

Mini Project 2
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Part 1

A Values of small signal parameters h_{fe} , h_{ie} , and h_{oe} for $V_{CE} = 10V$, $I_C = 1mA$, $f = 1kHz$, and $T = 25^\circ C$ for a 2222N2A NPN transistor

Parameter (Units)	Minimum Value	Maximum Value
h_{fe}	50	300
$h_{ie} (k\Omega)$	2.0	8.0
$h_{oe} (\mu S)$	5.0	35

Values found from:

https://alltransistors.com/pdfview.php?doc=mtp2n2222a_p2n2222a.pdf&dire=_motorola

B Plot V_{be} vs I_b , V_{ce} vs I_c with characteristic I_b , and V_{ce} vs I_c with characteristic V_{be} graphs, calculate β , g_m , r_π , r_o , and Early Voltage (V_a)

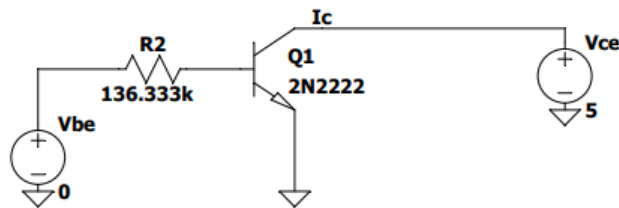


Figure 1.1. Circuit used to calculate I_b vs V_{be} graph

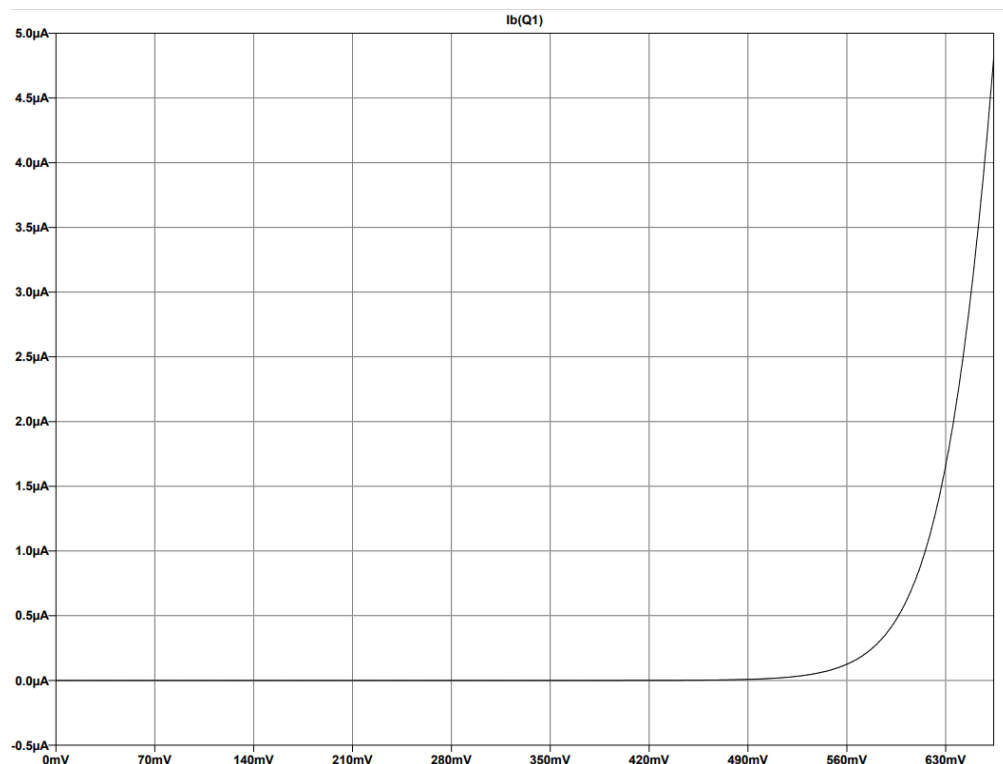


Figure 1.2. Resultant I_b vs V_{be} relationship

I used the circuit in the previous part to measure the current going into the Base of the NPN amplifier. I adjusted the V_{ce} and V_{be} elements to measure the remaining relationships shown in the next pages.

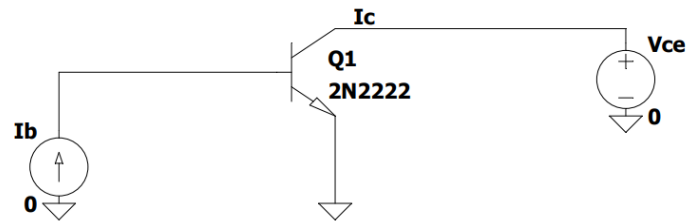


Figure 1.3. Circuit used to calculate I_c vs V_{ce} graph with characteristic I_b

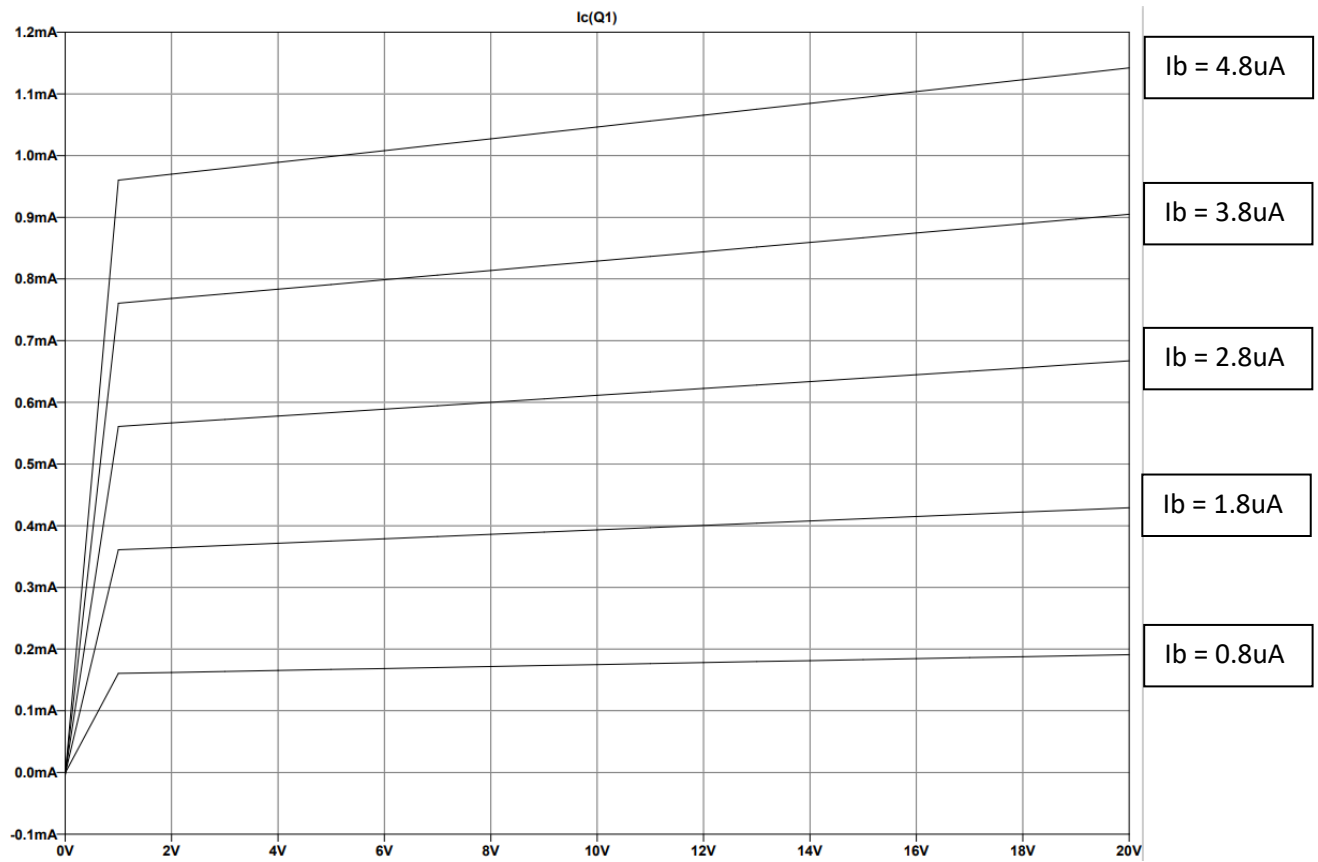


Figure 1.4. Resultant I_c vs V_{ce} relationship with characteristic I_b

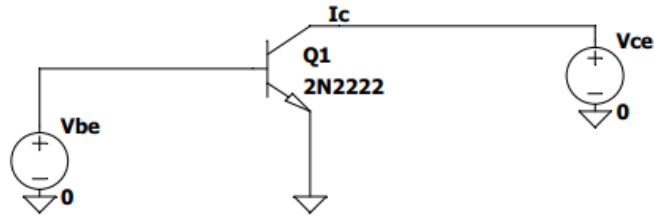


Figure 1.5. Circuit used to calculate I_c vs V_{ce} graph with characteristic V_{be}

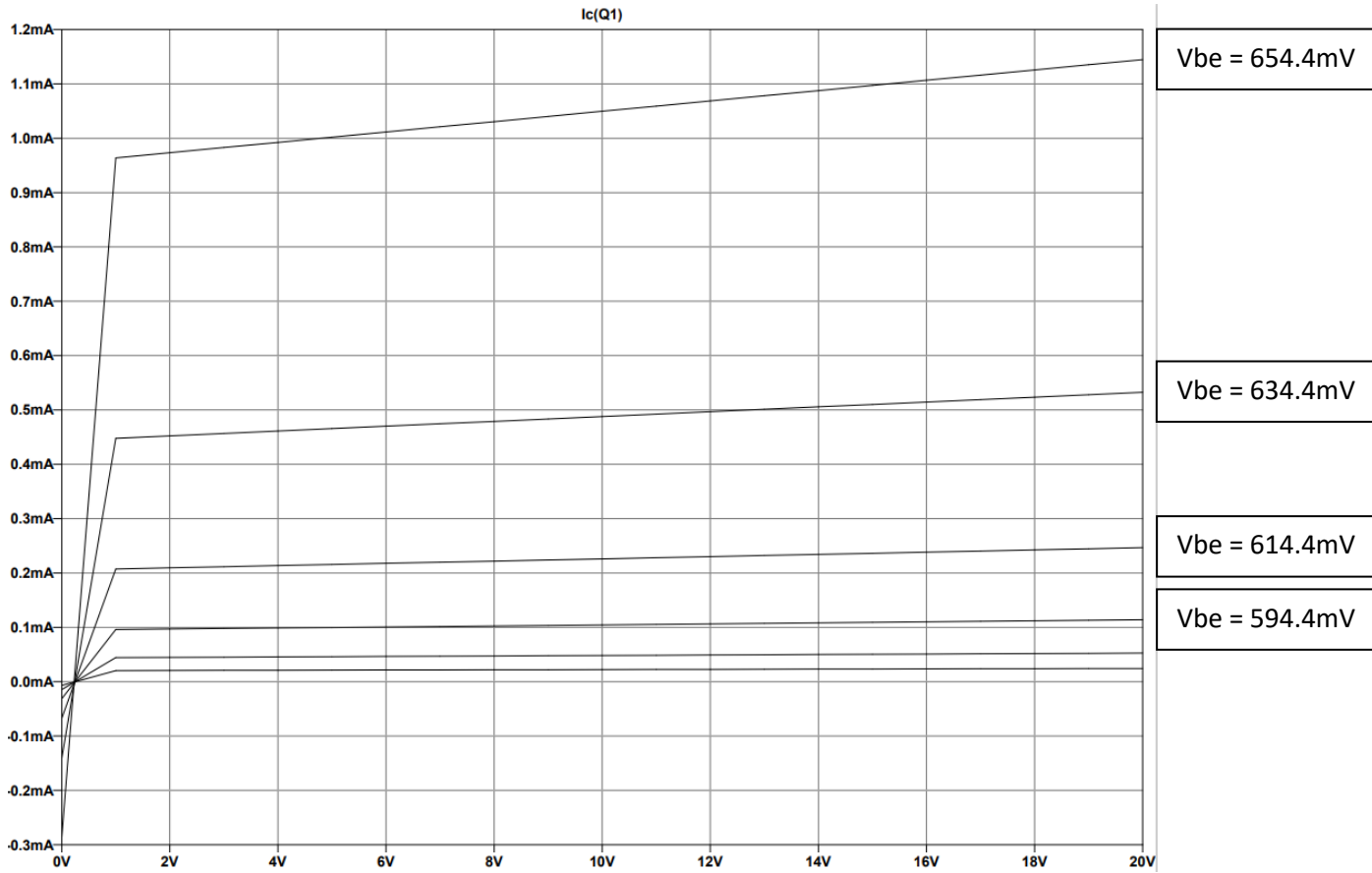


Figure 1.6. Resultant I_c vs V_{ce} relationship with characteristic V_{be}

We want the operating $I_c = 1\text{mA}$ at $V_{ce} = 5\text{V}$. We see that this operating point occurs at $I_b = 4.8\mu\text{A}$ and $V_{be} = 654.4\text{mV}$.

$$\beta = \frac{I_c}{I_b} = \frac{1\text{mA}}{4.8\mu\text{A}} = 210.526$$

$$g_m = \frac{I_c}{V_T} = \frac{1\text{mA}}{25\text{mV}} = 0.04\text{S}$$

$$r_{\pi} = \frac{\beta}{g_m} = \frac{210.526}{0.04\text{S}} = 5.26\text{k}\Omega$$

To find V_a , I needed to find where the I_c vs V_{ce} graph intersects with the x-axis.

$$y = mx + b \quad m = \frac{1.05mA - 1mA}{10V - 5V} = 10m\Omega$$

$$b = y - mx = 1.05mA - 10\mu(10) = 0.95 \text{ mA}$$

$$I_c = 10m\Omega * V_{ce} + 0.95mA \rightarrow I_c = 0 \rightarrow 10m\Omega * V_{ce} = -0.95 \rightarrow V_{ce} = -95 = -V_a$$

Therefore, **$V_a = 95V$**

$$r_o = \frac{V_a}{I_c} = \frac{95V}{1mA} = 95k\Omega$$

h_{fe} is equivalent to β . Since β is within the range of 50 to 300 it is a good calculation

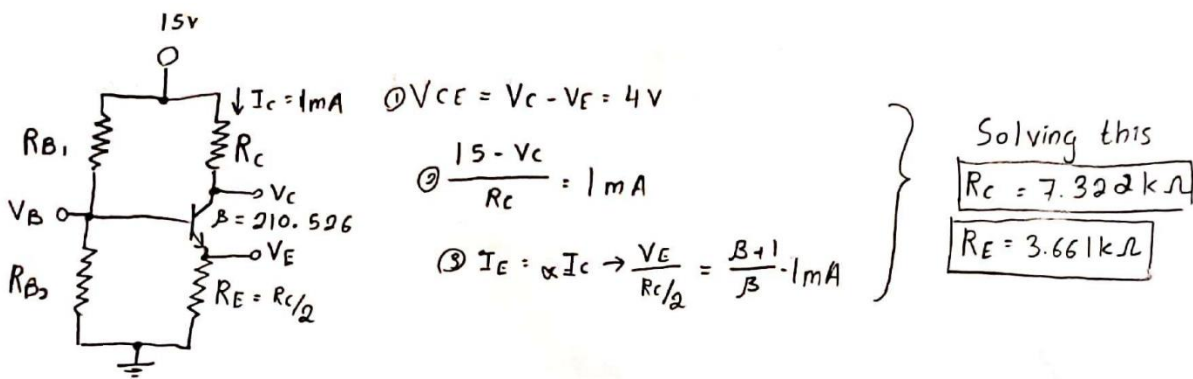
h_{ie} is equivalent to r_{π} . Since r_{π} is within the range of 2.0k to 8.0k it is a pretty good calculation.

h_{oe} is equivalent to r_o^{-1} . Since r_o is within the range of $5.0\mu^{-1}$ and $35\mu^{-1}$ it is a good calculation.

C

- i) Forward bias the NPN for $V_{ce} \leq 4V$ in bias network. Calculate all resistors values and DC Operating pt

First, I started by trying to find R_c and R_e by using some basic NPN relations and KCL equations, as well as parameters from the previous part



I set $R_{B1} = 50k$, I used trial and error until I found an R_{B2} that brought $I_c = 1mA$, its operating point. $R_{B2} = 20.8k$. This is the resultant circuit

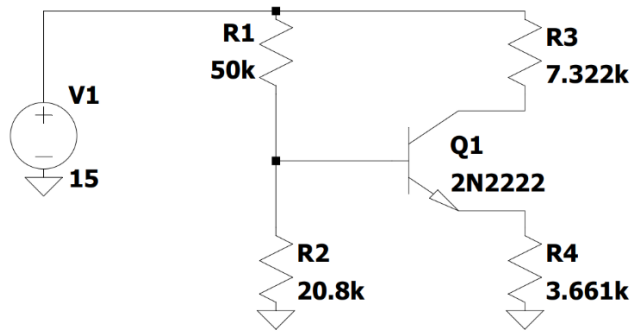


Figure 1.7. Bias network circuit built using calculated resistor values

I analyze the circuit and find the DC operating point.

$I_C = 1\text{mA}$ $I_E = 1.001\text{mA}$ $I_B = 4.86\mu\text{A}$ $V_{BE} = 0.7\text{V}$ $V_{CE} = 3.99\text{V}$

ii) Use $1/3^{\text{rd}}$ rule to bias the circuit

Below is my work for the $1/3^{\text{rd}}$ rule to calculate R_{B1} , R_{B2} , R_E , and R_C . I used these resistors to value the network below

$$V_C = \frac{2}{3}(15\text{V}) = 10\text{V} \quad V_E = \frac{1}{3}(15\text{V}) = 5\text{V} \quad \beta = 210.526 \quad I_C = 1\text{mA} \quad I_E \approx I_C = 1\text{mA}$$

$$V_{BE} \approx 0.7\text{V} \quad I_B = I_C / \beta = \frac{1\text{mA}}{210.526} = 4.75\mu\text{A}$$

$$R_{B1} = \frac{\frac{2}{3}(15\text{V}) - 0.7\text{V}}{1\text{mA} / \beta} = 1.349 \cdot 10^5 \Omega$$

$$R_{B2} = \frac{\frac{1}{3}(15\text{V}) - 0.7\text{V}}{I_E \left(\frac{1}{\beta} - \frac{1}{\beta+1} \right)} = 8.88 \cdot 10^4 \Omega$$

$$R_C = \frac{15 - V_C}{I_C} = 5\text{k}$$

$$R_E = \frac{5 - 0}{I_E} = 5\text{k}$$

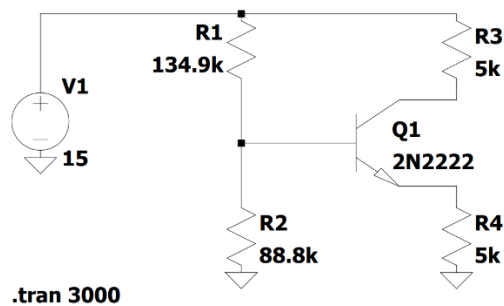


Figure 1.8. Bias network circuit using $1/3^{\text{rd}}$ rule

I analyze the circuit and find the DC operating point.

$I_C = 1.003\text{mA}$ $I_E = 1.008\text{mA}$ $I_B = 4.827\mu\text{A}$ $V_{BE} = 0.7\text{V}$ $V_{CE} = 4.969\text{V}$

iii) Use commonly available resistors to replace the resistors found using the $1/3^{\text{rd}}$ rule

Below is the transformed version of Figure 1.8 with commonly available resistors

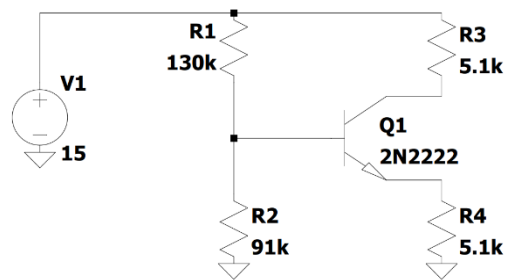


Figure 1.9. Bias network circuit using $1/3^{\text{rd}}$ rule and commonly available resistors

I analyzed the circuit and find the DC Operating point.

$I_c = 1.026\text{mA}$ $I_e = 1.031\text{mA}$ $I_b = 4.954\mu\text{A}$ $V_{be} = 0.7\text{V}$ $V_{ce} = 4.513\text{V}$

iv) Comment on the DC operating points between the different circuits in i – iii

By comparing the 3 DC operating points, I notice that I_c consistently is around 0.1mA, likewise I_e is also always around 0.1mA. I_b is also very close together and V_{be} are very close as well. V_{ce} are a little bit different, where V_{ce} in the circuit in part i is close to 4V whereas the circuits in parts ii – iii were closer to 5V, however, the circuit in part iii is closer to the original circuit than part i was.

Based on these observations I can conclude that the $1/3^{\text{rd}}$ rule is accurate enough for our purposes and adjusting resistor values to commonly available resistors did not affect the accuracy of our operating points.

D Using the circuit in Part C iii, find DC operating points with the 2N3904 transistor and 2N4401 transistor.

I used the same circuit as Part C iii and simply changed the transistors between operating points.

2N3904 NPN DC Operating Points:

$I_c = 1.022\text{mA}$ $I_e = 1.025\text{mA}$ $I_b = 3.279\mu\text{A}$ $V_{be} = 0.7\text{V}$ $V_{ce} = 4.768\text{V}$

2N4401 NPN DC Operating Points:

$I_c = 1.022\text{mA}$ $I_e = 1.025\text{mA}$ $I_b = 3.279\mu\text{A}$ $V_{be} = 0.7\text{V}$ $V_{ce} = 4.768\text{V}$

Comparing the 3 operating points, I_c is very similar, and I_e is also quite similar. I_b of 2N2222A is quite different compared to the other 2 transistors. V_{be} is similar and V_{ce} is also quite similar, on I_b is different.

Also, interestingly, the DC Operating points of 2N3904 and 2N4401 are equivalent.

Part 2

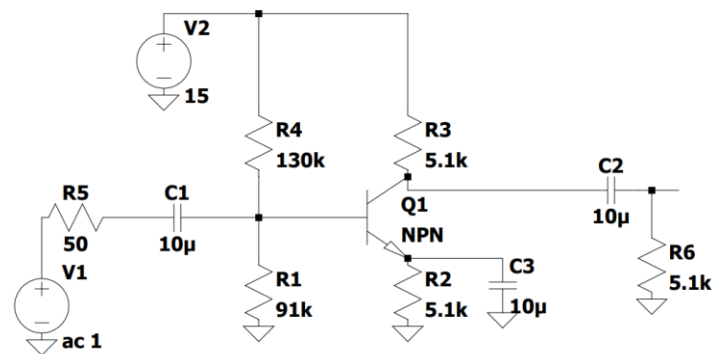


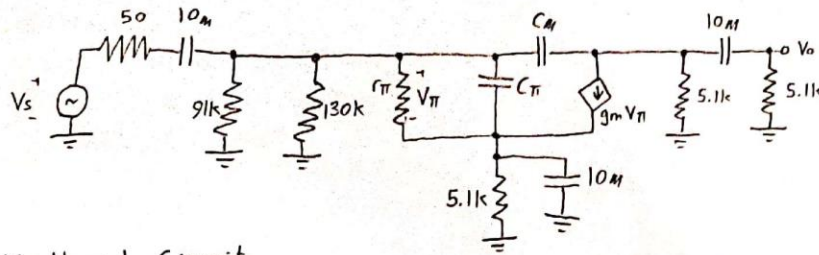
Figure 2.1. Common Emitter Amplifier

The R_{Load} (R_6 in this model) was chosen by trial and error. I tried multiple load resistors and found that the output power ($V \cdot I$) was highest when $R_{Load} = R_c = R_e = 5.1k$.

A Calculate poles and zeroes of this circuit and then measure them. Do this for all NPNs (2N2222A, 2N3904, 2N4401)

Showing the work for all 3 transistors would take a lot of space, so I will show the general working using symbols and use the same method for all the poles and zeroes for each transistor.

Hybrid- π Model



$$\beta = I_c / I_B$$

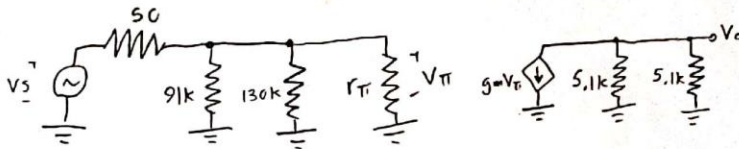
$$g_m = I_c / V_T$$

$$r_{\pi} = \beta / g_m$$

$$C_{\pi} = 2 \cdot C_{JE} + T_F \cdot g_m \approx 10^{-12} F$$

$$C_M = \frac{C_{JC}}{(1 + \frac{V_{CE}}{V_{JC}})^{m_{JC}}} \approx 10^{-12} F$$

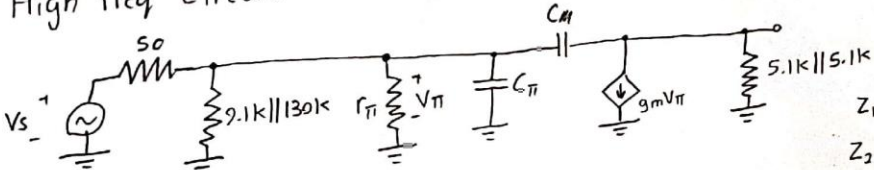
Midband Circuit



$$\frac{V_{\pi}}{V_s} = \frac{r_{\pi}}{50 + 91k \parallel 130k \parallel r_{\pi}}, \quad \frac{V_o}{V_{\pi}} = -g_m (5.1k \parallel 10M)$$

$$A_m = \frac{V_o}{V_s} = \frac{V_{\pi}}{V_s} \cdot \frac{V_o}{V_{\pi}}$$

High freq Circuit

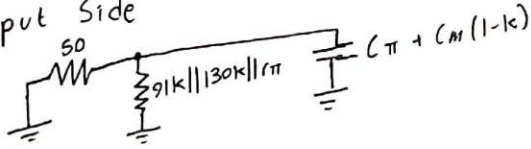


$$k = -g_m (5.1k \parallel 10M)$$

$$Z_1 = Z_{-1-k} \rightarrow \frac{1}{C_1 s} = \frac{1}{C_M s} \cdot \frac{1}{1-k} \rightarrow C_1 = C_M (1-k)$$

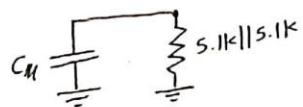
$$Z_2 = Z_{\frac{k}{1-k}} \rightarrow C_2 = C_M$$

Input Side



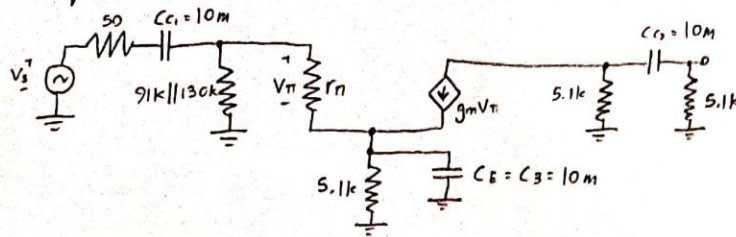
$$\omega_{HP1} = \frac{1}{(C_{\pi} + C_M (1-k)) (91k \parallel 130k \parallel r_{\pi})}$$

Output side



$$\omega_{HP2} = \frac{1}{C_M (5.1k \parallel 10M)}$$

Low freq Circuit



$$\omega L_{Z1} = \omega L_{Z2} = 0$$

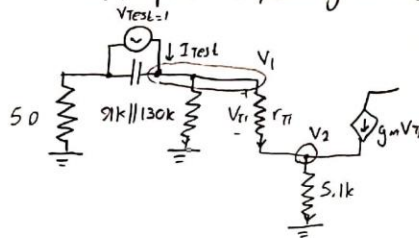
$$\text{3rd zero @ } Z_E = \infty \text{ or } Y_E = 0$$

$$Y_E = \frac{1}{5.1k} + s C_E = 0$$

$$s = -\frac{1}{5.1k \cdot C_E} \rightarrow \omega_{LZ3} = \frac{1}{10m \cdot 5.1k}$$

Because of where C_{c1} is, we choose it so it will short before other capacitors, or else it would act like a low-pass circuit @ low freq. From C_{c1} 's point of view, the other caps are DCs.

- Focus on C_{c1} , open everything else, apply a test voltage instead of C_{c1} to find R @ C_{c1}



$$I_{\text{Test}} = \frac{V_1}{91k \parallel 130k} + \frac{V_1 - V_2}{r_{\pi}}$$

$$g_m (V_1 - V_2) + \frac{V_1 - V_2}{r_{\pi}} = \frac{V_2}{5.1k}$$

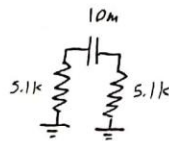
$$I_{\text{Test}} = \frac{1 - V_1}{50}$$

$$R_{eq} = \frac{V_{\text{Test}}}{I_{\text{Test}}} = \frac{1}{I_{\text{Test}}}$$

Solve

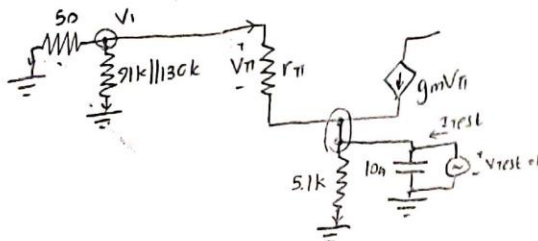
$$\omega_{LP1} = \frac{1}{10m \cdot R_{eq}}$$

- Focus on C_{c2} , it exists at output so we ignore rest of the circuit



$$\omega_{LP2} = \frac{1}{10m (5.1k \parallel 5.1k)} = 9.804 \text{ Hz}$$

- Focus on C_E (we will also call C_3 so pole numbering is consistent) - SC every other capacitor
Apply V_{Test} to get equivalent R across C_E



$$\frac{V_1}{50} + \frac{V_1}{91k \parallel 130k} = \frac{V_1 - 1}{r_{\pi}}$$

$$I_{\text{Test}} + g_m V_{\pi} + \frac{V_1 - 1}{r_{\pi}} = \frac{1}{5.1k}$$

$$V_{\pi} = V_1 - V_2$$

$$R_{eq} = \frac{1}{I_{\text{Test}}}$$

Solve

$$\omega_{LP3} = \frac{1}{10m \cdot R_{eq}}$$

Analyzing 2N2222A

$g_m = 0.04\text{S}$ $r_{\pi} = 5.26\text{k}\Omega$ $C_{\pi} = 40.411\text{pF}$ $C_{\mu} = 8.349\text{pF}$

$A_m = -111$ $\omega_{Hp1} = 20.74\text{MHz}$ $\omega_{Hp2} = 201.3\text{MHz}$ $\omega_{Lz1} = \omega_{Lz2} = 0$

$\omega_{Lz3} = 19.608\text{Hz}$ $\omega_{Lp1} = 1.932\text{Hz}$ $\omega_{Lp2} = 9.804\text{Hz}$ $\omega_{Lp3} = 4.006\text{kHz}$

Output bode plot from simulated circuit

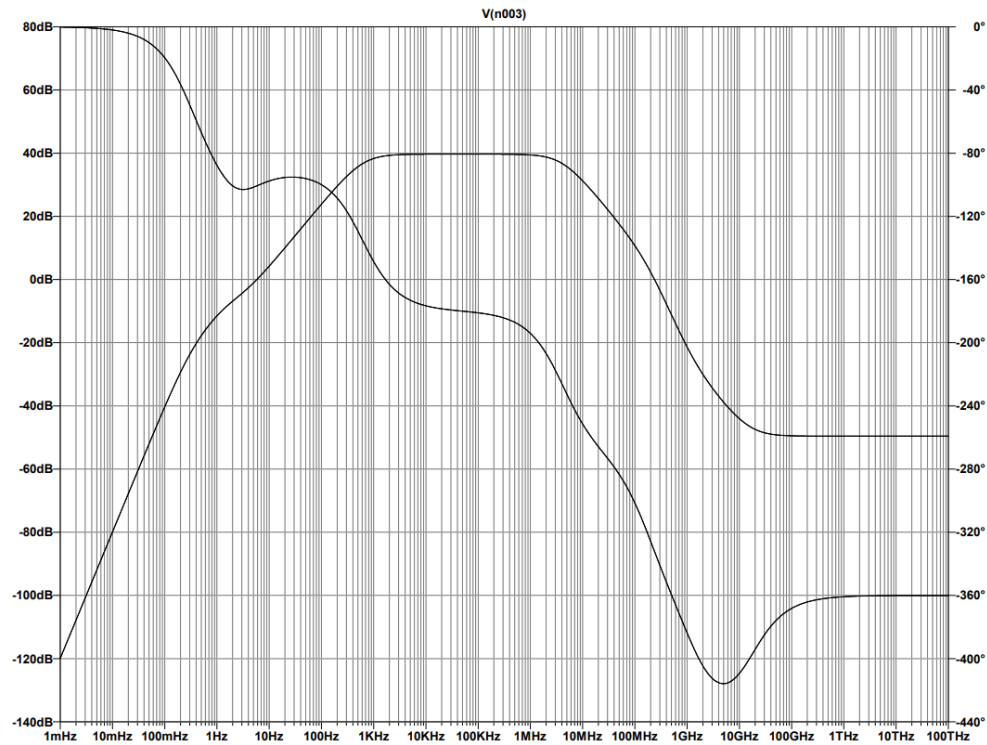


Figure 2.2. 2N2222A CE amplifier bode plot

To measure poles from the simulated circuit, I used linear approximation

These are the comparisons between the calculated and measured (approximate) locations of poles and zeroes

	ω_{Lp1}	ω_{Lp2}	ω_{Lp3}	ω_{Lz1}	ω_{Lz2}	ω_{Lz3}	ω_{Hp1}	ω_{Hp2}	ω_{Hz1}	ω_{Hz2}
Calculated	1.959	9.804	4.001E3	0	0	19.608	2.074E7	2.013E8	DNE	DNE
Measured	1.30	6.50	3.80E3	0	0	11.0	1.20E7	7.2E8	6.5E9	1.2E10

Analyzing 2N3904

$g_m = 0.04\text{U}$ $r_\pi = 7.43\text{k}\Omega$ $C_\pi = 25\text{pF}$ $C_\mu = 1.948\text{pF}$

$A_m = -105.3$ $w_{Hp1} = 22.45\text{MHz}$ $w_{Hp2} = 201.3\text{MHz}$ $w_{Lz1} = w_{Lz2} = 0$

$w_{Lz3} = 19.608\text{Hz}$ $w_{Lp1} = 1.932\text{Hz}$ $w_{Lp2} = 9.804\text{Hz}$ $w_{Lp3} = 4.006\text{kHz}$

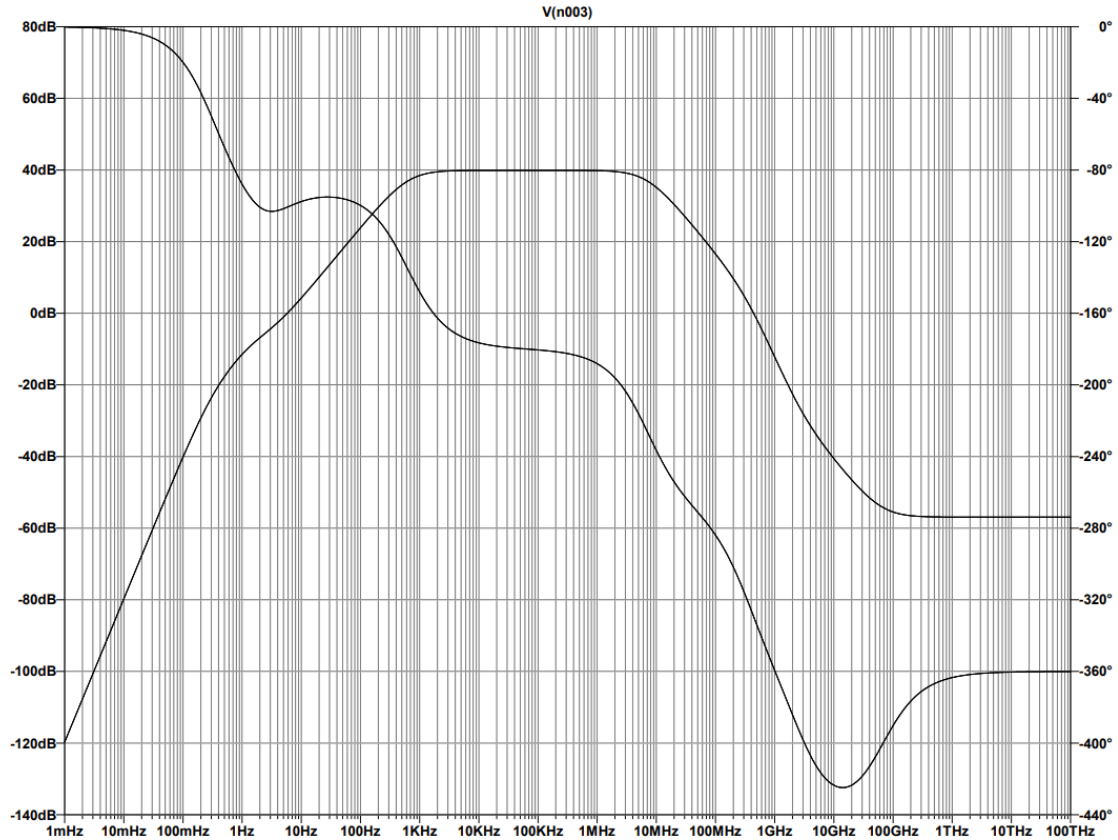


Figure 2.3. 2N3904 CE amplifier bode plot

	w_{Lp1}	w_{Lp2}	w_{Lp3}	w_{Lz1}	w_{Lz2}	w_{Lz3}	w_{Hp1}	w_{Hp2}	w_{Hz1}	w_{Hz2}
Calculated	1.932	9.804	4.006E3	0	0	19.608	2.254E7	2.013E8	DNE	DNE
Measured	1.350	7.890	4.10E3	0	0	16.50	3.4E7	4.2E8	4.3E10	8.9E10

Analyzing 2N4401

$g_m = 0.04\text{U}$ $r_\pi = 3.01\text{k}\Omega$ $C_\pi = 0.6712\text{pF}$ $C_\mu = 5.470\text{pF}$

$A_m = -105.1$ $w_{Hp1} = 22.45\text{MHz}$ $w_{Hp2} = 71.70\text{MHz}$ $w_{Lz1} = w_{Lz2} = 0$

$w_{Lz3} = 19.608\text{Hz}$ $w_{Lp1} = 2.028\text{Hz}$ $w_{Lp2} = 9.804\text{Hz}$ $w_{Lp3} = 3.957\text{kHz}$

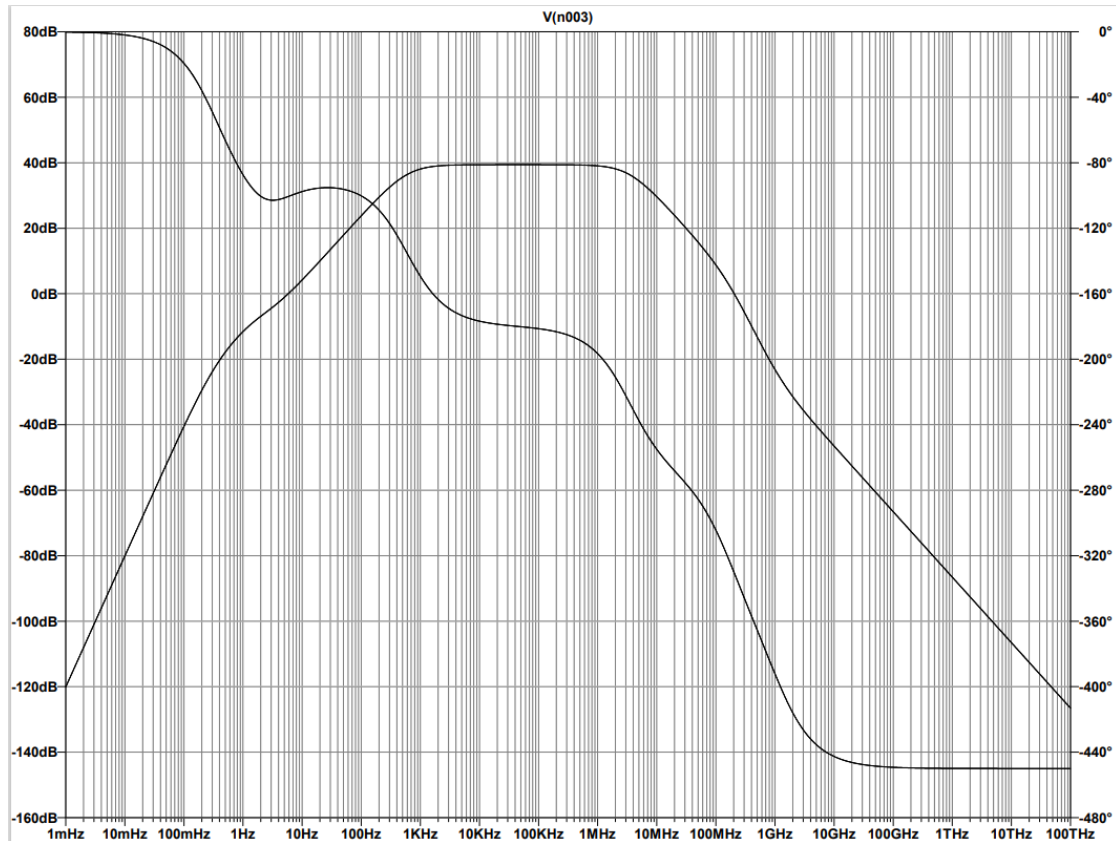


Figure 2.4. 2N4401 CE amplifier bode plot

	W_{Lp1}	W_{Lp2}	W_{Lp3}	W_{Lz1}	W_{Lz2}	W_{Lz3}	W_{Hp1}	W_{Hp2}	W_{Hz1}	W_{Hz2}
Calculated	2.028	9.804	3.957E3	0	0	19.608	2.254E7	7.170E7	DNE	DNE
Measured	1.350	6.890	2.1E3	0	0	16.50	3.4E7	4.2E7	4.3E10	8.9E10

B Change input voltage amplitude until the V_o/V_s trend is no longer linear, set a midband frequency

I observe that from the 2N2222A transistor, my midband occurs from a little less than 10kHz and around 10MHz. I set my focus frequency to 10kHz.

Through my circuit simulation software, I measured the amplitude of the output (V_o) and constantly changed my input (V_s). I plotted the values on Excel and plotted the trend

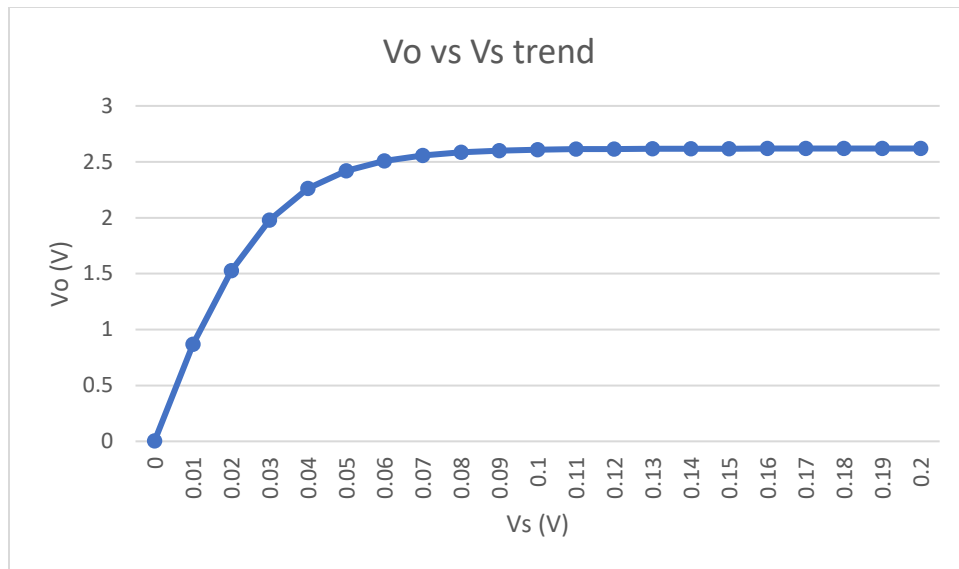
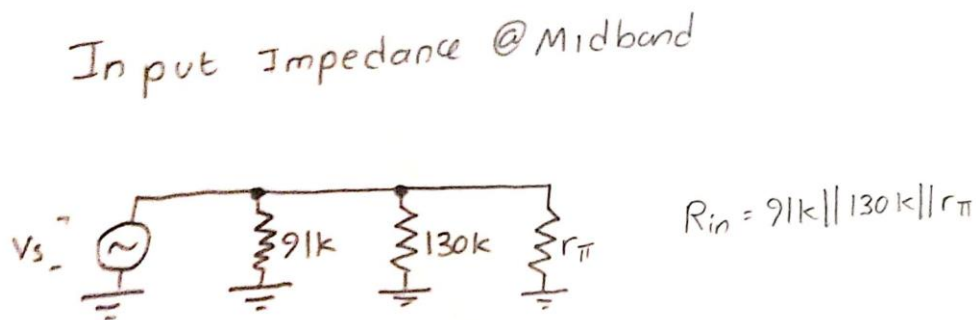


Figure 2.5. Vo vs Vs trend

Looking at the graph, it looks like it stops being linear when $V_s = 15\text{mV}$

C Measuring input impedance, take out 50-ohm resistor

This is how I will calculate input impedance for the circuit at midband.



Scanned with CamScanner

To measure input impedance, I will input $V_s = 15\text{mV}$ (V_{in}), and measure the amplitude of the current going through the V_s (I_{in}). Then through Ampere's Law, $R_{in} = V_{in} / I_{in}$

2N222A

Calculated: $r_{\pi} = 5.26k$ $R_{in} = 4.789k$

Measured: $R_{in} = (15\text{mV}/4.645\text{mA}) - 50 = 6.526\text{k}$

2N3904

Calculated: $r_{\pi} = 7.432\text{k}$ $R_{in} = 6.256\text{k}$

Measured: $R_{in} = (15\text{mV}/1.886\text{mA}) - 50 = 67.903\text{k}$

2N222A

Calculated: $r_{\pi} = 3.04\text{k}$ $R_{in} = 2.853\text{k}$

Measured: $R_{in} = (15\text{mV}/3.665\text{mA}) - 50 = 4.043\text{k}$

D Measuring output impedance, include 50-ohm resistor

I manually set the load resistance to be equal to 5.1k, so the calculated $R_{out} = 5.1\text{k}$

To measure output impedance, I will input $V_s = 15\text{mV}$, and measure V_o (V_o), and measure the amplitude of the current going through the V_o (I_o). Then through Ampere's Law, $R_o = V_o / I_o$

2N222A

Calculated: $R_{out} = 5.1\text{k}$

Measured: $R_{in} = (1.223\text{V}/0.2399\text{mA}) = 5.1\text{k}$

2N3904

Calculated: $R_{out} = 5.1\text{k}$

Measured: $R_{in} = (1.250\text{V}/0.2452\text{mA}) = 5.1\text{k}$

2N222A

Calculated: $R_{out} = 5.1\text{k}$

Measured: $R_{in} = (1.184\text{V}/0.2321\text{mA}) = 5.1\text{k}$

Interestingly, the R_{outs} of each NPN is the same and exactly what my calculated R_{out} is

E Which transistor gives the best performance

For performance, I would choose the 2N3904 transistor. The reason I would choose this is because it has the largest midband frequency range. This indicates that the CE Amplifier will work for a larger range of frequencies, making it a much more versatile amplifier, although the difference in range isn't that great compared to other amplifiers so any of the transistors are viable choices.