

①  $d_f = 2.2 \text{ km}$

$C_{ci, \min} = 1.2 \text{ mg/L}$

$k = -1.23 \frac{1}{\text{hr}}$

$C_{ci, 0} = 5 \text{ mg/L}$

$r = -k C_{ci}$

a)

$$V \frac{dC_{ci}}{dt} = \underbrace{in}_{\cancel{\text{in}}} - \underbrace{out}_{\cancel{\text{out}}} + \underbrace{acc}_{\cancel{\text{acc}}} + \underbrace{deg}_{\cancel{\text{deg}}}$$

$$\cancel{V} \frac{dC_{ci}}{dt} = rV = -kC_{ci} \cancel{V}$$

$$\int_5^{1.2} \frac{dC_{ci}}{C_{ci}} = \int_0^t -k dt$$

$$\ln C_{ci} \Big|_5^{1.2} = -kt \Big|_0^t$$

$$\ln(1.2) - \ln(5) = -1.427 = -kt$$

$$t = \frac{-1.427}{-1.23 \frac{1}{\text{hr}}}$$

$$\boxed{t = 1.16 \text{ hrs}}$$

b)  $A_{\text{pipe}} = \pi(1)^2 = 3.14 \text{ m}^2$

$V_{\text{pipe}} = (3.14 \text{ m}^2)(2200 \text{ m}) = 6911.5 \text{ m}^3$

$v = \left(37 \frac{\text{m}^3}{\text{min}}\right) \left(\frac{1}{3.14 \text{ m}^2}\right) = 11.78 \frac{\text{m}}{\text{min}}$

→ if  $C_{ci}$  takes 1.16 hrs = 69.6 mins to degrade from 5 mg/L to 1.2 mg/L then,

$$d = \left(11.78 \frac{\text{m}}{\text{min}}\right)(69.6 \text{ min}) = 819.88 \text{ m}$$

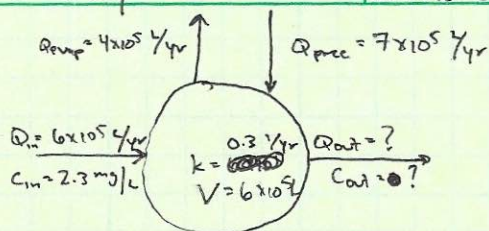
is how far the water travels before needing to be boosted.

$$\# \text{ of booster stations} = \frac{d_f}{d} = \frac{2200 \text{ m}}{819.9 \text{ m}} = 2.68 = 2$$

$$\boxed{\begin{array}{l} d_{\text{booster \#1}} = 819 \text{ m} \\ d_{\text{booster \#2}} = 1638 \text{ m} \end{array}}$$



②

Assumptions

- steady state
- liquid is incompressible
- lake is well mixed

I) find  $Q_{out}$  &  $C_{out}$ 

$$\frac{dV}{dt} = Q_{in} + Q_{prec} - Q_{evap} - Q_{out}$$

$$Q_{out} = Q_{in} + Q_{prec} - Q_{evap}$$

$$= 6 \times 10^5 \frac{L}{yr} + 7 \times 10^5 \frac{L}{yr} - 4 \times 10^5 \frac{L}{yr}$$

$$Q_{out} = 9 \times 10^5 \frac{L}{yr}$$

$$V \frac{dC}{dt} = Q_{in} C_{in} - Q_{out} C_{out} + rV$$

$$r = -\left(0.3 \frac{1}{yr}\right) C_{out}$$

$$= Q_{in} C_{in} - Q_{out} C_{out} - 0.3 \frac{1}{yr} C_{out} V$$

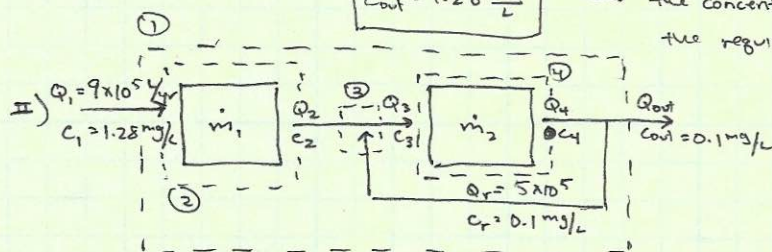
$$= \left(6 \times 10^5 \frac{L}{yr}\right) \left(2.3 \frac{mg}{L}\right) - \left(9 \times 10^5 \frac{L}{yr}\right) C_{out} - \left(0.3 \frac{1}{yr}\right) \left(6 \times 10^5 L\right) C_{out}$$

$$\left(1.08 \times 10^6 \frac{L}{yr}\right) C_{out} = 1.38 \times 10^6 \frac{mg}{yr}$$

$$C_{out} = \frac{\left(1.38 \times 10^6 \frac{mg}{yr}\right)}{\left(1.08 \times 10^6 \frac{L}{yr}\right)}$$

$$C_{out} = 1.28 \frac{mg}{L}$$

→ the concentration is not being lowered to the requisite  $0.1 \frac{mg}{L}$



$$\dot{m}_1 = \frac{1}{2} \dot{m}_2$$

$$C_4 = C_r = C_{out} = 0.1 \frac{mg}{L}$$

Assume: Steady-state, liquid is incompressible

$$MB \#1: \frac{dV}{dt} = Q_1 - Q_{out}$$

$$Q_{out} = 9 \times 10^5 \frac{L}{yr}$$

$$MB \#2: \frac{dV}{dt} = Q_1 - Q_2$$

$$Q_2 = 9 \times 10^5 \frac{L}{yr}$$

$$MB \#3: \frac{dV}{dt} = Q_2 + Q_r - Q_3$$

$$Q_3 = Q_2 + Q_r$$

$$Q_3 = 9 \times 10^5 + 5 \times 10^5 \frac{L}{yr}$$

$$Q_3 = 14 \times 10^5 \frac{L}{yr}$$

$$MB \#4: \frac{dV}{dt} = Q_3 - Q_4 \Rightarrow Q_4 = 14 \times 10^5 \frac{L}{yr}$$

$$V \frac{dC}{dt} = Q_3 C_3 - Q_4 C_4 - \dot{m}_2$$

$$= Q_2 C_2 + Q_r C_r - Q_4 C_4 - 2(Q_1 C_1 - Q_2 C_2)$$

$$= 3Q_2 C_2 + Q_r C_r - Q_4 C_4 - 2Q_1 C_1$$

$$3Q_2 C_2 = Q_4 C_4 + 2Q_1 C_1 - Q_r C_r$$

$$= \left(14 \times 10^5 \frac{L}{yr}\right) \left(0.1 \frac{mg}{L}\right) + 2 \left(9 \times 10^5 \frac{L}{yr}\right) \left(1.28 \frac{mg}{L}\right) - \left(5 \times 10^5 \frac{L}{yr}\right) \left(0.1 \frac{mg}{L}\right)$$

$$C_2 = \frac{\left(2.394 \times 10^6 \frac{mg}{yr}\right)}{3 \left(9 \times 10^5 \frac{L}{yr}\right)}$$

$$C_2 = 0.887 \frac{mg}{L}$$

$$\dot{m}_1 = Q_1 C_1 - Q_2 C_2 = \left(9 \times 10^5 \frac{L}{yr}\right) \left(1.28 \frac{mg}{L}\right) - \left(9 \times 10^5 \frac{L}{yr}\right) \left(0.887 \frac{mg}{L}\right)$$

$$\dot{m}_1 = 3.53 \times 10^5 \frac{mg}{yr}$$

$$\dot{m}_2 = 2 \dot{m}_1 = 2 \left(3.53 \times 10^5 \frac{mg}{yr}\right)$$

$$\dot{m}_2 = 7.07 \times 10^5 \frac{mg}{yr}$$

$$C_3 = \frac{Q_2 C_2 + Q_r C_r}{Q_3}$$

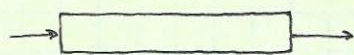
$$= \frac{\left(9 \times 10^5 \frac{L}{yr}\right) \left(0.887 \frac{mg}{L}\right) + \left(5 \times 10^5 \frac{L}{yr}\right) \left(0.1 \frac{mg}{L}\right)}{\left(14 \times 10^5 \frac{L}{yr}\right)}$$

$$C_3 = 0.606 \frac{mg}{L}$$



$$k\tau = 10$$

(13) i)



Plug Flow Reactor

Assume steady-state, no dispersion, constant A

$$V \frac{dc}{dt} = Qc_{in} - Qc_{out} + rV$$

$$r = -kc$$

$$V = A\Delta x$$

$$Qc_{in} - Qc_{out} = Qc_{in} + Q(\Delta c)$$

$$0 = Qc_{in} - Q(c_{in} + \Delta c) - kCA\Delta x$$

$$= -Q\Delta c - kCA\Delta x$$

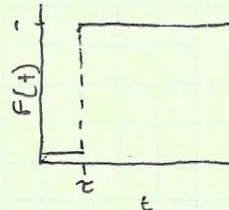
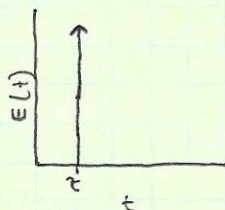
$$\Delta x \rightarrow 0 \quad \Delta x = dx \quad \Delta c = dc$$

$$\int_{c_{in}}^{c_{out}} \frac{1}{c} dc = -k \frac{A}{Q} \int_0^L dx$$

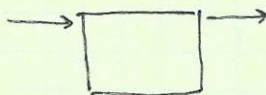
$$\ln \left( \frac{c_{out}}{c_{in}} \right) = -k \frac{AL}{Q} = -k \frac{V}{Q} = -k\tau$$

$$\frac{c_{out}}{c_{in}} = e^{-k\tau}$$

$$\boxed{\frac{c_{out}}{c_{in}} = 4.54 \times 10^{-5}}$$



ii)



CSTR

Assume steady state

$$V \frac{dc}{dt} = Qc_{in} - Qc_{out} + rV$$

$$r = -kc_{out}$$

$$= Q(c_{in} - c_{out}) - kc_{out}V$$

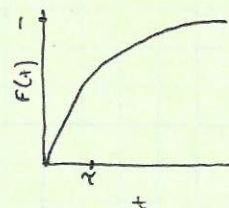
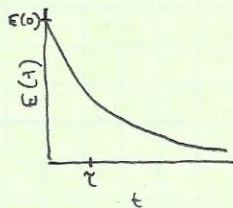
$$k \frac{V}{Q} = k\tau = \frac{(c_{in} - c_{out})}{c_{out}}$$

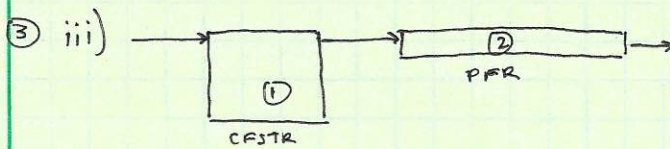
$$k\tau = \frac{c_{in}}{c_{out}} - 1$$

$$\frac{c_{in}}{c_{out}} = 1 + k\tau$$

$$\frac{c_{out}}{c_{in}} = \frac{1}{1 + k\tau} = \frac{1}{1 + 10}$$

$$\boxed{\frac{c_{out}}{c_{in}} = 0.091}$$





using  $\frac{C_{out}}{C_{in}}$  relationships defined in i & ii for PFR and CFSTR respectively:

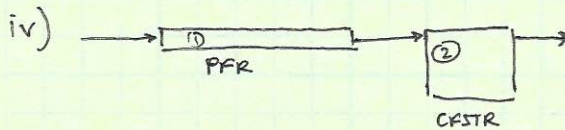
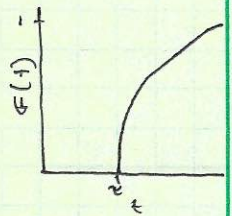
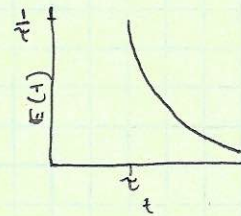
$$C_{out,1} = C_{in,2} \quad C_{out,1} = \frac{C_{in,1}}{1+k\tau}$$

$$C_{out,2} = C_{in,2} e^{-k\tau}$$

$$C_{out} = \frac{C_{in}}{1+k\tau} e^{-k\tau}$$

$$\frac{C_{out}}{C_{in}} = \frac{1}{1+k\tau} e^{-k\tau} = \frac{1}{1+10} e^{-10}$$

$$\boxed{\frac{C_{out}}{C_{in}} = 4.127 \times 10^{-6}}$$



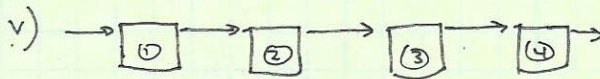
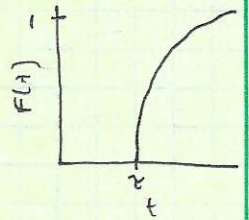
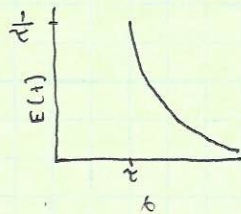
using relationships from i & ii for PFR and CFSTR, respectively:

$$C_{out,1} = C_{in,2} \quad C_{out,1} = C_{in,1} e^{-k\tau} \quad C_{out,2} = \frac{C_{in,2}}{1+k\tau} = \frac{C_{out,1}}{1+k\tau}$$

$$C_{out,2} = \frac{C_{in} e^{-k\tau}}{1+k\tau}$$

$$\frac{C_{out}}{C_{in}} = \frac{e^{-k\tau}}{1+k\tau} = \frac{e^{-10}}{11}$$

$$\boxed{\frac{C_{out}}{C_{in}} = 4.127 \times 10^{-6}}$$



Using eq. from ii for CFSTR:

$$C_{out,1} = C_{in,2} \quad C_{out,2} = C_{in,3} \quad C_{out,3} = C_{in,4}$$

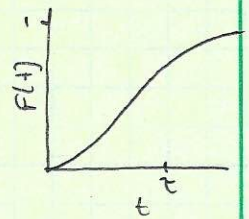
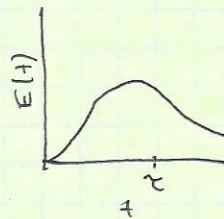
$$C_{out,1} = \frac{C_{in,1}}{1+k\tau} \quad ; \quad C_{out,2} = \frac{C_{in,2}}{1+k\tau} = \frac{C_{out,1}}{1+k\tau} = \frac{C_{in,1}}{(1+k\tau)(1+k\tau)} = \frac{C_{in,1}}{(1+k\tau)^2}$$

$$C_{out,3} = \frac{C_{in,3}}{1+k\tau} = \frac{C_{out,2}}{1+k\tau} = \frac{C_{in,1}}{(1+k\tau)^3}$$

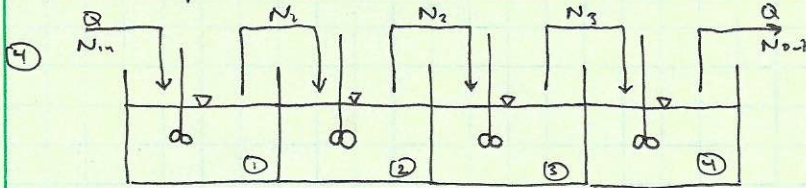
$$C_{out,4} = \frac{C_{in,4}}{1+k\tau} = \frac{C_{out,3}}{1+k\tau} = \frac{C_{in,1}}{(1+k\tau)^4}$$

$$\frac{C_{out}}{C_{in}} = \frac{1}{(1+k\tau)^4} = \frac{1}{11^4}$$

$$\boxed{\frac{C_{out}}{C_{in}} = 6.83 \times 10^{-5}}$$







Assumption:

- steady-state
- $\tau_1 = \tau_2 = \tau_3 = \tau_4$

$$r = -kC^n N$$

$$N_{in} = 105 \text{ organisms/L}$$

$$k = 0.11 \frac{\text{L}^{0.92}}{\text{mg}^{0.92} \cdot \text{min}}$$

$$C = 5 \text{ mg/L}$$

$$n = 0.92$$

$$\tau_{TOT} = 40 \text{ min}$$

$$\tau_i = 40 \text{ min} / 4 = 10 \text{ min}$$

#1:

~~$$V \frac{dN_1}{dt} = QN_{in} - QN_1 + rV$$~~

$$V \frac{dN_1}{dt} = QN_{in} - QN_1 + rV$$

$$= Q(N_{in} - N_1) - kC^n N_1 V$$

$$\frac{V}{Q} = \frac{N_{in} - N_1}{kC^n N_1} = \tau_1$$

$$kC^n \tau_1 = \frac{N_{in}}{N_1} - 1$$

$$\frac{N_1}{N_{in}} = \frac{1}{1 + kC^n \tau_1}$$

$$N_1 = \frac{N_{in}}{1 + kC^n \tau_1} = \frac{(105 \text{ org/L})}{1 + (0.11 \frac{\text{L}^{0.92}}{\text{mg}^{0.92} \cdot \text{min}})(5 \text{ mg/L})^{0.92}(10 \text{ min})} = \frac{(105 \text{ org/L})}{5.117}$$

$$N_1 = 20.52 \text{ organisms/L}$$

#2: using equation derived above substituting  $N_{in}$  with  $N_1$  and  $N_1$  with  $N_2$

$$N_2 = \frac{N_1}{1 + kC^n \tau_2} = \frac{20.52 \text{ org/L}}{5.117}$$

$$N_2 = 4.01 \text{ organisms/L}$$

#3:

$$N_3 = \frac{N_2}{1 + kC^n \tau_3} = \frac{4.01 \text{ org/L}}{5.117}$$

$$N_3 = 0.784 \text{ org/L}$$

#4:

$$N_{out} = \frac{N_3}{1 + kC^n \tau_4} = \frac{0.784 \text{ org/L}}{5.117}$$

$$N_{out} = 0.153 \text{ organisms/L}$$



⑤

Time (min)	$C_A$ (mol/L)
0	167
1	16.1
2	8.5

a) from experimental data what is  $k$ ?

↳ data was plotted as  $C_A$  vs  $t$  (zero-order),  $\ln(C_A)$  vs  $t$  (first-order), and  $\frac{1}{C_A}$  vs  $t$  (second-order) in R, code on next page. The second order was the closest to linearity. Linear model was fit to  $\frac{1}{C_A}$  vs  $t$  to find  $k$  given the second order reaction equation:

$$\frac{1}{C_A} = \frac{1}{C_{A0}} + kt$$

$k$  is given by slope of the line

$$k = 0.0558 \frac{\text{L}}{\text{mol} \cdot \text{min}}$$

b) would a CSTR or PFR be desirable to achieve 99% removal?

↳ can assess this by comparing  $\tau$  required to achieve 99% removal

• Assume steady-state

$$C_{in} = 167 \frac{\text{mol}}{\text{L}}$$

$$\eta = 0.99 = \frac{C_{in} - C_{out}}{C_{in}}$$

$$C_{out} = C_{in} - 0.99(C_{in}) = 167 \frac{\text{mol}}{\text{L}} - 0.99(167 \frac{\text{mol}}{\text{L}})$$

$$C_{out} = 1.67 \frac{\text{mol}}{\text{L}}$$

CSTR:

↳ for second-order rxn:

$$\tau = \frac{1}{k_2 C_{out}} \left( \frac{C_{in}}{C_{out}} - 1 \right) = \frac{1}{(0.0558 \frac{\text{L}}{\text{mol} \cdot \text{min}})(1.67 \frac{\text{mol}}{\text{L}})} \left( \frac{167 \frac{\text{mol}}{\text{L}}}{1.67 \frac{\text{mol}}{\text{L}}} - 1 \right)$$

$$\tau = 1062.39 \text{ min}$$

PFR:

↳ for second-order rxn:

$$\tau = \frac{1}{k_2 C_{in}} \left( \frac{C_{in}}{C_{out}} - 1 \right) = \frac{1}{(0.0558 \frac{\text{L}}{\text{mol} \cdot \text{min}})(167 \frac{\text{mol}}{\text{L}})} \left( \frac{167 \frac{\text{mol}}{\text{L}}}{1.67 \frac{\text{mol}}{\text{L}}} - 1 \right)$$

$$\tau = 10.63 \text{ min}$$

$$\tau_{PFR} \ll \tau_{CSTR}$$

↳ choose to use a PFR to remove compound A

```
#=====
# This script contains work for ENVE 660 Midterm
# Question #5
#
# Tyler Bradley
# 2018-02-09
#=====
```

Reading in required libraries

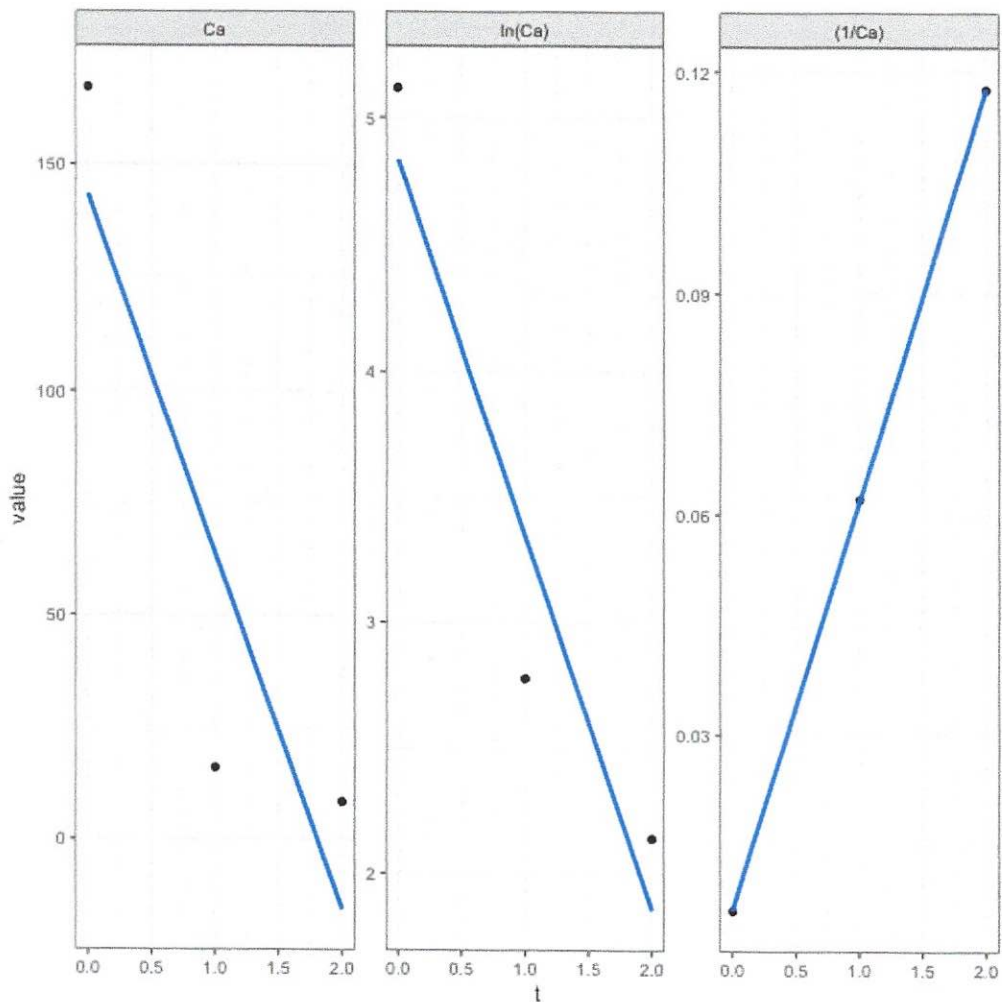
```
library(tidyverse)
```

Writing in experimental data

```
df <-tribble(
  ~t, ~Ca,
  0, 167,
  1, 16.1,
  2, 8.5
)
```

Plotting zero, first, and second order relationships as Ca vs t, ln(Ca) vs t, and (1/Ca) vs t, respectively

```
df %>%
  mutate(
    ln_Ca = log(Ca), # log() function defaults to ln()
    Ca_inv = (1/Ca)
  ) %>%
  gather(key = order, value = value, Ca:Ca_inv) %>%
  mutate(order = factor(order, levels = c("Ca", "ln_Ca", "Ca_inv"),
    labels = c("Ca", "ln(Ca)", "(1/Ca)"))) %>%
  ggplot(aes(t, value)) +
  facet_wrap(~ order, scales = "free") +
  geom_point() +
  geom_smooth(method = "lm", se = FALSE) +
  theme_bw()
```



Linear model fit to  $(1/Ca)$  vs  $t$  since it has the best fit

```
model <- df %>%
  mutate(Ca_inv = 1/Ca) %>%
  lm(Ca_inv ~ t, data = .)
```

getting the model coefficients  $k = 0.0558295$

```
broom::tidy(model)
```

```
##      term      estimate std.error statistic    p.value
## 1 (Intercept) 0.006086111 0.0002193283  27.74886 0.022932275
## 2           t 0.055829517 0.0001698910  328.61962 0.001937248
```



time (s)	Tracer Conc. (g/m <sup>3</sup> )	$t \cdot C(t)$ ( $\frac{g \cdot s}{m^3}$ )	$(t - t_{avg})^2 \cdot C(t)$ ( $\frac{g \cdot s^2}{m^3}$ )
0	0	0	0
100	5	500	<del>100000</del> $2.25 \times 10^5$
200	13	2600	$1.64 \times 10^5$
300	14	4200	$2.12 \times 10^3$
400	8	3200	$6.15 \times 10^4$
500	5	2500	$1.76 \times 10^5$
600	2	1200	$1.66 \times 10^5$
700	1	700	$1.50 \times 10^5$
800	0	0	0

$$t_{avg} = \frac{\int_0^{\infty} t \cdot C(t) dt}{\int_0^{\infty} C(t) dt}$$

using Simpson's Rule:

$$\int_a^b C(t) dt = \frac{h}{3} [f(a) + 4 \cdot f(\frac{a+b}{2}) + f(b)] \quad h = \frac{b-a}{2}$$

applying it every three data points ( $h = 100$ )

$$\int_0^{\infty} C(t) dt = \frac{100}{3} (0 + 4(5) + 13) + \frac{100}{3} (13 + 4(14) + 8) + \frac{100}{3} (8 + 4(5) + 2) + \frac{100}{3} (2 + 4(1) + 0)$$

$$= 4866.67 \text{ g/m}^3$$

$$\int_0^{\infty} t \cdot C(t) dt = \frac{100}{3} (0 + 4(500) + 2600) + \frac{100}{3} (2600 + 4(4200) + 3200) + \frac{100}{3} (3200 + 4(2500) + 1200) + \frac{100}{3} (1200 + 4(700) + 0)$$

$$= 1.52 \times 10^6 \frac{g \cdot s}{m^3}$$

$$t_{avg} = \frac{1.52 \times 10^6 \frac{g \cdot s}{m^3}}{4866.67 \frac{g}{m^3}}$$

$$t_{avg} = 312.3 \text{ s}$$

$$\sigma^2 = \frac{\int_0^{\infty} (t - t_{avg})^2 \cdot C(t) dt}{\int_0^{\infty} C(t) dt}$$

$$\int_0^{\infty} (t - t_{avg})^2 \cdot C(t) dt = \frac{100}{3} (0 + 4(2.25 \times 10^5) + 1.64 \times 10^5) + \frac{100}{3} (1.64 \times 10^5 + 4(2.12 \times 10^3) + 6.15 \times 10^4) +$$

$$\frac{100}{3} (6.15 \times 10^4 + 4(1.76 \times 10^5) + 1.66 \times 10^5) + \frac{100}{3} (1.66 \times 10^5 + 4(1.5 \times 10^5) + 0)$$

$$= 9.98 \times 10^7 \frac{g \cdot s^2}{m^3}$$

$$\sigma^2 = \frac{9.98 \times 10^7 \frac{g \cdot s^2}{m^3}}{4866.67 \frac{g}{m^3}} = 20517 \text{ s}^2$$

$$\sigma = 143 \text{ s}$$

\* why is this question worth 8 points?  
 ↳ your dog is 8 years old

