

Effects of Boundary Conditions on Magnetic Friction

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December 10, 2017

I would like to express my deepest gratitude to Prof. Naomichi Hatano whose enormous support and insightful comments were invaluable during the course of my study. I am also indebt to Ryo Tamura who provided technical help and sincere encouragement. I would also like to express my gratitude to my family for their moral support and warm encouragements.

Abstract

In the present thesis, hogehoge. Moreover, fugafuga.

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Chapter 1

Introduction

The system is one of the simplest model of two-dimensional magnetic friction. Its spatial and spin dimensionality are far from realistic materials around us. However, we can use several facts from the exact solution for the two-dimensional Ising model, which makes the analysis easier than higher-dimensional cases.

Chapter 2

Velocity-driven Non-equilibrium Phase Transitions in Ising Models

Chapter 3

Numerical Simulations

3.1 Setup of the Model

Sliding friction is a form of energy dissipation on the surface between a moving object and its substrate. The dissipated energy is originated in the kinetic energy of the moving object. We here consider constantly moving case in which an external force maintains the motion of the object with endless supply of its kinetic energy. This view leads to its *non-equilibrium steady state*. When the system is in a non-equilibrium steady state, it is often easy to calculate several *energy currents* such as the frictional heat, its power and so on. Applying the view to our case where two square lattices of the Ising model slide against each other, we can formulate the problem as follows.

1. We prepare a square lattice of the Ising model of size $L_x \times L_z$ and impose periodic boundary conditions in the transverse (x) direction. We first set the system in the equilibrium state of a temperature T , whereas we set the open boundary conditions in the longitudinal (z) direction for the moment (fig).
2. We cut the system along the x -direction into two parts, maintaining interactions on the

cut (fig).

3. We slide two parts along the cut plane with relative velocity v . In other words, we shift the upper half by a lattice constant every $1/v$ unit time.

The Hamiltonian of the system is given by

$$\hat{H} = \hat{H}_{\text{upper}} + \hat{H}_{\text{lower}} + \hat{H}_{\text{slip}}(t), \quad (3.1)$$

where

$$\hat{H}_{\text{upper}} := -J_{\text{upper}} \sum_{\langle i,j \rangle \in \text{upper}} \hat{\sigma}_i \hat{\sigma}_j, \quad (3.2)$$

$$\hat{H}_{\text{lower}} := -J_{\text{lower}} \sum_{\langle i,j \rangle \in \text{lower}} \hat{\sigma}_i \hat{\sigma}_j, \quad (3.3)$$

$$\hat{H}_{\text{slip}}(t) := -J_{\text{slip}} \sum_{\langle i,j(t) \rangle \in \text{slip}} \hat{\sigma}_i \hat{\sigma}_{j(t)}. \quad (3.4)$$

Shift operations lead the system to repeated *pumping* and *dissipation* processes as follows (fig):

1. A shift operation excites the energy on the slip plane by the ammount $\langle \hat{H}_{\text{slip}}(t') - \hat{H}_{\text{slip}}(t) \rangle$.
2. The excited energy on the slip plane dispenses to the entire system $\langle \hat{H}_{\text{upper}} + \hat{H}_{\text{lower}} + \hat{H}_{\text{slip}}(t) \rangle$.
3. The excited entire system relaxes toward the equilibrium the heat bath.

The excited and relaxed amounts of energy per unit time correspond to the energy pumping

and dissipation, respectively. The energy pumping $P(t)$ and dissipation $D(t)$ are given by

$$P(t) := \sum_{i_v=0}^{v-1} \left\langle \hat{H}_{\text{slip}} \left(t' - 1 + \frac{i_v}{v} \right) - \hat{H}_{\text{slip}} \left(t - 1 + \frac{i_v}{v} \right) \right\rangle_{\text{st}}, \quad (3.5)$$

$$D(t) := \sum_{i_v=0}^{v-1} \left\langle \hat{H}_{\text{slip}} \left(t - 1 + \frac{i_v + 1}{v} \right) - \hat{H}_{\text{slip}} \left(t' - 1 + \frac{i_v}{v} \right) \right\rangle_{\text{st}}. \quad (3.6)$$

3.2 Definitions of Physical Quantities

We now consider the case in which that the system is in a non-equilibrium steady state. We define the frictional force density $f(L_z, T)$ by

$$f(L_z, T) := \lim_{L_x \rightarrow \infty} \frac{F(L_x, L_z, T)}{L_x}, \quad (3.7)$$

where $F(L_x, L_z, T)$ is the frictional force of a system of size $L_x \times L_z$ at a temperature T . We numerically formulate the large-size limit $L_x \rightarrow \infty$ as follows.

— Numerical large-size limit $L_x \rightarrow \infty$ —

If the quantity $F(L_x, L_z, T)/L_x$ is independent on L_x , $F(L_x, L_z, T)/L_x$ is a good approximation for $f(L_z, T)$.

In numerical simulations, we calculate the frictional force $F(L_x, L_z, T)$ using its power $D(L_x, L_z, T)$ by the formula

$$F(L_x, L_z, T) = \frac{D(L_x, L_z, T)}{v}, \quad (3.8)$$

where the quantity $D(L_x, L_z, T)$ is the long-time limit of $D(t)$ for the lattice of $L_x \times L_z$ at a temperature T .

We can easily verify the formula (3.8) by considering general cases in which the frictional

force and its power are both time dependent. Denoting the frictional force $F(x)$ at the position x , it holds that

$$\int_{t_0}^{t_1} dt D(t) = \int_{x(t_0)}^{x(t_1)} dx F(x) = \int_{t_0}^{t_1} \frac{dx}{dt} dt F(x(t)) = v \int_{t_0}^{t_1} dt F(x(t)), \quad (3.9)$$

for a time dependent $D(t)$, because $dx/dt = v$. Under the assumption of a non-equilibrium steady state, in the long-time limit, the integrands in both hand sides of the relation (3.9) are still equal to each other, and hence

$$D(L_x, L_z, T) = vF(L_x, L_z, T). \quad (3.10)$$

From now we call the quantity $D(L_x, L_z, T)$ *energy dissipation*.

Our models always reach non-equilibrium steady states in the long-time limit $t \rightarrow \infty$, which depend on the temperature T and the sliding velocity v ; We will prove in App. A. We use the fact that $\lim_{t \rightarrow \infty} |D(t)| = \lim_{t \rightarrow \infty} |P(t)|$ in order to calculate average value \bar{D} with less fluctuation by using the value \bar{P} [1–3]. We therefore have

$$P(L_x, L_z, T) = vF(L_x, L_z, T). \quad (3.11)$$

3.3 Non-equilibrium Monte Carlo Simulation

Energy dissipation process towards the heat bath occurs via a spin flip. This fundamental processes do not only describe equilibrium states, but also non-equilibrium steady states for a fixed temperature T [4]. Using Monte Carlo method, we can simulate this process.

3.3.1 Introduction the Time Scale to Ising Models

The Ising model which we deal with is a kind of kinetic Ising models [4], in which its time dependent statistics plays several important roles. In order to calculate dynamical observables such as the frictional power (3.11) and its dissipation rate (3.8), we have to define a *unit time* for finite size systems. We now consider the case in which a homogeneous spin chain of the volume L and a heat bath with the temperature T are interacting. This system are well described with enough large number of the spins. Denoting such a number N , we can consider two macroscopically equivalent models as follows:

- An N -spin chain with the lattice constant $a = L/N$,
- An $(M \times N)$ -spin chain with the lattice constant $a = L/(M \times N)$,

where M is the large number which have the same property as N . Since both of models well describe the system of volume L , typical time scale¹ of each system should be the same. And under the *homogeneous* assumption that for both models each spin is independently interacting with the heat bath, the dynamics of any spin in the former and that of any M -spins subsystem in the latter are effectively equivalent. Thus as long as we consider the dynamics of same volume systems, we can define the unit time scale using its number of spins. This concept can be easily implemented on the ordinary *equilibrium* Monte Carlo simulation for classical spin systems.

For the equilibrium Monte Carlo simulation, the most naive approach for the equilibrium state is the single flip algorithm, where we perform the sequence a random selection of the spin and its flipping with temperature dependent probability $p(T)$. We often use the Metropolis probability $p_M(T) := \min\{1, e^{-\frac{\Delta E}{k_B T}}\}$ as the probability $p(T)$, where ΔE is the energy difference

¹If we use the same criterion, any time scale may be introduced. For example, we can define a *typical time scale* as the time taken to flip all the spin.

by the flipping. The Metropolis probability $p_M(T)$ have a good property, called *detailed balanced condition*, which certainly leads the system towards the true equilibrium state with enough many repetition of the algorithm. This process and randomness well describes the interaction and the homogeneousness with the heat bath. We often call *Monte Carlo step* a single process of the algorithm, and define *Monte Carlo sweep* N -times process, where N is the number of spins. According to the earlier discussion, the unit time in the system is nothing but the Monte Carlo sweep. Thus the more spins the system contains, the higher time resolution we can simulate with.

3.3.2 Slip Plane with the Velocity v

Using the introduced time scale, we can also introduce the slip plane with the velocity v to the system with N -spins. Corresponding to the setup in Sec. 3.1, we perform the extended single flip algorithm as follows:

1. **Shifting:** We shift the upper half by a lattice constant
2. **Flipping:** We perform ordinary single flips for N/v times.
3. We repeat the process 1 + 2 for $(v - 1)$ times.

In the extended algorithm, the upper half slides with the velocity v in a unit time at regular intervals. We prove the fact that this algorithm lead the system of any size to the non-equilibrium steady state depending the temperature T and the velocity v .

3.3.3 Calculation Method

The observables which we are interested in are the frictional power $P(t)$ and its dissipation rate $D(t)$. In Monte Carlo simulations, the frictional power $P(t)$ is the energy difference by

the shifting operation and the dissipation rate is that by the flipping for a unit time. Both observables have the same absolute value in the long time limit.

Chapter 4

Result of Simulation

4.1 Settings of the Parameters

In the simulation, we fixed the velocity to $v = 10$ and the parameter regions for the temperatures T and the longitudinal size L_z are set as follows:

$$\frac{k_B T}{J} \in \{0.0, 0.1, 0.2, \dots, 1.9, 2.0, 2.02, 2.04, \dots, 2.48, 2.50, 2.6, 2.7, \dots, 5.0\}, \quad (4.1)$$

$$L_z \in \{4, 6, 8, 10, 12, 14, 16\}. \quad (4.2)$$

For all the parameters, we relaxed the system for 5000 [MCs] toward the equilibrium state and relaxed for 5000 [MCs] toward the non-equilibrium steady state by swicthing to nonzero v , using Metropolis probability $p_M(T)$.

The quantitis which we calculated are frictional force density $f(L_z, T)$, bulk energy density $\epsilon_b(L_z, T)$ and bulk heat capacity $c_b(L_z, T)$ for two cases that the boundary conditions on the z -direction are *anti-parallel* and *parallel*. For all the quantities, we performed *sample average* over 480 samples and *time average* over the latter 4500 [MCs]¹.

¹This time length for averaging is based on the criterion that it is much longer than the correlation time of

4.2 Behavior of Frictional Force Density $f(L_z, T)$

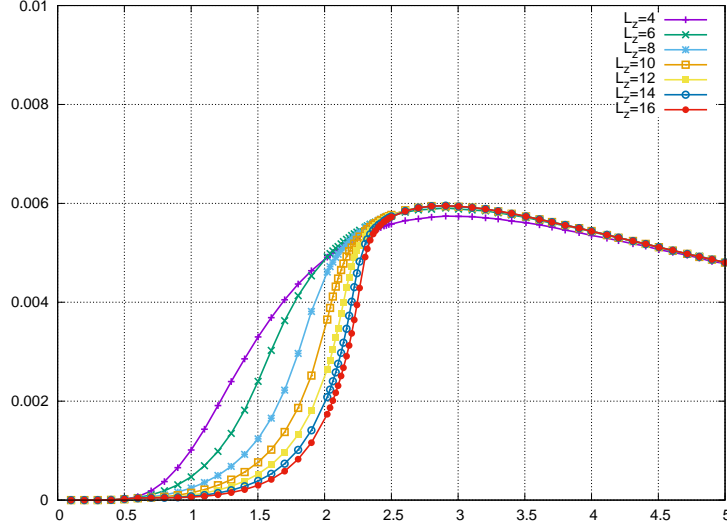


Figure 4.1: The temperature T dependence of the frictional force density $f(L_z, T)$ with the anti-parallel boundary condition along the z -direction for each longitudinal size L_z are plotted.

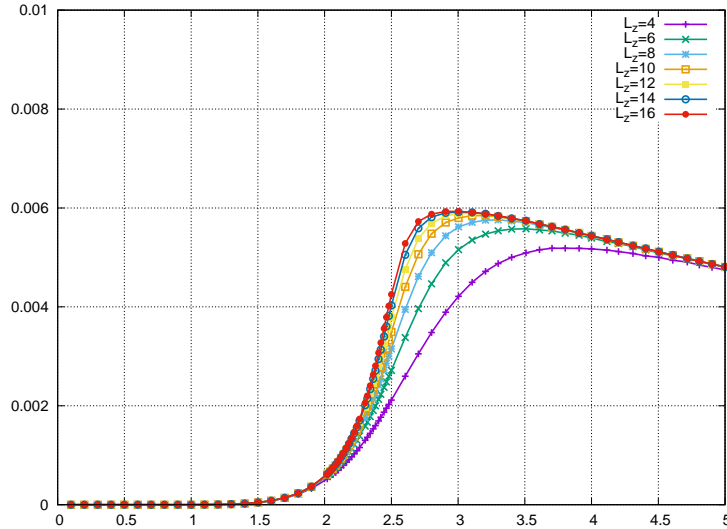


Figure 4.2: The temperature T dependence of the frictional force density $f(L_z, T)$ with the parallel boundary condition along the z -direction for each longitudinal size L_z are plotted.

the system, and the former data over $5000 + 500$ [MCs] are unwanted. The correlation time for each parameter is estimated by checking the relaxation of $P(t)$ and $D(t)$.

4.3 Behavior of Bulk Energy Density $\epsilon_b(L_z, T)$

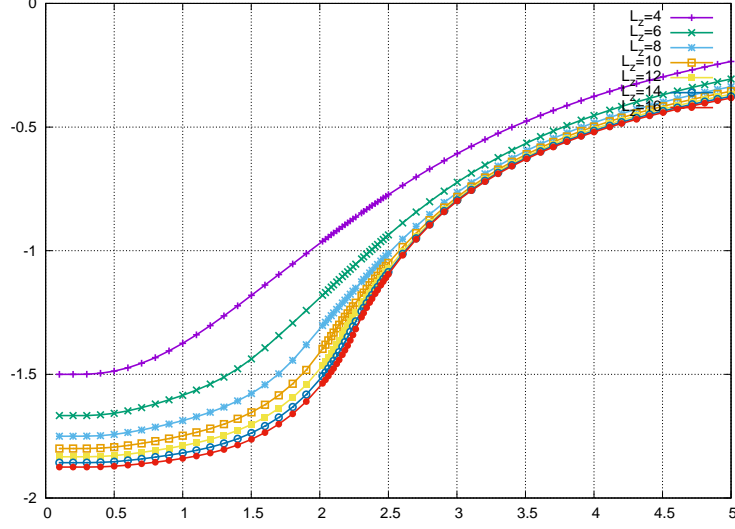


Figure 4.3: The temperature T dependence of the bulk energy density $\epsilon(L_z, T)$ with the anti-parallel boundary condition along the z -direction for each longitudinal size L_z are plotted.

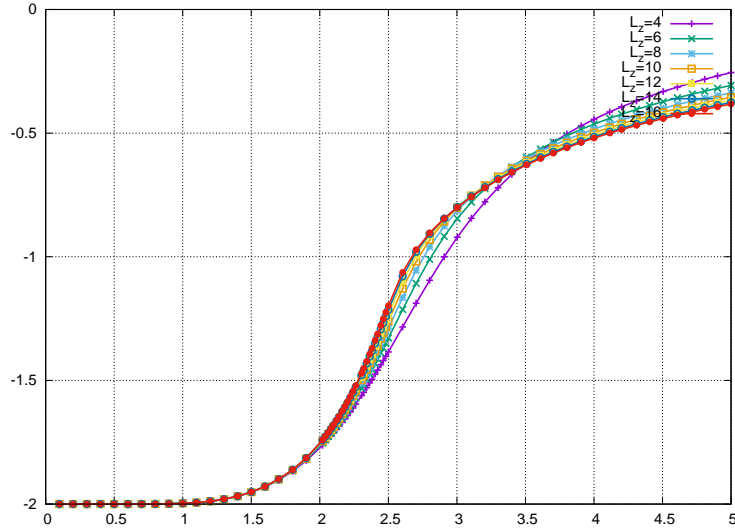


Figure 4.4: The temperature T dependence of the bulk energy density $\epsilon(L_z, T)$ with the parallel boundary condition along the z -direction for each longitudinal size L_z are plotted.

4.4 Behavior of Bulk Heat Capacity $c_b(L_z, T)$

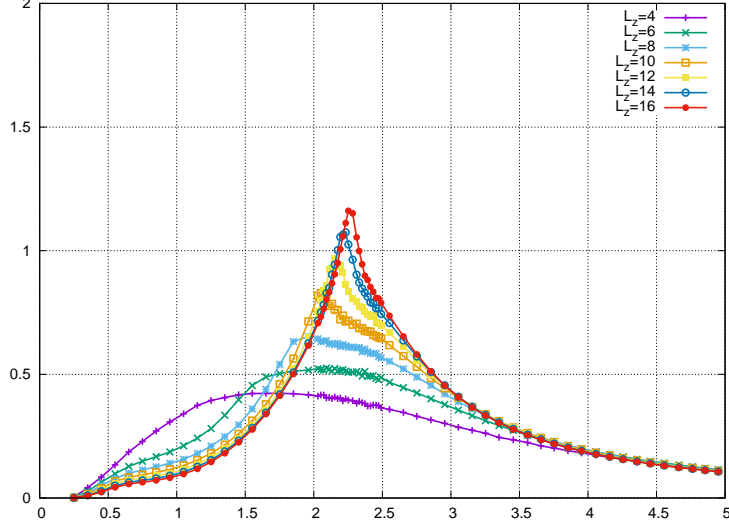


Figure 4.5: The temperature T dependence of the bulk heat capacity $c(L_z, T)$ with the anti-parallel boundary condition along the z -direction for each longitudinal size L_z are plotted.

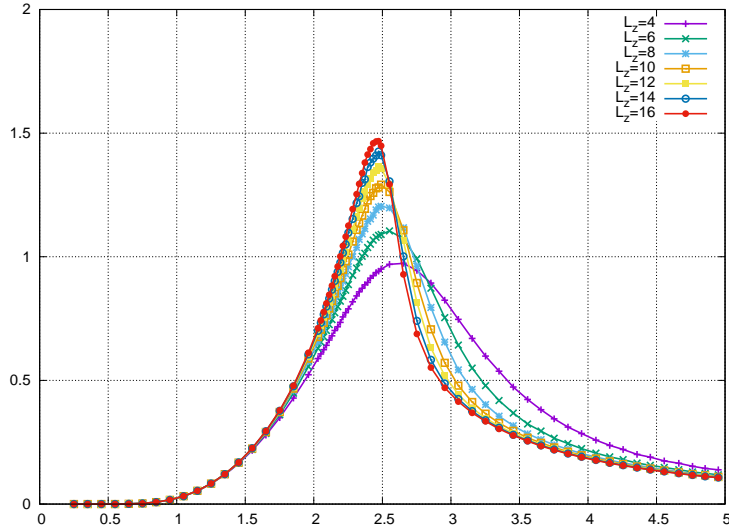


Figure 4.6: The temperature T dependence of the bulk heat capacity $c(L_z, T)$ with the parallel boundary condition along the z -direction for each longitudinal size L_z are plotted.

Chapter 5

Summary and Discussion

Summary.

Appendix A

Proof of the existence of NESS

Appendix B

Simulation Algorithms

Algorithm 1 Single Flip Algorithm for a Monte Carlo Time (Equilibrium)

```
for  $i_{\text{step}} = 1, \dots, N_{\text{size}}$  do
  randomly chose a spin
  flip by the probability  $\min\{1, e^{\beta\Delta E}\}$ 
end for
measurement
```

Algorithm 2 Single Flip Algorithm for a Monte Carlo Time (Non-equilibrium)

```
pump = 0
diss = 0
for  $i_v = 1, \dots, v$  do
  prev  $\leftarrow$  energy on the slip plane
  sliding
  next  $\leftarrow$  energy on the slip plane
  pump = pump + (next - prev)
  prev  $\leftarrow$  energy on the entire system
  for  $i_{\text{step}} = 1, \dots, N_{\text{size}}/v$  do
    flip by the probability  $\min\{1, e^{\beta\Delta E}\}$ 
  end for
  next  $\leftarrow$  energy on the entire system
  diss = diss + (next - prev)
end for
measurement
```

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