

# Ve215 Electric Circuits

Author: Sung-Liang Chen

Presenter : Mohamed Atef

Fall 2016

# Chapter 7

## First-Order Circuits

## 7.1 Introduction

- In this chapter, we examine two types of simple circuits: a circuit comprising a resistor and a capacitor and a circuit comprising a resistor and an inductor. These are called *RC* and *RL* circuits, respectively.

- $RC$  and  $RL$  circuits are characterized by first-order differential equations. Hence, the circuits are collectively called *first-order* circuits.
- There are two ways to excite the circuits. The first way is by energy initially stored in the capacitive or inductive element. The second way is by independent sources.

## 7.2 The Source-Free $RC$ Circuit

- A source-free  $RC$  circuit occurs when its dc source is suddenly disconnected. The energy already stored in the capacitor is released to the resistor.

Consider the circuit in Fig. 7.1. The capacitor is initially charged, we assume that at time  $t = 0$ , the initial voltage is

$$v(0) = V_0$$

with the corresponding value of energy stored as

$$w_C(0) = \frac{1}{2} C V_0^2$$

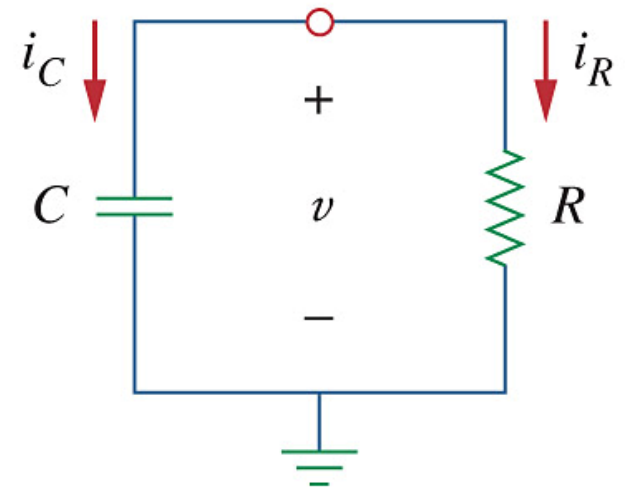


Figure 7.1 A source-free  $RC$  circuit.

Our objective is to determine the circuit response, say, the capacitor voltage  $v$ .

$$i_C + i_R = 0$$

$$i_C = C \frac{dv}{dt}, i_R = \frac{v}{R}$$

$$C \frac{dv}{dt} + \frac{v}{R} = 0$$

or

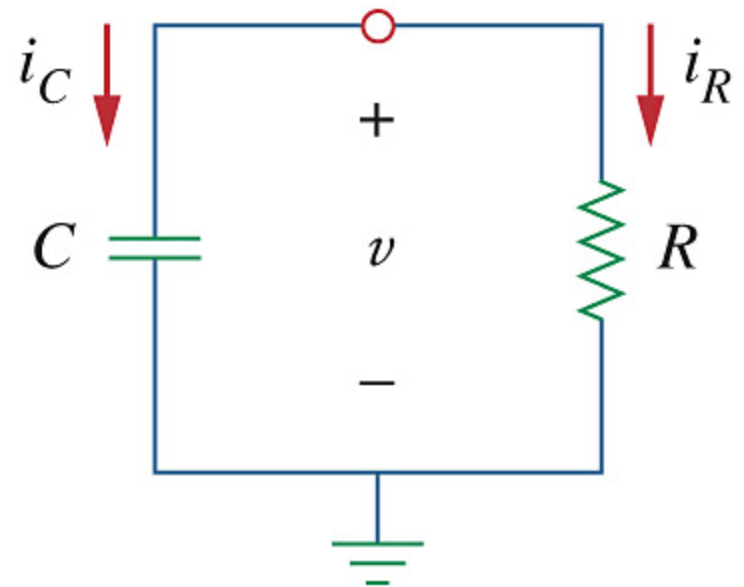


Figure 7.1 A source-free  $RC$  circuit.

$$\frac{dv}{dt} + \frac{v}{RC} = 0$$

This is a first-order differential equation.

$$r + \frac{1}{RC} = 0$$

$$r = -\frac{1}{RC}$$

$$v = Ae^{rt} = Ae^{-\frac{t}{RC}}$$

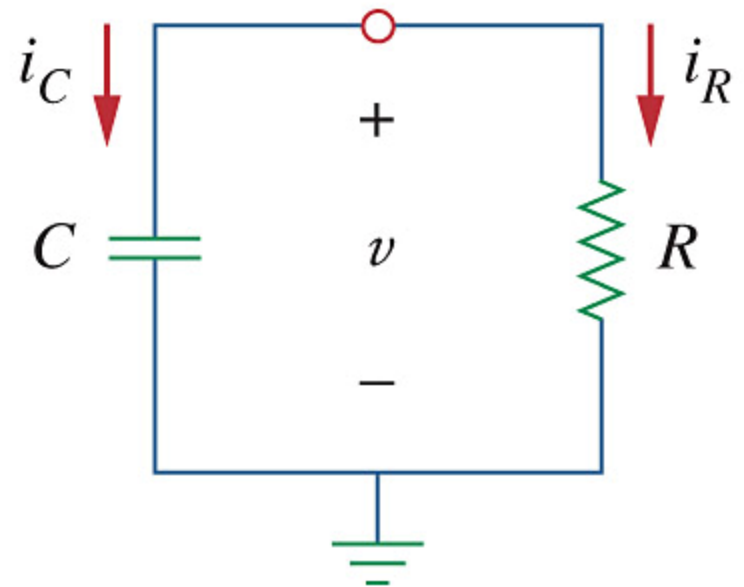


Figure 7.1 A source-free  $RC$  circuit.



$$v(0) = A = V_0$$

$$v = V_0 e^{-\frac{t}{RC}}$$

Since the response is due to  $V_0$  (i.e., the *initial state* of the circuit) and not due to some external voltage or current source (i.e., the input to the circuit), it is called the zero - input response of the circuit.

= source free

The response of the source-free  $RC$  circuit is illustrated in Fig. 7.2. Note that at  $t = 0$ ,  $v = V_0$ . As  $t$  increases,  $v$  decreases toward zero. The rapidity with which  $v$  decreases is expressed in terms of the *time constant*, denoted by  $\tau$ .

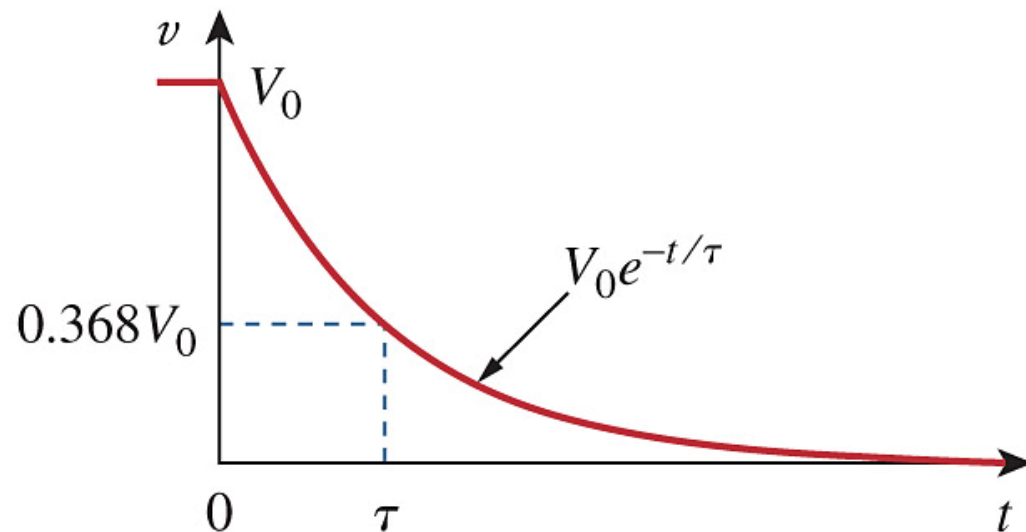


Figure 7.2 The voltage response of the source-free  $RC$  circuit.

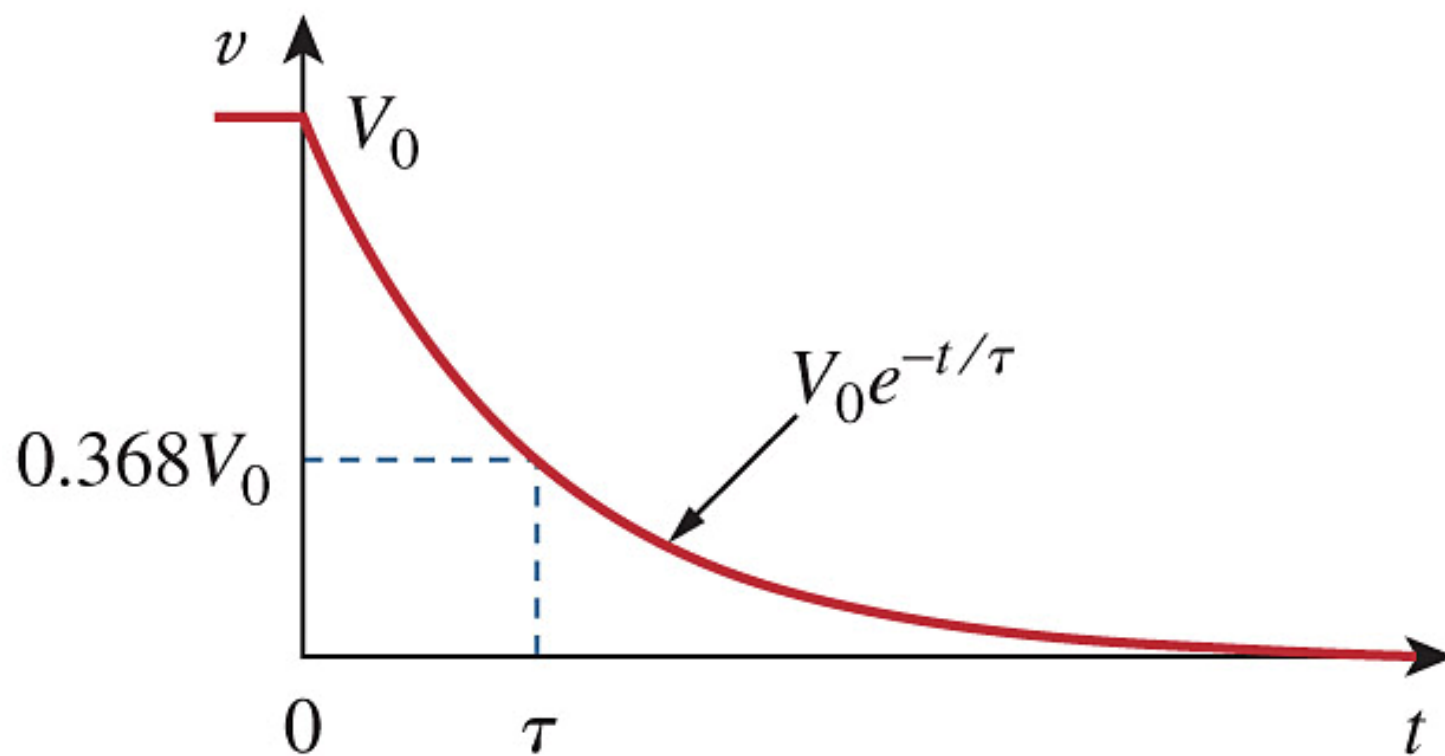


Figure 7.2 The voltage response of the source-free  $RC$  circuit.

The *time constant* of a circuit is the time required for the response to decay to a factor of  $1/e$  or 36.8 % of its initial value.

This implies that at  $t = \tau$ ,

$$v = V_0 e^{-\frac{\tau}{RC}} = V_0 e^{-1}$$

or

$$\tau = RC$$

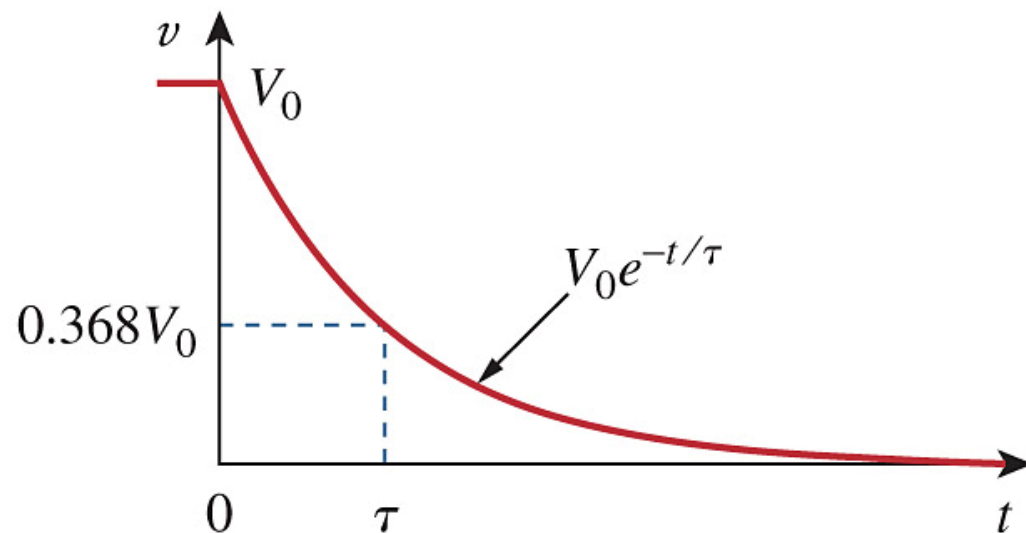
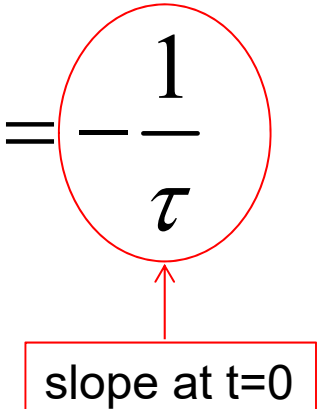


Figure 7.2 The voltage response of the source-free  $RC$  circuit.

In terms of the time constant,

$$v = V_0 e^{-t/\tau}$$

The time constant may be viewed from another perspective. Evaluating the derivative of  $v / V_0$  at  $t = 0$ , we obtain

$$\left. \frac{d}{dt} \left( \frac{v}{V_0} \right) \right|_{t=0} = -\frac{1}{\tau} e^{-t/\tau} \bigg|_{t=0} = -\frac{1}{\tau}$$


slope at  $t=0$

Thus, the time constant is the initial rate of decay. To find  $\tau$  from the response curve, draw the tangent to the curve at  $t = 0$ , as shown in Fig. 7.3. The tangent intercepts with the time axis at  $t = \tau$ .

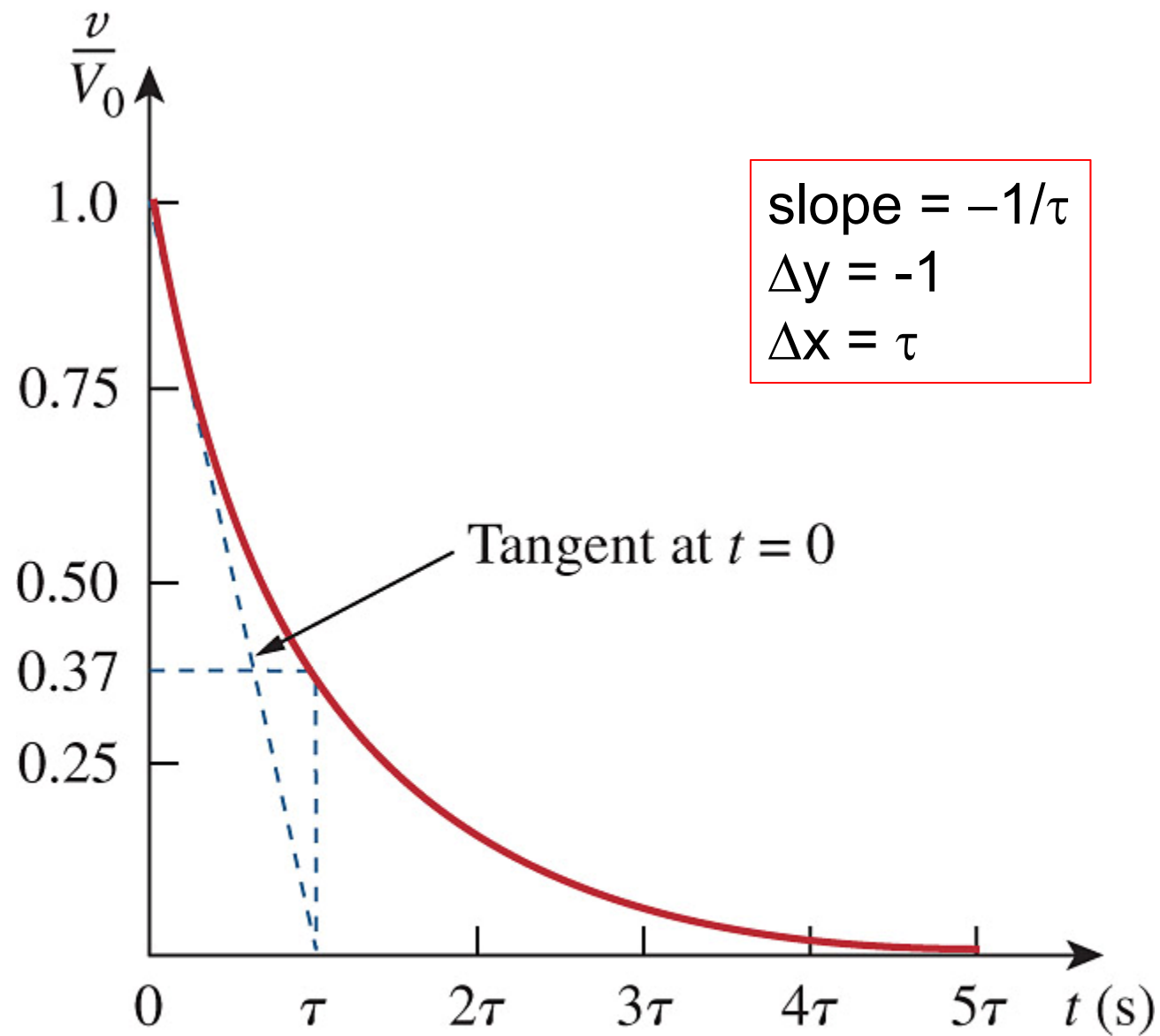


Figure 7.3 Graphical determination of the time constant from the response curve.

Five values of  $v / V_0 = e^{-t/\tau}$  are shown in Table 7.1. It is evident from Table 7.1 that  $v$  is less than 1% of  $V_0$  after  $5\tau$ . Thus, it is customary to assume that the capacitor is fully discharged after five time constants.



**TABLE 7.1** Values of  $v / V_0 = e^{-t/\tau}$

$t$	$\tau$	$2\tau$	$3\tau$	$4\tau$	$5\tau$
$v / V_0$	0.36788	0.13534	0.04979	0.01832	0.00674

In other words, it takes  $5\tau$  for the circuit to reach its *final state* or *steady state* when no changes take place with time.

The smaller the time constant, the more rapidly the voltage decreases, that is, the faster the response. This is illustrated in Fig. 7.4. A circuit with a small time constant gives a fast response in that it reaches the steady state quickly due to quick dissipation of energy stored.

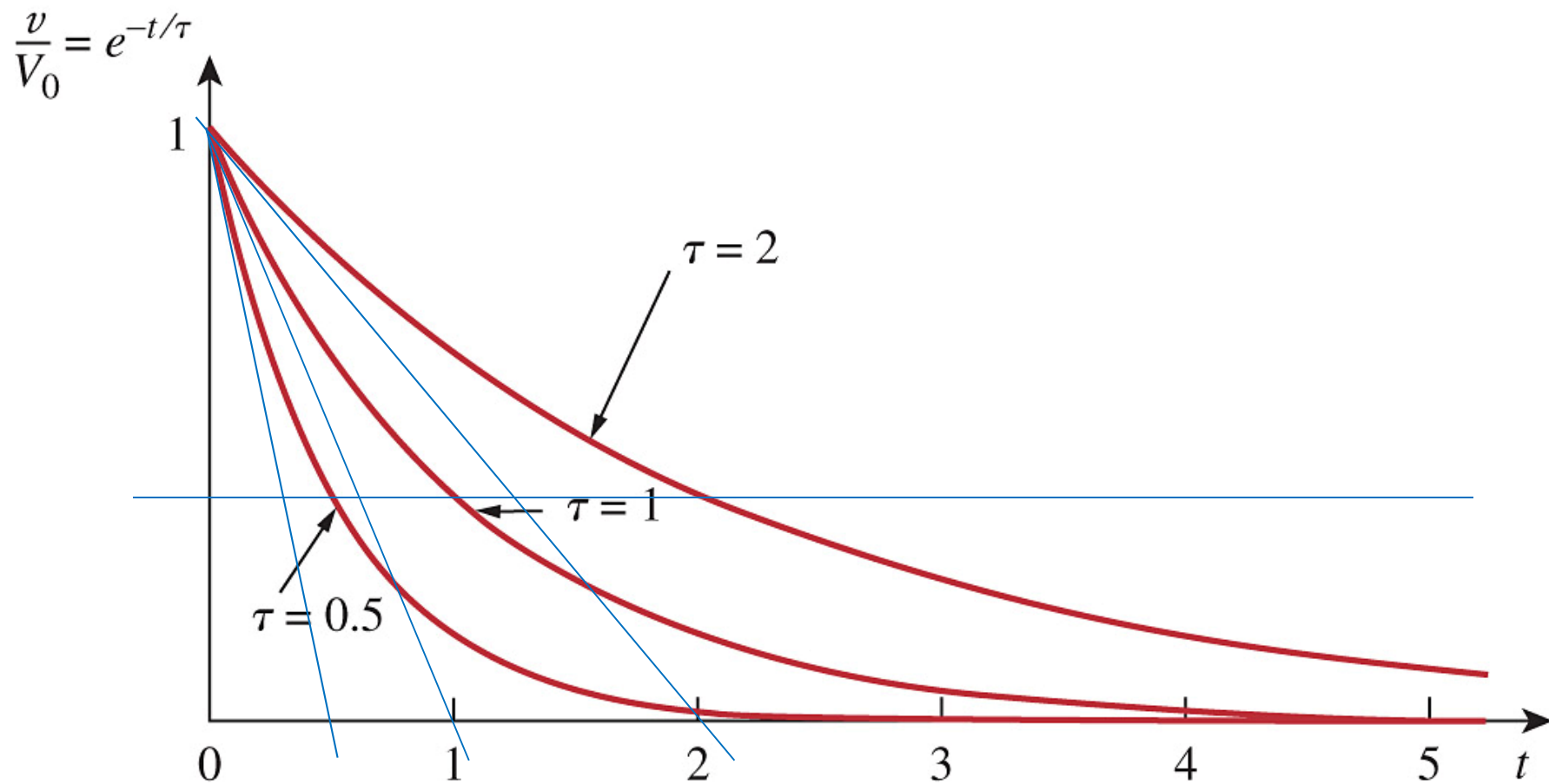


Figure 7.4 Plot of  $v/V_0$  for various values of the time constant.

With the voltage  $v = V_0 e^{-t/\tau}$ , we can find the resistor current

$$i_R = \frac{v}{R} = \frac{V_0}{R} e^{-t/\tau}$$

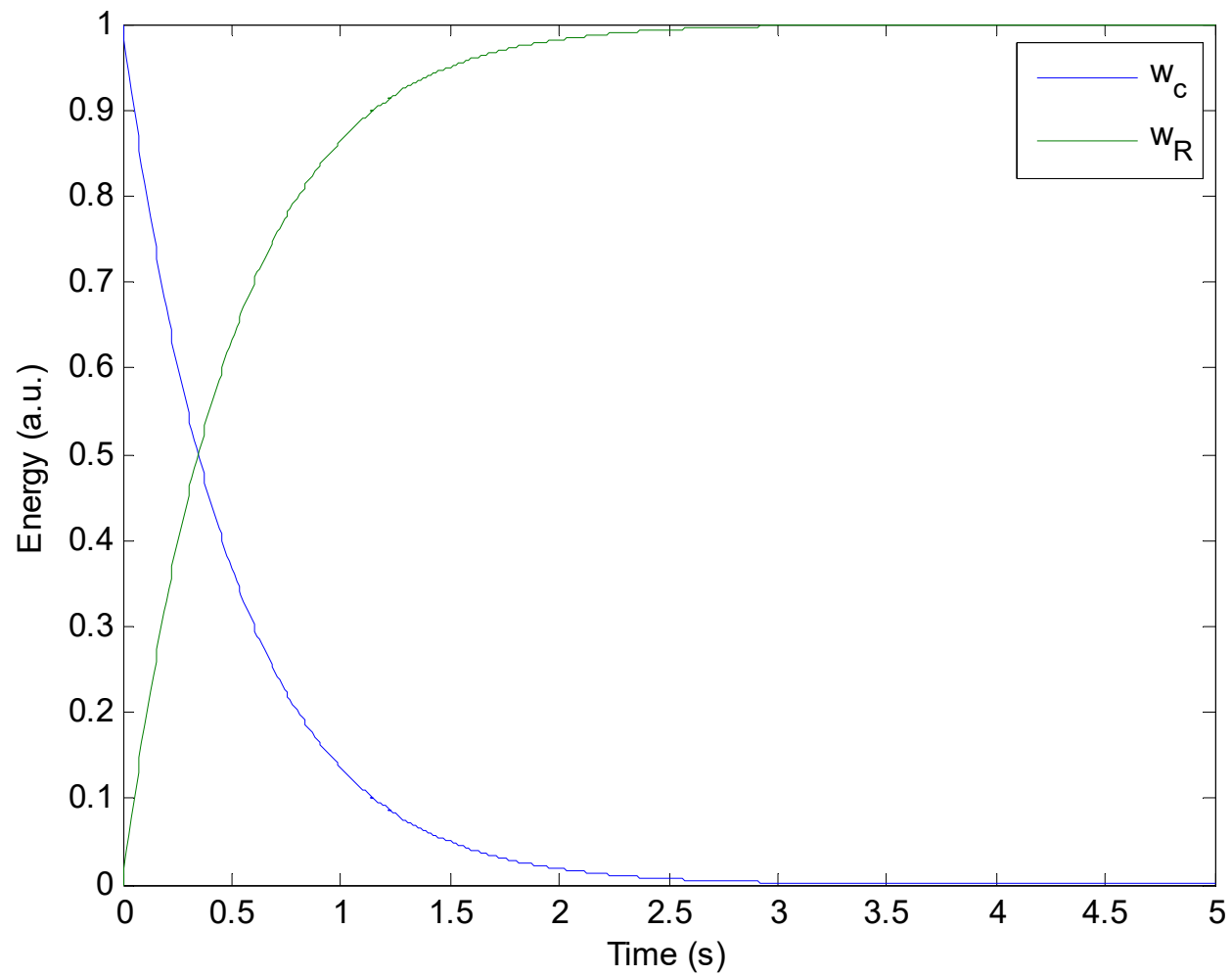
The power dissipated in the resistor is

$$p = v i_R = \frac{V_0^2}{R} e^{-2t/\tau}$$

The energy absorbed by the resistor up to time  $t$  is

$$w_R = \int_0^t \left( \frac{V_0^2}{R} e^{-2t/\tau} \right) dt = \frac{V_0^2}{R} \frac{e^{-2t/\tau}}{-2/\tau} \Big|_0^t$$
$$= \frac{1}{2} C V_0^2 (1 - e^{-2t/\tau})$$

Notice that as  $t \rightarrow \infty$ ,  $w_R \rightarrow \frac{1}{2} C V_0^2 = w_C(0)$ , the energy initially stored in the capacitor.



$\tau = 1\text{s}$

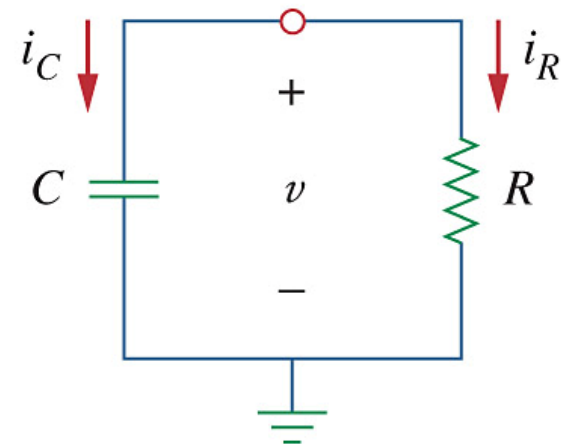


Figure 7.1 A source-free  
 $RC$  circuit.

In summary, the key to working with a source-free  $RC$  circuit is to find

1. The initial voltage  $v(0) = V_0$  across the capacitor.

2. The time constant  $\tau = RC$ , where  $R$  is often the equivalent resistance at the terminals of  $C$ .

With these two items, we obtain the response as the capacitor voltage  $v_C = v = v(0)e^{-t/\tau}$ . Once  $v_C$  is first obtained, other variables  $(i_C, v_R, i_R)$  can be obtained.



**Practice Problem 7.1** Refer to the circuit in Fig. 7.7. Let  $v_C(0) = 45$  V. Determine  $v_C$ ,  $v_x$ , and  $i_o$  for  $t \geq 0$ .

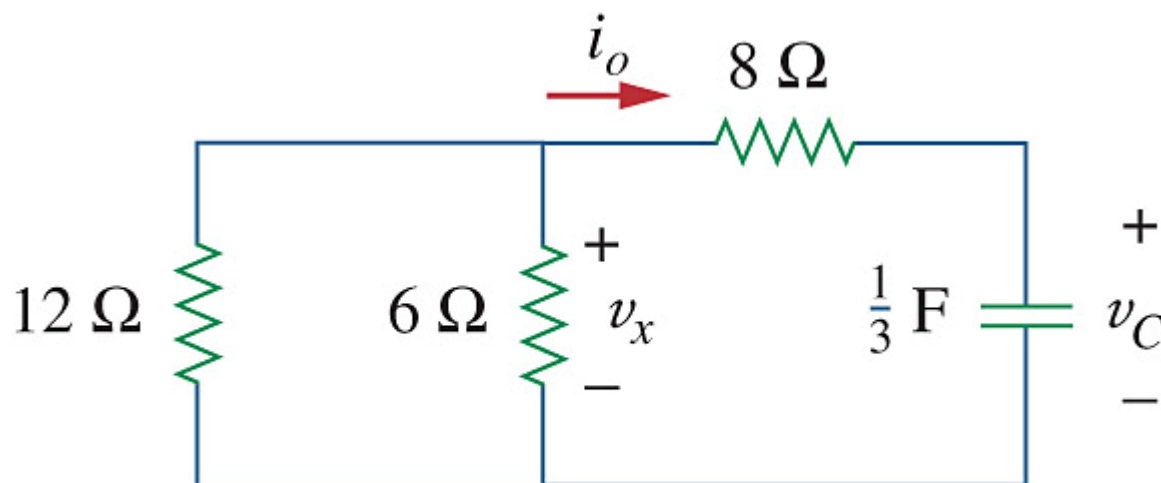


Figure 7.7 An  $RC$  circuit.

## Solution :

The equivalent resistance seen at the terminals of the capacitor is

$$R_{eq} = 8 + 12 \parallel 6 = 12 \text{ } (\Omega)$$

The time constant is

$$\tau = R_{eq} C = 12 \times \frac{1}{3} = 4 \text{ (s)}$$

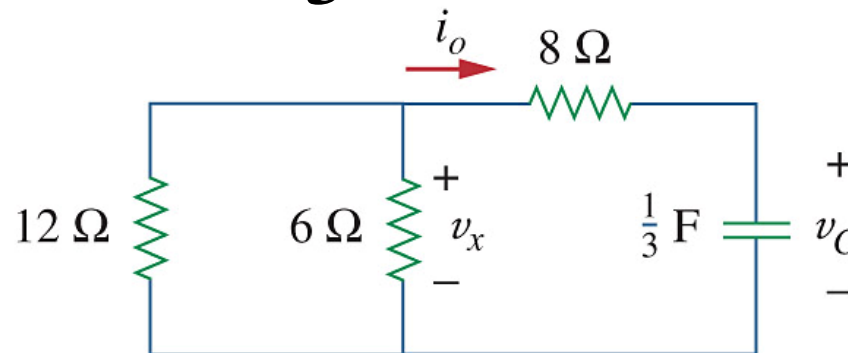


Figure 7.7 An  $RC$  circuit.

The capacitor voltage is

$$v_C = v_C(0)e^{-t/\tau} = 45e^{-t/4} = 45e^{-0.25t} \text{ (V)}$$

$$i_o = C \frac{dv_C}{dt} = \frac{1}{3} \times \frac{d}{dt} (45e^{-0.25t})$$

$$= 15 \times (-0.25e^{-t/4}) = -3.75e^{-t/4} \text{ (A)}$$

$$v_x = 8i_o + v_C = 8 \times (-3.75e^{-0.25t}) + 45e^{-0.25t}$$

$$= 15e^{-0.25t} \text{ (V)}$$

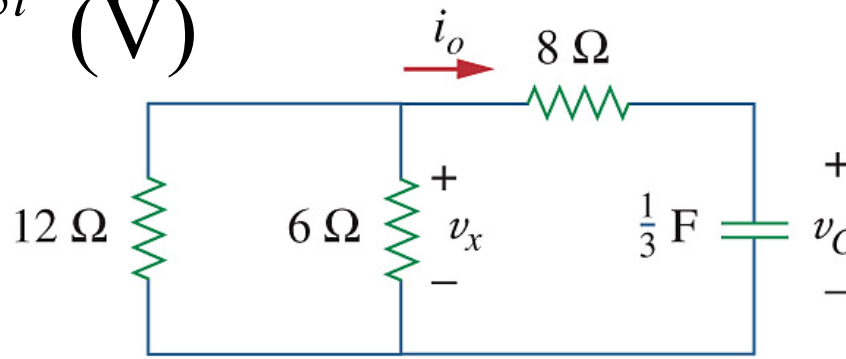


Figure 7.7 An  $RC$  circuit.

**Practice Problem 7.12** If the switch in Fig. 7.10 opens at  $t = 0$ , find  $v(t)$  for  $t \geq 0$  and  $w_C(0)$ .

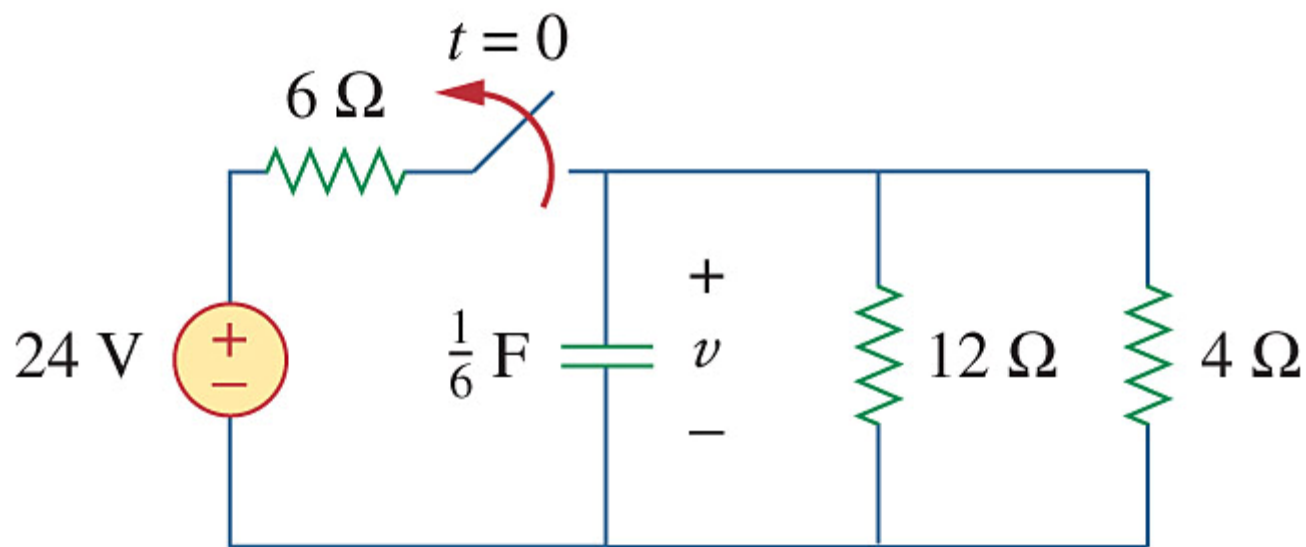


Figure 7.10

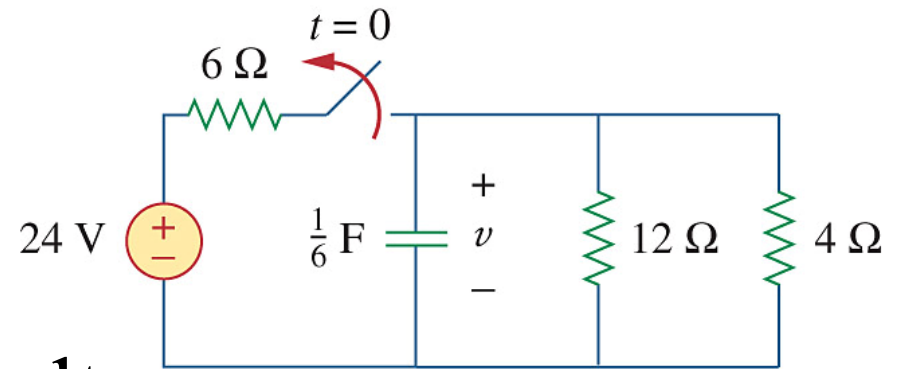


Figure 7.10

**Solution :**

When  $t \leq 0$ , the capacitor voltage

$$v(t) = 24 \times \frac{12 \parallel 4}{6 + 12 \parallel 4} = 8 \text{ (V)}$$

Hence,  $v(0) = 8 \text{ V}$ .

When  $t \geq 0$ , the circuit becomes a source-free  $RC$  circuit with

$$\tau = R_{eq} C = (12 \parallel 4) \times \frac{1}{6} = \frac{1}{2} \text{ (s)}$$

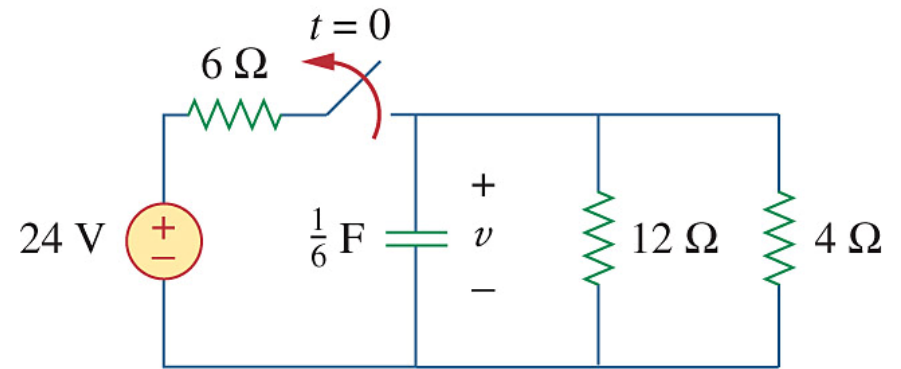


Figure 7.10

Therefore,

$$v(t) = v(0)e^{-t/\tau} = 8e^{-t/(1/2)} = 8e^{-2t} \text{ (V)}$$

$$w_C(0) = \frac{1}{2} C (v(0))^2 = \frac{1}{2} \times \frac{1}{6} \times 8^2$$

$$= \frac{16}{3} \approx 5.33 \text{ (J)}$$

## 7.3 The Source-Free $RL$ Circuit

Consider the circuit in Fig. 7.11. Our goal is to determine the circuit response, which we assume to be the current  $i$  through the inductor. The inductor has an initial current

$$i(0) = I_0$$

with the corresponding energy

$$w_L(0) = \frac{1}{2} L I_0^2$$

$$v_L + v_R = 0$$

$$v_L = L \frac{di}{dt}, v_R = iR$$

$$L \frac{di}{dt} + iR = 0$$

or

$$\frac{di}{dt} + \frac{R}{L} i = 0$$

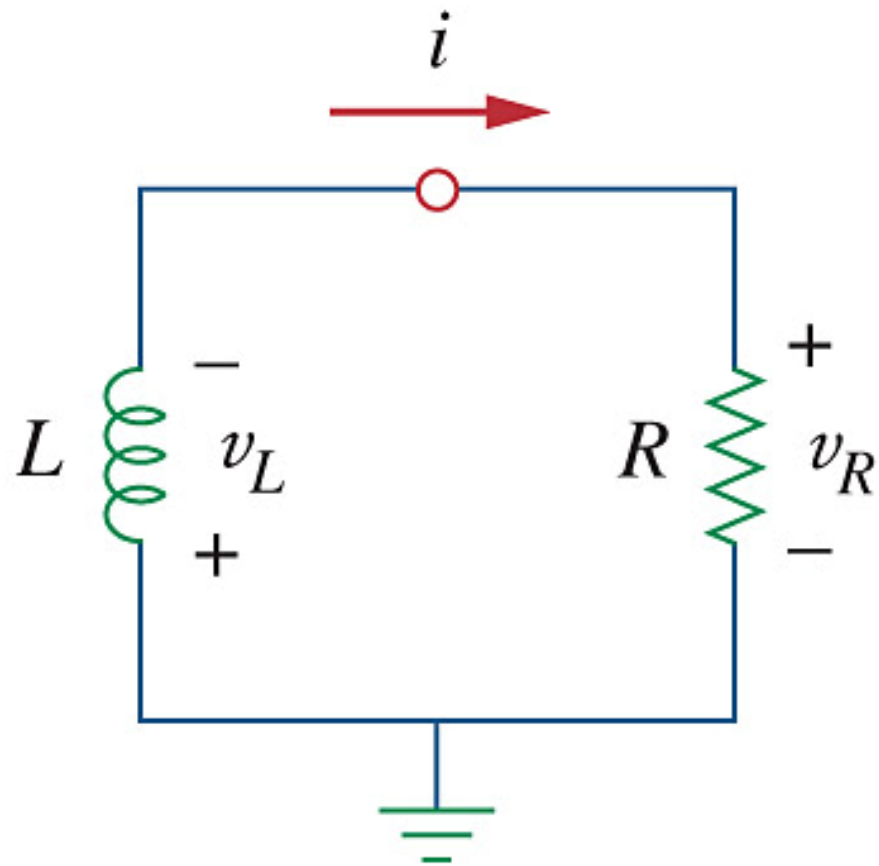


Figure 7.11 A source-free  $RL$  circuit.



$$r + \frac{R}{L} = 0$$

$$r = -\frac{R}{L}$$

$$i = Be^{rt} = Be^{-\frac{R}{L}t} = Be^{-\frac{t}{(L/R)}}$$

$$i(0) = B = I_0$$

$$i = I_0 e^{-\frac{t}{(L/R)}}$$

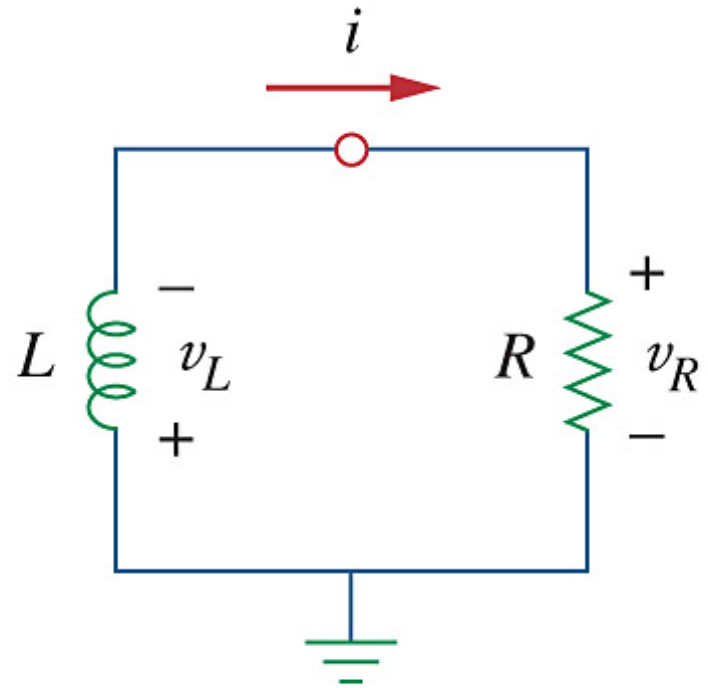


Figure 7.11 A source-free  $RL$  circuit.

Let  $\tau = L / R$ , we have

$$i = I_0 e^{-t/\tau}$$

The current response is shown in Fig. 7.12.

Since the response is due only to  $I_0$  (i.e., the initial state of the circuit), it is called the zero-input response of the circuit.

= source free

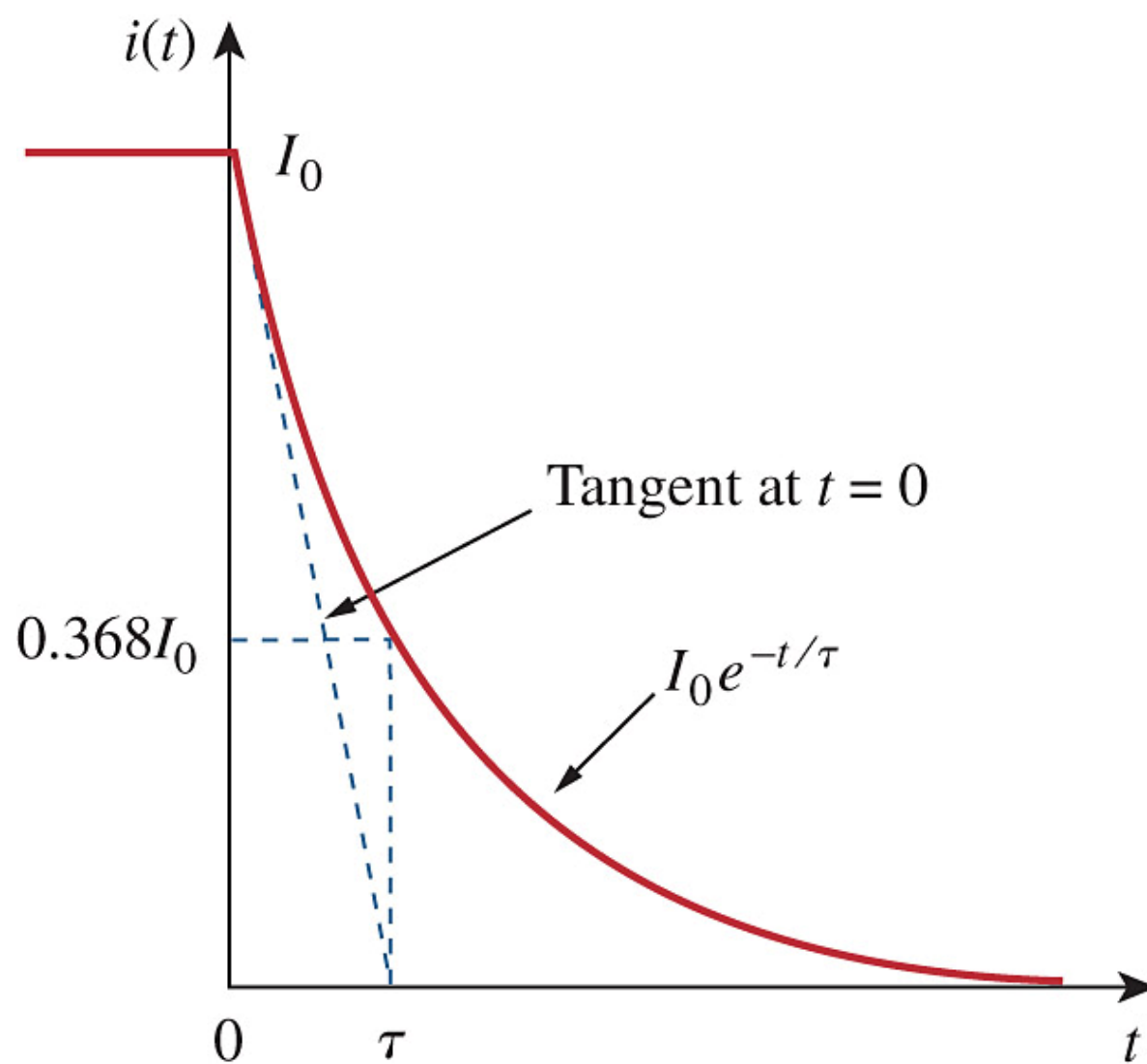


Figure 7.12 The current response of the source-free  $RL$  circuit.

With the current  $i = I_0 e^{-t/\tau}$ , we can find the resistor voltage

$$v_R = iR = I_0 R e^{-t/\tau}$$

The power dissipated in the resistor is

$$p = v_R i = I_0^2 R e^{-2t/\tau}$$

The energy absorbed by the resistor up to time  $t$  is

$$w_R = \int_0^t \left( I_0^2 R e^{-2t/\tau} \right) dt = I_0^2 R \frac{e^{-2t/\tau}}{-2/\tau} \Big|_0^t$$
$$= \frac{1}{2} L I_0^2 \left( 1 - e^{-2t/\tau} \right)$$

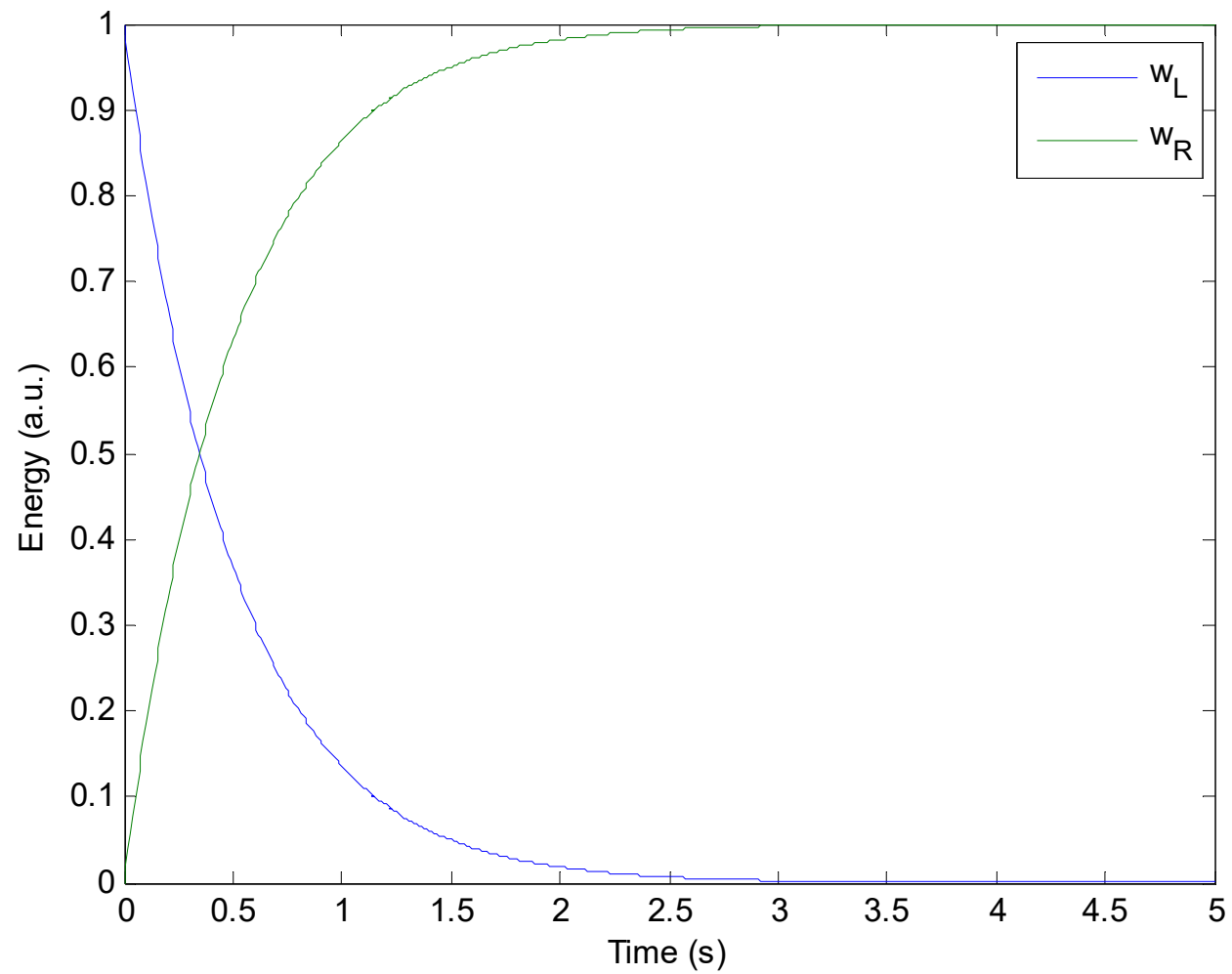
Notice that as  $t \rightarrow \infty$ ,  $w_R \rightarrow \frac{1}{2} L I_0^2 = w_L(0)$ , the energy initially stored in the inductor.

The key to working with a source-free  $RL$  circuit is to find

1. The initial current  $i(0) = I_0$  through the inductor.

2. The time constant  $\tau = L / R$ , where  $R$  is often the equivalent resistance at the terminals of  $L$ .

With the two items, we obtain the response as the inductor current  $i_L = i = i(0)e^{-t/\tau}$ . Once  $i_L$  is first obtained, other variables ( $v_L, v_R, i_R$ ) can be obtained.



$\tau = 1\text{s}$

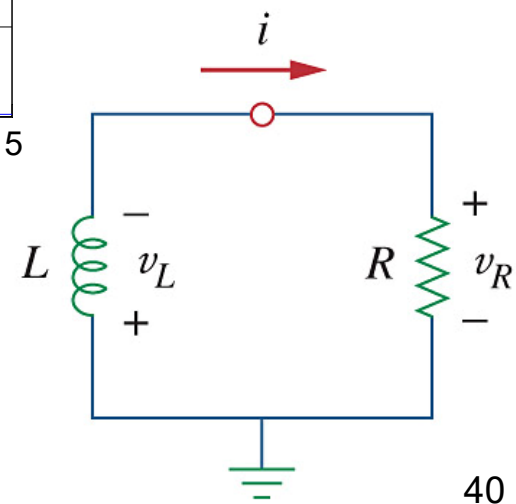


Figure 7.11 A source-free  $RL$  circuit.



**Practice Problem 7.4** For the circuit in Fig. 7.18, find  $i(t)$  for  $t > 0$ .

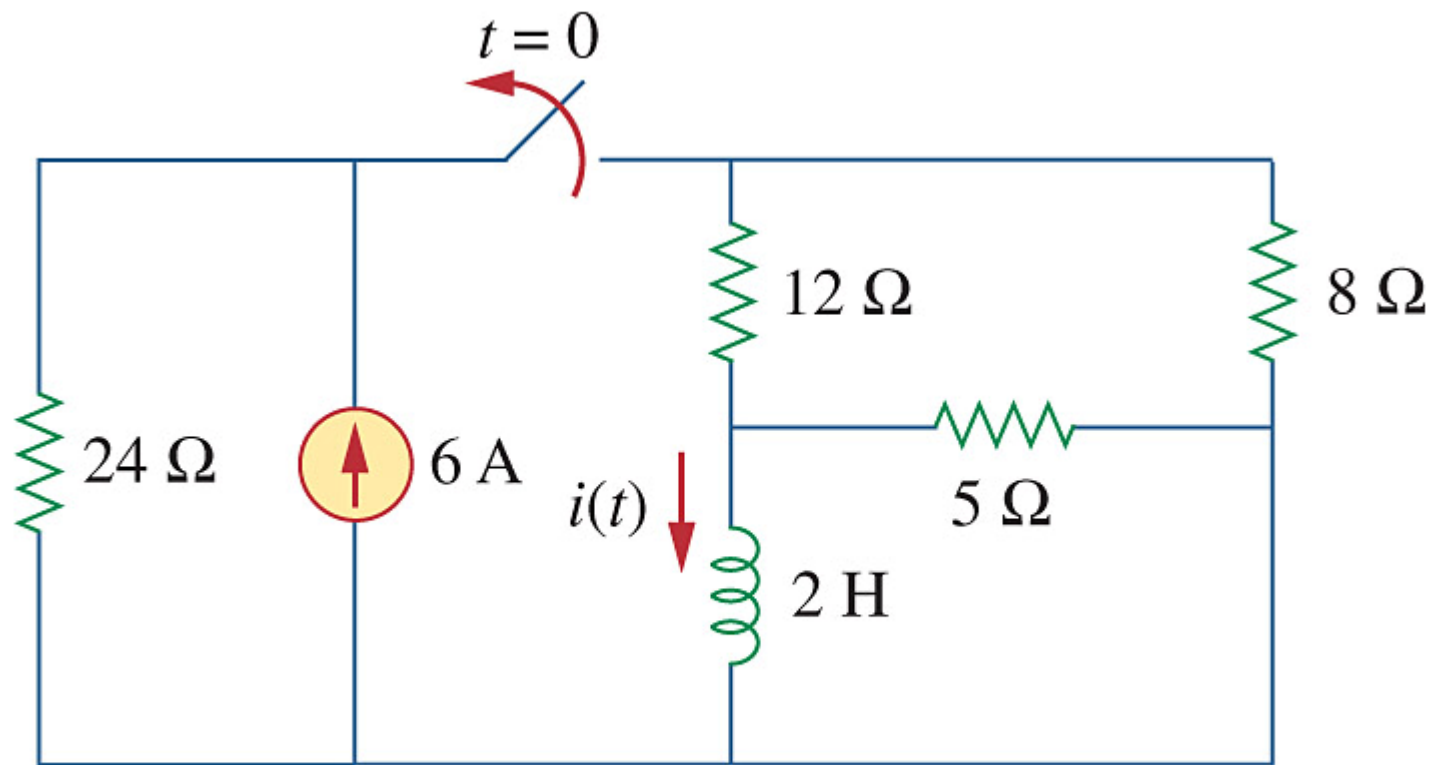


Figure 7.18

## Solution :

When  $t < 0$ , the current through the  $5\text{-}\Omega$  resistor is zero.

$$i(t) = 6 \times \frac{24 \parallel 8}{24 \parallel 8 + 12} = 2 \text{ (A)}$$

When  $t > 0$ ,

$$R_{eq} = 5 \parallel (12 + 8) = 4 \text{ (}\Omega\text{)}$$

$$\tau = L / R_{eq} = 2 / 4 = 0.5 \text{ (s)}$$

$$i(t) = i(0)e^{-t/\tau} = 2e^{-t/0.5} = 2e^{-2t} \text{ (A)}$$

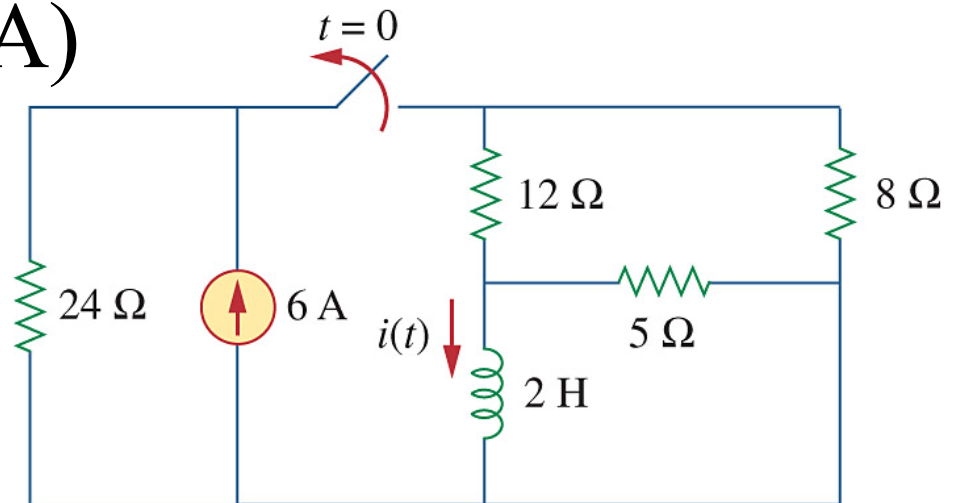


Figure 7.18

## 7.4 Singularity Functions

- Singularity functions (also called *switching functions*) are functions that either are discontinuous or have discontinuous derivatives. They serve as good approximations to switching operations.
- The three most widely used singularity functions in circuit analysis are the *unit step*, the *unit impulse*, and the *unit ramp* functions.

# I. Unit Step

The unit step function  $u(t)$  is 0 for negative values of  $t$  and 1 for positive values of  $t$ . In mathematical terms,

$$u(t) = \begin{cases} 0, & t < 0 \\ 1, & t > 0 \end{cases}$$

The unit step function is not defined at  $t = 0$ , where it changes abruptly from 0 to 1.

Figure 7.23 depicts the unit step function.

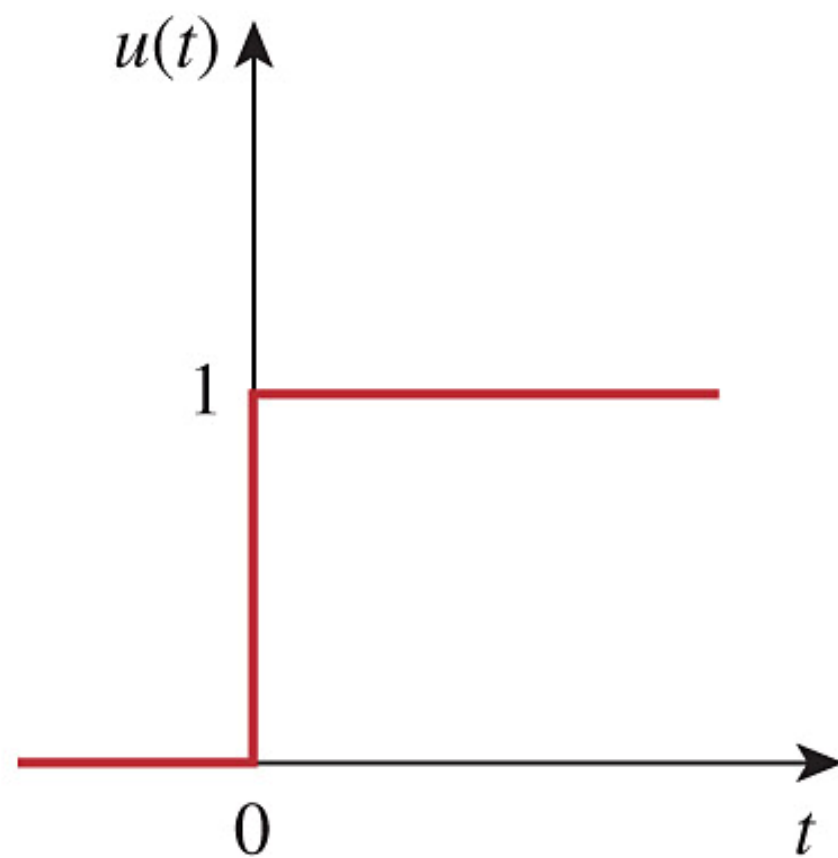


Figure 7.23 The unit step function.

If the abrupt change occurs at  $t = t_0$  (where  $t_0 > 0$ ) instead of  $t = 0$ , the mathematical representation becomes

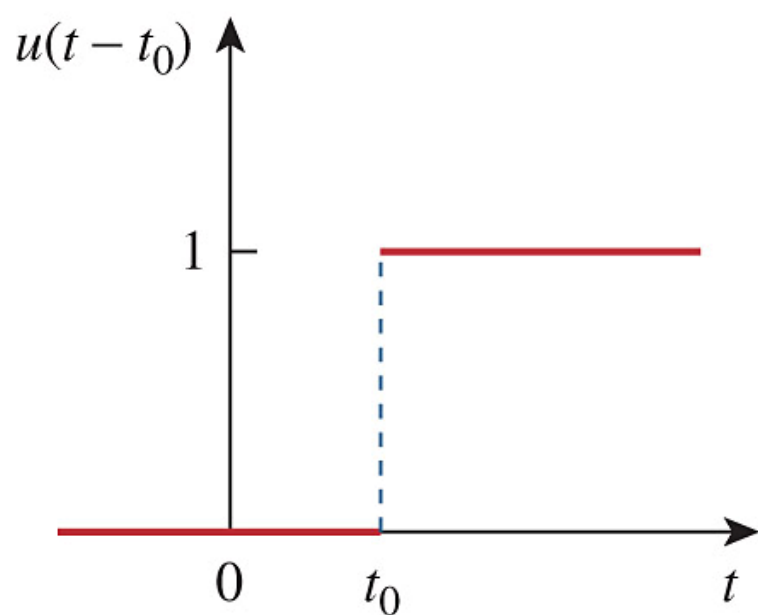
$$u(t - t_0) = \begin{cases} 0, & t < t_0 \\ 1, & t > t_0 \end{cases}$$

meaning that  $u(t)$  is delayed by  $t_0$  seconds.

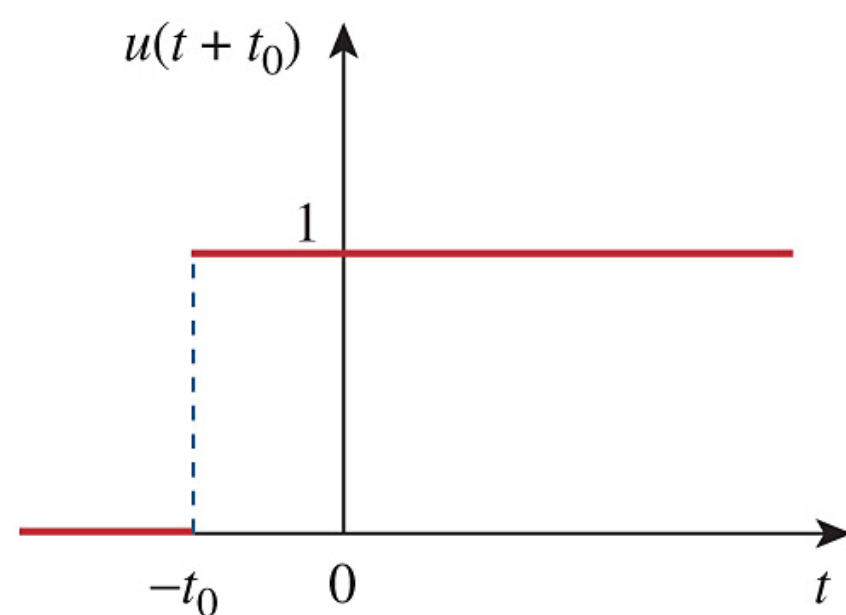
If the abrupt change occurs at  $t = -t_0$  (where  $t_0 > 0$ ) instead of  $t = 0$ , the mathematical representation becomes

$$u(t + t_0) = \begin{cases} 0, & t < -t_0 \\ 1, & t > -t_0 \end{cases}$$

meaning that  $u(t)$  is advanced by  $t_0$  seconds.



(a)



(b)

Figure 7.24 (a) The delayed version of the unit step, (b) the advanced version of the unit step.



In general, the step function is  $Ku(t)$ , where  $K$  is a constant.

Switching operations create abrupt changes in voltages and currents. An abrupt change can be represented by the step function. Two examples are given in Figures 7.25 and 7.26.

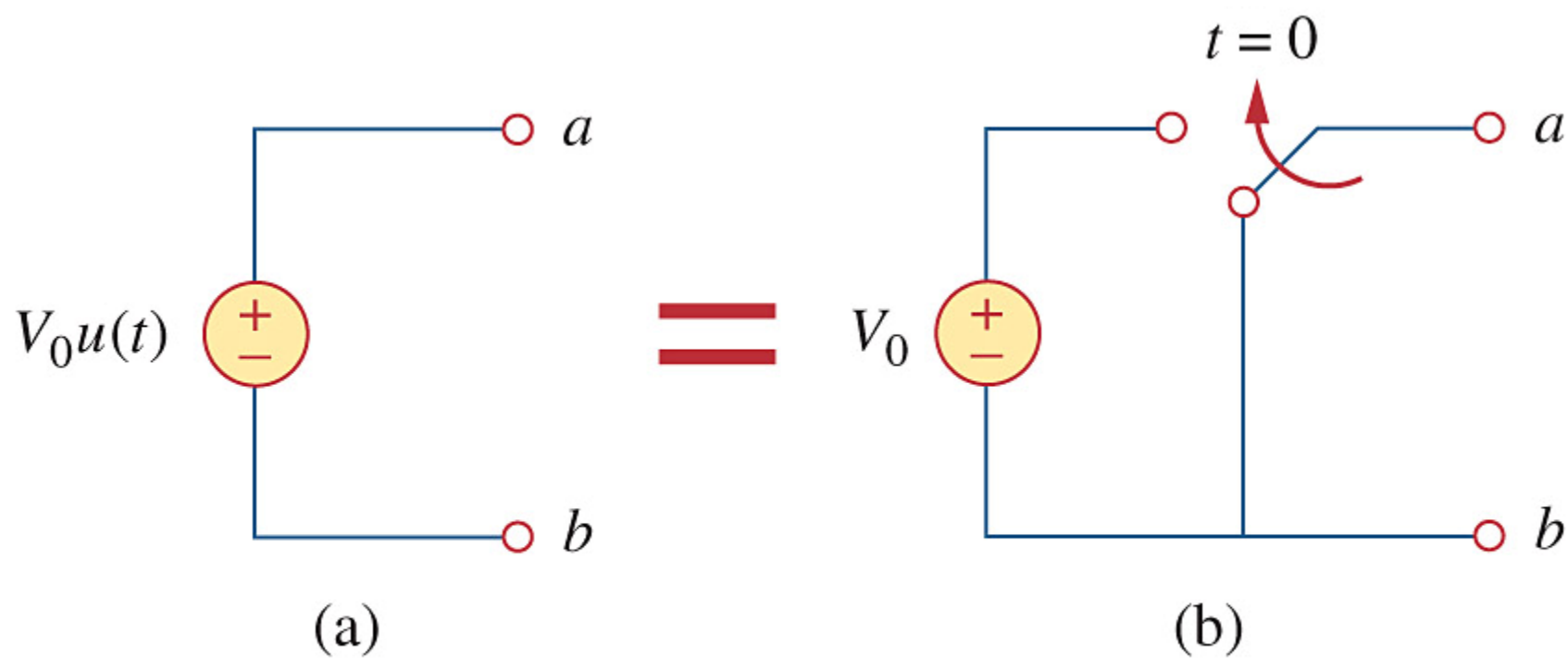


Figure 7.25 (a) Voltage source of  $V_0 u(t)$ , (b) its equivalent circuit.

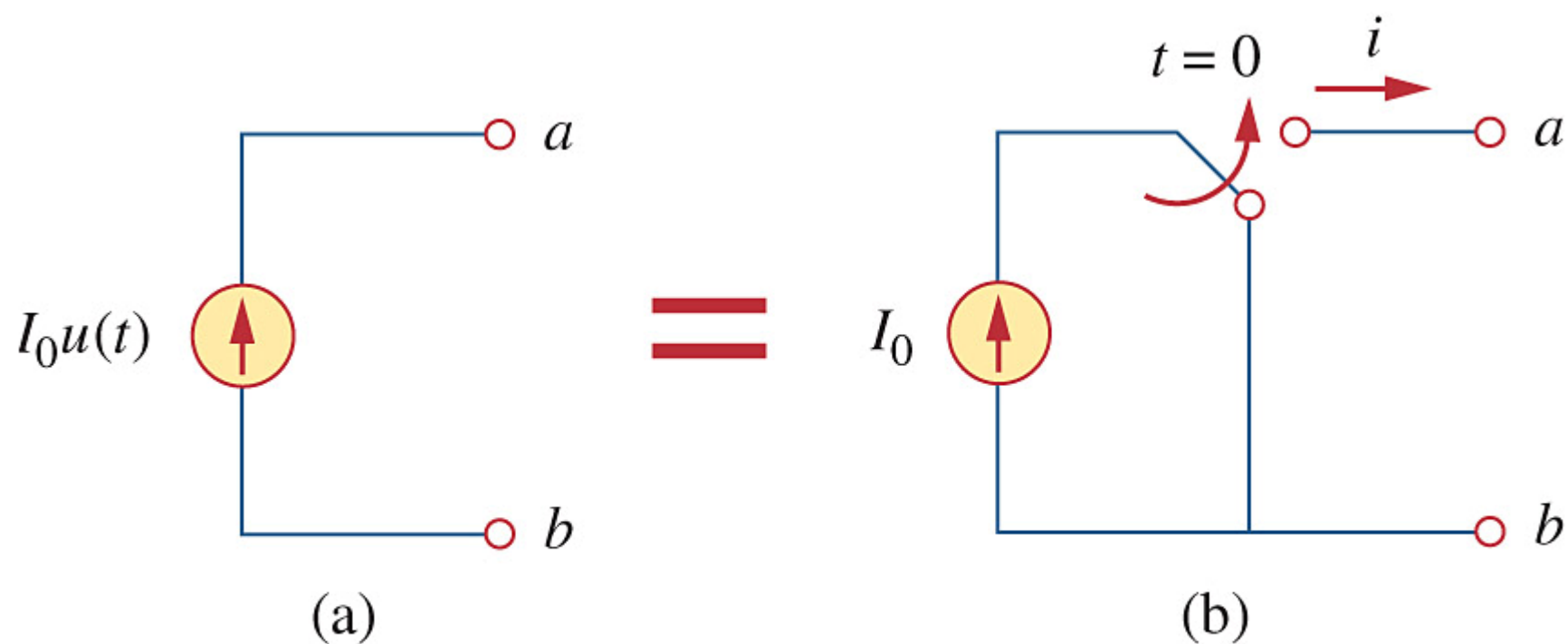
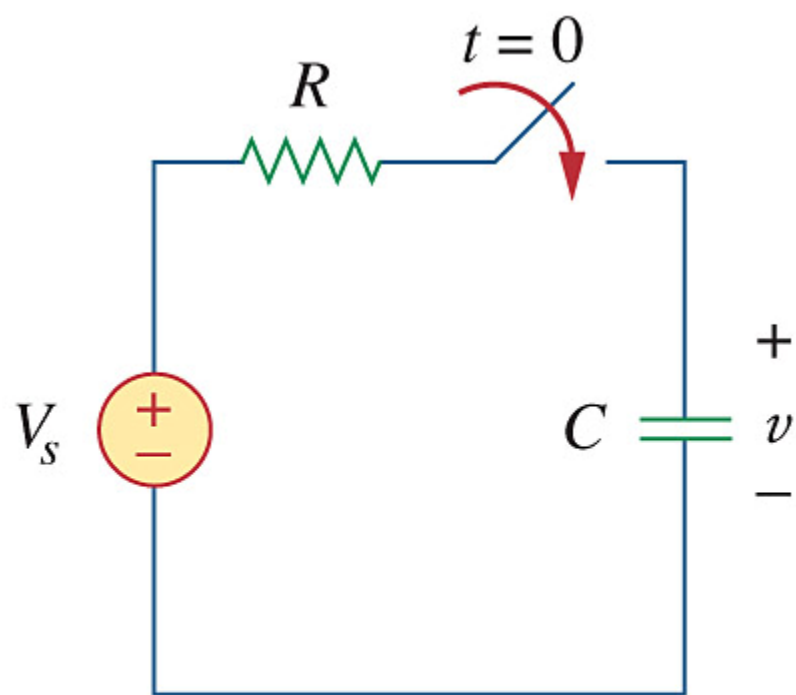


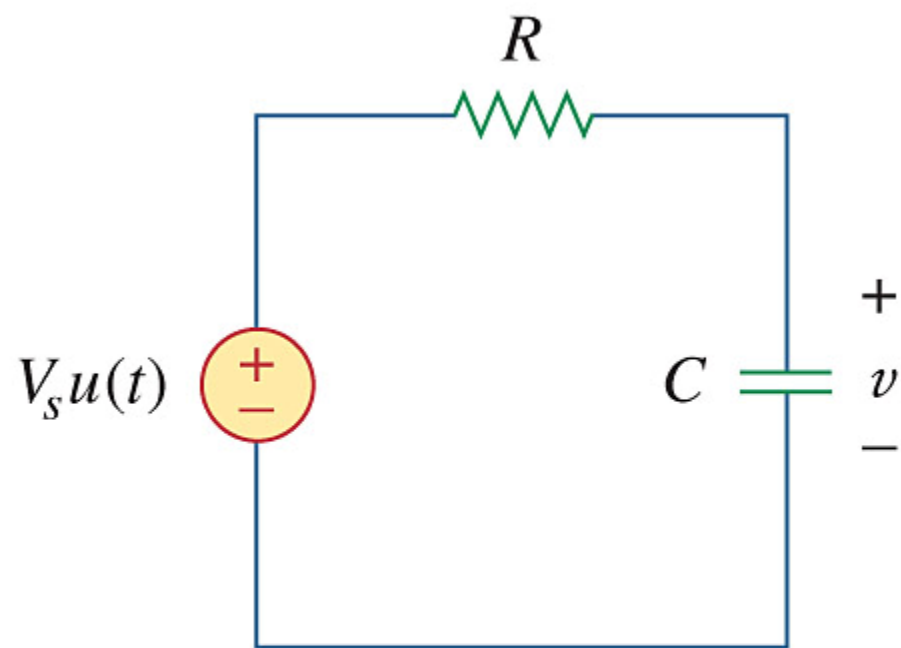
Figure 7.26 (a) Current source of  $I_0 u(t)$ , (b) its equivalent circuit.

## 7.5 An $RC$ Circuit with Step Input

Consider the  $RC$  circuit in Fig. 7.40(a) which can be replaced by the circuit in Fig. 7.40(b), where  $V_s$  is a constant dc voltage source. Again, we select the capacitor voltage  $v$  as the circuit response to be determined. We assume an initial voltage  $V_0$  on the capacitor.



(a)



(b)

Figure 7.40 An  $RC$  circuit with voltage step input.

Thus, to find the response of a first-order  $RC$  circuit requires three things:

1. The initial capacitor voltage  $v(0^+)$ .
2. The final capacitor voltage  $v(\infty)$ .
3. The time constant  $\tau = RC$ .

This is known as the *three - factor method*.

Source-free RC circuit is a special case when  $v(\infty) = 0$

Since the voltage across the capacitor cannot change instantaneously,

$$v(0^+) = \underline{v(0^-) = V_0}$$

For  $t > 0$ ,

Initial condition

$$\left( C \frac{dv}{dt} \right) R + v = V_s$$

or

$$\frac{dv}{dt} + \frac{1}{\tau} v = \frac{V_s}{\tau}, \text{ where } \tau = RC$$

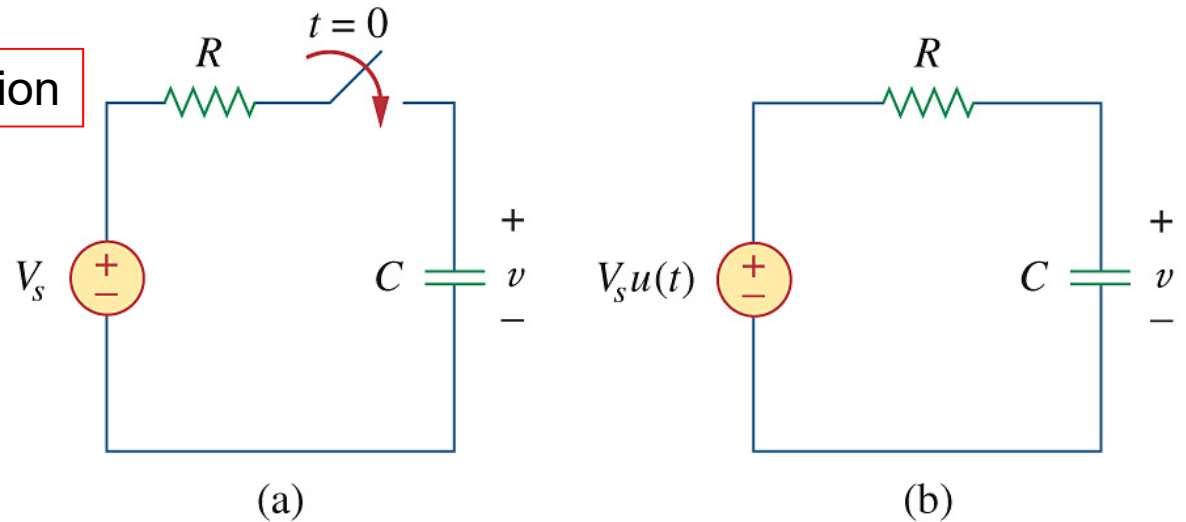


Figure 7.40 An  $RC$  circuit with voltage step input.

## Method2

$$r + \frac{1}{\tau} = 0 \Rightarrow r = -\frac{1}{\tau}$$

The homogeneous solution or *natural response*

$$v_n(t) = Ae^{-t/\tau}$$

Suppose the particular solution or *forced response*

$$v_f(t) = B$$



$$\frac{dB}{dt} + \frac{1}{\tau} B = \frac{V_s}{\tau} \Rightarrow B = V_s$$

The complete solution or *complete response*  
or *total response*

$$v(t) = v_n(t) + v_f(t) = Ae^{-t/\tau} + V_s$$

When  $t = 0^+$ ,

$$v(0^+) = A + V_s = V_0 \Rightarrow A = V_0 - V_s$$

Hence,

$$v(t) = (V_0 - V_s)e^{-t/\tau} + V_s$$

This is the response of the  $RC$  circuit to a sudden application of a constant dc source, assuming the capacitor is initially charged.

Assuming that  $V_s > V_0 > 0$ , a plot of  $v(t)$  is shown in Fig. 7.41.

Whichever way we look at it, the complete response may be written as

$$v(t) = v(\infty) + [v(0^+) - v(\infty)]e^{-t/\tau}$$

where  $v(0^+)$  is the *initial value* (i.e., the value at  $t = 0^+$ ) and  $v(\infty)$  is the *final value* (or steady-state value).

$$\begin{aligned} \text{At } t = 0, v(0^+) &= v(\infty) + [v(0^+) - v(\infty)] \times 1 = v(0^+) \\ \text{At } t \rightarrow \infty, v(\infty) &= v(\infty) + [v(0^+) - v(\infty)] \times 0 = v(\infty) \end{aligned}$$

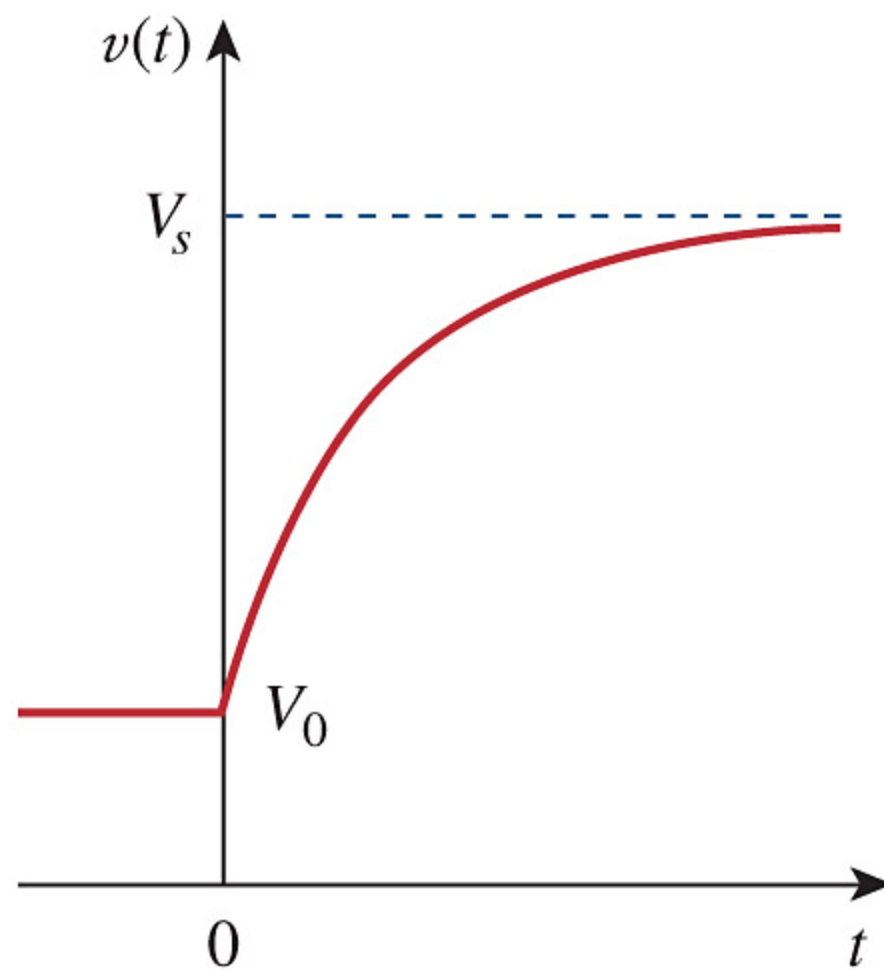


Figure 7.41 Response of an  $RC$  circuit.

If the capacitor is uncharged initially, i.e.,

$V_0 = 0$ , then

$$v(t) = V_s (1 - e^{t/\tau}), \quad t > 0$$

or

$$v(t) = V_s (1 - e^{t/\tau}) u(t)$$

Initial condition



This is the *zero - state response*. The zero-state response corresponding to a unit-step input is called the *unit - step response*.

# Interpretation 1: natural and forced responses

The complete response consists of two components:

$$(a) \ v(t) = v_n(t) + v_f(t)$$

where  $v_n(t) = \underline{(V_0 - V_s)e^{-t/\tau}}$  is the natural response (homogeneous solution), and  $v_f(t) = \underline{V_s}$  is the forced response (particular solution). Basically,  $v_f(t)$  has the same form as the input (external "force").

## Interpretation 2: temporary and steady state

$$(c) \ v(t) = v_t(t) + v_{ss}(t)$$

where  $v_t(t) = \underline{(V_0 - V_s)}e^{-t/\tau}$  is the temporary response (will die out with time) and  $v_{ss}(t) = \underline{V_s}$  is the response as  $t \rightarrow \infty$ .

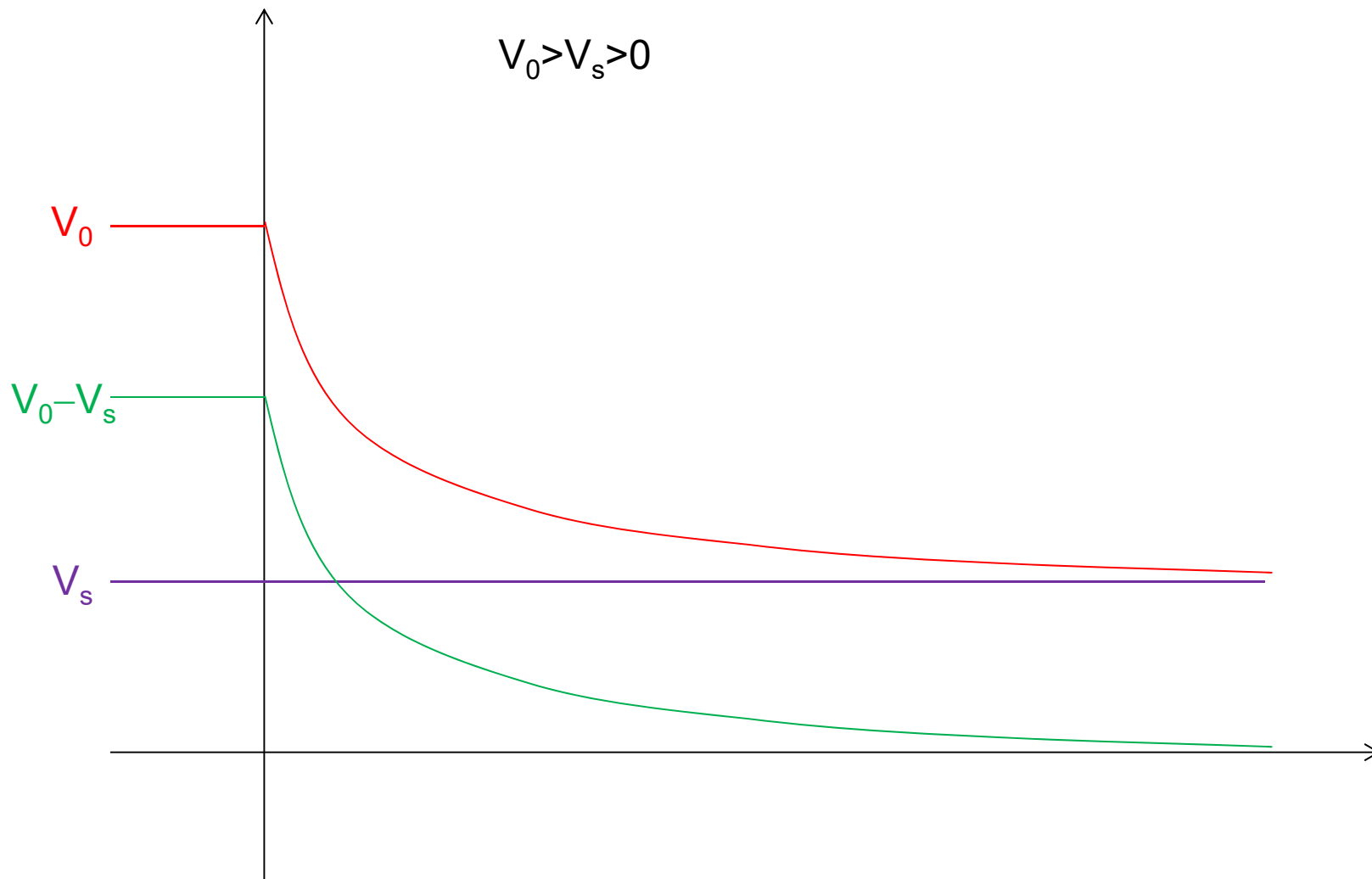
- Interpretation 1 is similar to interpretation 2

$$v(t) = \underbrace{V_s}_{\text{Forced response; Steady state}} + \underbrace{(V_0 - V_s)e^{-t/\tau}}_{\text{Homogeneous response; Temporary response}}, \quad t > 0$$

Forced response;  
Steady state

Homogeneous response;  
Temporary response





$$v(t) = \underline{V_s} + \underline{(V_0 - V_s)e^{-t/\tau}}, \quad t > 0$$

Forced response;  
Steady state

Homogeneous response;  
Temporary response

**Example 7.10** The switch in Fig.7.43 has been in position *A* for a long time. At  $t = 0$ , the switch moves to *B*. Determine  $v(t)$  for  $t > 0$  and calculate its value at  $t = 1$  s and 4s.

**Solution :**

For  $t < 0$ ,

$$v(t) = 24 \times \frac{5}{3+5} = 15 \text{ (V)}$$

$$v(0^-) = 15 \text{ V}$$

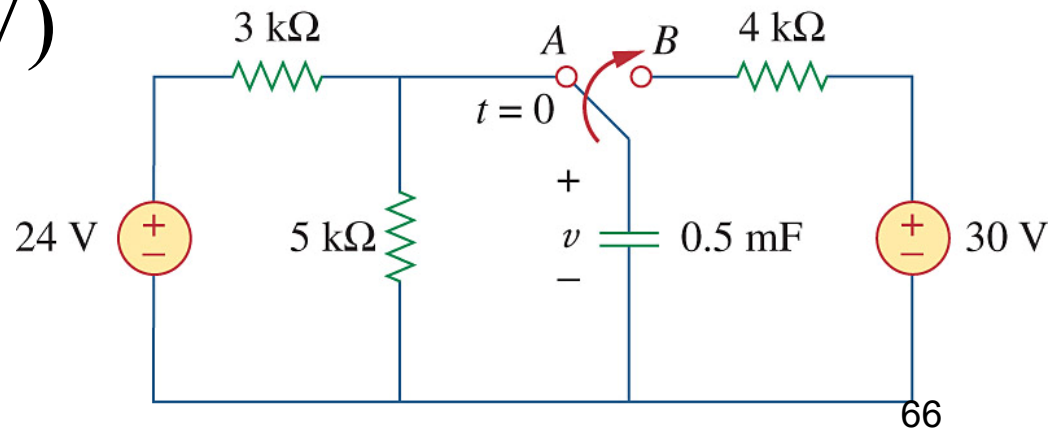


Figure 7.43

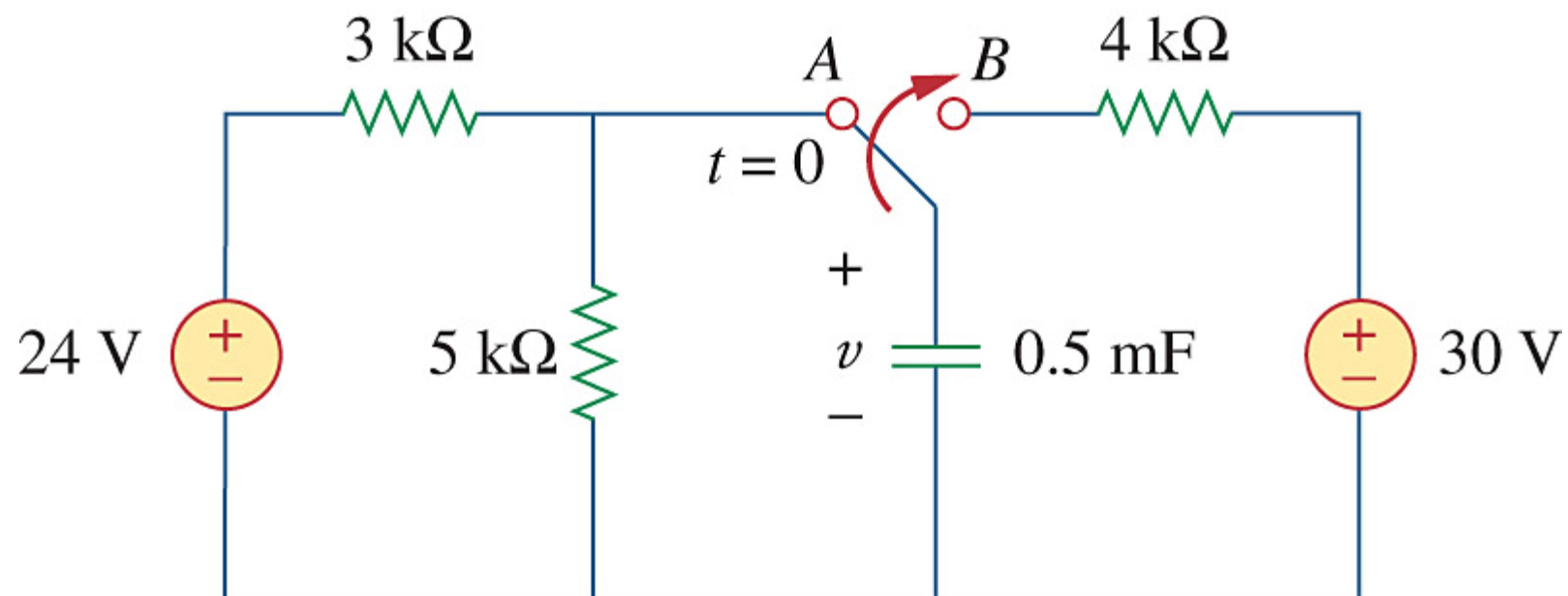


Figure 7.43

For  $t > 0$ ,

$$v(0^+) = v(0^-) = 15 \text{ V}$$

$$v(\infty) = 30 \text{ V}$$

$$\tau = 4 \times 10^3 \times 0.5 \times 10^{-3} = 2 \text{ (s)}$$

$$v(t) = v(\infty) + [v(0^+) - v(\infty)]e^{-t/\tau}$$

$$= 30 + (15 - 30)e^{-t/2} = 30 - 15e^{-0.5t} \text{ (V)}$$

$$v(1) = 30 - 15e^{-0.5 \times 1} \approx 20.90 \text{ (V)}$$

$$v(4) = 30 - 15e^{-0.5 \times 4} \approx 27.97 \text{ (V)}$$

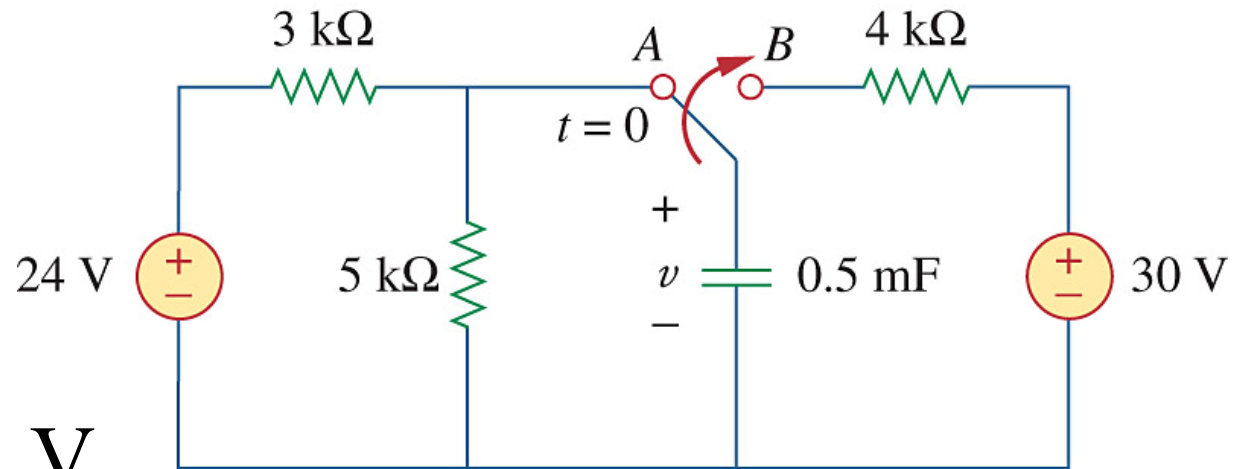


Figure 7.43

**Practice Problem 7.11** The switch in Fig. 7.43 is closed at  $t = 0$ . Find  $i(t)$  and  $v(t)$  for all time.

**Solution :**

For  $t < 0$ ,

$$i(t) = 0 \text{ A}$$

$$v(t) = 20 \text{ V}$$

$$v(0^-) = 20 \text{ V}$$

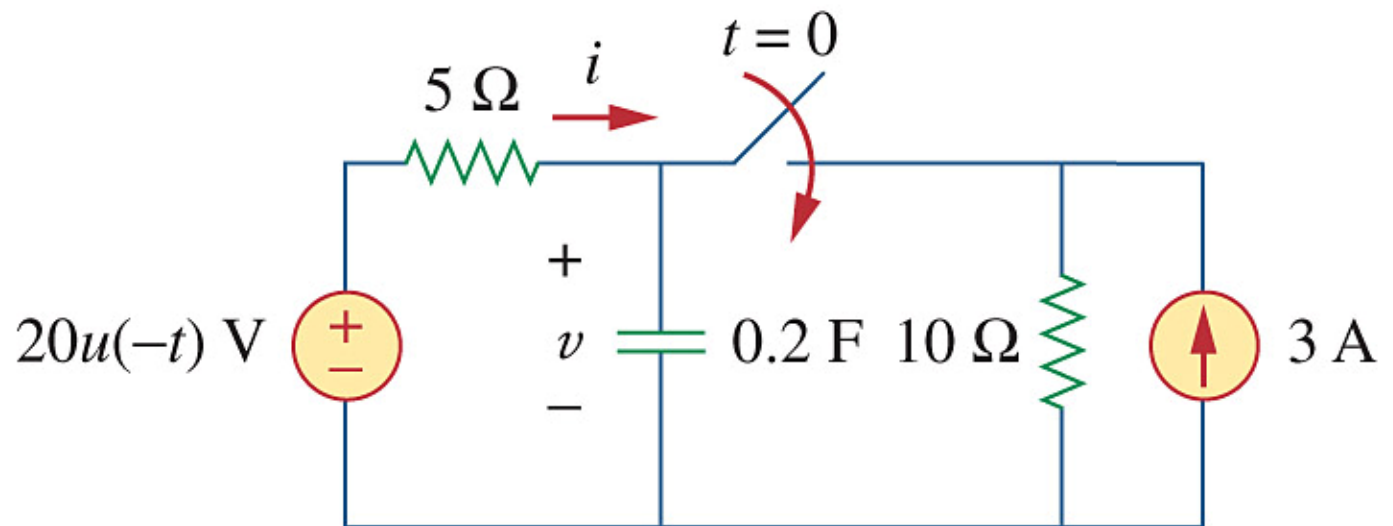


Figure 7.47

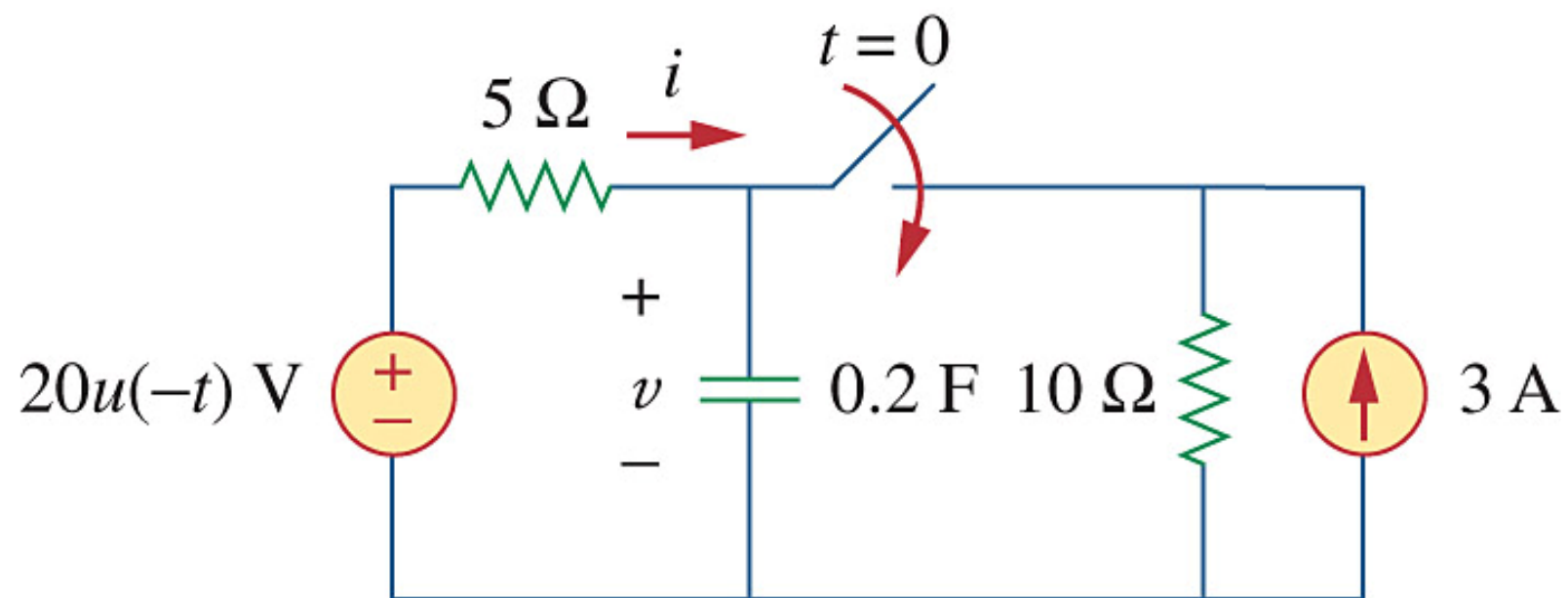


Figure 7.47

For  $t > 0$ ,

$$v(0^+) = v(0^-) = 20 \text{ V}$$

$$v(\infty) = 3 \times (5 \parallel 10) = 10 \text{ (V)}$$

$$\tau = (5 \parallel 10) \times 0.2 = \frac{2}{3} \text{ (s)}$$

$$v(t) = v(\infty) + [v(0^+) - v(\infty)]e^{-t/\tau}$$

$$= 10 + (20 - 10)e^{-t/(2/3)} = 10(1 + e^{-1.5t}) \text{ (V)}$$

$$i(t) = -\frac{v(t)}{5} = -2(1 + e^{-1.5t}) \text{ (A)}$$

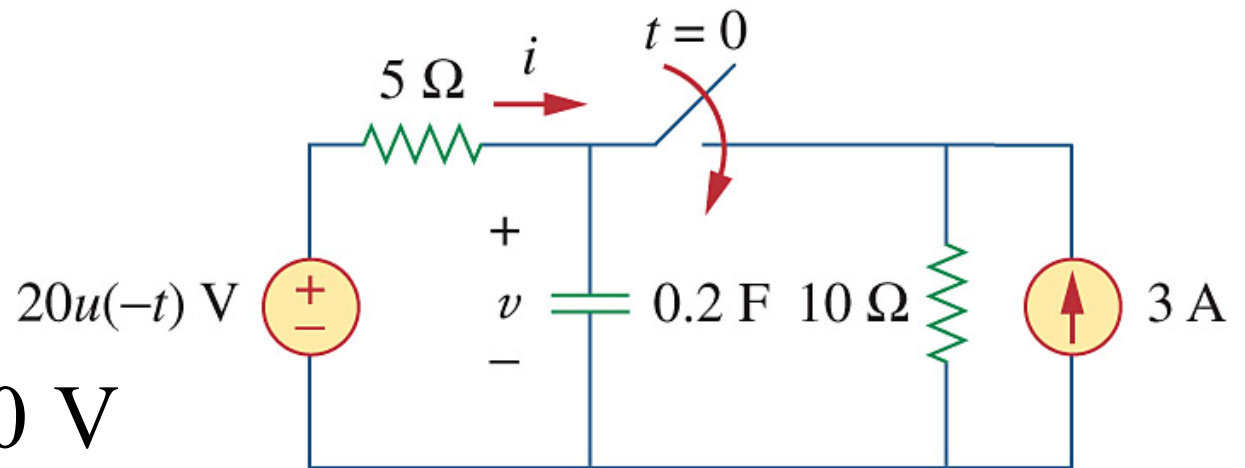


Figure 7.47

$v(0^+)$ : by the value of  $v(0^-)$   
 $v(\infty)$ : by the circuit at  $t > 0$

## 7.6 An $RL$ Circuit with Step Input

Consider the  $RL$  circuit in Fig. 7.48(a) which can be replaced by the circuit in Fig. 7.48(b), where  $V_s$  is a constant dc voltage source. We select the inductor current  $i$  as the circuit response to be determined. We assume an initial current  $I_0$  in the inductor.



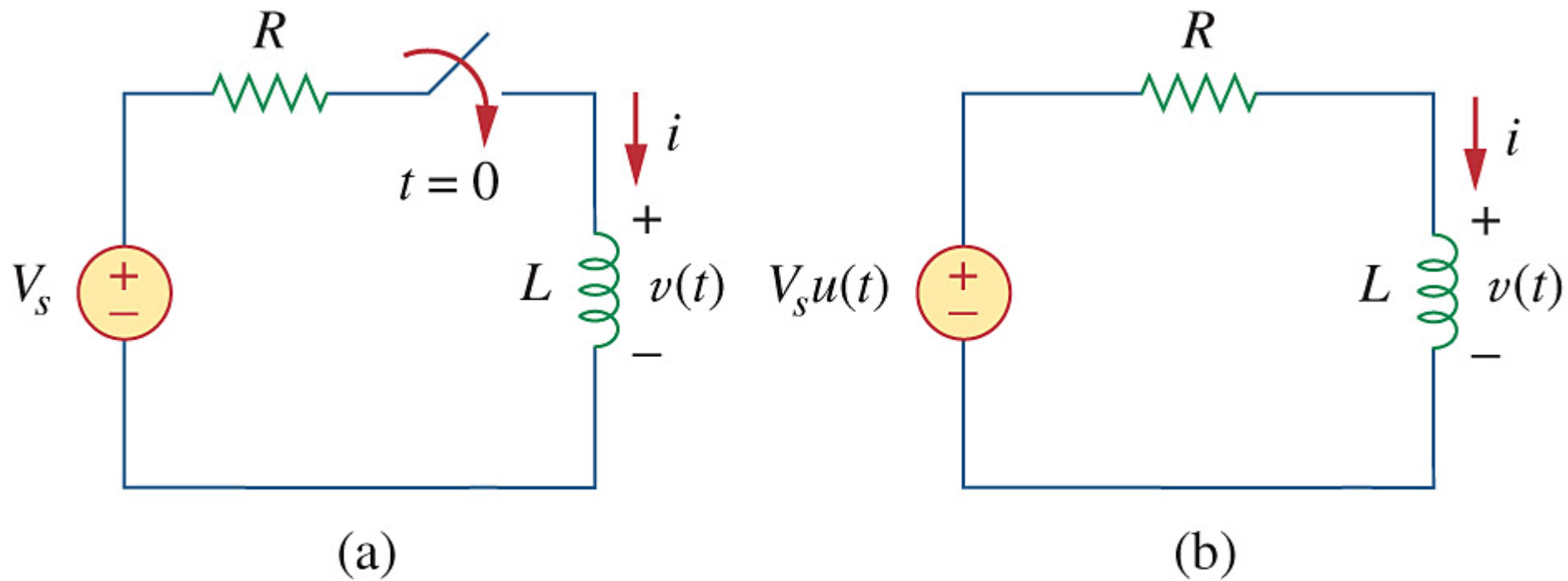


Figure 7.48 An  $RL$  circuit with a step input voltage.

Since the current through the inductor cannot change instantaneously,

$$i(0^+) = i(0^-) = I_0$$

For  $t > 0$ ,

$$iR + L \frac{di}{dt} = V_s$$

or

$$\frac{di}{dt} + \frac{1}{\tau} i = \frac{V_s / R}{\tau}, \text{ where } \tau = \frac{L}{R}$$

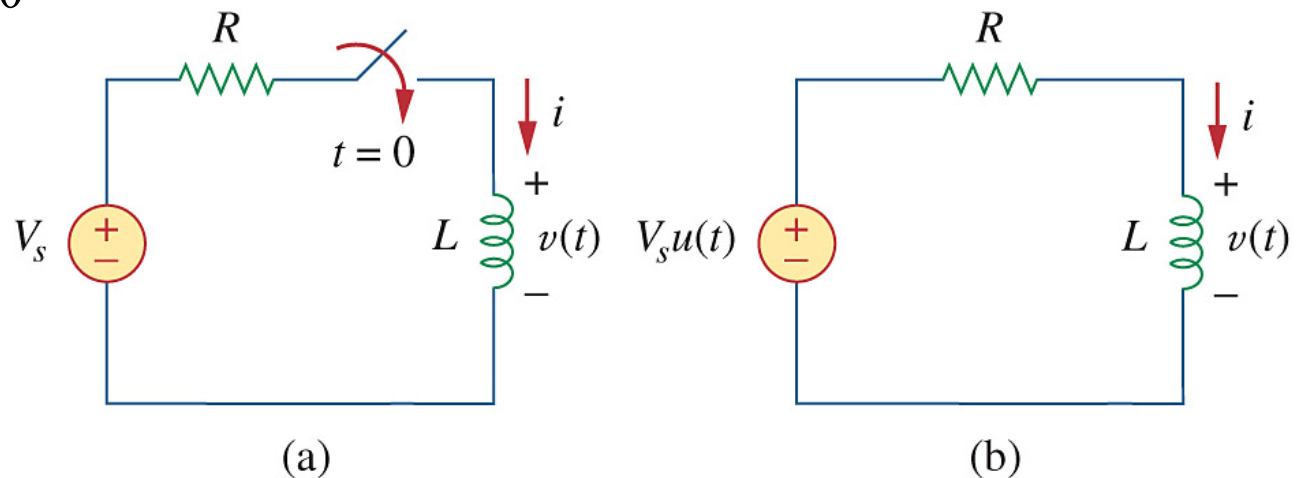


Figure 7.48 An  $RL$  circuit with a step input voltage.

RL

$$\frac{di}{dt} + \frac{1}{\tau} i = \frac{V_s / R}{\tau}, \text{ where } \tau = \frac{L}{R}$$

RC

$$\frac{dv}{dt} + \frac{1}{\tau} v = \frac{V_s}{\tau}, \text{ where } \tau = RC$$

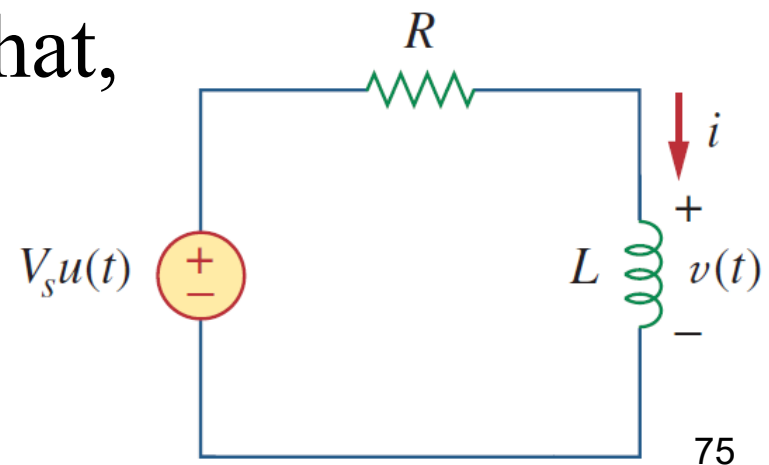
Since this differential equation has the same form as that describing the  $RC$  circuit,

$$i(t) = \frac{V_s}{R} + \left( I_0 - \frac{V_s}{R} \right) e^{-t/\tau}$$

$$v(t) = (V_0 - V_s) e^{-t/\tau} + V_s$$

It is evident from Fig. 7.48 that,

$$i(\infty) = \frac{V_s}{R}$$



(b)

75

The complete response can be written as

$$i(t) = i(\infty) + \left[ i(0^+) - i(\infty) \right] e^{-t/\tau}$$

Thus, to find the response of a first-order *RL* circuit requires three things:

1. The initial inductor current  $i(0^+)$ .
2. The final inductor current  $i(\infty)$ .
3. The time constant  $\tau = L / R$ .

Source-free RL circuit is a special case when  $i(\infty) = 0$

The response of the  $RL$  circuit to a sudden application of a constant dc source is shown in Fig, 4.49, assuming that

$$I_0 > \frac{V_s}{R} > 0$$

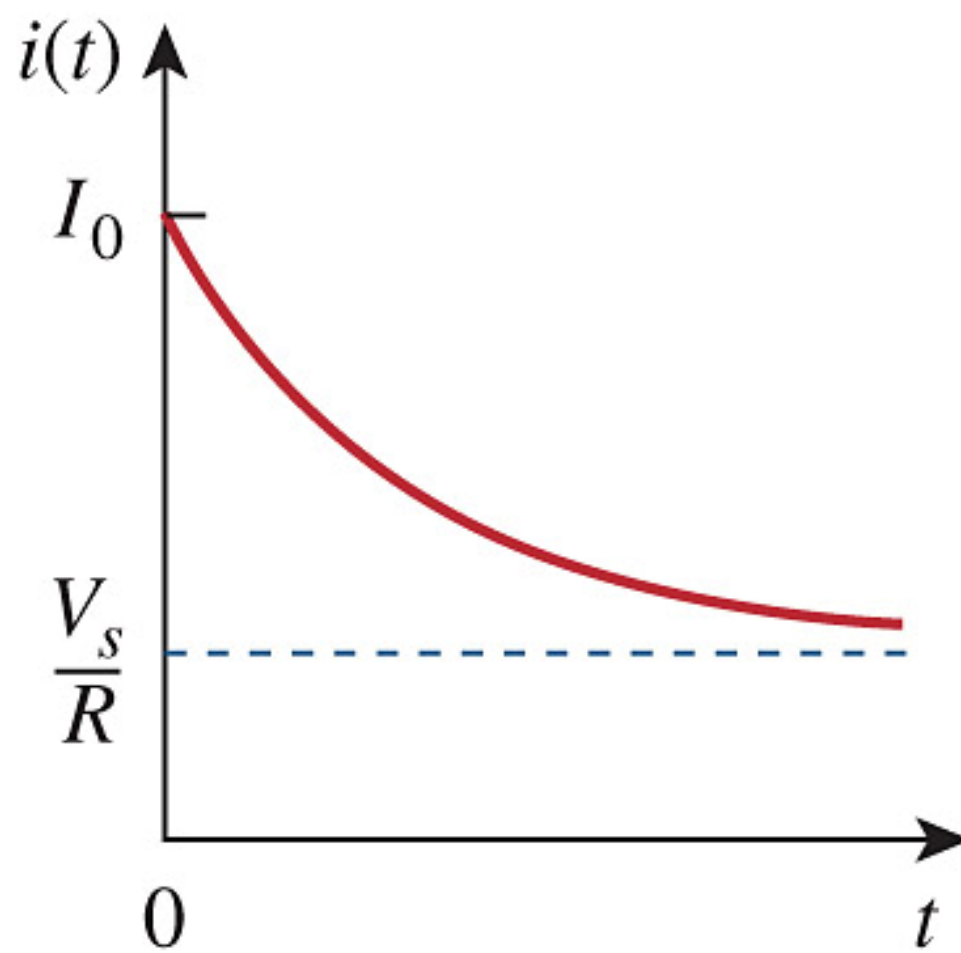
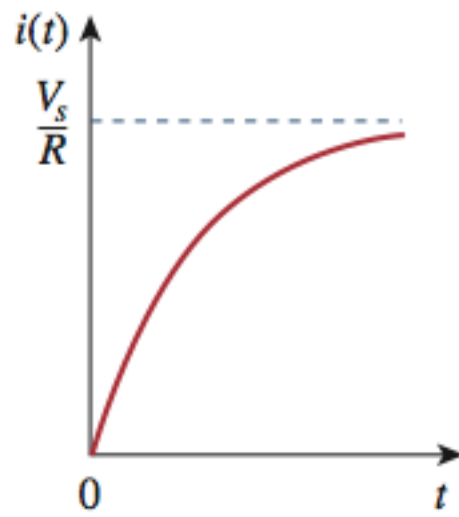
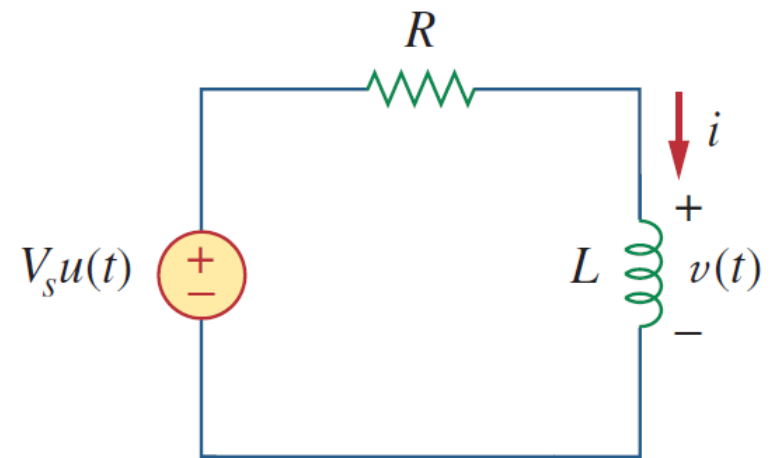
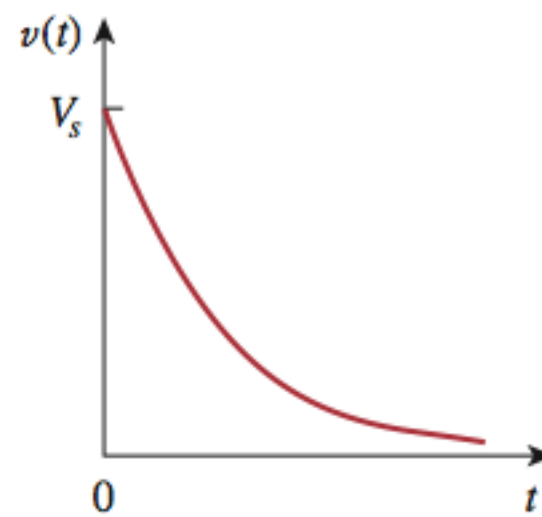


Figure 7.49 Total response of the  $RL$  circuit.



(a)



(b)

**Example 7.13** At  $t = 0$ , switch 1 in Fig. 7.53 is closed, and switch 2 is closed 4 s later. Find  $i(t)$  for  $t > 0$ . Calculate  $i$  for  $t = 2$  s and  $t = 5$  s.

**Solution :**

For  $t < 0$ ,

$$i(t) = 0$$

$$i(0^-) = 0$$

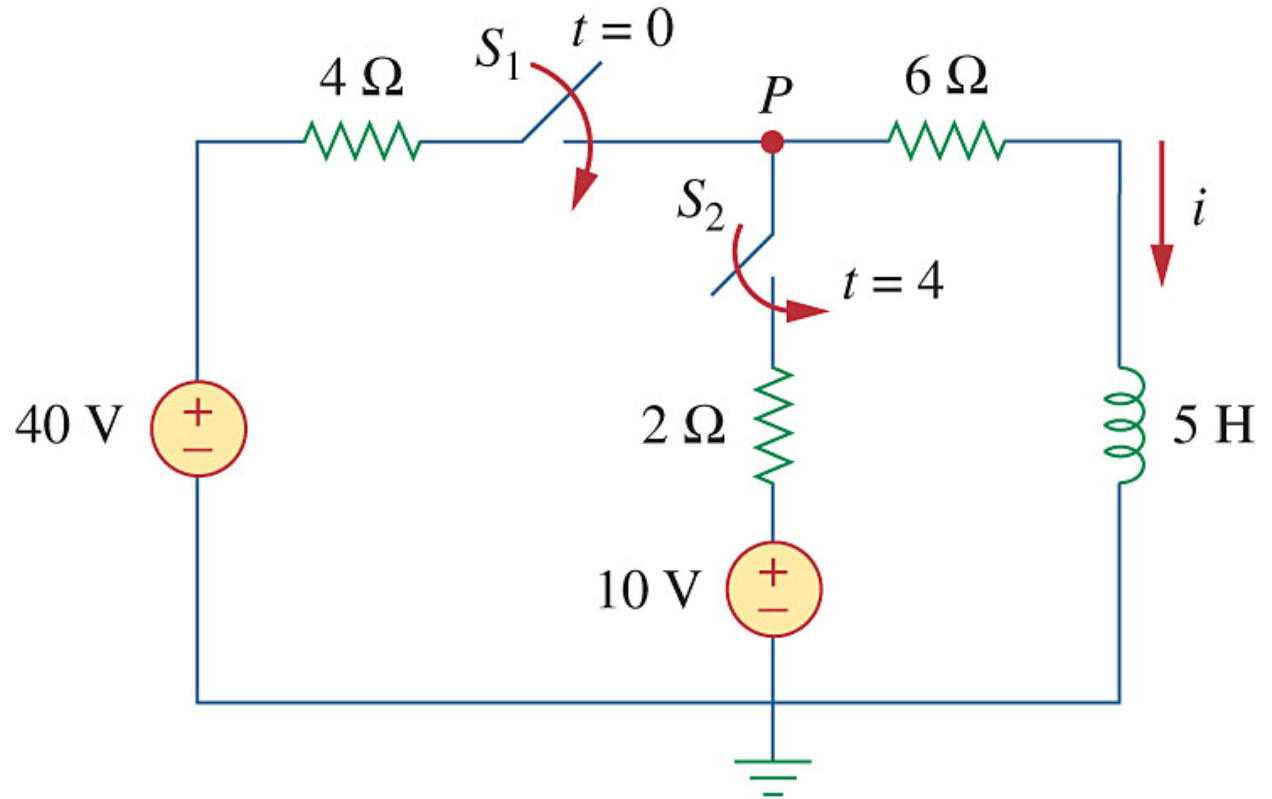


Figure 7.53



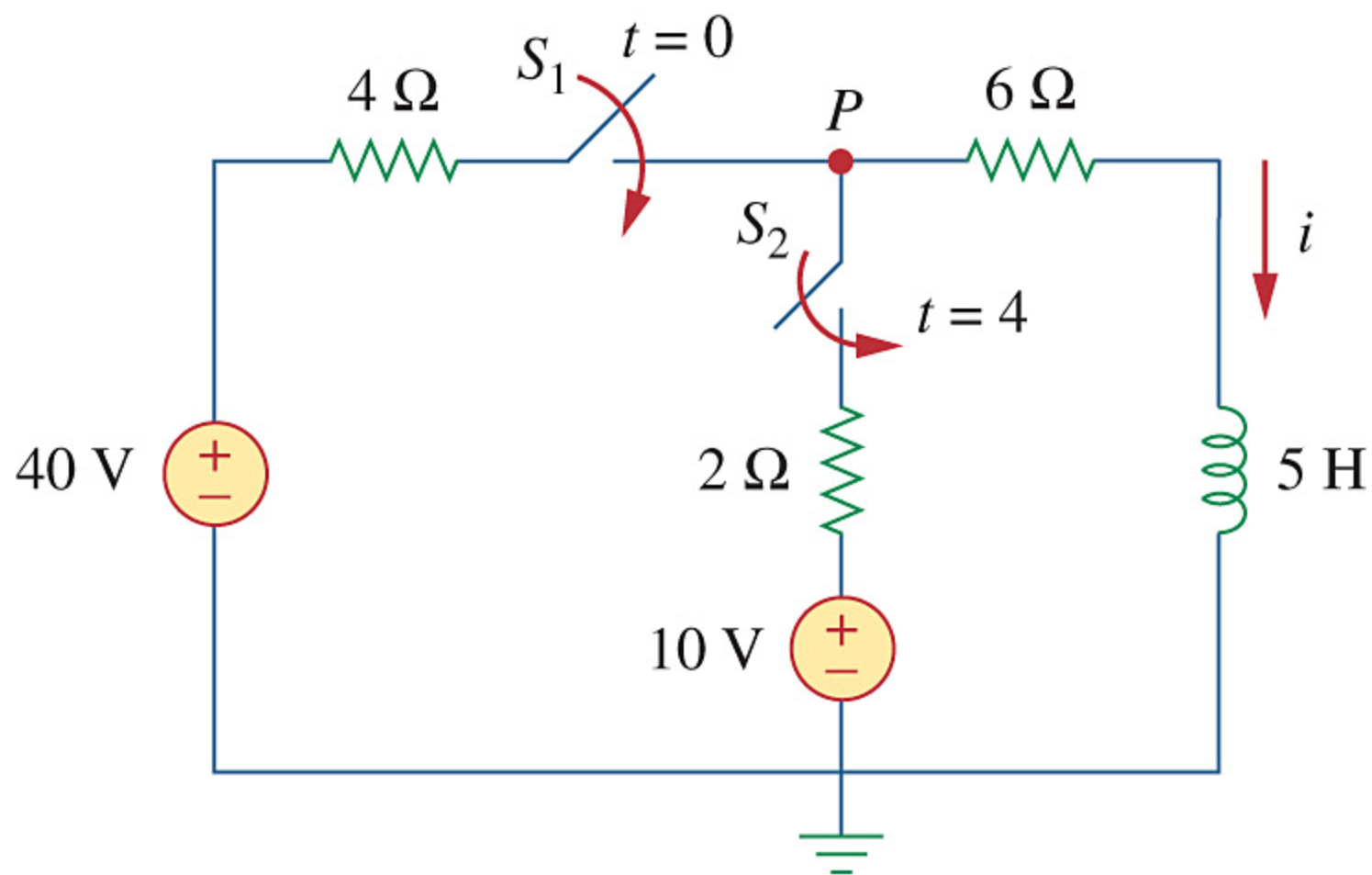


Figure 7.53

For  $t > 0$ ,

$$i(0^+) = i(0^-) = 0$$

For  $0 < t \leq 4$ ,

$$i(\infty) = \frac{40}{4 + 6} = 4 \text{ (A)}$$

$$\tau = \frac{5}{4 + 6} = 0.5 \text{ (s)}$$

$$i(t) = 4 + (0 - 4)e^{-t/0.5} = 4(1 - e^{-2t}) \text{ (A)}$$

$$i(2) = 4(1 - e^{-2 \times 2}) \approx 3.93 \text{ (A)}$$

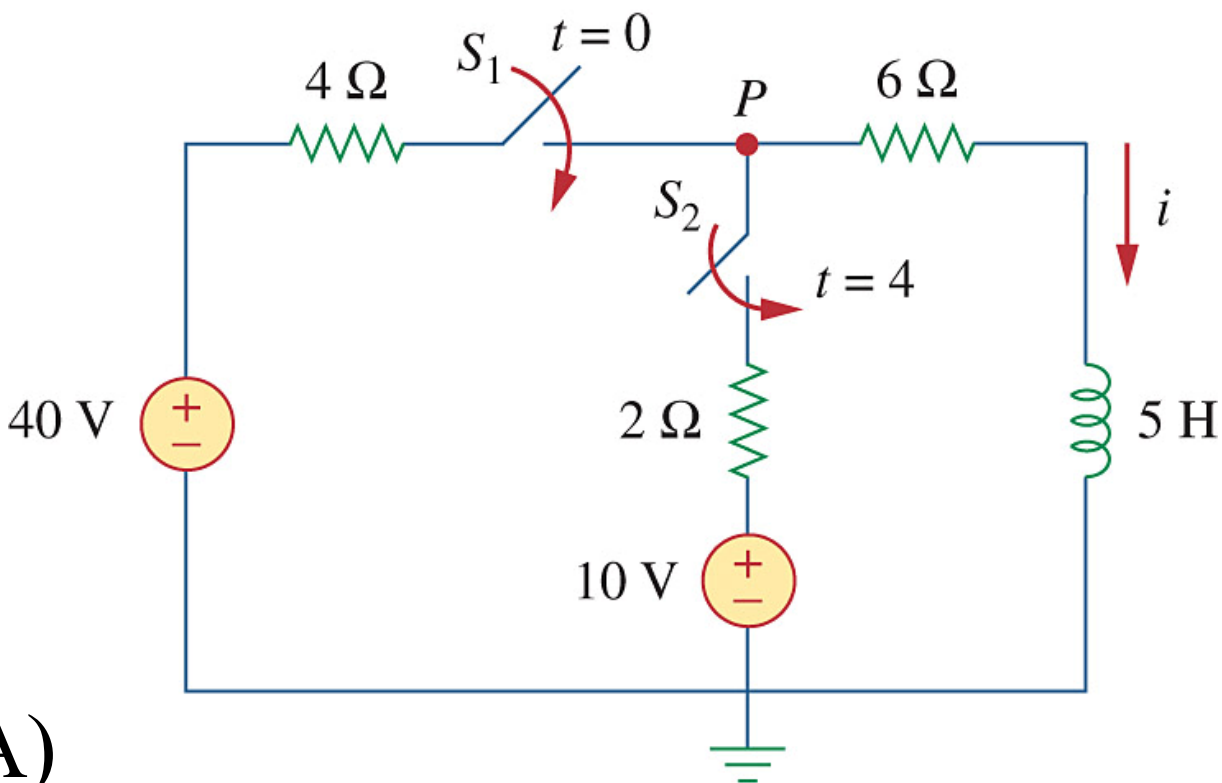


Figure 7.53

For  $t > 4$ ,

$$i(4^+) = i(4^-) = 4(1 - e^{-2 \times 4}) = 4(1 - e^{-8}) \text{ (A)}$$

$$v_P(\infty) = 40 \times \frac{2 \parallel 6}{4 + 2 \parallel 6} + 10 \times \frac{4 \parallel 6}{2 + 4 \parallel 6}$$

$$= \frac{180}{11} \text{ (V)}$$

$$i(\infty) = \frac{v_P(\infty)}{6} = \frac{30}{11} \text{ (A)}$$

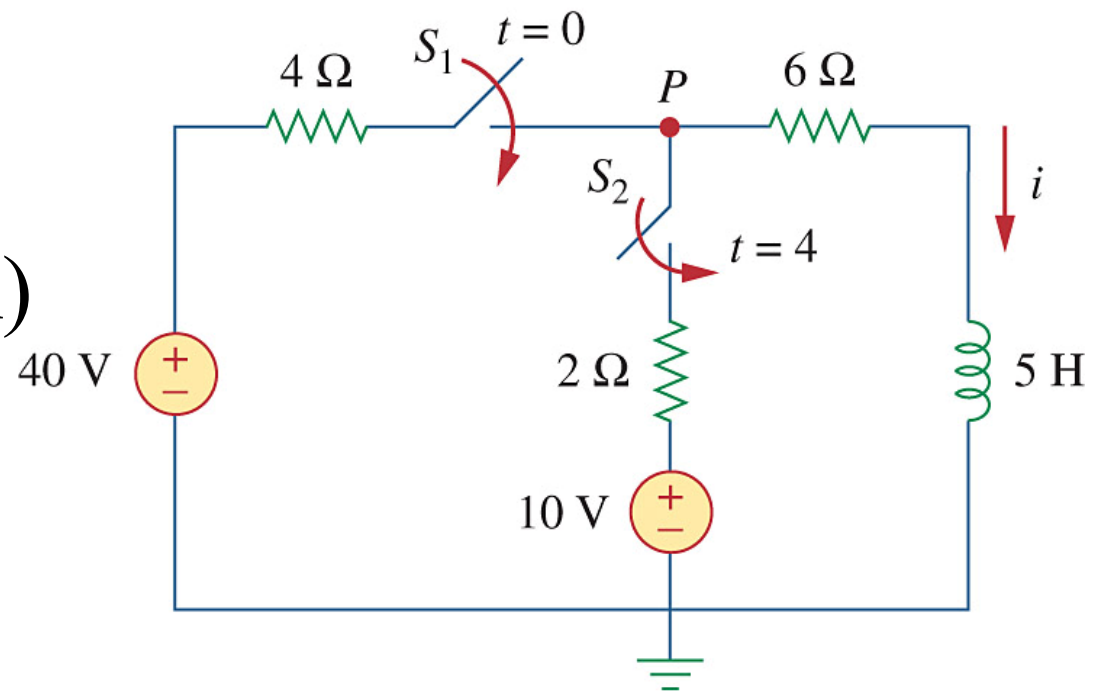


Figure 7.53

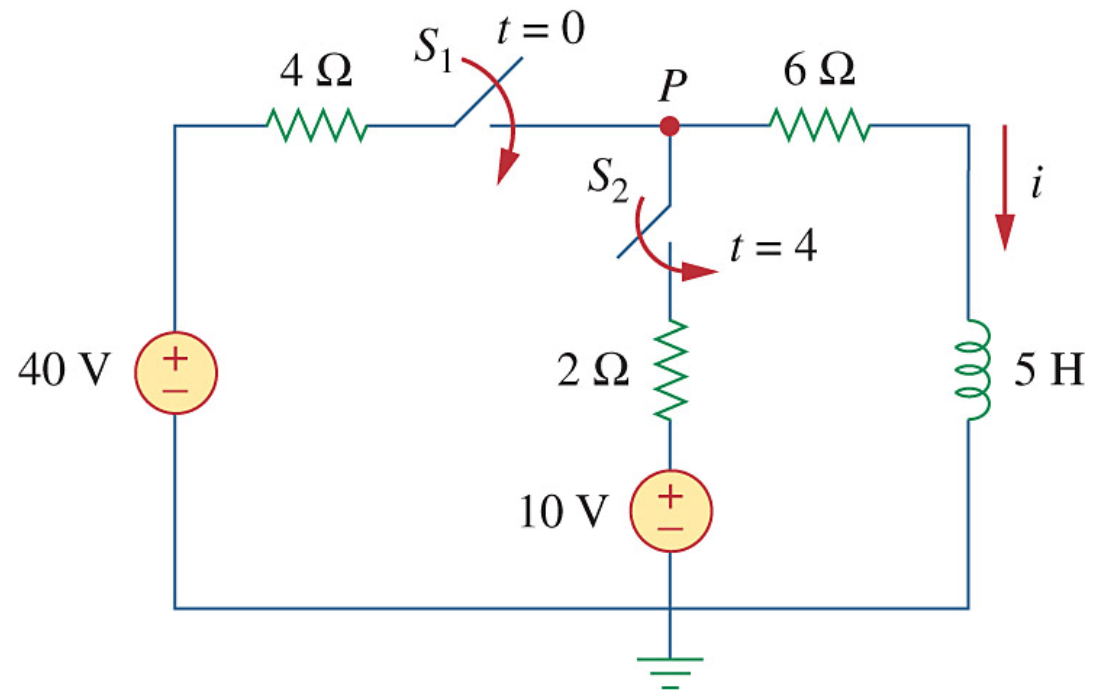


Figure 7.53

$$\tau = \frac{5}{6 + 4 \parallel 2} = \frac{15}{22} \text{ (s)}$$

$$i(t) = \frac{30}{11} + \left( 4(1 - e^{-8}) - \frac{30}{11} \right) e^{-\underline{(t-4)}/(15/22)}$$

Time shift property

$$\approx 2.7273 + 1.2714e^{-1.4667(t-4)} \text{ (A)}$$

$$i(5) = 2.7273 + 1.2714e^{-1.4667(5-4)} \approx 3.02 \text{ (A)}$$

## 7.7 First-Order Op Amp Circuits

**Example 7.14** For the op amp circuit in Fig. 7.55(a), find  $v_o$  for  $t > 0$ , given that  $v(0) = 3$  V. Let  $R_f = 80$  k $\Omega$ ,  $R_1 = 20$  k $\Omega$ , and  $C = 5$   $\mu$ F.

**Solution :**

$$\left( C \frac{dv}{dt} \right) R_1 + v = 0, \quad t > 0$$

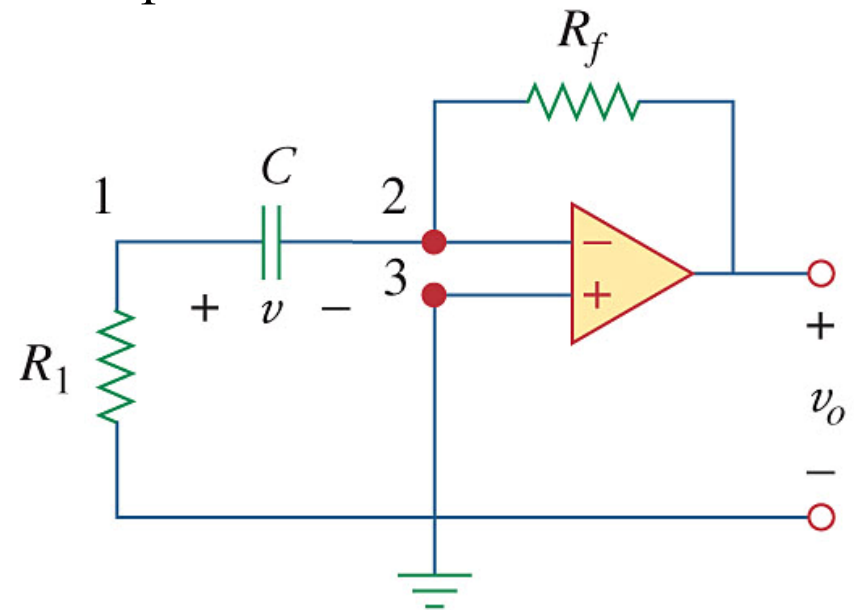


Figure 7.55(a)

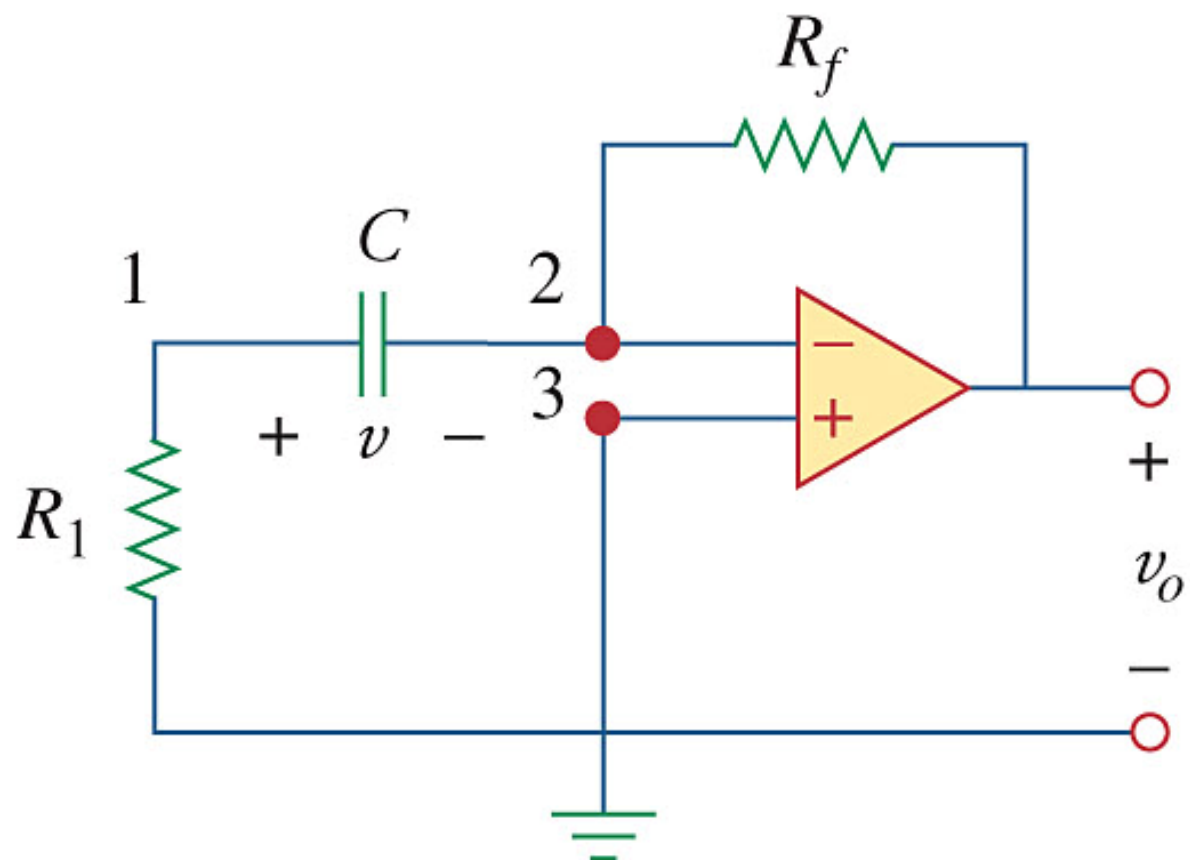


Figure 7.55(a)

or

$$\frac{dv}{dt} + \frac{1}{\tau}v = 0$$

where,

$$\tau = R_1 C = 20 \times 10^3 \times 5 \times 10^{-6} = 0.1 \text{ (s)}$$

$$v = v(0)e^{-t/\tau} = 3e^{-t/0.1} = 3e^{-10t} \text{ (V)}$$

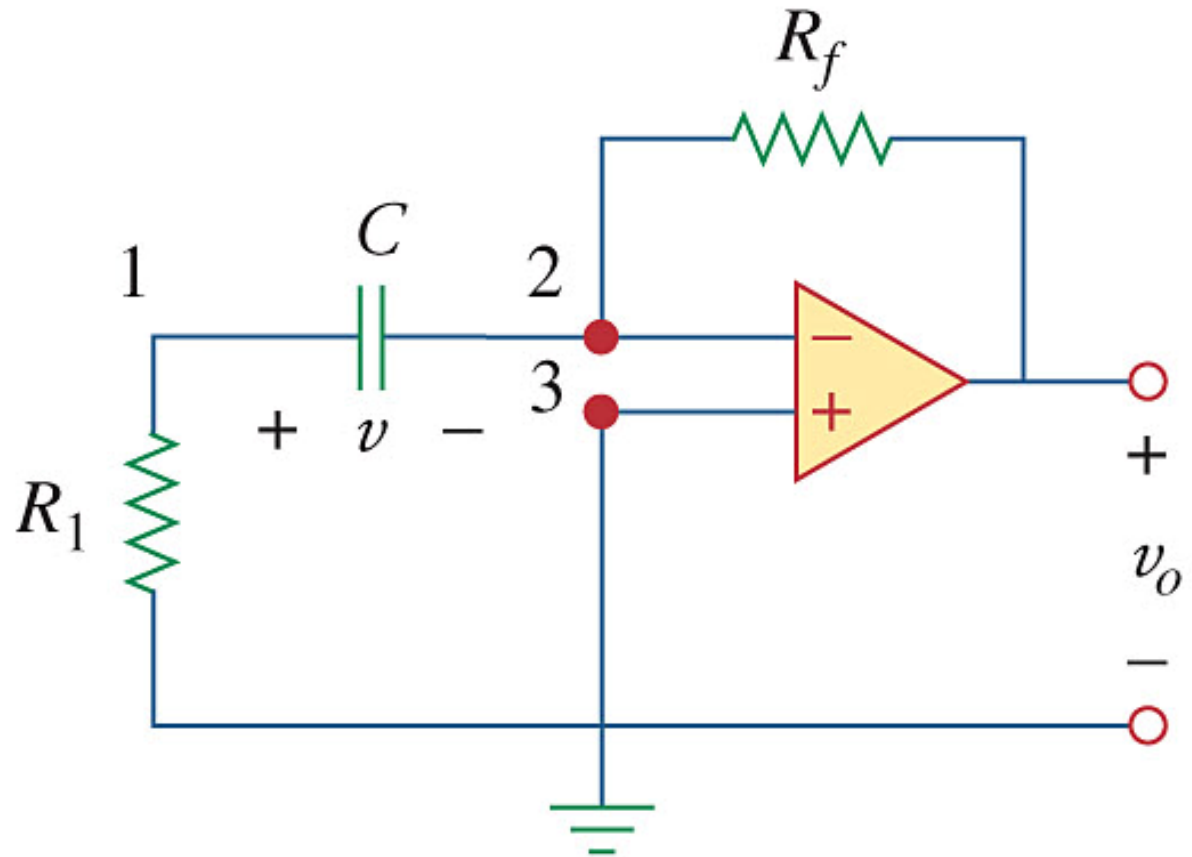


Figure 7.55(a)

$$v_o = -\left(C \frac{dv}{dt}\right) R_f$$

$$= -\left(5 \times 10^{-6} \frac{d}{dt}(3e^{-10t})\right) \times 80 \times 10^3$$

$$= -0.4 \times \left(3 \times (-10e^{-10t})\right)$$

$$= 12e^{-10t} \text{ (V)}$$

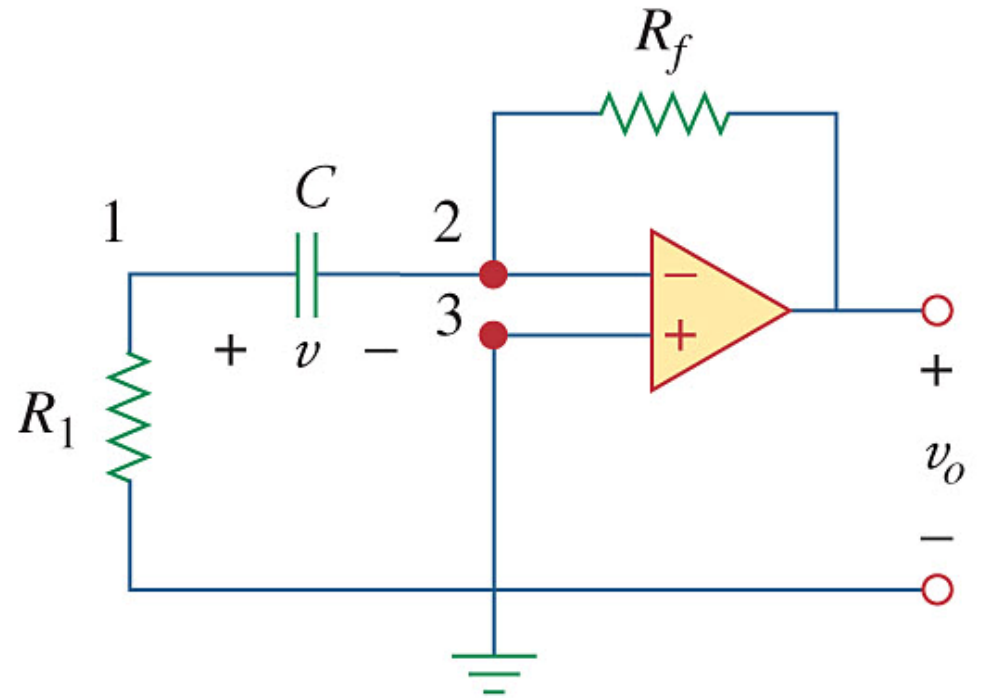


Figure 7.55(a)



## 7.7 First-Order Op Amp Circuits

**Example 7.15** Determine  $v(t)$  and  $v_o(t)$  in the circuit of Fig. 7.57.

**Solution :**

For  $t < 0$ ,

$$v_1(t) = 0, v_o(t) = 0, v(t) = 0$$

$$v(0^-) = 0$$

For  $t > 0$ ,

$$v_1(t) = 3 \times \frac{20}{10 + 20} = 2 \text{ (V)}$$

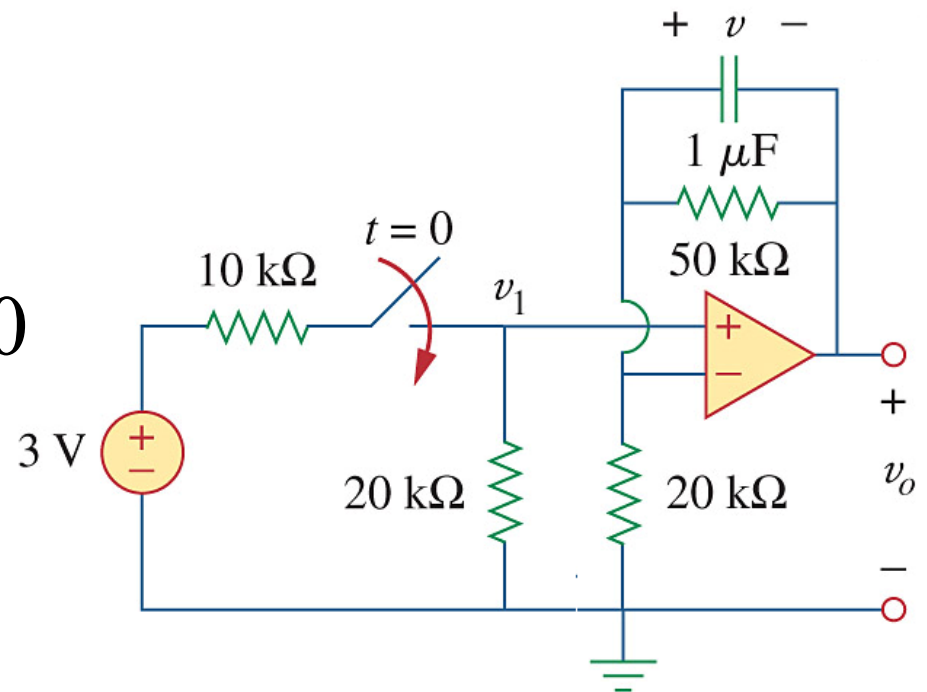


Figure 7.57

# Circuit for $t < 0$

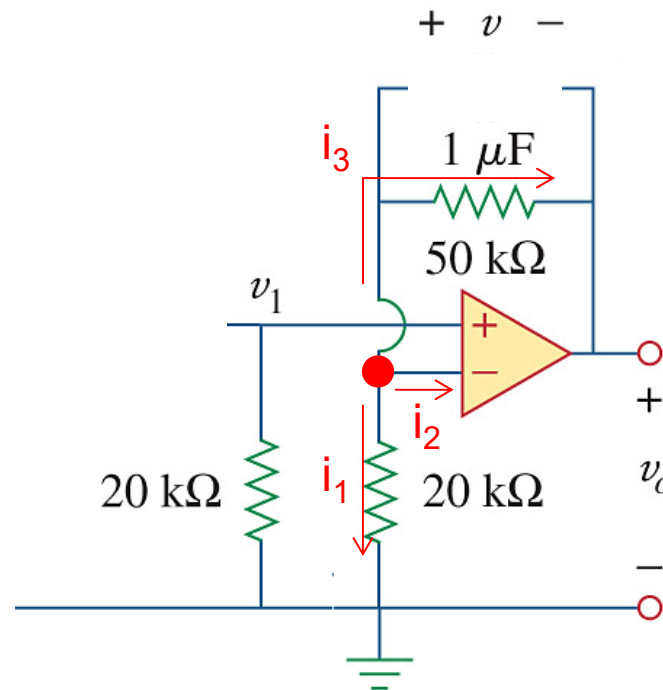


Figure 7.57

$$i_+ = 0 \Rightarrow v_1 = 0 \Rightarrow v_- = 0$$

$$\text{KCL: } i_1 + i_2 + i_3 = 0$$

$$i_1 = 0, i_2 = 0 \Rightarrow i_3 = 0$$

$$v_o(0^+) = -v(0^+) = -v(0^-) = 0$$

$$v_1 = 0$$

OR

Non-inverting amplifier

$$v_o = 0$$

$$\Rightarrow v(0^+) = v(0^-) = 0$$

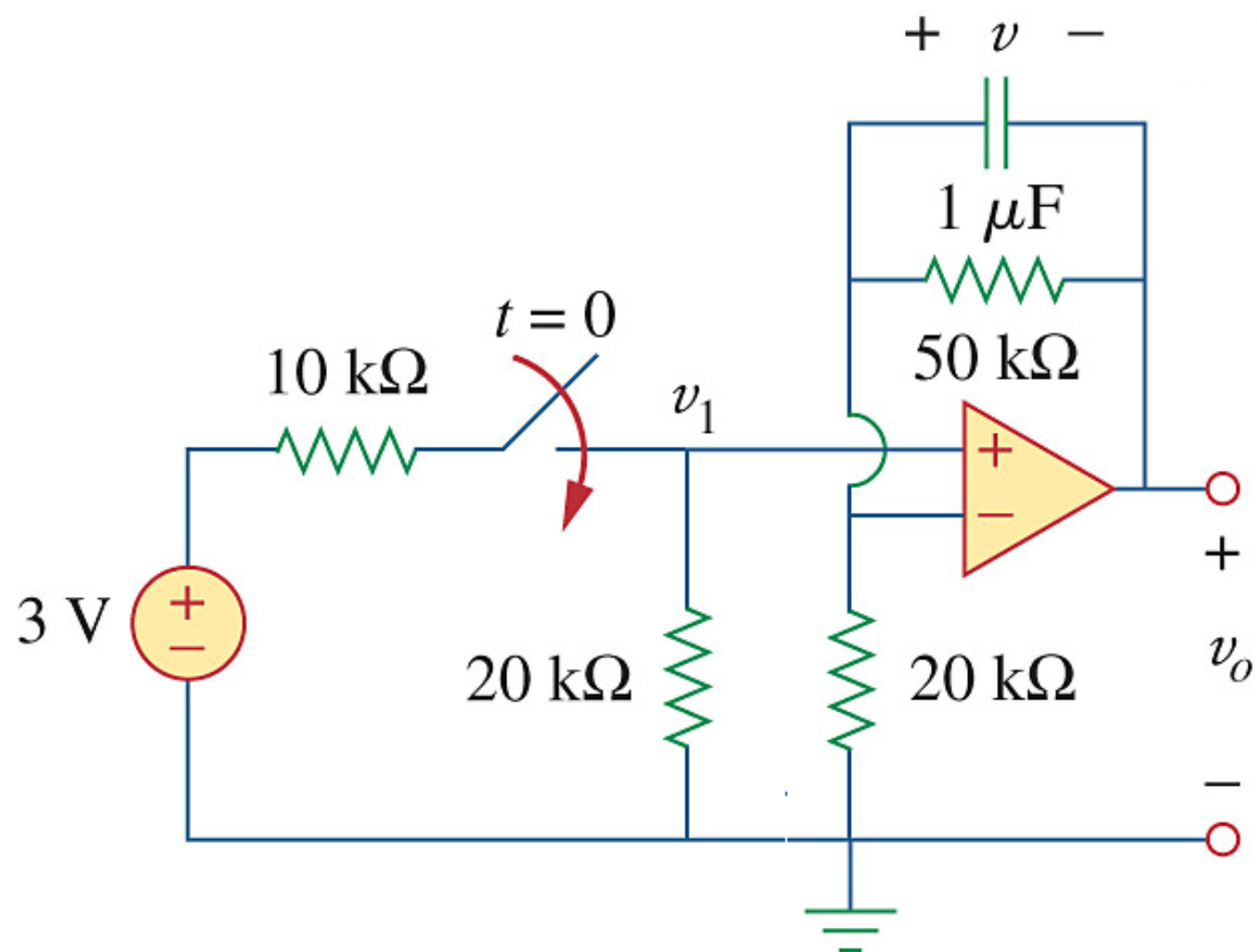


Figure 7.57

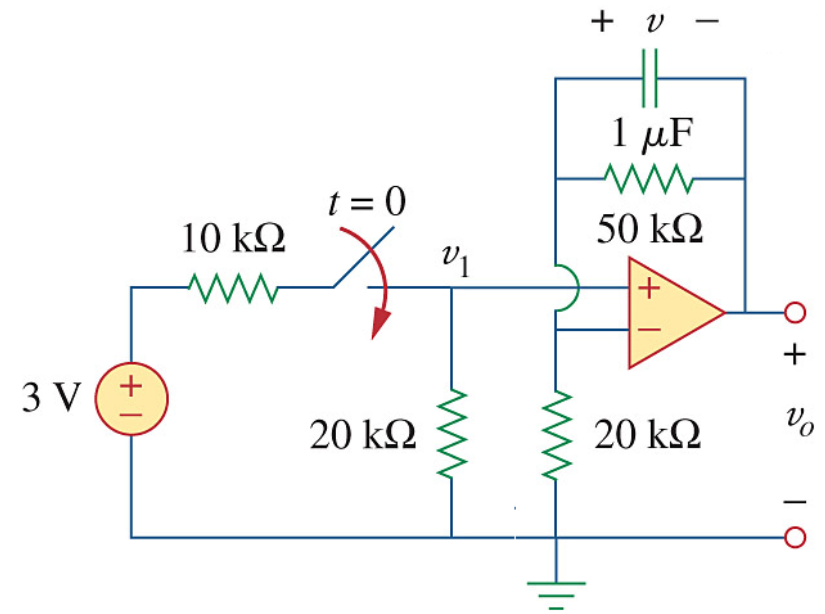


Figure 7.57

$$(1 \times 10^{-6}) \frac{dv}{dt} + \frac{v}{50 \times 10^3} = -\frac{2}{20 \times 10^3}$$

$$\frac{dv}{dt} + 20v = -100$$

$$v(0) = 0$$

$$v(\infty) = v_1(\infty) - v_o(\infty) = 2 - 2(1 + 5/2) = -5$$

$$v(t) = Ae^{-20t} + B = 5e^{-20t} - 5 \text{ (V)}$$

$$v_o(t) = -v(t) + 2 = 7 - 5e^{-20t} \text{ (V)}$$

## 7.9 Applications

**7.9.1. Delay Circuits** An  $RC$  circuit can be used to provide various delays. Figure 7.73 show a *glow - lamp relaxation oscillator* circuit.

In operation,  $C$  charges through  $R_1 + R_2$  until the breakdown voltage (70 V) of the neon lamp is reached.

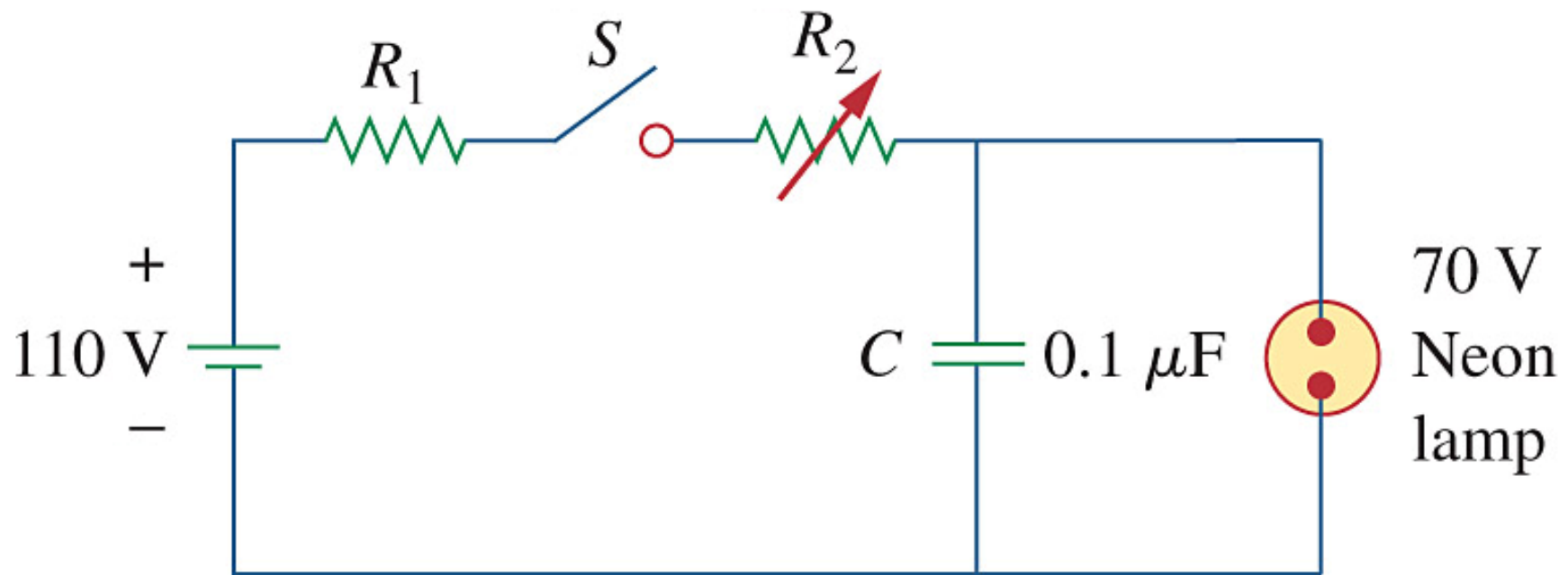


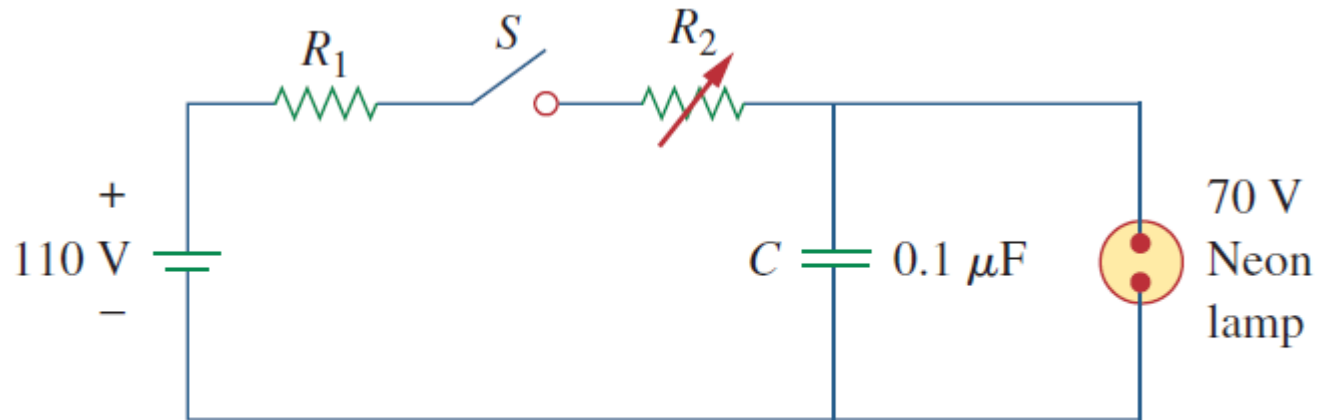
Figure 7.23 An  $RC$  delay circuit. The lamp acts as an open circuit until the voltage across it exceeds the breakdown voltage. When the voltage level is reached, the lamp becomes highly conductive and glows with a characteristic color.

At that point,  $C$  discharges through the lamp and produces an orange flash.

When the voltage across  $C$  drops below the voltage necessary to keep the lamp conducting, say 50 V, the lamp goes dark. Then  $C$  begins to charge and the cycle repeats.

To see the neon-lamp flash,  $R_1 + R_2$  should be greater than  $1\text{ M}\Omega$ . Otherwise the flash rate will be faster than the 18 pulses per second discernible by the human eye and the lamp will appear continuously on.





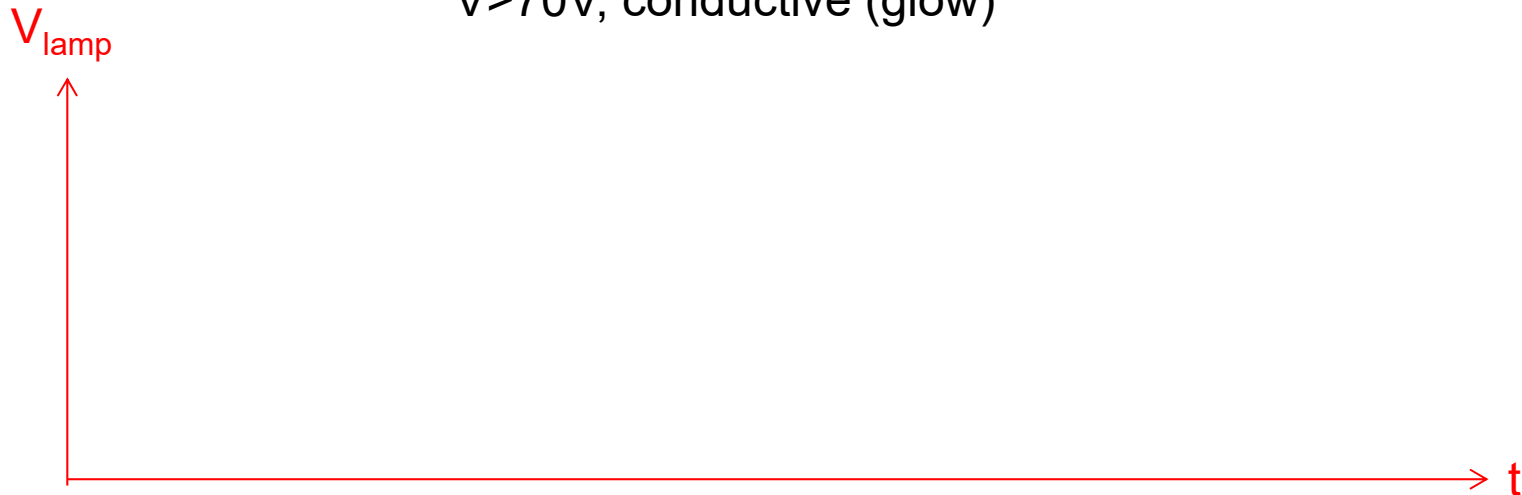
**Figure 7.73**

An  $RC$  delay circuit.

**Lamp:**

$V < 50\text{V}$ , lamp open circuit (dark)

$V > 70\text{V}$ , conductive (glow)



**Example 7.19** Consider the circuit in Fig. 7.73, and assume that  $R_1 = 1.5 \text{ M}\Omega$ ,  $0 < R_2 < 2.5 \text{ M}\Omega$ . (a) Calculate the extreme limits of the time constant of the circuit. (b) How long does it take for the lamp to glow for the first time after the switch is closed? Let  $R_2$  assume its largest value.

**Solution :**

$$(a) \tau = (R_1 + R_2)C$$

$$\tau_{\min} = (1.5 \times 10^6 + 0) \times 0.1 \times 10^{-6} \\ = 0.15 \text{ (s)}$$

$$\tau_{\max} = (1.5 \times 10^6 + 2.5 \times 10^6) \times 0.1 \times 10^{-6} \\ = 0.4 \text{ (s)}$$

$$(b) \ v_C(0^+) = 0, \ v_C(\infty) = 110 \text{ V}, \ \tau = 0.4 \text{ s}$$

$$v_C(t) = v_C(\infty) + [v_C(0^+) - v_C(\infty)]e^{-t/\tau}$$

$$t = \tau \ln \left( \frac{v_C(0^+) - v_C(\infty)}{v_C(t) - v_C(\infty)} \right)$$

$$= 0.4 \ln \left( \frac{0 - 110}{70 - 110} \right) \approx 0.4046 \text{ (s)}$$

The lamp glows after the switch is closed for 0.4046 seconds.

**7.9.2 Photoflash Unit** Figure 7.75 shows a simplified circuit. It consists of a high-voltage dc supply, a current-limiting large resistor  $R_1$ , and a capacitor  $C$  in parallel with the flashlamp of low resistance  $R_2$ .

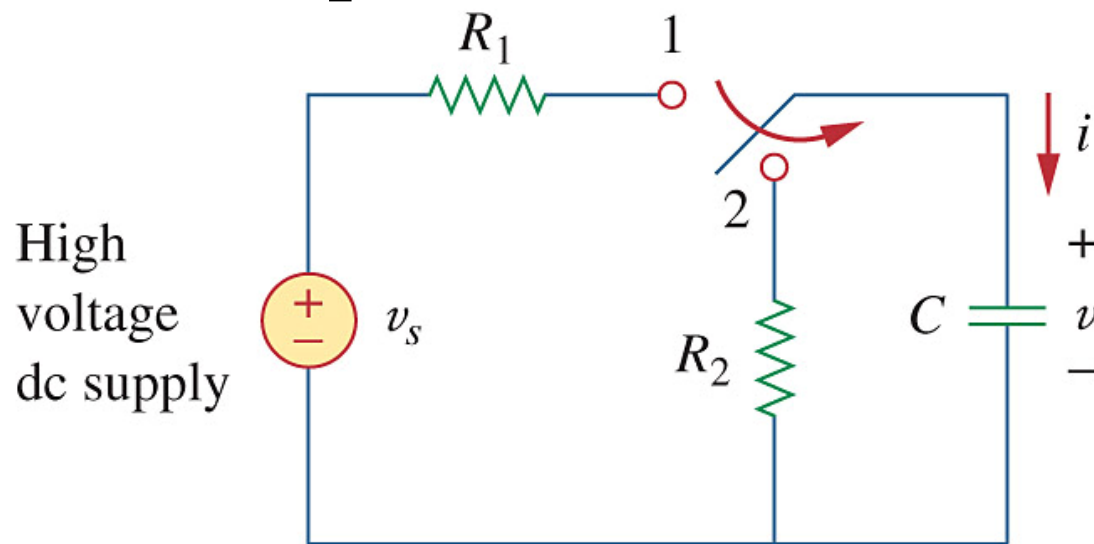


Figure 7.75 Circuit for a flash unit providing slow charge in position 1 and fast discharge in position 2.

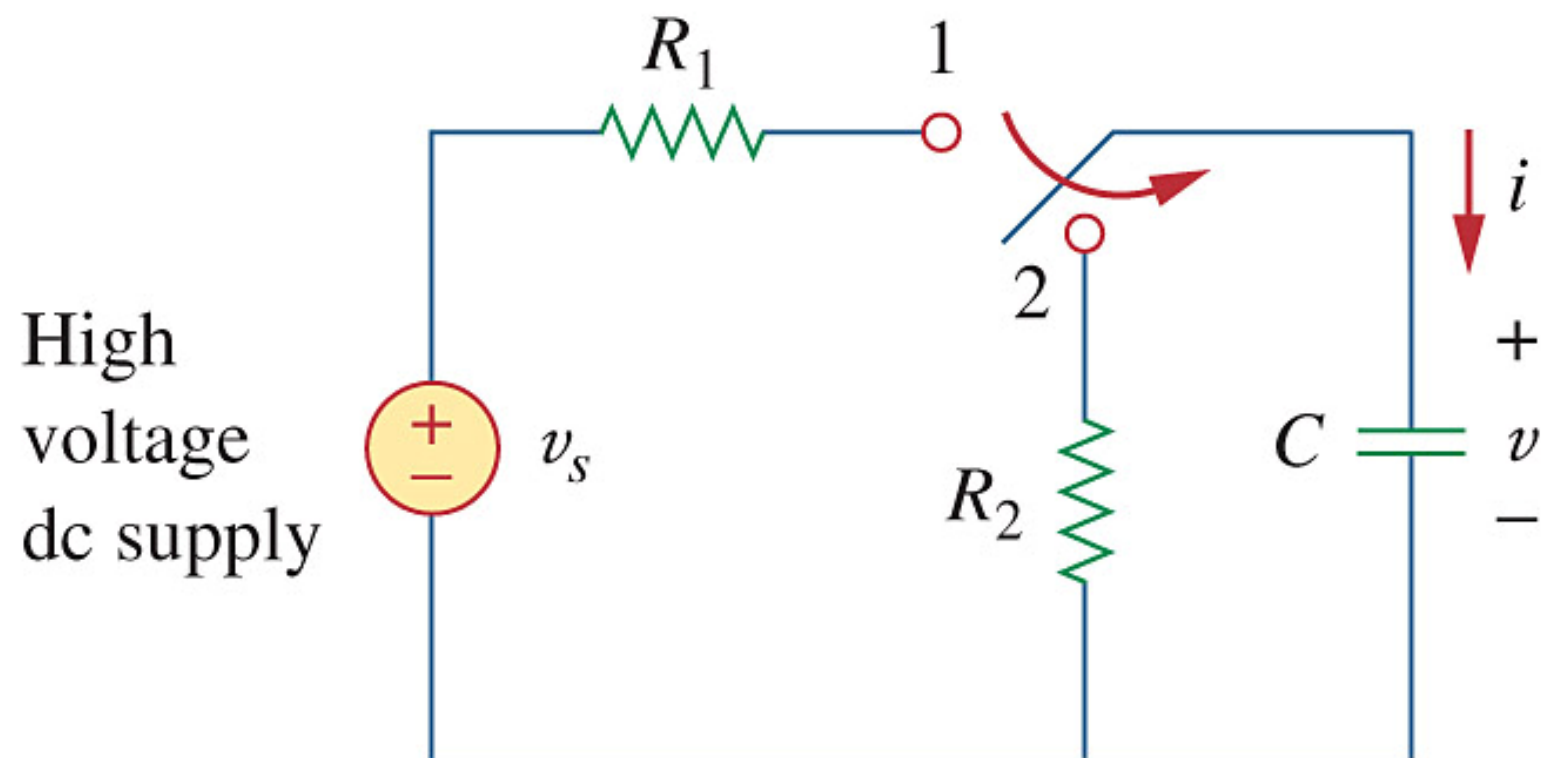


Figure 7.75 Circuit for a flash unit providing slow charge in position 1 and fast discharge in position 2.

When the switch is in position 1,  $C$  charges. As shown in Fig. 7.76, the capacitor voltage rises gradually from zero to  $V_s$ , while its current decreases gradually from  $I_1 = V_s / R_1$  to zero. The charging time is approximately

$$t_{\text{charge}} = 5R_1C$$

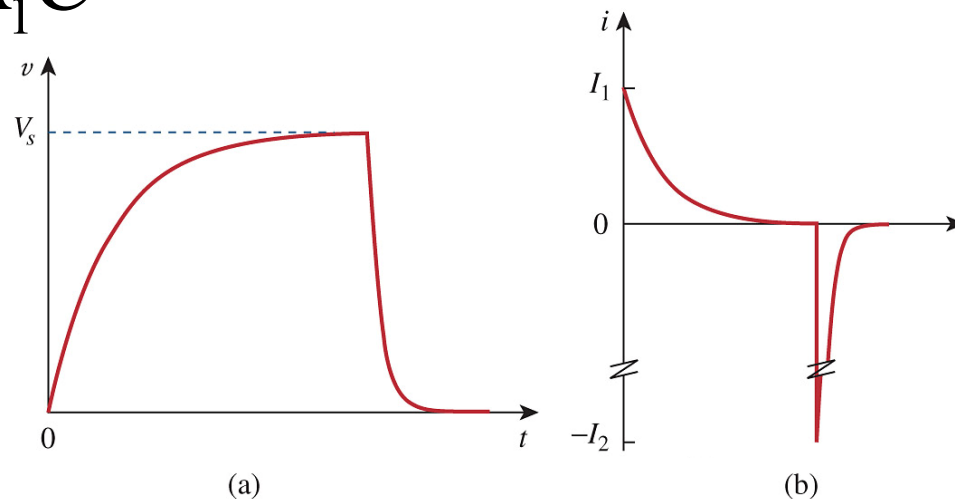


Figure 7.76 (a) Capacitor voltage showing slow charge and fast discharge, (b) capacitor current showing low charging current  $I_1$  and high discharge current  $I_2$ .

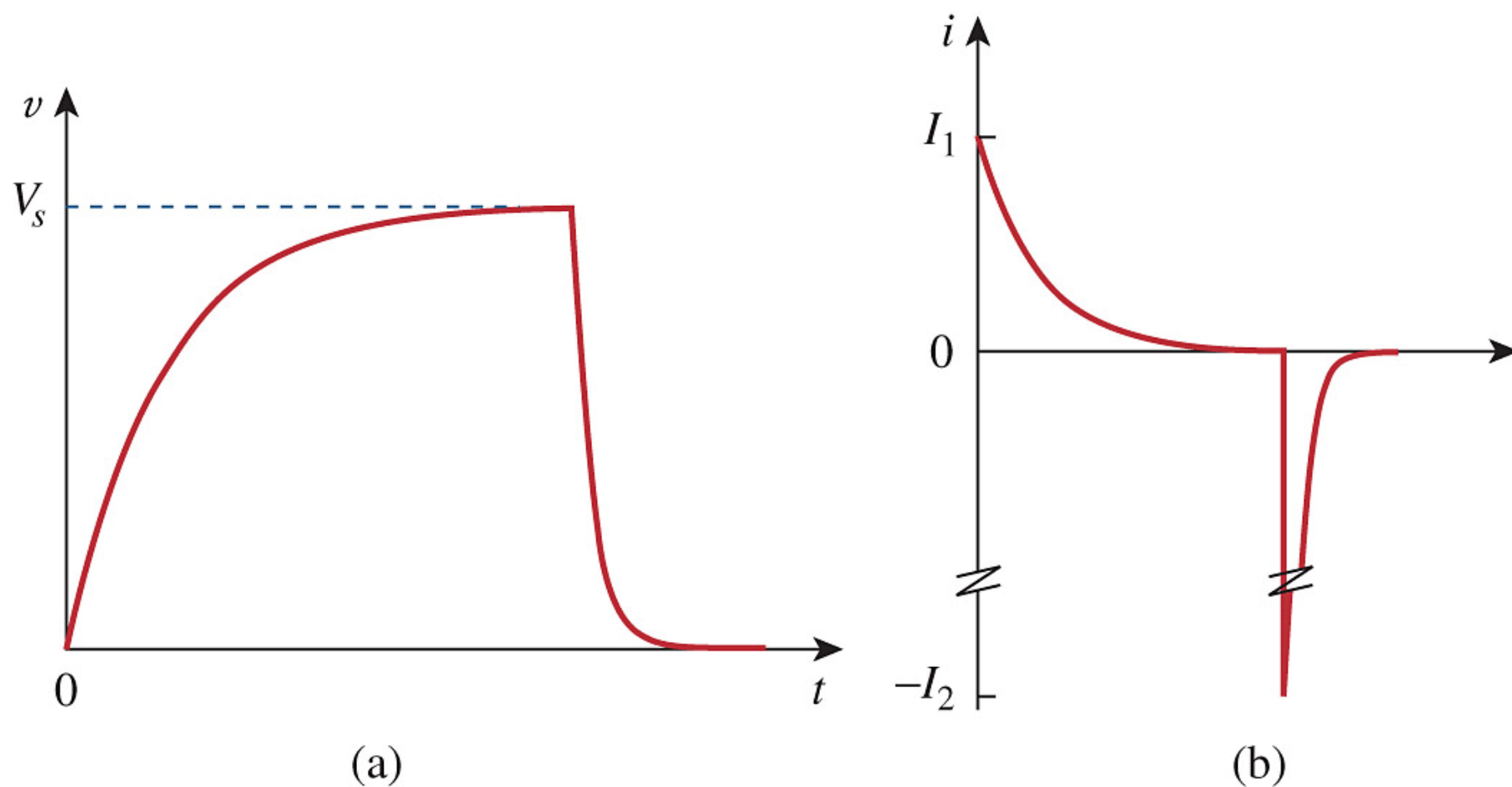


Figure 7.76 (a) Capacitor voltage showing slow charge and fast discharge, (b) capacitor current showing low charging current  $I_1$  and high discharge current  $I_2$ .



With the switch in position 2,  $C$  is discharged. The low resistance  $R_2$  of the photolamp permits a high discharge current with peak  $I_2 = V_s / R_2$  in a short duration. Discharging takes place in approximately

$$t_{\text{discharge}} = 5R_2C$$

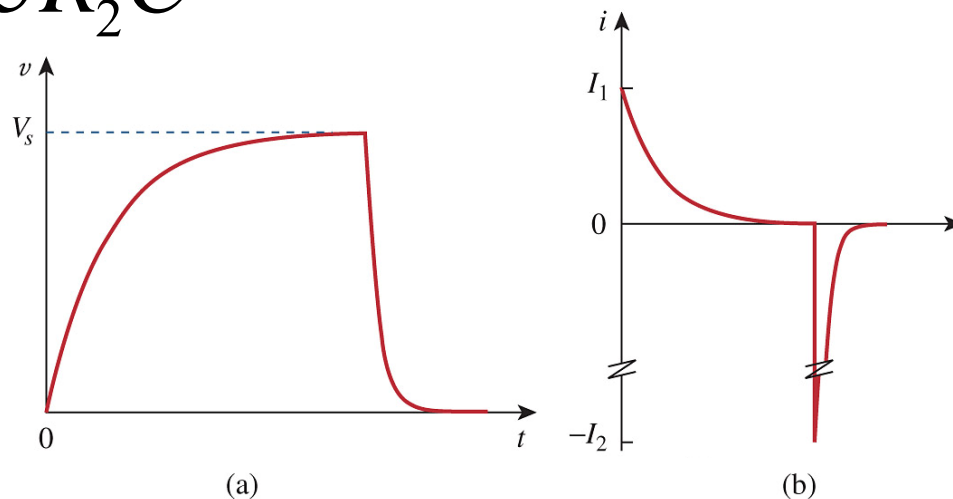


Figure 7.76 (a) Capacitor voltage showing slow charge and fast discharge, (b) capacitor current showing low charging current  $I_1$  and high discharge current  $I_2$ .