b) \quad \partial_t \mathbf{m} + \nabla \cdot (\mathbf{v} \otimes \mathbf{m} + p(\mathbf{u}) \mathbb{I}_d) = \mathbf{0},$$

$$(2.1c) \quad \partial_t E + \nabla \cdot (\mathbf{v}(E + p(\mathbf{u}))) = 0.$$

Here,  $\mathbb{I}_d$  is the  $d \times d$  identity matrix. We introduce the short-hand notation for the flux of the system:  $\mathbf{f}(\mathbf{u}) := (\mathbf{v} \alpha_k \rho_k, \mathbf{v} \otimes \mathbf{m} + p(\mathbf{u}) \mathbb{I}_d, \mathbf{v}(E + p(\mathbf{u})))^\top$ . We also define the mass fractions of each species by  $Y_k := \alpha_k \rho_k / \rho(\mathbf{u})$  and the respective volume fractions by  $\alpha_k := \alpha_k \rho_k / \rho_k$  where  $\rho_k$  is the material density defined through the equation of state (see Remark 2.3). We denote the mass fraction and volume fraction vector quantities by  $\mathbf{Y}(\mathbf{u}) := (Y_1, \dots, Y_{n_s})^\top$  and  $\boldsymbol{\alpha}(\mathbf{u}) := (\alpha_1, \dots, \alpha_{n_s})^\top$ , respectively. For the sake of simplicity, we may drop the dependence on  $\mathbf{u}$  when discussing the mass and volume fractions.

*Remark 2.1* (Alternative formulation). It is common in the literature to formulate the system (2.1) in terms of the species mass fractions. Either in terms of the  $n_s - 1$  species mass fractions with the bulk density  $\rho$  (see: [24, Eqn. 1.1]):

$$(2.2a) \quad \partial_t(\rho Y_k) + \nabla \cdot (\mathbf{v} \rho Y_k) = 0, \quad k \in \{1, \dots, n_s - 1\},$$

$$(2.2b) \quad \partial_t \rho + \nabla \cdot (\mathbf{v} \rho) = 0,$$

$$(2.2c) \quad \partial_t \mathbf{m} + \nabla \cdot (\mathbf{v} \otimes \mathbf{m} + p(\mathbf{u}) \mathbb{I}_d) = \mathbf{0},$$

$$(2.2d) \quad \partial_t E + \nabla \cdot (\mathbf{v}(E + p(\mathbf{u}))) = 0,$$

or just in terms of each species mass fraction:

$$(2.3a) \quad \partial_t(\rho Y_k) + \nabla \cdot (\mathbf{v} \rho Y_k) = 0, \quad k \in \{1, \dots, n_s\},$$

$$(2.3b) \quad \partial_t \mathbf{m} + \nabla \cdot (\mathbf{v} \otimes \mathbf{m} + p(\mathbf{u}) \mathbb{I}_d) = \mathbf{0},$$

$$(2.3c) \quad \partial_t E + \nabla \cdot (\mathbf{v}(E + p(\mathbf{u}))) = 0.$$

As stated in Larroutrou and Fezoui [24, Remark 1], each of these system formulations, (2.1), (2.2), and (2.3) are equivalent.  $\square$

**2.1. Thermodynamics.** We assume that each species is governed by an ideal gas equation of state. We further assume that the system is in thermal equilibrium and mechanical equilibrium. Then, the bulk pressure for the ideal mixture is given by:

$$(2.4) \quad p(\mathbf{u}) := (\gamma(\mathbf{Y}) - 1)\varepsilon(\mathbf{u}), \text{ where } \gamma(\mathbf{Y}) := \frac{\sum_{k=1}^{n_s} Y_k c_{p,k}}{\sum_{k=1}^{n_s} Y_k c_{v,k}} = \frac{c_p(\mathbf{Y})}{c_v(\mathbf{Y})},$$

denotes the mixture adiabatic index and  $\{c_{p,k}\}_{k=1}^{n_s}$  and  $\{c_{v,k}\}_{k=1}^{n_s}$  are the material specific heat capacities at constant pressure and volume, respectively. Note that  $\gamma$ ,  $c_v$ , and  $c_p$  are technically functions of the conservative variables  $\mathbf{u}$ ; however, we write only their dependence on  $\mathbf{Y}$  for simplicity and clarity. We define the ratio of specific heats by:  $\gamma_k := c_{p,k}/c_{v,k}$  and the specific gas constant by:  $r_k := c_{p,k} - c_{v,k}$  for all  $k \in \{1:n_s\}$ . Note that in [24, Prop. 2] it was shown that the system (2.1) is hyperbolic if  $\gamma_k > 1$  holds for each species.

Since each species is governed by an ideal gas, the temperature is defined by  $c_{v,k}T = e_k$  and taking the mass fraction average we see that  $\sum_{k=1}^{n_s} Y_k e_k = c_v(\mathbf{Y})T$ . Similarly we can take the mass fraction average of the  $p$ - $T$ - $\rho_k$  relation,  $\frac{p}{\rho_k} = r_k T$ , to find  $\frac{p}{\rho} = r(\mathbf{Y})T$  where we used the identity,  $\sum_{k=1}^{n_s} \frac{Y_k}{\rho_k} = \sum_{k=1}^{n_s} \frac{\alpha_k}{\rho} = \frac{1}{\rho}$  and  $r(\mathbf{Y}) := c_p(\mathbf{Y}) - c_v(\mathbf{Y})$ . The specific internal energy identity follows:

$$\sum_{k=1}^{n_s} Y_k e_k = c_v(\mathbf{Y})T = \frac{pc_v(\mathbf{Y})}{r(\mathbf{Y})\rho} = \frac{p}{(\gamma(\mathbf{Y}) - 1)\rho} = e(\mathbf{u}).$$

In general, the temperature is recovered from:

$$(2.5) \quad T(\mathbf{u}) := \frac{e(\mathbf{u})}{c_v(\mathbf{Y})}.$$

The mixture entropy is defined by  $\rho s(\mathbf{u}) = \sum_{k=1}^{n_s} \alpha_k \rho_k s_k(\rho_k, e_k)$ . It is assumed that each material satisfies the Gibbs identity:  $T ds_k = de_k + p d\tau_k$ , where  $\tau_k = \rho_k^{-1}$ . Hence, the specific entropy for each material,  $k \in \{1:n_s\}$ , is given by,  $s_k = c_{v,k} \log(e_k/\rho_k^{\gamma_k-1}) + s_{\infty,k}$ , where  $s_{\infty,k}$  is some reference specific entropy. The mixture specific entropy is defined by:

$$(2.6) \quad s := \sum_{k=1}^{n_s} Y_k s_k = \sum_{k=1}^{n_s} Y_k c_{v,k} \log\left(\frac{e_k}{\rho_k^{\gamma_k-1}}\right) + Y_k s_{\infty,k}.$$

Using each material Gibbs' identity and the mass fraction average of the material specific entropies, we have the mixture Gibbs' identity:

$$(2.7) \quad T ds = de + p d\tau - \sum_{k=1}^{n_s} (e_k + p\tau_k - Ts_k) dY_k.$$

This is used in the derivation of the solution to the Riemann problem in Section 3.

Notice that the mixture entropy (2.6) is not written in terms of the conserved variable  $\mathbf{u}$  since it includes material quantities  $\{\rho_k\}_{k=1}^{n_s}$  and  $\{e_k\}_{k=1}^{n_s}$  which are found via the equation of state of each species. It can be shown that the mixture entropy in terms of the conserved variables is given by ([35, Eqn. 16a]):

$$(2.8a) \quad s(\mathbf{u}) := c_v(\mathbf{Y}) \log\left(\frac{\rho e(\mathbf{u})}{\rho^{\gamma(\mathbf{Y})}}\right) + K(\mathbf{Y}), \text{ where}$$

$$(2.8b) \quad K(\mathbf{Y}) := \sum_{k=1}^{n_s} Y_k \left( c_{v,k} \log\left(\frac{c_{v,k}}{c_v(\mathbf{Y})} \left(\frac{r_k}{r(\mathbf{Y})}\right)^{\gamma_k-1}\right) + s_{\infty,k} \right),$$

Without loss of generality, we assume that  $s_{\infty,k} = 0$  for all  $k \in \{1:n_s\}$ .

154     *Remark 2.2* (Mixture adiabatic index). In the literature, it is common to only  
 155     report the species adiabatic index,  $\{\gamma_k\}$ , rather than the specific heat capacities,  $\{c_{p,k}\}$   
 156     and  $\{c_{v,k}\}$ . Discrepancies in the choice of  $\{c_{p,k}\}$  and  $\{c_{v,k}\}$  can result in drastically  
 157     different values of the mixture adiabatic index  $\gamma(\mathbf{Y})$ . Consider the following valid  
 158     but extreme example. Let  $\gamma_1 = 1.4$  and  $\gamma_2 = 1.8$ . Then one may choose,  $c_{p,1} = 1.4$ ,  
 159      $c_{v,1} = 1$ ,  $c_{p,2} = 1800$ , and  $c_{v,2} = 1000$ . Let  $Y_1 = Y_2 = 1/2$ . Then, the the mixture  
 160     adiabatic index becomes,  $\gamma(\mathbf{Y}) = 1801.4/1001 \approx 1.8$ . Whereas, if  $c_{p,2} = 1.8$  and  
 161      $c_{v,2} = 1$ , then  $\gamma(\mathbf{Y}) = 1.6$ .  $\square$

162     *Remark 2.3* (Dalton's Law and material quantities). Note that the assumption of  
 163     mechanical equilibrium is not necessary to recover the mixture pressure (2.4). That  
 164     is to say, only thermal equilibrium and Dalton's law's are sufficient (see: Proposition  
 165     A.1). However, thermal equilibrium and Dalton's law alone are not enough to  
 166     recover the individual material densities  $\{\rho_k\}_{k=1}^{n_s}$ . Assuming mechanical equilibrium,  
 167     the material densities are then given by  $\rho_k := \frac{p}{(\gamma_k - 1)v_k}$  and the volume fractions are  
 168     recovered by  $\alpha_k := \frac{\alpha_k \rho_k}{\rho_k}$ .  $\square$

169     **2.2. Model properties.** We now discuss properties of the model (2.1). It was  
 170     shown in Gouasmi et al. [16] that the total mixture entropy  $-\rho s(\mathbf{u})$  is a convex  
 171     functional and proved that a local minimum principle on the mixture specific entropy  
 172     similar to that of Tadmor [37]. We recall the result of [16]. Let  $\mathbf{u}(\mathbf{x}, t)$  be an entropy  
 173     solution to (2.1). Then the following is satisfied:

174     (2.9)                         
$$\text{ess inf}_{\|\mathbf{x}\|_{\ell^2} \leq R} s(\mathbf{u}(\mathbf{x}, t)) \geq \text{ess inf}_{\|\mathbf{x}\|_{\ell^2} \leq R + tv_{\max}} s(\mathbf{u}(\mathbf{x}, 0)),$$

175     where  $R \geq 0$  is some radius and  $v_{\max}$  denotes the maximum speed of information  
 176     propagation. Furthermore, it was shown that the system (2.1) admits an entropy  
 177     pair.

178     **DEFINITION 2.4** (Entropy solutions). *We define the following entropy and entropy  
 179     flux:*

180     (2.10)                         
$$\eta(\mathbf{u}) := -\rho s(\mathbf{u}), \quad \mathbf{q}(\mathbf{u}) := -\mathbf{v} \rho s(\mathbf{u}).$$

181     Then the pair  $(\eta(\mathbf{u}), \mathbf{q}(\mathbf{u}))$  is an entropy pair for the system (2.1) weakly satisfying  
 182      $\nabla \cdot \mathbf{q} = (\nabla_{\mathbf{u}} \eta(\mathbf{u}))^\top \nabla \cdot \mathbf{f}(\mathbf{u})$ . The solution  $\mathbf{u}(\mathbf{x}, t)$  is an entropy solution for (2.1) if it is  
 183     a weak solution to the system and satisfies the following inequality in the weak sense:  
 184      $\partial_t \eta(\mathbf{u}) + \nabla \cdot \mathbf{q}(\mathbf{u}) \leq 0$ .

185     Following Guermond and Popov [17, Def. 2.3], we now define the invariant set of the  
 186     system.

187     **DEFINITION 2.5** (Invariant set). *The following convex domain is an invariant set  
 188     for the multi-species model (2.1):*

189     (2.11)                         
$$\mathcal{A} := \left\{ \mathbf{u} \in \mathbb{R}^{d+1+n_s} : \alpha_k \rho_k \geq 0, k \in \{1:n_s\}, e(\mathbf{u}) > 0, s(\mathbf{u}) \geq s_{\min} \right\},$$

190     where  $s_{\min} := \text{ess inf}_{\mathbf{x} \in D} s(\mathbf{u}_0(\mathbf{x}))$ .

191     We see that (2.9) implies the invariant set condition:  $s(\mathbf{u}) \geq s_{\min}$ .

192     The goal of this work is to construct a first-order numerical method that is  
 193     invariant-domain preserving with respect to (2.11) and satisfies discrete entropy in-  
 194     qualities. Furthermore, we would like to extend the method to second-order accuracy  
 195     while remaining invariant-domain preserving. The starting point for the first-order

methodology is the work of [17]. It is shown in [17, Sec. 4] if one can find the maximum wave speed to the Riemann problem for a hyperbolic system, then the first-order method proposed therein is invariant-domain preserving and satisfies discrete entropy inequalities.

**3. The Riemann problem.** In this section, we discuss the Riemann problem for the multi-species model (2.1). For the sake of completeness, we give the full solution to the Riemann problem. To the best of our knowledge, the elementary wave structure for the model with two species was first analyzed in Larrouture and Fezoui [24]. Furthermore, we present the maximum wave speed in the Riemann problem which is necessary for constructing a first-order invariant-domain preserving approximation that satisfies discrete entropy inequalities. To the best of our knowledge, the maximum wave speed for the multi-species model has never been explicitly derived.

**3.1. Set up and summary.** Let  $\mathbf{n}$  be any unit vector in  $\mathbb{R}^d$ . Then the one-dimensional Riemann problem for the multi-species model projected in the direction  $\mathbf{n}$  is given by:

$$(3.1) \quad \partial_t \mathbf{u} + \partial_x (\mathbf{f}(\mathbf{u}) \mathbf{n}) = \mathbf{0}, \quad \mathbf{u}(\mathbf{x}, 0) = \begin{cases} \mathbf{u}_L, & \text{if } x < 0, \\ \mathbf{u}_R, & \text{if } x > 0. \end{cases}$$

Here  $\mathbf{u} := (\alpha_1 \rho_1, \dots, \alpha_{n_s} \rho_{n_s}, m, E)^\top$  where  $m := \mathbf{m} \cdot \mathbf{n}$  is the one-dimensional momentum in the direction of  $\mathbf{n}$ . Note that the one-dimensional velocity is defined by  $v := \mathbf{v} \cdot \mathbf{n} = m/\rho$ . The quantity  $\mathbf{u}_Z := ((\alpha_1 \rho_1)_Z, \dots, (\alpha_{n_s} \rho_{n_s})_Z, m_Z, E_Z)^\top$ ,  $Z \in \{L, R\}$ , denotes either the left or right data. We assume that  $\mathbf{u}_Z \in \mathcal{A}$ . It is shown in [24, Sec. 2.3] and in §3.2 that the elementary wave structure for (3.1) consists of two genuinely non-linear waves (either expansion or shock) and a linearly degenerate contact wave with multiplicity  $n_s$ . A consequence of this wave structure is that the derivation of the maximum wave speed is the same for all  $n_s \geq 2$  since the only modification would be an increase in multiplicity of the contact wave. Furthermore, it is shown that that the mass fractions  $Y_k$ , for all  $k \in \{1:n_s\}$ , are constant on each side of the contact wave (see Lemma 3.3). Consequently,  $\gamma(\mathbf{Y})$  is also constant on each side of the contact. This property is fundamental when deriving the maximum wave speed formula below. We now provide the novel formula.

**PROPOSITION 3.1** (Maximum wave speed). *Let  $Z \in \{L, R\}$ . Assume  $p^*$  is a solution to  $\varphi(p) = 0$  where*

$$(3.2a) \quad \varphi(p) := f_L(p) + f_R(p) + v_R - v_L,$$

$$(3.2b) \quad f_Z(p) = \begin{cases} (p - p_Z) \sqrt{\frac{A_Z}{p + B_Z}}, & \text{if } p > p_Z, \\ \frac{2c_Z}{\gamma_Z - 1} \left( \left( \frac{p}{p_Z} \right)^{\frac{\gamma_Z - 1}{2\gamma_Z}} - 1 \right), & \text{if } p \leq p_Z. \end{cases}$$

and  $A_Z = \frac{2}{(\gamma_Z + 1)\rho_Z}$ ,  $B_Z = \frac{\gamma_Z - 1}{\gamma_Z + 1} p_Z$ ,  $c_Z = \sqrt{\frac{\gamma_Z p_Z}{\rho_Z}}$ . Then the maximum wave speed is given by

$$(3.3) \quad \lambda_{\max}(\mathbf{u}_L, \mathbf{u}_R, \mathbf{n}_{LR}) := \max(|\lambda_L(p^*)|, |\lambda_R(p^*)|),$$

232 where

$$233 \quad \lambda_L(p^*) := v_L - c_L \sqrt{1 + \frac{\gamma_L + 1}{2\gamma_L} \max\left(\frac{p^* - p_L}{p_L}, 0\right)},$$

$$234 \quad \lambda_R(p^*) := v_R + c_R \sqrt{1 + \frac{\gamma_R + 1}{2\gamma_R} \max\left(\frac{p^* - p_R}{p_R}, 0\right)}.$$

235 **3.2. Elementary wave structure.** We now give a brief overview of the ele-  
236 mentary wave structure. To simplify the elementary wave analysis, we introduce the  
237 following mapping:  $\mathbf{u} \mapsto \boldsymbol{\theta}(\mathbf{u})$  where

$$238 \quad (3.4) \quad \boldsymbol{\theta}(\mathbf{u}) := \left( \frac{\alpha_1 \rho_1}{\rho(\mathbf{u})}, \dots, \frac{\alpha_{n_s-1} \rho_{n_s-1}}{\rho(\mathbf{u})}, \rho(\mathbf{u}), \frac{m}{\rho(\mathbf{u})}, E - \frac{m^2}{2\rho(\mathbf{u})} \right)^T.$$

239 Using the mass fraction notation, we have that  $\boldsymbol{\theta} = (Y_1, \dots, Y_{n_s-1}, \rho, v, \rho e)^T$ . Note  
240 that the mapping  $\mathbf{u} \mapsto \boldsymbol{\theta}(\mathbf{u})$  is a smooth diffeomorphism. It can be shown that the  
241 eigenvalues of the Jacobian matrix,  $D_{\mathbf{u}}(\mathbf{f}(\mathbf{u})\mathbf{n})$ , correspond exactly to the eigenvalues  
242 of the matrix  $\mathbb{B}(\boldsymbol{\theta}) := (D_{\boldsymbol{\theta}}\mathbf{u}(\boldsymbol{\theta}))^{-1} D(\mathbf{f}(\mathbf{u}(\boldsymbol{\theta}))\mathbf{n}) D_{\boldsymbol{\theta}}\mathbf{u}(\boldsymbol{\theta})$  (see: [14, Chpt. II, Sec. 2.1.1]).  
243 That is, a smooth diffeomorphic change of variables does not affect the eigenvalues of  
244 the Jacobian matrix. In short, the conservation law (3.1) can be written as:

$$245 \quad (3.5a) \quad \partial_t Y_i + v \partial_x Y_i = 0, \quad \text{for } i \in \{1:n_s - 1\},$$

$$246 \quad (3.5b) \quad \partial_t \rho + v \partial_x \rho + \rho \partial_x v = 0,$$

$$247 \quad (3.5c) \quad \partial_t v + v \partial_x v + \rho^{-1} \partial_x p = 0,$$

$$248 \quad (3.5d) \quad \partial_t (\rho e) + v \partial_x (\rho e) + (\rho e + p) \partial_x v = 0.$$

249 It can be shown that the transformed Jacobian matrix is:

$$250 \quad (3.6) \quad \mathbb{B}(\boldsymbol{\theta}) = \begin{bmatrix} v \mathbb{I}_{n_s-1} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathbf{0}^T & v & \rho & 0 \\ \rho^{-1} (D_{\mathbf{Y}} p)^T & 0 & v & \frac{\gamma-1}{\rho} \\ \mathbf{0}^T & 0 & \rho e + P & v \end{bmatrix},$$

251 where  $(D_{\mathbf{Y}} p)^T = (\frac{\partial p}{\partial Y_1}, \dots, \frac{\partial p}{\partial Y_{n_s-1}})$ . The eigenvalues are given by  $\lambda_1(\boldsymbol{\theta}) = v - c$ ,  
252  $\lambda_{n_s+2} = v + c$ , and  $\lambda_i = v$  for  $i \in \{2:n_s + 1\}$ , where  $c = \sqrt{\gamma p / \rho}$ . The corresponding  
253 eigenvectors (as functions of  $\boldsymbol{\theta}$ ) are given by:

$$254 \quad (3.7) \quad \mathbf{r}_1 = \begin{pmatrix} \mathbf{0}_{n_s-1} \\ \frac{\gamma-1}{\rho} \\ -\frac{c}{\gamma-1} \\ c \end{pmatrix}, \quad \mathbf{r}_i = \begin{pmatrix} \mathbf{e}_{i-1} \\ 0 \\ 0 \\ -\frac{1}{\gamma-1} \frac{\partial P}{\partial Y_{i-1}} \end{pmatrix}, \quad \mathbf{r}_{n_s+1} = \begin{pmatrix} \mathbf{0}_{n_s-1} \\ 1 \\ 0 \\ 0 \end{pmatrix}, \quad \mathbf{r}_{n_s+2} = \begin{pmatrix} \mathbf{0}_{n_s-1} \\ \frac{c}{\rho} \\ \frac{\gamma-1}{\rho} \\ c \end{pmatrix}$$

255 for  $i \in \{2:n_s\}$  where  $\{\mathbf{e}_i\}_{i \in \{1:n_s-1\}}$  is the canonical basis for  $\mathbb{R}^{n_s-1}$ .

256 LEMMA 3.2. *The 1-wave and the  $(n_s + 2)$ -wave are genuinely nonlinear and the  
257  $i$ -waves for  $i \in \{1:n_s + 1\}$  are linearly degenerate.*

258 *Proof.* The wave structure is unaffected by the change of variables as shown in

259 [14, Chpt II, Sec. 2.1.1]. The derivative of  $\lambda_1$  is

$$260 \quad (3.8) \quad D_{\boldsymbol{\theta}} \lambda_1(\boldsymbol{\theta}) = \begin{pmatrix} -\frac{(2\gamma-1)c}{2\gamma(\gamma-1)} \left( \frac{\gamma_1-\gamma}{c_v/c_{v,1}} \right) \\ \vdots \\ -\frac{(2\gamma-1)c}{2\gamma(\gamma-1)} \left( \frac{\gamma_{n_s-1}-\gamma}{c_v/c_{v,n_s-1}} \right) \\ \frac{c}{2\rho} \\ 1 \\ -\frac{c}{2\rho e} \end{pmatrix}.$$

261 Thus,  $D_{\boldsymbol{\theta}} \lambda_1(\boldsymbol{\theta}) \cdot \mathbf{r}_1(\boldsymbol{\theta}) = \frac{\gamma-1}{2\rho} - \frac{\gamma-1}{\rho} - \frac{\gamma(\gamma-1)}{2\rho} = -\frac{\gamma^2-1}{2\rho} < 0$ . A similar result holds  
262 for  $\lambda_{n_s+2}$ . Then note that  $D_{\boldsymbol{\theta}} \lambda_i(\boldsymbol{\theta}) = (\mathbf{0}_{n_s}, 1, 0)^T$  for all  $i \in \{2:n_s+1\}$ , hence  
263  $D_{\boldsymbol{\theta}} \lambda_i(\boldsymbol{\theta}) \cdot \mathbf{r}_i(\boldsymbol{\theta}) = 0$ . This completes the proof.  $\square$

264 **3.3. Solution to the Riemann problem.** We now give the full solution to  
265 the Riemann problem. We first show that the mass fractions are constant across each  
266 nonlinear wave.

267 **LEMMA 3.3** (Mass fractions). *Let  $Y_k(x, t)$  be the mass fraction weak solution to  
268 the Riemann problem (3.1) for each  $k \in \{1:n_s\}$ . Then  $Y_k(x, t) = Y_{k,L}$  for all  $x < v^*t$   
269 and  $Y_k(x, t) = Y_{k,R}$  for all  $x > v^*t$  for all  $t > 0$  where  $v^*$  denotes the speed of the  
270 contact.*

271 *Proof.* Assume that the left state,  $L$ , is connected to the state across the 1-  
272 wave by a shock wave. Then the multi-species system satisfies the Rankine-Hugoniot  
273 relations:  $S_L(\mathbf{u}_L - \mathbf{u}_{*L}) = (\mathbf{f}(\mathbf{u}_L) - \mathbf{f}(\mathbf{u}_{*L}))\mathbf{n}$ . In particular,  $S_L(\rho_L Y_{i,L} - \rho_{*L} Y_{i,*L}) =$   
274  $(\rho_L v_L Y_{i,L} - \rho_{*L} v_{*L} Y_{i,*L})$ . This identity can be rewritten as,  $\rho_L Y_{i,L} (S_L - v_L) =$   
275  $\rho_{*L} Y_{i,*L} (S_L - v_{*L})$ . From the conservation of mass, we have  $\rho_L (S_L - v_L) = \rho_{*L} (S_L -$   
276  $v_{*L})$  and therefore we conclude that  $Y_{i,L} = Y_{i,*L}$  for all  $i \in \{1:n_s\}$ .

277 Assume now that the left state is connected across a 1-wave by an expansion  
278 wave. Note that  $Y_k$  satisfies  $\frac{DY_k}{Dt} := \partial_t Y_k + v_k \partial_x Y_k = 0$  hence  $Y_k$  is constant across  
279 an expansion wave. This same reasoning can be applied across the right wave.  $\square$

280 Since each  $Y_k$  is constant across the left and right waves, we conclude that  $\gamma(\mathbf{Y})$   
281 is constant across the left and right waves. Therefore, left of the contact ( $x/t < v_*$ ),  
282 the pressure law obeys  $p = (\gamma_L - 1)\rho e$ . Across the right wave the pressure law is given  
283 by  $p = (\gamma_R - 1)\rho e$ . Furthermore, from the Gibbs mixture identity (2.7) the differential  
284 relationship on the left and right waves is:

$$285 \quad (3.9) \quad T ds = de + p d\tau.$$

286 Hence, across the genuinely nonlinear waves, the pressure is  $p = -\partial_\tau e(\tau, s)$ . Fur-  
287 thermore, it can be shown that the specific entropy,  $s$ , satisfies  $\partial_t s + \mathbf{v} \cdot \nabla s = 0$  as  
288 indicated in [16, Sec. 2]. Hence,  $s$  is constant across expansions. From (2.8), the  
289 specific internal energy as a function of  $s$ ,  $\tau$ , and  $\mathbf{Y}$  is,

$$290 \quad (3.10) \quad e(\mathbf{u}) := \tau(\mathbf{u})^{-(\gamma(\mathbf{Y})-1)} \exp\left(\frac{s(\mathbf{u}) - K(\mathbf{Y})}{c_v(\mathbf{Y})}\right).$$

291 From the differential relation (3.9), the pressure on an expansion wave (as a function  
292 of  $\rho$ ) is,

$$293 \quad (3.11) \quad p = (\gamma(\mathbf{Y}_Z) - 1)\rho^{\gamma(\mathbf{Y}_Z)} \exp\left(\frac{1}{c_v(\mathbf{Y}_Z)}(s_Z - K(\mathbf{Y}_Z))\right) = C_Z \rho^{\gamma_Z},$$

294 for  $Z \in \{L, R\}$ . The constant  $C_Z$ , can be computed simply by  $C_Z = p_Z / \rho_Z^{\gamma_Z}$  since the  
 295 expansion waves begins from the constant state. We also have the same structure for  
 296 the Riemann invariants as in the single material case, in particular, the 1-Riemann  
 297 invariant is  $w_1(\boldsymbol{\theta}) = v + \frac{2c}{\gamma - 1}$  and the  $(n_s + 2)$ -Riemann invariant is  $w_{n_s + 2}(\boldsymbol{\theta}) = v - \frac{2c}{\gamma - 1}$ .

298 Since  $\gamma = \gamma_L$  to the left of the contact and  $\gamma = \gamma_R$  to the right of the contact, the  
 299 pressure law is given by  $p = (\gamma_Z - 1)\rho e$  for  $Z \in \{L, R\}$  on each side of the contact,  
 300 respectively. The solution to this Riemann problem can be computed exactly as done  
 301 in Clayton et al. [8, Sec. 4] for  $\rho$ ,  $p$ , and  $v$ . (A “two-gamma” approximation was  
 302 used in [8] for interpolating general equations of state, inspired by Abgrall and Karni  
 303 [1]; the connection to the multi-species model (2.1) was not yet made at the time of  
 304 the publication.) Once  $\rho$ ,  $p$ , and  $v$  are known, the partial densities are computed by  
 305  $\alpha_k \rho_k = \rho Y_k$ , since the mass fractions,  $\{Y_k\}$ , are piecewise constant. The fundamental  
 306 methodology of constructing the solution can also be found in Toro [38, Sec. 4],  
 307 Godlewski and Raviart [14, Chpt. III, Sec. 3], and Lax [26]. For brevity, we simply  
 308 present the result.

309 The pressure in the star domain is determined by solving the following nonlinear  
 310 equation:

311 (3.12) 
$$\varphi(p) := f_L(p) + f_R(p) + v_R - v_L = 0,$$

312 where

313 (3.13) 
$$f_Z(p) = \begin{cases} (p - p_Z) \sqrt{\frac{A_Z}{p + B_Z}}, & \text{if } p > p_Z, \\ \frac{2c_Z}{\gamma_Z - 1} \left( \left( \frac{p}{p_Z} \right)^{\frac{\gamma_Z - 1}{2\gamma_Z}} - 1 \right), & \text{if } p \leq p_Z, \end{cases}$$

314 for  $Z \in \{L, R\}$  and where  $A_Z = \frac{2}{(\gamma_Z + 1)\rho_Z}$ ,  $B_Z = \frac{\gamma_Z - 1}{\gamma_Z + 1}p_Z$ , and  $c_Z = \sqrt{\frac{\gamma_Z p_Z}{\rho_Z}}$ . The  
 315 details for this derivation can be found in and are independent of the number of  
 316 materials present. Let  $\mathbf{c}(x, t) := (\rho(x, t), v(x, t), p(x, t))^T$  be the primitive state of the  
 317 solution to the Riemann problem for the multi-component Euler equations. Define  
 318 the self-similar parameter  $\xi := \frac{x}{t}$ . Then the weak entropy solution to the Riemann  
 319 problem is given by:

320 (3.14) 
$$\mathbf{c}(x, t) := \begin{cases} \mathbf{c}_L, & \text{if } \xi < \lambda_L^-(p^*), \\ \mathbf{c}_{LL}(\xi), & \text{if } \lambda_L^-(p^*) \leq \xi < \lambda_L^+(p^*), \\ \mathbf{c}_L^*, & \text{if } \lambda_L^+(p^*) \leq \xi < v^*, \\ \mathbf{c}_R^*, & \text{if } v^* \leq \xi < \lambda_R^-(p^*) \\ \mathbf{c}_{RR}(\xi), & \text{if } \lambda_R^-(p^*) \leq \xi < \lambda_R^+(p^*), \\ \mathbf{c}_R, & \text{if } \lambda_R^+(p^*) \leq \xi \end{cases}$$

321 where

322 (3.15a) 
$$\mathbf{c}_{LL}(\xi) = \left( \rho_L \left( \frac{2}{\gamma_L + 1} + \frac{(\gamma_L - 1)(v_L - \xi)}{(\gamma_L + 1)c_L} \right)^{\frac{2}{\gamma_L - 1}}, v_L - f_L(p(\xi)), p_L(\xi) \right)^T$$

323 (3.15b) 
$$\mathbf{c}_L^* = \begin{cases} \mathbf{c}_{LL}(\lambda_L^+), & \text{if } p^* < p_L \\ (\rho_L^*, v^*, p^*)^T & \text{if } p^* \geq p_L \end{cases}$$

324 (3.15c) 
$$\mathbf{c}_{RR}(\xi) = \left( \rho_R \left( \frac{2}{\gamma_R + 1} - \frac{(\gamma_R - 1)(v_R - \xi)}{(\gamma_R + 1)c_R} \right)^{\frac{2}{\gamma_R - 1}}, v_R + f_R(p(\xi)), p_R(\xi) \right)^T$$

325 (3.15d) 
$$\mathbf{c}_R^* = \begin{cases} \mathbf{c}_{RR}(\lambda_R^-), & \text{if } p^* < p_R \\ (\rho_R^*, v^*, p^*)^T & \text{if } p^* \geq p_R \end{cases}$$

326 where  $\rho_L(\xi) = \rho_L \left( \frac{2}{\gamma_L+1} + \frac{\gamma_L-1}{(\gamma_L+1)c_L} (v_L - \xi) \right)^{\frac{2}{\gamma_L-1}}$ ,  $\rho_R(\xi) = \rho_R \left( \frac{2}{\gamma_R+1} - \frac{\gamma_R-1}{(\gamma_R+1)c_R} (v_R - \xi) \right)^{\frac{2}{\gamma_R-1}}$ ,  $p_L(\xi) := C_L \rho_L(\xi)^{\gamma_L}$ , and  $p_R(\xi) := C_R \rho_R(\xi)^{\gamma_R}$ . Across a shock, the density  
 327 is:  
 328

$$329 \quad (3.16) \quad \rho_Z^* = \frac{\rho_Z \left( \frac{p^*}{p_Z} + \frac{\gamma_Z-1}{\gamma_Z+1} \right)}{\frac{\gamma_Z-1}{\gamma_Z+1} \frac{p^*}{p_Z} + 1},$$

330 for  $Z \in \{L, R\}$  where  $p^*$  solves (3.12) and  $v^* = v_L - f_L(p^*) = v_R + f_R(p^*)$ . The wave  
 331 speeds are given by:

$$332 \quad \lambda_L^-(p^*) := v_L - c_L \sqrt{1 + \frac{\gamma_L+1}{2\gamma_L} \max \left( \frac{p^* - p_L}{p_L}, 0 \right)},$$

$$333 \quad \lambda_L^+(p^*) := \begin{cases} v_L - f_L(p^*) - c_L \left( \frac{p^*}{p_L} \right)^{\frac{\gamma_L-1}{2\gamma_L}}, & \text{if } p^* < p_L \\ \lambda_L^-(p^*), & \text{if } p^* \geq p_L, \end{cases}$$

$$334 \quad \lambda_R^+(p^*) := v_R + c_R \sqrt{1 + \frac{\gamma_R+1}{2\gamma_R} \max \left( \frac{p^* - p_R}{p_R}, 0 \right)},$$

$$335 \quad \lambda_R^-(p^*) := \begin{cases} v_R + f_R(p^*) + c_R \left( \frac{p^*}{p_R} \right)^{\frac{\gamma_R-1}{2\gamma_R}}, & \text{if } p^* < p_R, \\ \lambda_R^+(p^*), & \text{if } p^* \geq p_R. \end{cases}$$

336 From Clayton et al. [8], the waves are well ordered from the following lemma.

337 LEMMA 3.4. For  $\gamma_L, \gamma_R > 1$  and  $c_L, c_R > 0$ , we have that,

$$338 \quad \lambda_L^-(p^*) \leq \lambda_L^+(p^*) \leq v_L^* \leq v_R^* \leq \lambda_R^-(p^*) \leq \lambda_R^+(p^*).$$

339 We now present an essential result necessary for constructing the numerical method ■  
 340 described in Section 4.

341 LEMMA 3.5 (Minimum entropy in the Riemann solution). Let  $\mathbf{u}(x, t)$  be the weak  
 342 solution to the Riemann problem (3.1) defined by (3.14). Let  $\hat{\lambda}_{\max}$  denote an upper  
 343 bound on the maximum wave speed. Let the average of the Riemann solution be given  
 344 by:  $\bar{\mathbf{u}}(t) := \frac{1}{2\hat{\lambda}_{\max}t} \int_{-\hat{\lambda}_{\max}t}^{\hat{\lambda}_{\max}t} \mathbf{u}(x, t) dx$ . Then  $\bar{\mathbf{u}}(t)$  satisfies:

$$345 \quad (3.17) \quad s(\bar{\mathbf{u}}(t)) \geq \min(s(\mathbf{u}_L), s(\mathbf{u}_R)).$$

346 Proof. Since  $(\rho s)(\mathbf{u})$  is concave, we can apply Jensen's inequality:

$$347 \quad (3.18) \quad (\rho s)(\bar{\mathbf{u}}(t)) \geq \frac{1}{2\hat{\lambda}_{\max}t} \int_{-\hat{\lambda}_{\max}t}^{\hat{\lambda}_{\max}t} (\rho s)(\mathbf{u}(x, t)) dx.$$

348 Consider the case that the  $L$ -wave is an expansion wave. Then the entropy is constant  
 349 up to the contact:  $v^* = x/t$ . That is,  $s(\mathbf{u}(x, t)) = s_L$  for all  $x < v^*t$ . In the case, that  
 350 the left wave is a shock, one has that the specific entropy must increase. This can be  
 351 seen by noting that left of the contact,  $x < v^*t$ , the equation of state behaves as a single  
 352 material equation of state due to Lemma 3.3. As such, since the shock is compressive,  
 353 the entropy must increase (See: Godlewski and Raviart [14, Chpt. III, Sec. 2] for  
 354 more details). Therefore,  $s(\mathbf{u}(x, t)) \geq s_L$  for all  $x < v^*t$ . The same reasoning can  
 355 be applied across the right wave. Therefore,  $s(\mathbf{u}(x, t)) \geq \min(s_L, s_R)$ , pointwise a.e.  
 356 for all  $t > 0$ . Therefore,  $(\rho s)(\bar{\mathbf{u}}(t)) \geq \frac{\min(s_L, s_R)}{2\hat{\lambda}_{\max}t} \int_{-\hat{\lambda}_{\max}t}^{\hat{\lambda}_{\max}t} \rho(x, t) dx = \bar{\rho}(t) \min(s_L, s_R)$ .  
 357 But  $(\rho s)(\bar{\mathbf{u}}(t)) = \bar{\rho}(t)s(\bar{\mathbf{u}}(t))$ , hence the result follows. □

358     **4. Approximation details.** The spatial approximation we adapt in this paper  
 359 is based on the invariant-domain preserving methodology introduced in Guermond and  
 360 Popov [17]. The low-order method can be thought of as a discretization-independent  
 361 generalization of the algorithm proposed in Lax [25, pg. 163]. Various extensions for  
 362 the compressible Euler equations have been proposed in [18, 8, 9, 7]. For the sake of  
 363 brevity, we omit the full approximation details and refer the reader to the previous  
 364 references.

365     **4.1. Low-order method.** We now introduce the low-order approximation. Let  
 366  $\mathcal{V}$  denote the index set enumerating the degrees of freedom. Let  $\mathcal{I}(i)$  denote an index  
 367 set for the local stencil for the degree of freedom,  $i$ . Then, for every  $i \in \mathcal{V}$  and  $j \in \mathcal{I}(i)$ ,  
 368 the low-order method with forward Euler time-stepping is given by:

$$369 \quad (4.1) \quad \frac{m_i}{\tau} (\mathbf{U}_i^{\text{L},n+1} - \mathbf{U}_i^n) = \sum_{j \in \mathcal{I}(i)} \left[ -(\mathbf{f}(\mathbf{U}_j^n) - \mathbf{f}(\mathbf{U}_i^n)) \mathbf{c}_{ij} + d_{ij}^{\text{L},n} (\mathbf{U}_j^n - \mathbf{U}_i^n) \right],$$

370 where

$$371 \quad (4.2) \quad d_{ij}^{\text{L},n} := \max(\hat{\lambda}_{\max}(\mathbf{U}_i^n, \mathbf{U}_j^n, \mathbf{n}_{ij}) \|\mathbf{c}_{ij}\|, \hat{\lambda}_{\max}(\mathbf{U}_j^n, \mathbf{U}_i^n, \mathbf{n}_{ji}) \|\mathbf{c}_{ji}\|)$$

372 and  $\hat{\lambda}_{\max} \geq \lambda_{\max}$  is a suitable upper bound on the maximum wave speed in the local  
 373 Riemann problem for  $(\mathbf{U}_i^n, \mathbf{U}_j^n, \mathbf{n}_{ij})$ . It is shown in [17, Rem. 3.1] that the method (4.1)  
 374 is globally mass conservative; that is to say  $\sum_{i \in \mathcal{V}} m_i \mathbf{U}_i^{\text{L},n+1} = \sum_{i \in \mathcal{V}} m_i \mathbf{U}_i^n$ . When  
 375 using linear finite elements as the underlying discretization, the method is formally  
 376 first-order accurate in space [17].

377 As shown in Proposition 3.1, the computation of the discrete local maximum wave  
 378 speed,  $\lambda_{\max}$ , would require the solution to a nonlinear equation for every  $(i, j)$  pair  
 379 which can be quite costly. Instead, we opt to use an upper bound on the maximum  
 380 wave speed,  $\hat{\lambda}_{\max}$ , which will be more efficient to compute. As referenced in Section 3,  
 381 the maximum wave speed can be found in Clayton et al. [8] as well as an algorithm  
 382 for computing the upper bound [8, Alg. 1] which we use in this work.

383     **THEOREM 4.1** (Invariant-domain preserving). *The low order method in (4.1) and  
 384 (4.2) using the upper bound on the maximum wave speed,  $\hat{\lambda}_{\max}$ , described in [8, Alg. 1]  
 385 under the CFL condition  $1 + \frac{2\tau d_{ii}^{\text{L},n+1}}{m_i} \geq 0$  is invariant-domain preserving. That is,  
 386  $\mathbf{U}_i^{\text{L},n+1} \in \mathcal{A}$  for all  $i \in \mathcal{V}$ . Furthermore, the update  $\mathbf{U}_i^{\text{L},n+1}$  satisfies discrete entropy  
 387 inequalities.*

388     *Proof.* The proof follows directly by the application of Theorem 4.1 and Theorem  
 389 4.7 in Guermond and Popov [17].  $\square$

390     **4.2. Local bounds.** An important and well-known property of the method (4.1)  
 391 is that it can be written as a convex combination of “bar states” under the CFL  
 392 condition  $1 + \frac{2\tau d_{ii}^{\text{L},n+1}}{m_i} \geq 0$ :

$$393 \quad (4.3a) \quad \mathbf{U}_i^{\text{L},n+1} = \left( 1 + \frac{2\tau d_{ii}^{\text{L},n+1}}{m_i} \right) \mathbf{U}_i^n + \sum_{j \in \mathcal{I}^*(i)} \frac{2\tau d_{ij}^{\text{L},n}}{m_i} \overline{\mathbf{U}}_{ij}^n, \text{ where}$$

$$394 \quad (4.3b) \quad \overline{\mathbf{U}}_{ij}^n = \frac{1}{2} (\mathbf{U}_i^n + \mathbf{U}_j^n) - \frac{1}{2d_{ij}^{\text{L},n}} (\mathbf{f}(\mathbf{U}_j^n) - \mathbf{f}(\mathbf{U}_i^n)) \mathbf{c}_{ij}.$$

395 When  $d_{ij}^{\text{L},n}$  is defined by (4.2), it can be shown that  $\overline{\mathbf{U}}_{ij}^n \in \mathcal{A}$  (see: [17, Thm 4.1]).

396     Remark 4.2 (Bar states). An important result regarding the bar states (4.3b)  
 397      $\{\bar{\mathbf{U}}_{ij}^n\}$  is that they are the average of the discrete Riemann solution. That is,  $\bar{\mathbf{U}}_{ij}^n =$   
 398      $\bar{\mathbf{u}}(t)$ , where  $\bar{\mathbf{u}}(t)$  is the average of the Riemann solution for the state  $(\mathbf{U}_i^n, \mathbf{U}_j^n, \mathbf{n}_{ij})$  at  
 399     the time  $t = \frac{\|\mathbf{c}_{ij}\|_{\ell^2}}{2d_{ij}^{L,n}}$ . This is a classical result (see: [17, Lemma 2.1]).  $\square$

400 Notice that (4.3a) is a *convex* combination of the states  $\{\bar{\mathbf{U}}_{ij}^n\}$  and therefore satisfies  
 401 local bounds in space and time. More specifically, we have that if  $\mathbf{U}_i^{L,n+1} \in \mathcal{A}$  for all  
 402  $i \in \mathcal{V}$ , then  $\Psi(\mathbf{U}_i^{L,n+1}) \geq \min_{j \in \mathcal{I}(i)} \Psi(\bar{\mathbf{U}}_{ij}^n)$  where  $\Psi(\mathbf{u})$  is any quasiconcave functional.  
 403 This fact will be used in the convex limiting section §5.2.

404     **4.3. Provisional high-order method.** We now present a provisional high-  
 405 order method with forward Euler time-stepping. The method follows that of [9,  
 406 Eqn. 3.1] where the modification here is in how the “entropy indicator” is defined  
 407 (see: §4.4). For every  $i \in \mathcal{V}$  and  $j \in \mathcal{I}(i)$ , we define the higher-order update:

$$408 \quad (4.4a) \quad \frac{m_i}{\tau} (\mathbf{U}_i^{H,n+1} - \mathbf{U}_i^n) = \sum_{j \in \mathcal{I}(i)} [\mathbf{F}_{ij}^{H,n} + b_{ij} \mathbf{F}_j^{H,n} - b_{ji} \mathbf{F}_i^{H,n}] \quad \text{with}$$

$$409 \quad (4.4b) \quad \mathbf{F}_{ij}^{H,n} := -(\mathbf{f}(\mathbf{U}_j) - \mathbf{f}(\mathbf{U}_i^n)) \mathbf{c}_{ij} + d_{ij}^{H,n} (\mathbf{U}_j^n - \mathbf{U}_i^n), \quad \mathbf{F}_i^{H,n} := \sum_{j \in \mathcal{I}(i)} \mathbf{F}_{ij}^{H,n}.$$

410 Here, two modifications have been made to the low-order method (4.1) to achieve  
 411 higher-order accuracy in space. (i) We replaced the lumped mass matrix by an ap-  
 412 proximation of the consistent mass matrix to reduce dispersive errors. That is to say,  
 413 with  $\mathbf{X} \in \mathbb{R}^I$ , where  $I := \text{card}(\mathcal{V})$ , we have  $(\mathbb{M}^{-1}\mathbf{X})_i \approx \mathbf{X}_i + \sum_{j \in \mathcal{I}(i)} (b_{ij}\mathbf{X}_j - b_{ji}\mathbf{X}_i)$   
 414 where  $b_{ij} := \delta_{ij} - \frac{m_{ij}}{m_j}$  and  $\delta_{ij}$  denoting the Kronecker symbol. (ii) We replaced the  
 415 low-order graph-viscosity coefficient by  $d_{ij}^{H,n} := \frac{1}{2}(\zeta_i^n + \zeta_j^n) \cdot d_{ij}^{L,n}$  where  $\zeta_i^n \in [0, 1]$   
 416 is an indicator for entropy production and scales like  $\mathcal{O}(h)$  for piecewise linear finite  
 417 elements where  $h$  is the typical mesh size.

418     **4.4. Entropy indicator.** We now introduce an entropy indicator which is in-  
 419 spired by [9, Sec. 3.2]. The idea is as follows. For every  $i$  and at every  $t^n$ , we consider  
 420 a surrogate evolution of the full mixture:  $\partial_t \mathbf{w} + \nabla \cdot \mathbf{f}^{i,n}(\mathbf{w}) = \mathbf{0}$  where  $\mathbf{w} := (\rho, \mathbf{m}, E)^\top$   
 421 and

$$422 \quad (4.5) \quad \mathbf{f}^{i,n}(\mathbf{w}) := \begin{pmatrix} \mathbf{m}, \\ \mathbf{v} \otimes \mathbf{m} + \tilde{p}^{i,n}(\mathbf{w}) \mathbb{I}_d, \\ \mathbf{v}(E + \tilde{p}^{i,n}(\mathbf{w})) \end{pmatrix}, \quad \tilde{p}^{i,n}(\mathbf{w}) := (\gamma_i^{\min,n} - 1) \rho e(\mathbf{w}),$$

423 where  $\gamma_i^{\min,n} := \min_{j \in \mathcal{I}(i)} \gamma(\mathbf{Y}_j^n)$ . Note that we have slightly abused notation by  
 424 introducing  $e$  as a function of  $\mathbf{w}$ ; however, we emphasize that  $e(\mathbf{w}) = e(\mathbf{u}) = \rho^{-1}E -$   
 425  $\frac{1}{2}\|\mathbf{v}\|_{\ell^2}^2$ . We further define the respective “surrogate entropy pair” for the flux (4.5)  
 426 by:

$$427 \quad (4.6a) \quad \eta^{i,n}(\mathbf{w}) := (\rho^2 e(\mathbf{w}))^{\frac{1}{\gamma_i^{\min,n+1}}} - \frac{\rho}{\rho_i^n} ((\rho_i^n)^2 e(\mathbf{W}_i^n))^{\frac{1}{\gamma_i^{\min,n+1}}},$$

$$428 \quad (4.6b) \quad \mathbf{F}^{i,n}(\mathbf{w}) := \mathbf{v} \eta^{i,n}(\mathbf{w}).$$

429 Here,  $\mathbf{W}_i^n := (\rho_i^n, \mathbf{m}(\mathbf{U}_i^n), E(\mathbf{U}_i^n))^\top$  where  $\rho_i^n := \sum_{k=1}^{n_s} \alpha_k \rho_k(\mathbf{U}_i^n)$ . The idea now is  
 430 to measure a discrete counterpart to:  $\nabla \cdot \mathbf{F}^{i,n}(\mathbf{w}) = (\nabla_{\mathbf{w}} \eta^{i,n}(\mathbf{w}))^\top \nabla \cdot \mathbf{f}^{i,n}(\mathbf{w})$  which

431 can be thought as an estimate to “entropy production”. This is done via the entropy  
 432 indicator  $\zeta_i^n$  defined by:

$$433 \quad (4.7a) \quad \zeta_i^n := \frac{|N_i^n|}{D_i^n + \frac{m_i}{|D|} \eta^{i,n}(\mathbf{W}_i^n)},$$

$$434 \quad (4.7b) \quad N_i^n := \sum_{j \in \mathcal{I}(i)} [\mathbf{F}^{i,n}(\mathbf{W}_j^n) \mathbf{c}_{ij} - (\nabla_{\mathbf{u}} \eta^{i,n}(\mathbf{W}_i^n))^T (\mathbf{f}^{i,n}(\mathbf{W}_j^n) \mathbf{c}_{ij})],$$

$$435 \quad (4.7c) \quad D_i^n := \left| \sum_{j \in \mathcal{I}(i)} \mathbf{F}^{i,n}(\mathbf{W}_j^n) \mathbf{c}_{ij} \right| + \sum_{j \in \mathcal{I}(i)} |(\nabla_{\mathbf{u}} \eta^{i,n}(\mathbf{w}_i^n))^T (\mathbf{f}^{i,n}(\mathbf{W}_j^n) \mathbf{c}_{ij})|,$$

436 where  $m_i$  is the respective mass associated with the degree of freedom  $i$  and  $|D|$  is  
 437 the measure of the spatial domain.

438 We illustrate the performance of the entropy indicator in Figure 1 with a two-  
 439 species extension of the standard Woodward-Colella blast wave benchmark [41] using  
 440 3201  $\mathbb{Q}_1$  degrees of freedom. We assume that the high-pressure regions contain only  
 441 air ( $\gamma_1 = \frac{1005}{718}$ ) and assume the low-pressure region contains only helium ( $\gamma_2 = \frac{5193}{3115}$ ).  
 442 The results are presented for the time snapshots  $t = \{0.015 \text{ s}, 0.038 \text{ s}\}$ . We see that the  
 443 entropy indicator (deep red) is almost zero everywhere except at the discontinuities  
 444 of the mixture density (black). We further see that at the mass fraction  $Y_1$  (teal)  
 445 discontinuities, the entropy indicator is small which implies the method is near optimal  
 446 at the species interface.

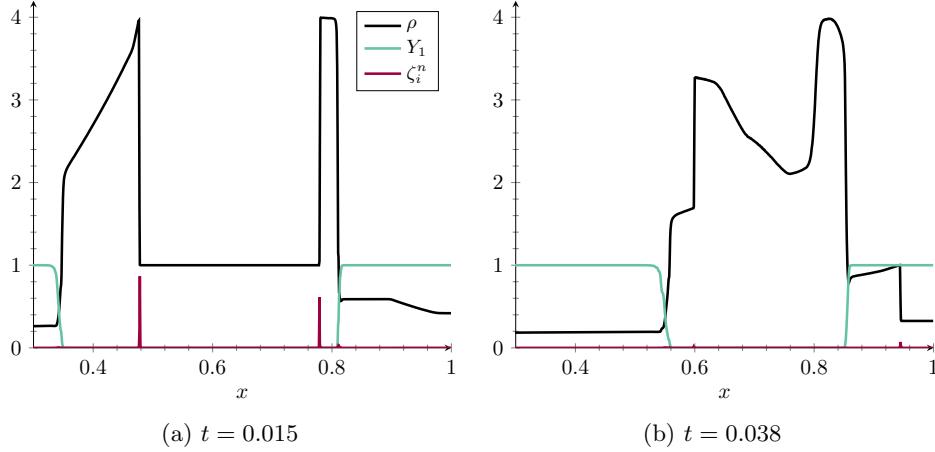


Fig. 1: Entropy indicator illustration with multi-species Woodward-Colella blast wave.

447 **5. Convex limiting.** It is discussed in [9] that the provisional high-order update  
 448  $\mathbf{U}^{H,n+1}$  defined in the previous section is not guaranteed to be invariant-domain  
 449 preserving. In this section, we present a convex limiting technique that corrects this  
 450 issue. The novelty of the approach in this paper is the limiting procedure for enforcing  
 451 the minimum principle on general concave functionals described in Section 5.2. This  
 452 procedure will be used to enforce: i) a local maximum and minimum principle on the  
 453 partial densities, ii) the positivity of the mixture internal energy and iii) the minimum  
 454 principle on the mixture entropy

455     **5.1. Set up.** The methodology is loosely based on the Flux-Corrected Transport  
 456 methodology (see: [42, 4, 22]) and follows directly the works of [18, 9]. The limited  
 457 update is given by:

458 (5.1a)                $\mathbf{U}_i^{n+1} = \sum_{j \in \mathcal{I}(i) \setminus \{i\}} \omega_i (\mathbf{U}_i^{\text{L},n+1} + \ell_{ij}^n \mathbf{P}_{ij}^n),$

459 (5.1b)                $\mathbf{P}_{ij}^n = \frac{\tau}{m_i \omega_i} (\mathbf{F}_{ij}^{\text{H},n} - \mathbf{F}_{ij}^{\text{L},n} + b_{ij} \mathbf{F}_j^{\text{H},n} - b_{ji} \mathbf{F}_i^{\text{H},n}).$

460 where the limiter coefficient is such that  $\ell_{ij}^n \in [0, 1]$  and is defined to be symmetric  
 461  $\ell_{ij}^n = \ell_{ji}^n$ . The weights  $\omega_i$  form a set of convex coefficients and are defined by  $\omega_i :=$   
 462  $\frac{1}{\text{card}(\mathcal{I}(i) \setminus \{i\})}$ . Note that when  $\ell_{ij}^n = 0$ , the update (5.1a) reduces to  $\mathbf{U}_i^{n+1} = \mathbf{U}_i^{\text{L},n+1}$ .  
 463 Similarly, when  $\ell_{ij}^n = 1$ , the update (5.1a) reduces to  $\mathbf{U}_i^{n+1} = \mathbf{U}_i^{\text{H},n+1}$ . Note that for  
 464 each  $i \in \mathcal{V}$ , the update (5.1a) is a convex combination of the states  $\mathbf{U}_i^{\text{L},n+1} + \ell_{ij}^n \mathbf{P}_{ij}^n$   
 465 for all  $j \in \mathcal{I}(i) \setminus \{i\}$ . Thus, if we can find an  $\ell_{ij}^n$  for each pair  $(i, j)$  such that  
 466  $\mathbf{U}_i^{\text{L},n+1} + \ell_{ij}^n \mathbf{P}_{ij}^n \in \mathcal{A}$ , then the update (5.1a) will be a convex combination of invariant-  
 467 domain preserving states and thus invariant-domain preserving itself. We now present  
 468 a general algorithm for finding the optimal limiter coefficient such that the limited  
 469 updated is invariant-domain preserving.

470     **5.2. General limiting on concave functionals.** In this section, we simplify  
 471 the limiting process described in [19] by using a linear interpolation between the low-  
 472 order update and high-order update. The method is only slightly more restrictive as  
 473 it requires the functional to be concave rather than quasiconcave as a function of the  
 474 conserved variable  $\mathbf{u}$ . We note that the partial densities are trivially concave and the  
 475 internal energy is concave (see [18, Sec. 4.1]). Furthermore, it was shown in Gouasmi  
 476 et al. [16, Sec. 2], that  $\rho s(\mathbf{u})$  is also concave. Thus, the constraints of interest for the  
 477 multi-species model (2.1) will all be concave. More specifically, we define:

478 (5.2a)                $\Psi_i^k(\mathbf{u}) := (\alpha_k \rho_k)(\mathbf{u}) - (\alpha_k \rho_k)_i^{\min,n},$

479 (5.2b)                $\Psi_i^{n_s+k}(\mathbf{u}) := (\alpha_k \rho_k)_i^{\max,n} - (\alpha_k \rho_k)(\mathbf{u}),$

480 (5.2c)                $\Psi_i^{2n_s+1}(\mathbf{u}) := \varepsilon(\mathbf{u}) - \varepsilon_i^{\min,n},$

481 (5.2d)                $\Psi_i^{2n_s+2}(\mathbf{u}) := \sigma(\mathbf{u}) - \sigma_i^{\min,n},$

482 for  $k \in \{1:n_s\}$  where  $\sigma(\mathbf{u}) := \rho s(\mathbf{u})$ . The local bounds are defined as follows:

483 (5.3a)                $(\alpha_k \rho_k)_i^{\min,n} := \min_{j \in \mathcal{I}(i)} (\overline{(\alpha_k \rho_k)}_{ij}^n, (\alpha_k \rho_k)_j), \quad \varepsilon_i^{\min} := \min_{j \in \mathcal{I}(i)} (\varepsilon(\overline{\mathbf{U}}_{ij}^n), \varepsilon(\mathbf{U}_j^n))$

484 (5.3b)                $(\alpha_k \rho_k)_i^{\max,n} := \max_{j \in \mathcal{I}(i)} (\overline{(\alpha_k \rho_k)}_{ij}^n, (\alpha_k \rho_k)_j), \quad \sigma_i^{\min} := \min_{j \in \mathcal{I}(i)} \sigma(\mathbf{U}_j^n),$

485 It was shown in §4.1 that the low-order update satisfies  $\Psi^\nu(\mathbf{U}_i^{\text{L},n+1}) \geq 0$  for all  $i \in \mathcal{V}$   
 486 and every  $\nu$  in the *ordered* set  $\{1:2n_s + 2\}$ . From Lemma 3.5 and Remark 4.2, we  
 487 see that the expected discrete minimum entropy principle is encoded in the inequality  
 488  $\Psi_i^{2n_s+2}(\mathbf{U}_i^{\text{L},n+1}) \geq 0$ .

489     **Remark 5.1** (Locally invariant-domain preserving). Note that the above bounds  
 490 can be used to define a *local* invariant set since  $\Psi^\nu(\mathbf{U}_i^{\text{L},n+1}) \geq 0$  for all  $i \in \mathcal{V}$ . That  
 491 is, for each degree of freedom  $i \in \mathcal{V}$  we define:

492 (5.4)                $\mathcal{B}_i := \bigcap_{\nu=1}^{2n_s+2} \mathcal{B}_i^\nu,$

493 where

494 (5.5)  $\mathcal{B}_i^\nu := \{\mathbf{U} \in \mathcal{A} : \Psi_i^\nu(\mathbf{U}) \geq 0, \forall j \in \mathcal{I}(i)\}.$

495 Then  $\mathbf{U}_i^{\text{L},n+1} \in \mathcal{B}_i \subset \mathcal{A}$  (recall  $\mathcal{A}$  is defined in (2.11)). This property is stronger than  
496 the typical “positivity-preserving” since it includes a local minimum principle on the  
497 specific entropy.  $\square$

498 We would like to emphasize that the order of the limiting is essential. For example,  
499 if the high-order partial densities are negative and one tries to first limit the entropy,  
500 then the method will fail as the entropy requires the logarithm of the mixture density.  
501 We define the interpolation between the low-order update and the high-order update  
502 as follows:

503 (5.6)  $g_{ij}^\nu(\ell) := \Psi_i^\nu(\mathbf{U}_i^{\text{L},n+1}) + \ell \frac{\Psi_i^\nu(\mathbf{U}_i^{\text{L},n+1} + \ell_{i,\nu-1}^j \mathbf{P}_{ij}^n) - \Psi_i^\nu(\mathbf{U}_i^{\text{L},n+1})}{\ell_{i,\nu-1}^j + \epsilon},$

504 for  $\ell \in [0, \ell_{i,\nu-1}^j]$ ,  $\ell_{i,0}^j := 1$ , and  $0 < \epsilon \ll 1$  is a machine precision constant to avoid  
505 division by zero. Note that  $g_{ij}^\nu(0) := \Psi_i^\nu(\mathbf{U}_i^{\text{L},n+1}) \geq 0$  for all  $\nu \in \{1:2n_s + 2\}$ . The  
506 goal is to find  $\ell_{i,\nu}^j \in [0, 1]$  such that  $g_{ij}^\nu(\ell_{i,\nu}^j) \geq 0$  for all  $\nu \in \{1:2n_s + 2\}$  in a sequential  
507 manner. If  $\Psi_i^\nu(\mathbf{U}_i^{\text{L},n+1} + \ell_{i,\nu-1}^j \mathbf{P}_{ij}^n) > 0$ , then  $\ell_{i,\nu}^j = \ell_{i,\nu-1}^j$ . If this is not the case, then  
508 we find the root of  $g_{ij}^\nu(\ell_{i,\nu}^j) = 0$  with a one step regula falsi approach which is given  
509 by:

510 (5.7)  $\ell_{i,\nu}^j = \min \left( \ell_{i,\nu}^j, \frac{-(\ell_{i,\nu-1}^j + \epsilon) \Psi_i^\nu(\mathbf{U}_i^{\text{L},n+1})}{\Psi_i^\nu(\mathbf{U}_i^{\text{L},n+1} + \ell_{i,\nu-1}^j \mathbf{P}_{ij}^n) - \Psi_i^\nu(\mathbf{U}_i^{\text{L},n+1})} \right).$

511 Under this sequential limiting, we see that  $\ell_{i,2n_s+2}^j \leq \ell_{i,2n_s+1}^j \leq \dots \leq \ell_{i,1}^j \leq \ell_{i,0}^j = 1$   
512 for every  $i \in \mathcal{V}$  and  $j \in \mathcal{I}(i) \setminus \{i\}$ .

513 In order to make the limiting methodology precise, we frame the problem as the  
514 construction of a symmetric matrix,  $\mathcal{L} \in \text{Sym}(|\mathcal{V}|, \mathbb{R})$ , defined by  $\mathcal{L} := \min(L, L^\top)$   
515 (with the min operation being defined component-wise). The entries of  $L$  are given  
516 by:

517 (5.8)  $(L)_{ij} := \begin{cases} \ell_{i,2n_s+2}^j, & \text{if } j \in \mathcal{I}(i) \setminus \{i\}, \\ 1, & \text{otherwise.} \end{cases}$

518 Note that the symmetrization of the limiter guarantees global mass conservation [18,  
519 Sec. 4.2]. The algorithm for computing the limiter for each  $(i, j)$  pair is given in  
520 Algorithm 1. We now give the main result of the paper.

521 **THEOREM 5.2** (Invariant-domain preserving). *Let the limited update  $\mathbf{U}_i^{n+1}$  be  
522 defined by (5.1) for all  $i \in \mathcal{V}$  combined with limiter procedure outlined in Algorithm 1  
523 for all  $j \in \mathcal{I}(i)$ . Then,  $\mathbf{U}_i^{n+1}$  is globally mass-conservative and satisfies the local  
524 bounds (5.2),  $\Psi_i^k(\mathbf{U}_i^{\text{L},n+1}) \geq 0$ , for all  $k \in \{1:2n_s + 2\}$ . That is, the update  $\mathbf{U}_i^{n+1}$  is  
525 invariant-domain preserving.*

526 **5.3. Relaxation of bounds.** It is known that one must relax the bounds for  
527 achieving optimal convergence in the  $L^\infty$  norm (see: [21] and [18, Sec. 4.7]). In this  
528 work, we directly follow [18, Sec. 4.7.1] for the relaxation of the partial density bounds

---

**Algorithm 1** Compute the limiter  $\ell_{ij}^n$  for the pair  $(i, j)$ 


---

**Input:**  $\{\mathbf{U}_i^{\text{L},n+1}\}$ ,  $\{\mathbf{P}_{ij}^n\}$ 
**Output:**  $\mathcal{L}$ 

```

1  $(L)_{ij} = 1$ , for all  $i, j \in \mathcal{V}$ .
2 for  $i \in \mathcal{V}$  do
3   for  $j \in \mathcal{I}(i) \setminus \{i\}$  do
4     for  $\nu \in \{1:2n_s + 2\}$  do
5       if  $\Psi_i^\nu(\mathbf{U}_i^{\text{L},n+1} + \ell_{i,\nu-1}^j \mathbf{P}_{ij}^n) \geq 0$  then
6          $\ell_{i,\nu}^j = \ell_{i,\nu-1}^j$ .
7       end
8       else
9         Compute  $\ell_{i,\nu}^j$  from (5.7).
10      end
11    end
12     $(L)_{ij} := \ell_{i,2n_s+2}^j$ 
13  end
14 end
15  $\mathcal{L} := \min(L, L^\top)$ 

```

---

529 and the mixture internal energy bound. As opposed to [18], we propose a different  
 530 relaxation of the specific entropy bound  $s^{\min}$ :

$$531 \quad (5.9) \quad s_{\text{relax}}^{\min,i} := \max \left( c_v(\mathbf{Y}_i) \log \left[ (1 - r_{h,i}) \exp \left( \frac{s^{\min,i}}{c_v(\mathbf{Y}_i)} \right) \right], s^{\min,i} - \Delta s^{\min,i} \right),$$

532 where  $r_{h,i} = \left( \frac{m_i}{|D|} \right)^{1.5/d}$  and

$$533 \quad (5.10) \quad \Delta s^{\min,i} = \max_{j \in \mathcal{I}(i) \setminus \{i\}} s\left(\frac{1}{2}(\mathbf{U}_i^n + \mathbf{U}_j^n)\right) - s^{\min,i}.$$

534 We note that the physical entropy in [18] was assumed to always be positive. However,  
 535 the physical entropy of the mixture (2.8) can be negative. Thus, if the specific entropy  
 536 happens to be close to zero, then typical relaxation of [18] in the form  $(1 - r_{h,i})s^{\min,i}$   
 537 fails to provide a proper relaxation, hence the reason for the “log-exp” transformation  
 538 in (5.9). We further note that the relaxation on the physical entropy leads to a  
 539 “weak” enforcement of the minimum entropy principle as stated in [18]. This is  
 540 observed numerically. Without the relaxation, the minimum entropy principle is  
 541 exactly enforced.

542 **6. Numerical illustrations.** We now illustrate the proposed methodology. In  
 543 particular, we i) verify the accuracy of the numerical method with smooth analytical  
 544 solutions and an exact solution to the Riemann problem; ii) compare with standard  
 545 benchmarks in the literature; iii) validate the proposed model by comparing with  
 546 small-scale experiments.

547 **6.1. Preliminaries.** The numerical tests are performed with the high performance code, **ryujin** [30, 20]. The code uses continuous  $\mathbb{Q}_1$  finite elements on quadrangular meshes for the spatial approximation and is built upon the **deal.II** finite element library [2]. For all tests, the time-stepping is done with a three stage, third-order Runge-Kutta method which is made to be invariant-domain preserving following

552 the techniques introduced in [11]. The time step size is defined by  $\tau := 3\tau_n$  where  $\tau_n$   
 553 is computed during the first stage of each time step using:

$$554 \quad \tau_n := \text{CFL} \max_{i \in \mathcal{V}} \frac{m_i}{2|d_{ii}^{L,n}|},$$

555 where  $\text{CFL} \in (0, 1]$  is a user-defined parameter. For the sake of simplicity, we set  
 556  $\text{CFL} = 0.5$  for all tests. All units are assumed to be SI units unless otherwise stated.

557 **6.2. Verification.** We now verify the accuracy of the numerical method. To  
 558 quantify the error, we introduce the following consolidated error indicator at time  $t$   
 559 which measures the  $L^q$ -norm for all components of the system:

$$560 \quad (6.1) \quad \delta^q(t) := \sum_{k=1}^m \frac{\|\mathbf{u}_{k,h}(t) - \mathbf{u}_k(t)\|_q}{\|\mathbf{u}_k(t)\|_q}.$$

561 Here,  $\mathbf{u}_k(t)$  is the exact state for the  $k$ -th component of the solution and  $\mathbf{u}_{h,k}(t)$  is  
 562 the spatial approximation of the  $k$ -th component.

563 **6.2.1. 1D two-species smooth traveling wave.** We consider a two-species  
 564 extension of the one-dimensional test proposed in [18]. The test consists of a two  
 565 traveling partial density waves with constant mixture pressure and mixture velocity.  
 566 Let  $\rho_0 = 1 \text{ kg m}^{-3}$  be the ambient mixture density. The partial density profiles are  
 567 defined by:

$$568 \quad (6.2a) \quad \rho(x, t) = \begin{cases} \rho_0 + 2^6(x_1 - x_0)^{-6}(x - v_0 t - x_0)^3(x_1 - x + v_0 t)^3, & \text{if } x_0 \leq x - v_0 t \leq x_1, \\ \rho_0, & \text{otherwise,} \end{cases}$$

569

$$570 \quad (6.2b) \quad (\alpha_1 \rho_1)_0(x, t) = \frac{3}{4} \times \rho(x, t), \quad (\alpha_2 \rho_2)_0(x, t) = \frac{1}{4} \times \rho(x, t),$$

571 where  $x_0 = 0.1 \text{ m}$  and  $x_1 = 0.3 \text{ m}$ . The mixture pressure and velocity are set to  
 572  $p(\mathbf{x}, t) = 1 \text{ Pa}$  and  $v(\mathbf{x}, t) = 1 \text{ m s}^{-1}$ , respectively. Each species is characterized by the  
 573 equation of state parameters  $\gamma_1 = \frac{1005}{718}$  and  $\gamma_2 = \frac{4041.4}{2420}$ . The computational domain is  
 574 defined by  $D = (0, 1 \text{ m})$  with Dirichlet boundary conditions. The tests are performed  
 575 on a sequence of uniform meshes. The final time is set to  $t_f = 0.6 \text{ s}$ . We report the  
 576 consolidated error  $\delta_q(t_f)$  for  $q = \{1, 2, \infty\}$  and respective convergence rates in Table 1.  
 577 We observe optimal convergence rates.

578 **6.2.2. Riemann problems.** We now verify the proposed method by comparing  
 579 with exact solutions to the Riemann problem which is provided in Section 3.2. In this  
 580 paper, we use the Riemann data given in [35, Tab. 2] for tests ‘‘RP1’’ and ‘‘RP2’’. We  
 581 recall the respective details in Table 2. The Riemann data is given for the variable  
 582  $\mathbf{w}(x, t) := (Y_1, \rho, v, p)^\top$ . We set  $Y_2 = 1 - Y_1$ . The conserved partial densities are set by  
 583  $\alpha_1 \rho_1 = Y_1 \rho$  and  $\alpha_2 \rho_2 = Y_2 \rho$ . For each test, the computational domain is defined by  
 584  $D = (0, 1 \text{ m})$  with Dirichlet boundary conditions. The diaphragm is set to  $x_0 = 0.5 \text{ m}$ .  
 585 The convergence tests are performed on a sequence of uniform meshes. We observe  
 586 an asymptotic rate of 1 which is expected in the  $L^1$ -norm. We show the output for  
 587 both Riemann problems with various refinement levels in Figure 2.

588 **6.3. Benchmarks.** We now benchmark the efficacy of the proposed scheme in  
 589 terms of canonical flow problems in the literature as well as novel problem configura-  
 590 tions.

| $I$   | $\delta^1(t_f)$         |      | $\delta^2(t_f)$        |      | $\delta^\infty(t_f)$   |      |
|-------|-------------------------|------|------------------------|------|------------------------|------|
| 101   | $1.738 \times 10^{-2}$  |      | $4.519 \times 10^{-2}$ |      | $1.462 \times 10^{-1}$ |      |
| 201   | $3.145 \times 10^{-3}$  | 2.47 | $1.021 \times 10^{-2}$ | 2.15 | $4.209 \times 10^{-2}$ | 1.8  |
| 401   | $2.775 \times 10^{-4}$  | 3.5  | $8.982 \times 10^{-4}$ | 3.51 | $4.930 \times 10^{-3}$ | 3.09 |
| 801   | $1.790 \times 10^{-5}$  | 3.96 | $4.748 \times 10^{-5}$ | 4.24 | $2.102 \times 10^{-4}$ | 4.55 |
| 1601  | $1.878 \times 10^{-6}$  | 3.25 | $6.039 \times 10^{-6}$ | 2.97 | $3.767 \times 10^{-5}$ | 2.48 |
| 3201  | $2.255 \times 10^{-7}$  | 3.06 | $8.543 \times 10^{-7}$ | 2.82 | $6.967 \times 10^{-6}$ | 2.43 |
| 6401  | $2.694 \times 10^{-8}$  | 3.06 | $1.211 \times 10^{-7}$ | 2.82 | $1.278 \times 10^{-6}$ | 2.45 |
| 12801 | $3.206 \times 10^{-9}$  | 3.07 | $1.721 \times 10^{-8}$ | 2.82 | $2.369 \times 10^{-7}$ | 2.43 |
| 25601 | $3.859 \times 10^{-10}$ | 3.05 | $2.451 \times 10^{-9}$ | 2.81 | $4.383 \times 10^{-8}$ | 2.43 |

Table 1: Errors and convergence rates for 1D two-species smooth traveling wave problem.

|     | $\mathbf{w}_L$                      | $\mathbf{w}_R$                      | $t_f$                | $\gamma_1$         | $\gamma_2$            |
|-----|-------------------------------------|-------------------------------------|----------------------|--------------------|-----------------------|
| RP1 | $(0.5, 1, 0, 1)^\top$               | $(0.5, 0.125, 0, 0.1)^\top$         | 0.2 s                | $\frac{1.5}{1.0}$  | $\frac{1.3}{1.0}$     |
| RP2 | $(1, 1.602, 0, 1 \times 10^6)^\top$ | $(0, 1.122, 0, 1 \times 10^5)^\top$ | $3 \times 10^{-4}$ s | $\frac{5.2}{3.12}$ | $\frac{1.402}{0.743}$ |

Table 2: Initial conditions and problem setup for the 1D Riemann problems.

| $I$   | $\delta^1(t_f)$        |      | $I$   | $\delta^1(t_f)$        |      |
|-------|------------------------|------|-------|------------------------|------|
| 101   | $6.909 \times 10^{-2}$ |      | 101   | $2.898 \times 10^{-1}$ |      |
| 201   | $3.586 \times 10^{-2}$ | 0.95 | 201   | $1.809 \times 10^{-1}$ | 0.68 |
| 401   | $1.972 \times 10^{-2}$ | 0.86 | 401   | $8.092 \times 10^{-2}$ | 1.16 |
| 801   | $1.168 \times 10^{-2}$ | 0.76 | 801   | $5.387 \times 10^{-2}$ | 0.59 |
| 1601  | $7.607 \times 10^{-3}$ | 0.62 | 1601  | $3.478 \times 10^{-2}$ | 0.63 |
| 3201  | $4.424 \times 10^{-3}$ | 0.78 | 3201  | $2.087 \times 10^{-2}$ | 0.74 |
| 6401  | $2.473 \times 10^{-3}$ | 0.84 | 6401  | $1.115 \times 10^{-2}$ | 0.9  |
| 12801 | $1.270 \times 10^{-3}$ | 0.96 | 12801 | $5.544 \times 10^{-3}$ | 1.01 |

(a) RP1

(b) RP2

Table 3: Errors and convergence rates for 1D Riemann problems.

591     **6.3.1. 2D – Shock-bubble interaction.** We first consider a two-dimensional  
592 shock-bubble interaction. Although there are many variations of this problem in the  
593 literature (e.g., [32, 34]), we choose to simulate the physical experiment described  
594 in [28]. The experiment consists of a shock wave traveling at Mach 1.43 in air  
595 ( $\gamma_1 = \frac{1005}{718}$ ) colliding with a krypton bubble ( $\gamma_2 = \frac{248}{149}$ ). We note that the phys-  
596 ical setup utilized a “straw” to fill the krypton in a thin soap bubble to prevent  
597 the gas from diffusing into the air. However, we note that the encapsulating soap  
598 bubble cannot be described by the current model and the “straw” cannot be prop-  
599 erly modeled in two dimensions. Thus, we consider the air and krypton as the only  
600 species in the numerical simulation. Let  $\rho_{\text{shock}} = 2.025655508041382 \text{ kg m}^{-3}$ ,  $v_{\text{shock}} =$   
601  $212.66552734375 \text{ m s}^{-1}$ ,  $p_{\text{shock}} = 224835 \text{ Pa}$ . Then, the initial state is given as follows:

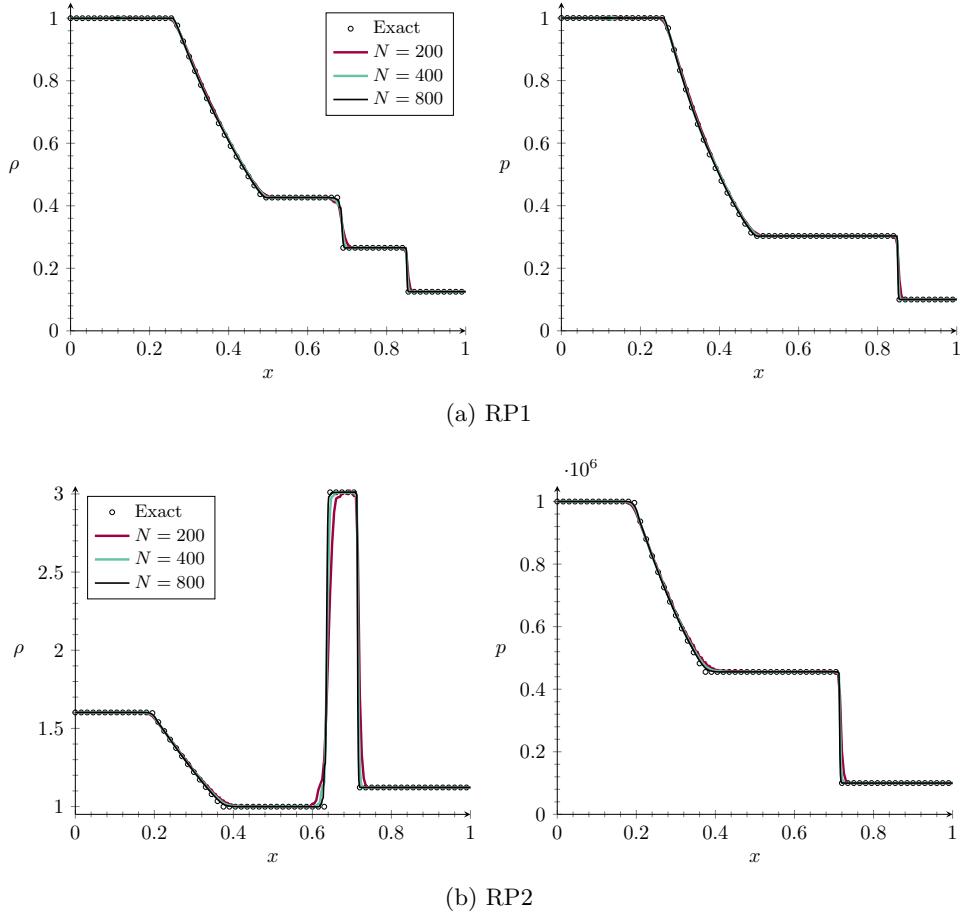


Fig. 2: Mixture density (left) and pressure (right) at  $t_f$  for the 1D Riemann problems computed using varying mesh resolutions.

602

$$603 \quad (6.3) \quad \mathbf{w}(\mathbf{x}, t) := \begin{cases} (1, \rho_{\text{shock}}, (v_{\text{shock}}, 0), p_{\text{shock}}), & \text{if } x_1 < 0.03 \text{ m} \\ (0, 3.408, \mathbf{0}, 101325), & \text{if } \|\mathbf{x} - \mathbf{x}_b\|_\ell \leq 0.022 \text{ m,} \\ (1, 1.163, \mathbf{0}, 101325), & \text{otherwise.} \end{cases}$$

604 where  $\mathbf{x}_b = (0.052 \text{ m}, 0.04 \text{ m})$  denotes the center of the bubble.

605 The computational domain is set to  $D = (-0.12 \text{ m}, 0.88 \text{ m}) \times (0, 0.08 \text{ m})$ . To  
606 ensure mesh convergence (or at least close to), we run the simulation with 20,496,281  
607  $\mathbb{Q}_1$  DOFs which corresponds to 16,000 elements in the  $x$ -direction and 1,280 elements  
608 in the  $y$ -direction. The final time is set to  $t_f = 1230 \mu\text{s}$ . The numerical Schlieren  
609 for the partial density  $\alpha_1 \rho_1$  plot is compared with the results in [28, Fig. 5]. In  
610 Figure 3, one sees that the vorticity in the physical experiment is not as noticeable  
611 compared to the numerical Schlieren. This difference has been discussed in Layes and  
612 Le Métayer [27, Sec. 4. B] and Giordano and Burtschell [13]. Overall, we resolve the

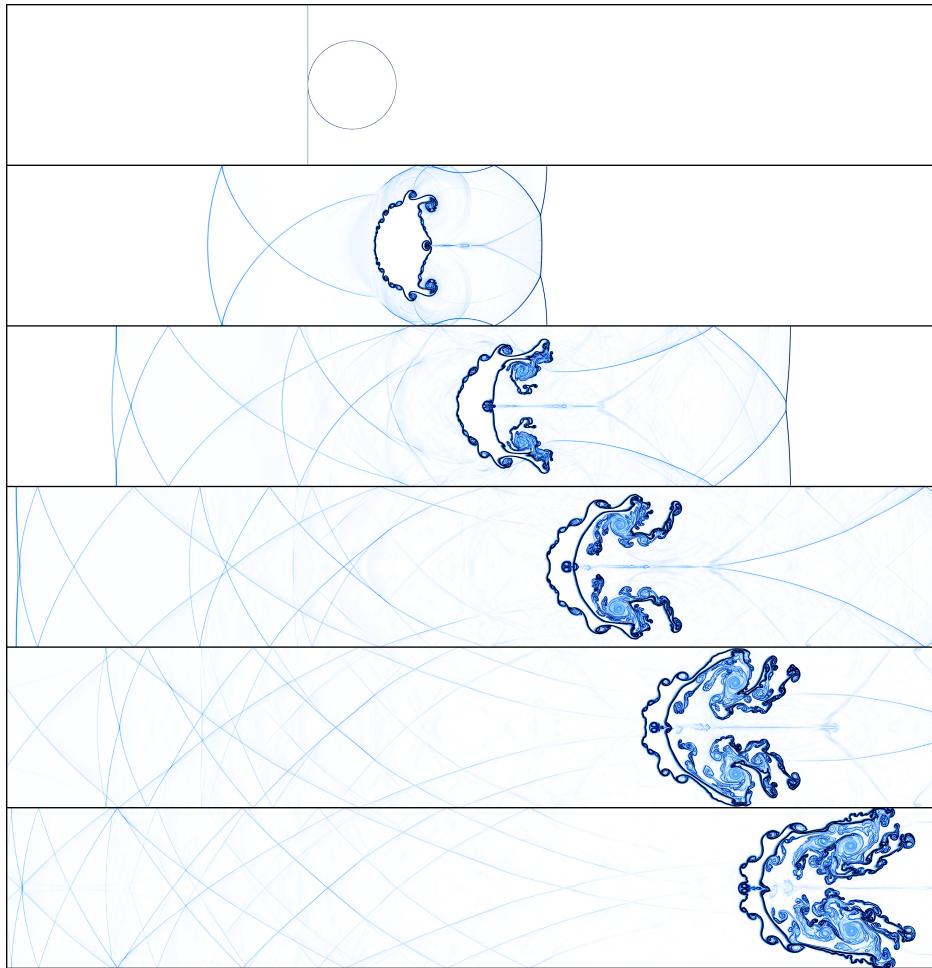


Fig. 3: 2D Shock-bubble – Numerical schlieren output (with respect to the air partial density) at  $t = \{0, 246, 492, 738, 984, 1230\} \mu s$ .

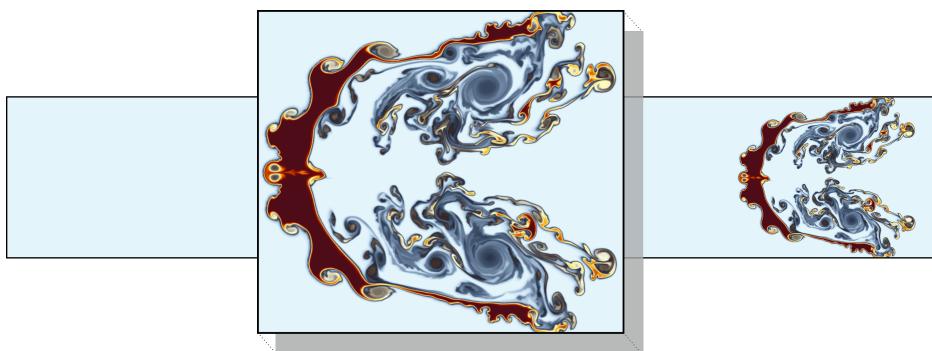


Fig. 4: 2D Shock-bubble – A zoomed in snapshot of the mass fraction for krypton at  $t = 1230 \mu s$ .

613 typical flow features of standard shock-bubble type problems and compare well with  
 614 the simulations presented in [27, Fig. 7].

615 **6.4. 2D – Simplified inertial confinement fusion configuration.** We now  
 616 perform a simulation of a multi-species implosion problem akin to inertial confinement  
 617 fusion (ICF)-type configurations inspired by [3, Sec. 6.6]. A demonstration of  
 618 physical experiments with similar setups can be found in Li et al. [29]. The  
 619 problem consists of a circular Mach 5 shock wave converging towards a species in-  
 620 terface inducing Richtmyer–Meshkov instabilities in the flow. These instabilities  
 621 are seeded by perturbations in the interface, which drive the flow into a chaotic  
 622 mixing state with distinct vortical structures. We simulate a shock wave moving  
 623 through ambient air ( $\gamma_1 = \frac{1.008}{0.72}$ ) with an internal helium region ( $\gamma_2 = \frac{5.1932}{3.115}$ ). Let  
 624  $\rho_{\text{shock}} = 5.002322673797607 \text{ kg m}^{-3}$ ,  $v_{\text{shock}} = 1.4966877698898315 \text{ ms}^{-1}$ ,  $p_{\text{shock}} =$   
 625  $2.8997678756713867 \text{ Pa}$ . The set up is as follows:

(6.4)

$$626 \quad \mathbf{w}(\mathbf{x}, t) := \begin{cases} (1, \rho_{\text{shock}}, -v_{\text{shock}} \frac{\mathbf{x}}{\|\mathbf{x}\|}, p_{\text{shock}}), & \text{if } 1.1 < \|\mathbf{x}\|, \\ (1, 1, \mathbf{0}, 0.1), & \text{if } 1 + 0.02 \cos(8\theta) < \|\mathbf{x}\| < 1.1, \\ (0, 0.05, \mathbf{0}, 0.1), & \text{otherwise,} \end{cases}$$

627 where  $\theta = \arctan(x_2/x_1)$ . See Figure 5 for the visual representation of the initial  
 628 conditions.

629 The computational domain is the disk characterized by  $R = 1.2 \text{ m}$  centered at  
 630  $(0, 0)$ . The mesh is composed of 12,582,912 elements with 12,587,009  $\mathbb{Q}_1$  degrees  
 631 of freedom. We enforce Dirichlet conditions on the boundary. The final time is  
 632 set to  $t_f = 0.5 \text{ s}$ . The contours of density (left) and mass fraction  $Y_1$  (right) are  
 633 shown in Figure 6 at various times  $t = \{0.2 \text{ s}, 0.4 \text{ s}, 0.6 \text{ s}\}$ . The effects of the interface  
 634 perturbation can be seen initially in the deformation of the shock structure and contact  
 635 line. These Richtmyer–Meshkov instabilities formed into several distinct quasi-radially  
 636 symmetric vortical structures stemming from the peaks of the interface perturbations.  
 637 The interaction of the shocks and contact discontinuities with these vortical structures  
 638 then forced the flow into a more chaotic mixing state. These small-scale flow features  
 639 and flow discontinuities were well-resolved by the proposed numerical approach.

640 **6.5. 3D – Axisymmetric triple point shock problem.** We now illustrate the  
 641 method with a three-dimensional triple point problem which was originally introduced  
 642 in Galera et al. [12, Sec. 8.3]. This problem is often used to demonstrate material  
 643 interface tracking in Lagrangian hydrodynamics as the problem naturally induces  
 644 vorticity. Instead of the usual set up, we consider a modification which can be thought  
 645 of as an “Eulerian” extension of the axisymmetric configuration introduced in Dobrev  
 646 et al. [10, Sec. 4.4]. Here, the high-pressure “left” state is unmodified, the usual  
 647 high-pressure high-density “bottom” state is now rotated about the  $x_1$ -axis creating  
 648 a cylinder, and the usual low-pressure low-density “top” state acts as the ambient  
 649 state outside the cylinder. For clarity, we illustrate this in Figure 7.

650 The set up is as follows. We set the parameters for each species by  $\gamma_1 = \frac{1.4}{1.0}$  and  
 651  $\gamma_2 = \frac{1.5}{1.0}$  and the initial set up is given by:

$$652 \quad (6.5) \quad \mathbf{w}(\mathbf{x}, 0) = \begin{cases} (0, 1, \mathbf{0}, 1), & \text{if } \mathbf{x} \in I, \\ (1, 1, \mathbf{0}, 0.1), & \text{if } \mathbf{x} \in II, \\ (1, 0.125, \mathbf{0}, 0.1), & \text{if } \mathbf{x} \in III, \end{cases}$$

653 where the subregions are defined by  $I := \{\mathbf{x} \in D : x_1 < 1\}$ ,  $II := \{\mathbf{x} \in D : x_1 \geq$

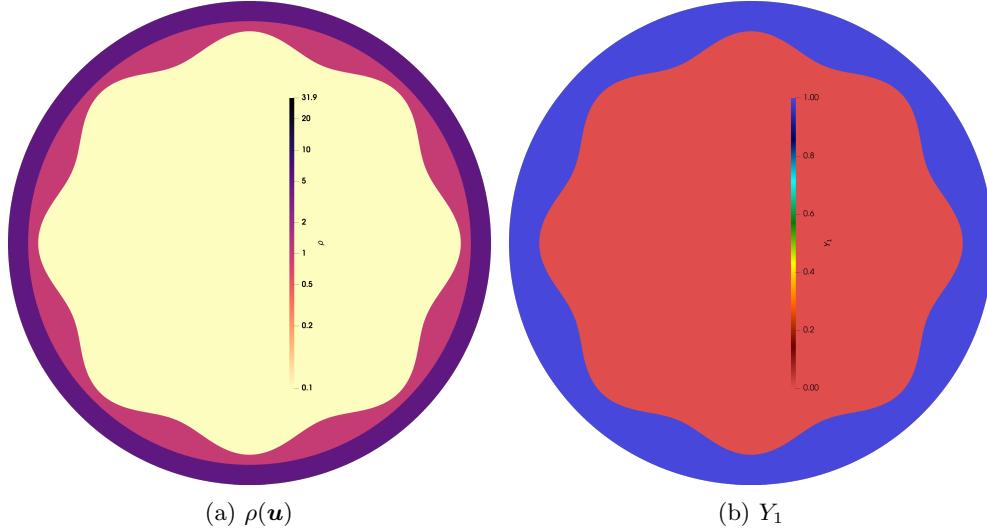


Fig. 5: 2D ICF-like problem – Initial set up.

654  $1, \sqrt{(x_2 - 1.5)^2 + x_3^2} \leq 0.5\}$ , and  $III := D \setminus (I \cup II)$ .

655 The computational domain is  $D := (0, 7 \text{ m}) \times (0, 3 \text{ m}) \times (0, 3 \text{ m})$  with slip boundary  
 656 conditions on all boundaries. For the sake of spatial resolution demonstration, we run  
 657 the simulation with two computational meshes. The first mesh, henceforth called the  
 658 “coarse mesh”, is composed of 4,114,121  $Q_1$  DOFs corresponding to 280 elements in  
 659 the  $x_1$ -direction, 120 elements in the  $x_2$ -direction and 120 elements in the  $x_3$ -direction.  
 660 The second mesh, henceforth called the “fine mesh”, is composed of 259,355,681  
 661  $Q_1$  DOFs corresponding to 1120 elements in the  $x_1$ -direction, 480 elements in the  $x_2$ -  
 662 direction and 480 elements in the  $x_3$ -direction. The simulation is run to the final time,  
 663  $t_f = 3 \text{ s}$ . We give the time snapshots for  $t = \{1 \text{ s}, 3 \text{ s}\}$  in Figure 8 for each mesh. The  
 664 representation in the figures is as follows. On the  $\{x_2 = 1.5\}$  and  $\{x_3 = 1.5\}$  planes,  
 665 we plot mixture density in a logarithmic scale. We then plot the  $\{0.5, 0.6, 0.7, 0.8, 0.9\}$   
 666 iso-volume contours of the species mass fraction  $Y_1$  in a solid color. These contours  
 667 are further cut along the  $\{x_2 = 0.8\}$  plane for visualization purposes. We see that the  
 668 typical flow features for this problem are well resolved along the shown planes.

669 **7. Conclusion.** This work presents a second-order accurate, invariant-domain  
 670 preserving numerical scheme for the compressible multi-species Euler equations which  
 671 ensures positivity of the species densities and internal energy/pressure as well as a  
 672 local minimum principle on the mixture entropy. We give the solution to the one-  
 673 dimensional Riemann problem for the multi-species formulation and derive an upper  
 674 bound on the maximum wave speed of the problem, which we then use to construct  
 675 a robust, first-order invariant-domain preserving approximation. This approach was  
 676 then extended to second-order accuracy using a modified convex limiting technique.  
 677 The numerical results demonstrate the scheme’s ability to handle challenging multi-  
 678 species flow problems with strong shocks and discontinuities, highlighting its potential  
 679 for use in high-fidelity simulations of compressible, multi-species flow phenomena.  
 680 Future work may extend this framework to include viscous effects, more complex

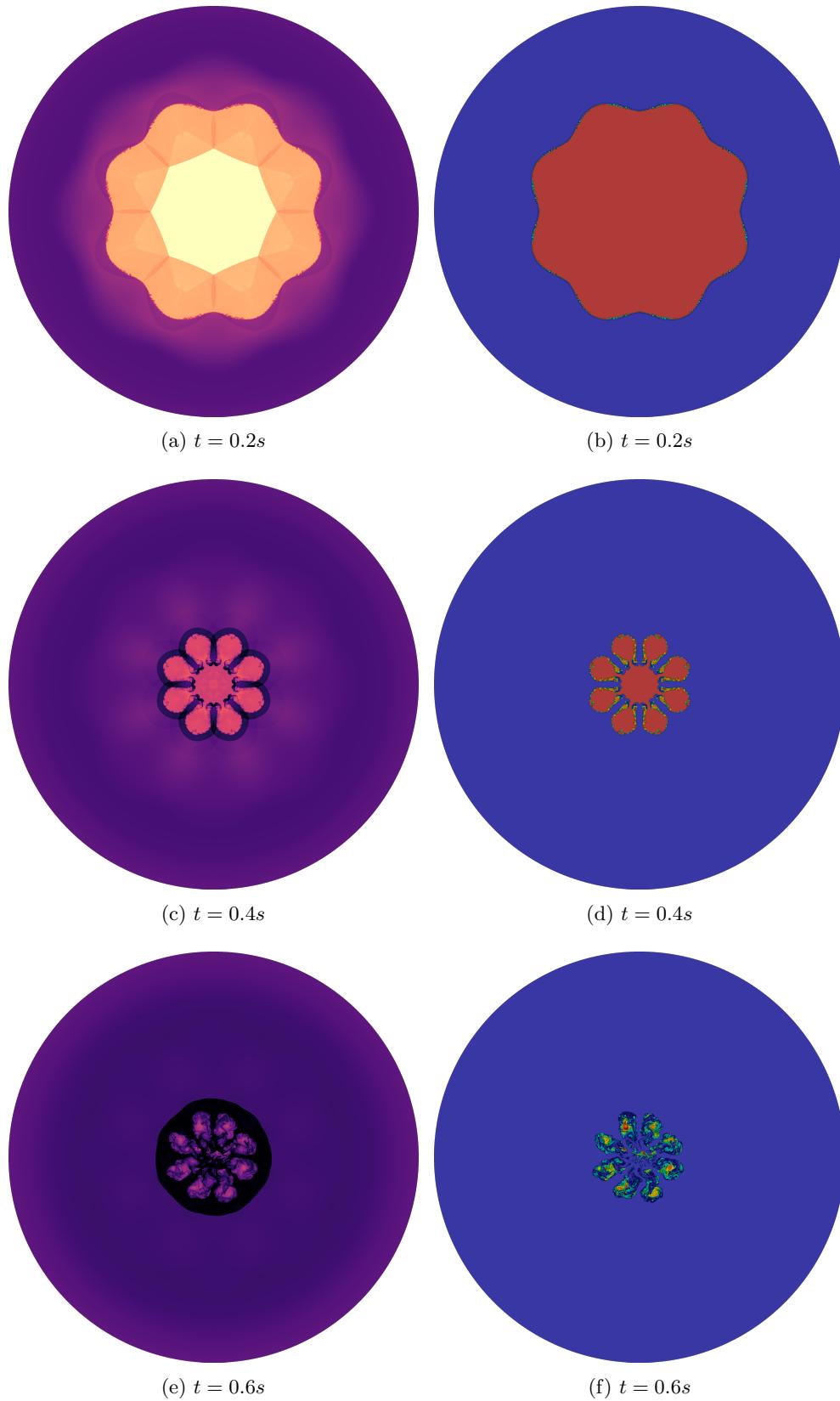


Fig. 6: 2D ICF-like problem – Contours of density in logarithmic scale (left) and species mass fraction  $Y_1$  (right) simulated using 12,587,009  $\mathbb{Q}^1$  degrees of freedom at varying time intervals. Legend identical to Figure 5.

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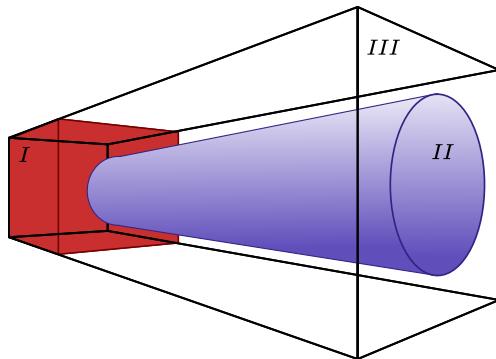


Fig. 7: 3D triple point problem – Initial setup.

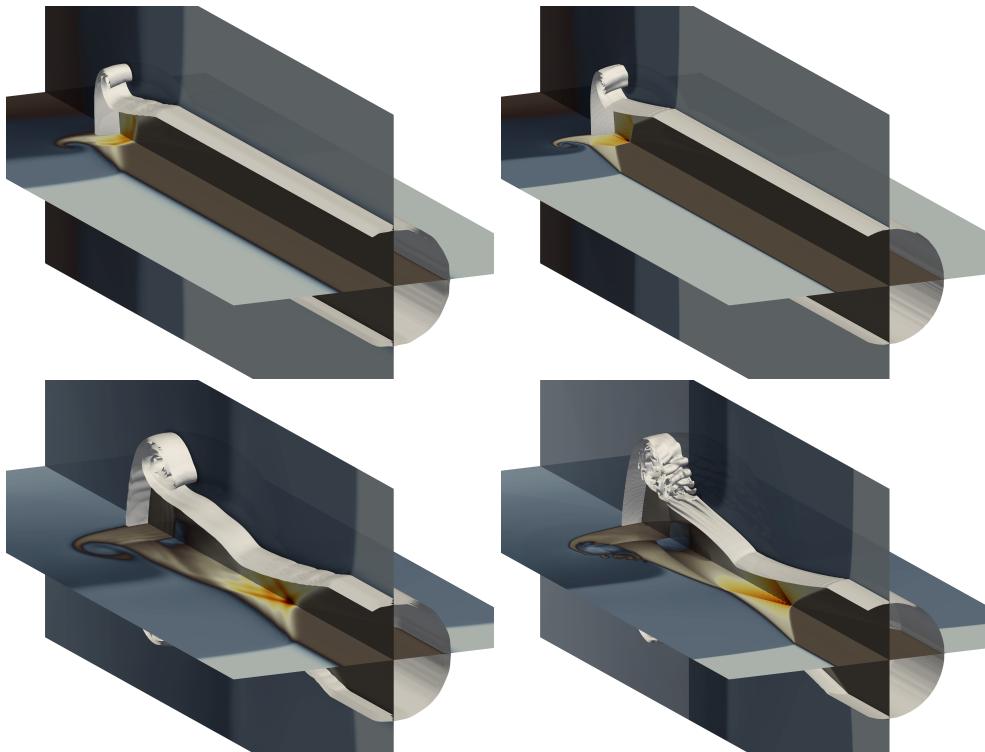


Fig. 8: 3D triple point problem – Time snapshots at  $t = \{1\text{ s}, 3\text{ s}\}$  with coarse mesh on the left and fine mesh on the right.

681 equations of state, or reactive flow physics.

682 **Appendix A. Thermal-Mechanical Equilibrium.** For the sake of completeness,  
683 we show how the assumption of thermal equilibrium, along with Dalton's law,  
684 yields the bulk pressure of the system (2.4) independent of the pressure equilibrium  
685 assumption.

686 PROPOSITION A.1. Assume thermal equilibrium holds,  $T = T_k = e_k/c_{v,k}$  for all  
 687  $k \in \{1:n_s\}$ , and that the pressure is given by Dalton's law  $p = \sum_{k=1}^{n_s} \alpha_k p_k(\rho_k, e_k)$  with  
 688  $p_k = (\gamma_k - 1)\rho_k e_k$ . Then

689 (A.1) 
$$p(\rho, e, \mathbf{Y}) = (\gamma(\mathbf{Y}) - 1)\rho e,$$

690 where  $\gamma(\mathbf{Y}) = c_p(\mathbf{Y})/c_v(\mathbf{Y})$ ,  $\rho = \sum_{k=1}^{n_s} \alpha_k \rho_k$ , and  $e = \sum_{k=1}^{n_s} Y_k e_k$ .

691 *Proof.* Using the definition of the pressure, we have the following,

692 
$$p = \sum_{k=1}^{n_s} \alpha_k p_k = \sum_{k=1}^{n_s} \alpha_k (\gamma_k - 1)\rho_k e_k = T \sum_{k=1}^{n_s} (\gamma_k - 1)\alpha_k \rho_k c_{v,k}.$$

693 Since  $c_{v,k}T = e_k$  for every  $k \in \{1:n_s\}$ , then the identity holds for any convex com-  
 694 bination of the  $n_s$  terms; in particular, the identity holds for mass averaging. Hence,  
 695  $c_v(\mathbf{Y})T = e$ . Then using that  $\alpha_k \rho_k = \rho Y_k$ , we have,

696 
$$p(\rho, e, \mathbf{Y}) = \frac{e}{c_v(\mathbf{Y})} \sum_{k=1}^{n_s} \alpha_k \rho_k (c_{p,k} - c_{v,k}) = \rho e \frac{c_p(\mathbf{Y}) - c_v(\mathbf{Y})}{c_v(\mathbf{Y})} = (\gamma(\mathbf{Y}) - 1)\rho e,$$

697 which completes the proof.  $\square$

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