

APPENDIX

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”Intelligent Locomotion Planning with Enhanced Postural Stability
for Lower-Limb Exoskeletons”

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1 Inertia matrix and gravity vector values:

The elements of inertia matrix M are

$$\begin{aligned}
M_{11} &= m_1 l_{c1}^2 + m_2 (l_1 + l_{c2})^2 + m_3 (l_1 + l_{c3})^2 + \\
&\quad m_4 (l_1 + l_3 + l_{c4})^2 + I_1 + I_2 + I_3 + I_4 \\
M_{12} &= m_2 l_{c2} (l_1 + l_{c2}) + m_3 l_{c3} (l_1 + l_{c3}) + \\
&\quad m_4 (l_3 + l_{c4}) (l_1 + l_3 + l_{c4}) + I_2 + I_3 + I_4 \\
M_{13} &= m_3 l_{c3} (l_1 + l_{c3}) + m_4 (l_3 + l_{c4}) (l_1 + l_3 + l_{c4}) + \\
&\quad I_3 + I_4 \\
M_{14} &= m_4 l_{c4} (l_1 + l_3 + l_{c4}) + I_4 \\
M_{22} &= m_2 l_{c2}^2 + m_3 l_{c3}^2 + m_4 (l_3 + l_{c4})^2 + I_2 + I_3 + I_4 \\
M_{23} &= m_3 l_{c3}^2 + m_4 (l_3 + l_{c4})^2 + I_3 + I_4 \\
M_{24} &= m_4 l_{c4} (l_3 + l_{c4}) + I_4 \\
M_{33} &= m_3 l_{c3}^2 + m_4 (l_3 + l_{c4})^2 + I_3 + I_4 \\
M_{34} &= m_4 l_{c4} (l_3 + l_{c4}) + I_4 \\
M_{44} &= m_4 l_{c4}^2 + I_4
\end{aligned} \tag{A1}$$

and the elements of gravity matrix G are obtained as

$$\begin{aligned}
G_{11} &= 3m_1 g l_1 + m_1 g l_{c1} \\
G_{12} &= G_{22} = m_2 g l_{c2} \\
G_{13} &= G_{23} = G_{33} = -m_3 g l_3 - m_3 g l_{c3} \\
G_{14} &= G_{24} = G_{34} = G_{44} = -m_4 g l_{c4}
\end{aligned} \tag{A2}$$

in which g is the gravitational acceleration.

2 DCM definition

The motion of HES center of mass can be divided into the convergent (C) and divergent (D) components as

$$\begin{aligned} C &= x_{CoM} - \frac{\dot{x}_{CoM}}{\sqrt{\alpha}} \\ D &= x_{CoM} + \frac{\dot{x}_{CoM}}{\sqrt{\alpha}} \end{aligned} \tag{A3}$$

where x_{CoM} and \dot{x}_{CoM} denote the position and velocity of the center of mass and α is a constant value defined in (8). Taking the time derivative of (A3) and substituting (7) in the absence of control input ($\tau=0$), the time derivative of the divergent and convergent parts are obtained as

$$\begin{aligned} \dot{C} &= -\sqrt{\alpha}C \\ \dot{D} &= \sqrt{\alpha}D \end{aligned} \tag{A4}$$

As seen, the convergent part of the motion (C) will converge to zero without any control effort. Therefore, controlling the divergent part of the motion (D) will guarantee the convergence of x_{CoM} to its corresponding desired value. Accordingly, the DCM is defined as

$$\zeta = x_{CoM} + \frac{\dot{x}_{CoM}}{\sqrt{\alpha}} \tag{A5}$$

and the paper is focused on the control of the DCM by adjusting the control input (τ in (7)).