

Introduction to Signals and Systems: V216

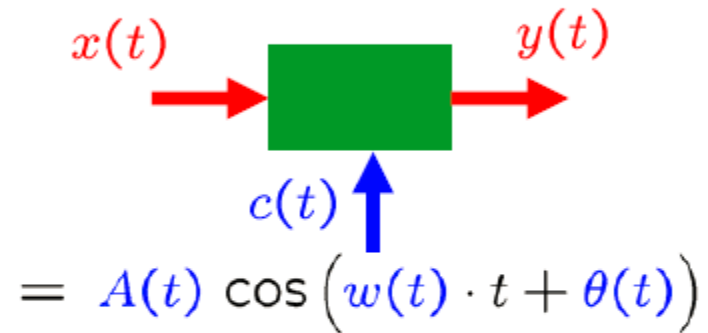
Lecture #13

Chapter 8: Communication Systems

Modulation and Demodulation

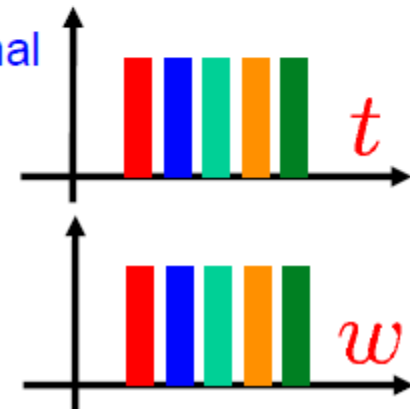
■ Modulation & Demodulation:

- M: Embedding an information-bearing signal into a second signal
- D: Extracting the information-bearing signal
- Methods:
 - > Amplitude Modulation (AM)
 - > Frequency Modulation (FM)



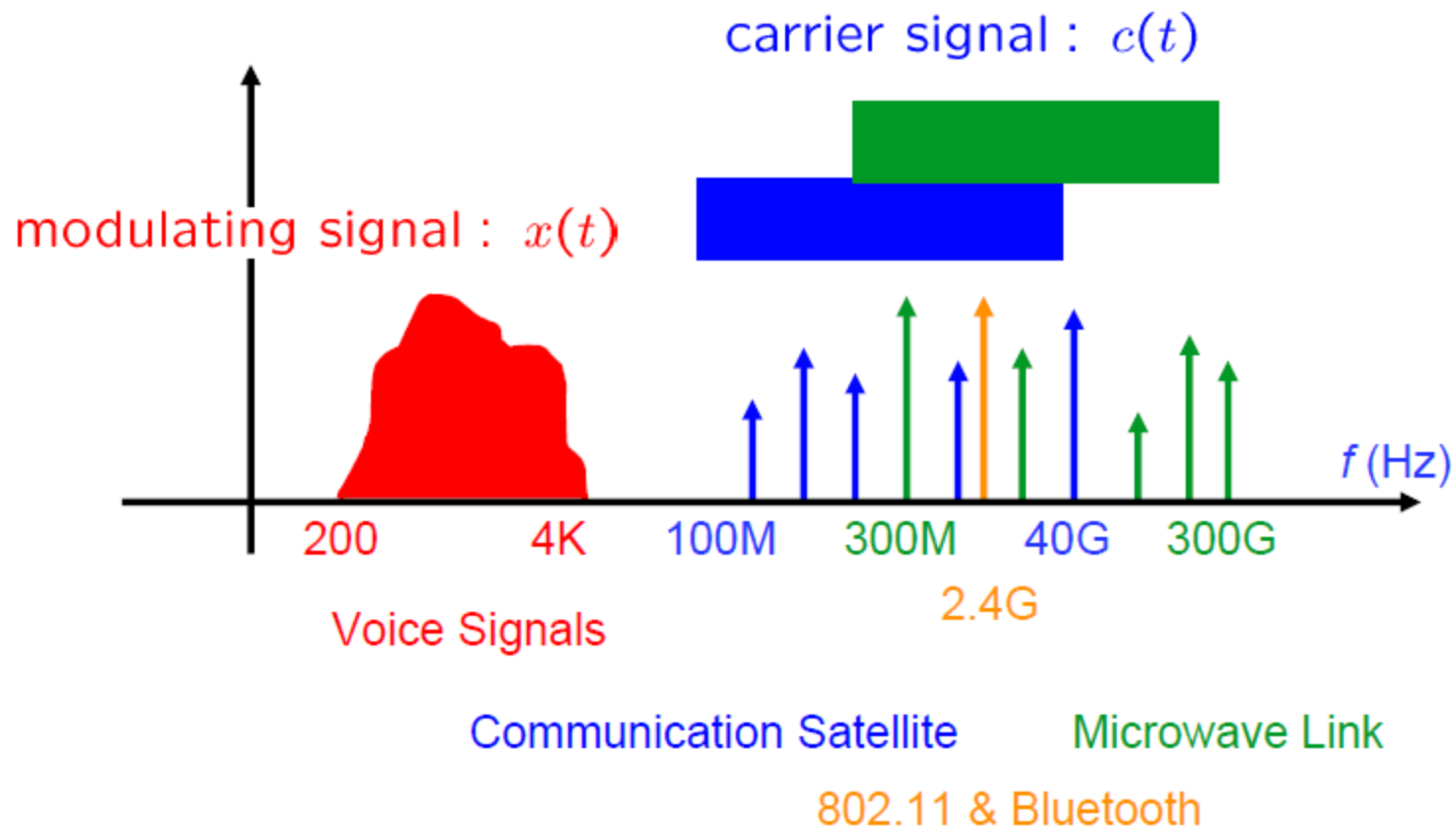
■ Multiplexing & Demultiplexing:

- Simultaneous transmission of more than one signal with overlapping spectra over the same channel
- Methods:
 - > Time-Division Multiplexing (TDM)
 - > Frequency-Division Multiplexing (FDM)



Modulation and Demodulation

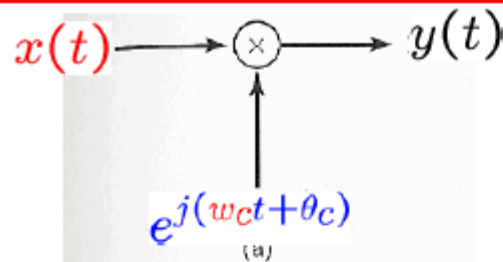
- Signal Frequency Characteristics:



modulated signal : $y(t) = x(t) c(t)$

AM Modulation

■ AM with a Complex Exponential Carrier:

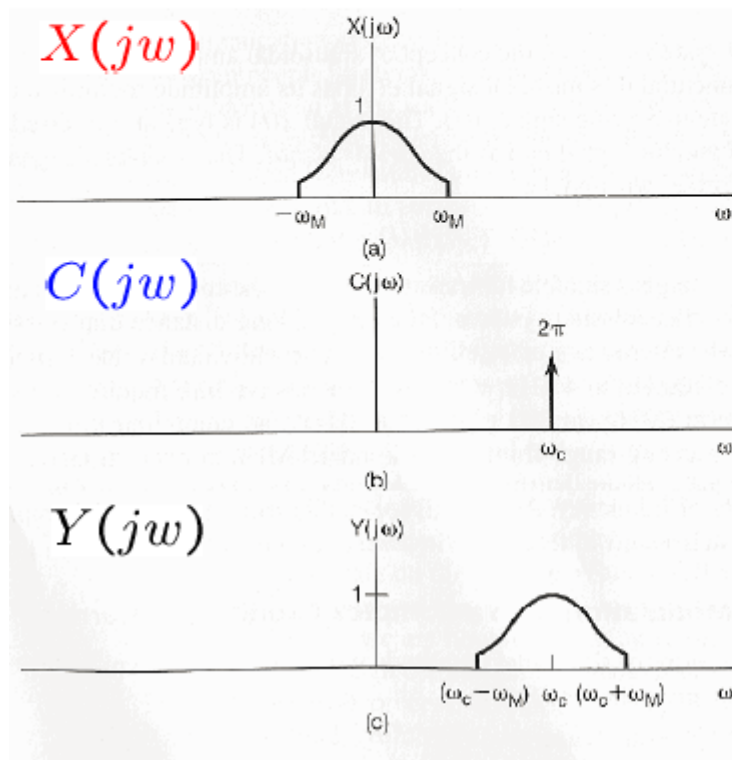


ω_c : carrier frequency

$$c(t) = e^{j(\omega_c t + \theta_c)}$$

$$y(t) = x(t) c(t) = x(t) e^{j\omega_c t}$$

$$\theta_c = 0$$



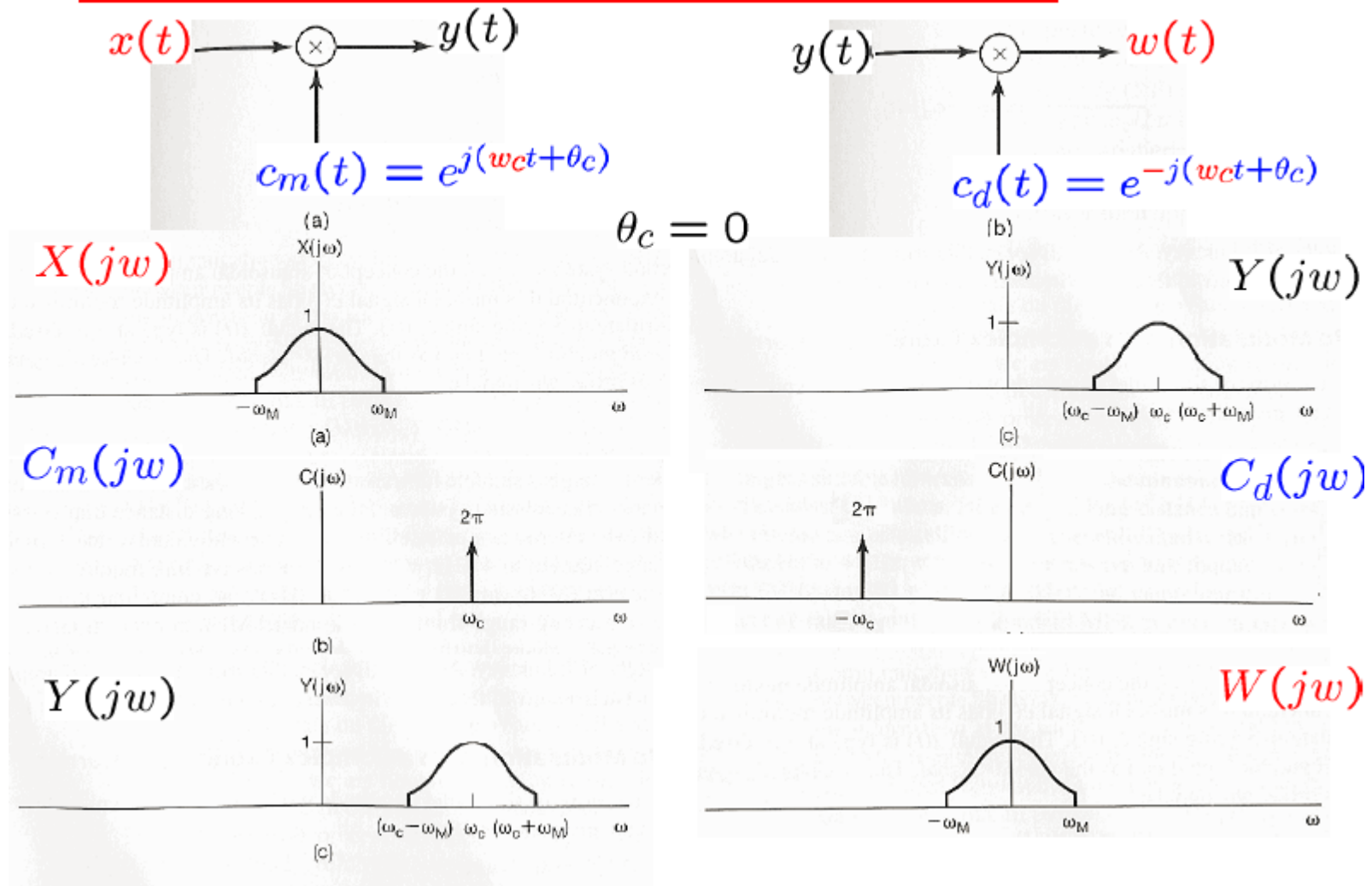
$$C(j\omega) = 2\pi \delta(\omega - \omega_c)$$

$$Y(j\omega) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} X(j\theta) C(j(\omega - \theta)) d\theta$$

$$Y(j\omega) = X(j(\omega - \omega_c))$$

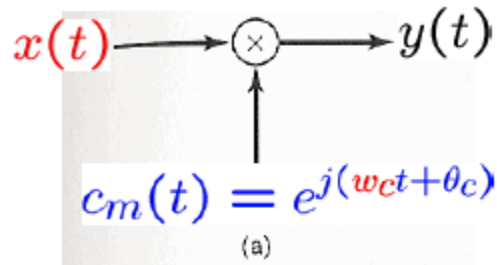
AM Modulation

■ AM with a Complex Exponential Carrier:

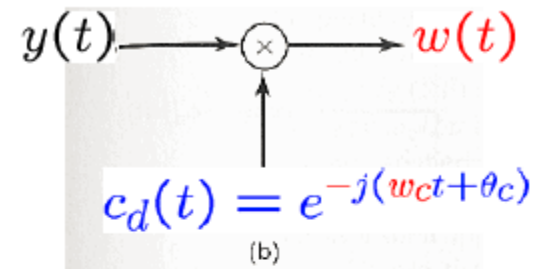


AM Modulation

- AM with a Complex Exponential Carrier:



$$\theta_c = 0$$



$$\begin{aligned} y(t) &= x(t) c_m(t) \\ &= x(t) e^{j w_c t} \end{aligned}$$

$$\begin{aligned} w(t) &= y(t) c_d(t) \\ &= y(t) e^{-j w_c t} \\ &= x(t) e^{j w_c t} e^{-j w_c t} \end{aligned}$$

$$\Rightarrow w(t) = x(t)$$

$$Y(jw) = X(j(w - w_c))$$

$$W(jw) = Y(j(w + w_c))$$

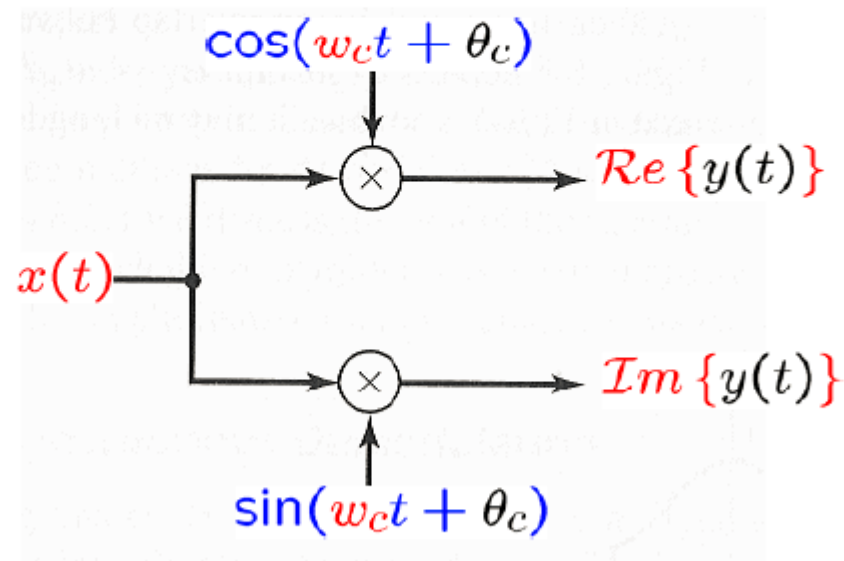
$$\Rightarrow W(jw) = X(jw)$$

AM Modulation

- AM with Sinusoidal Carriers:

$$c(t) = e^{j\omega_c t} = \cos(\omega_c t) + j \sin(\omega_c t)$$

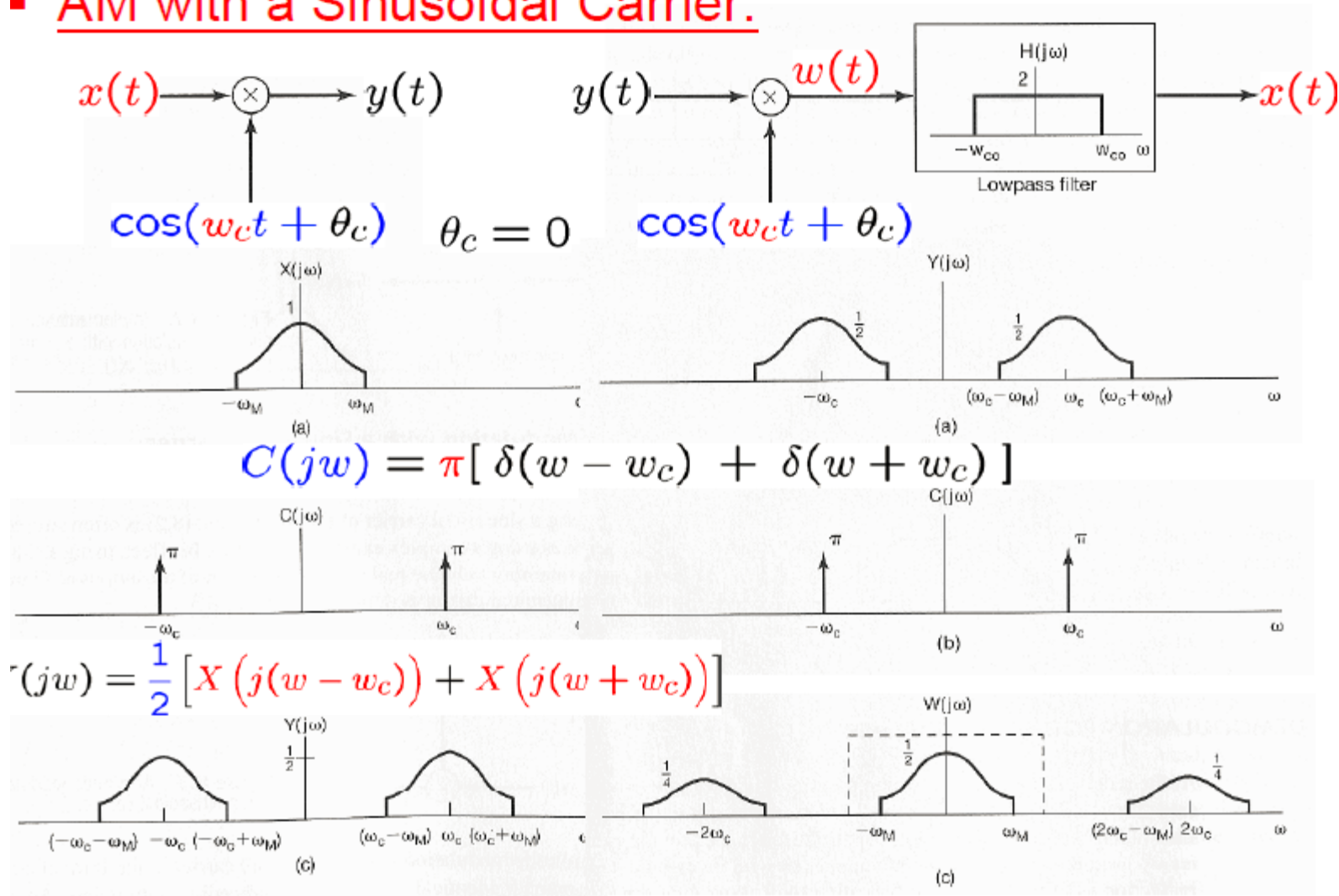
$$\Rightarrow y(t) = x(t) \cos(\omega_c t) + j x(t) \sin(\omega_c t)$$



phase difference of $c_1(\cdot), c_2(\cdot)$?

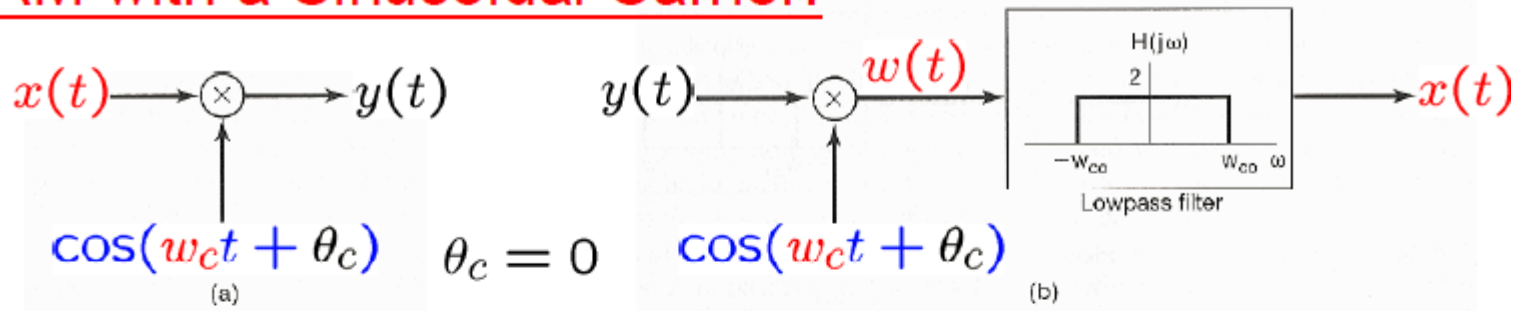
AM Modulation

AM with a Sinusoidal Carrier:



AM Modulation

- AM with a Sinusoidal Carrier:



$$y(t) = x(t) \cos(w_c t)$$

$$w(t) = y(t) \cos(w_c t)$$

$$\Rightarrow w(t) = x(t) \cos^2(w_c t)$$

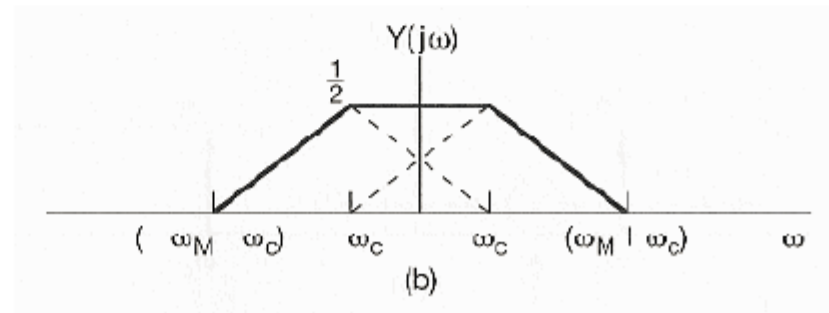
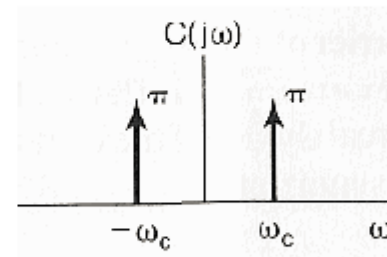
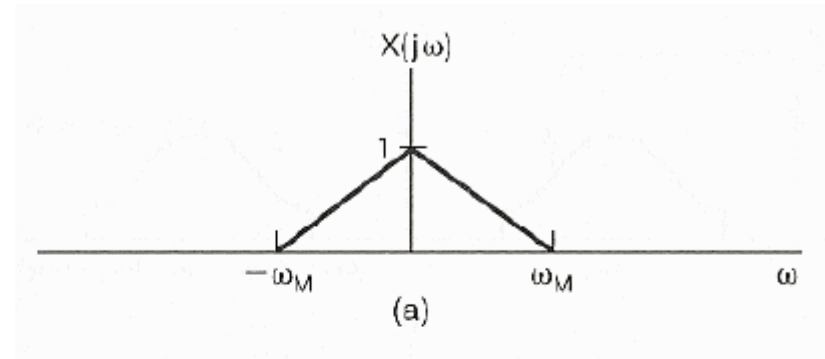
$$= x(t) \left[\frac{1}{2} + \frac{1}{2} \cos(2w_c t) \right]$$

$$= \frac{1}{2} x(t) + \frac{1}{2} x(t) \cos(2w_c t)$$

AM Modulation

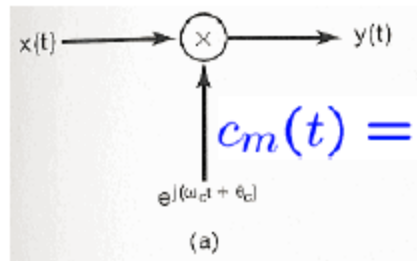
■ Overlapping of AM with a Sinusoidal Carrier:

- If $\omega_c < \omega_M$,



AM Demodulation

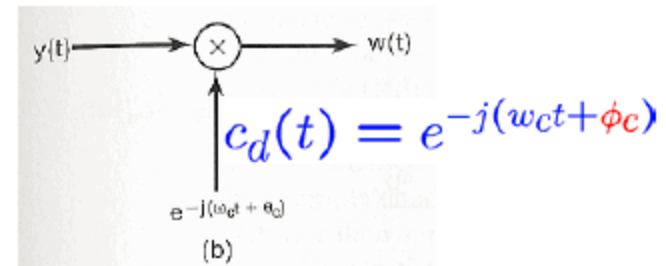
- Not Synchronized in Phase:



$$y(t) = x(t) c_m(t)$$

$$= x(t) e^{j(\omega_c t + \theta_c)}$$

$$\theta_c \neq \phi_c$$



$$w(t) = y(t) c_d(t)$$

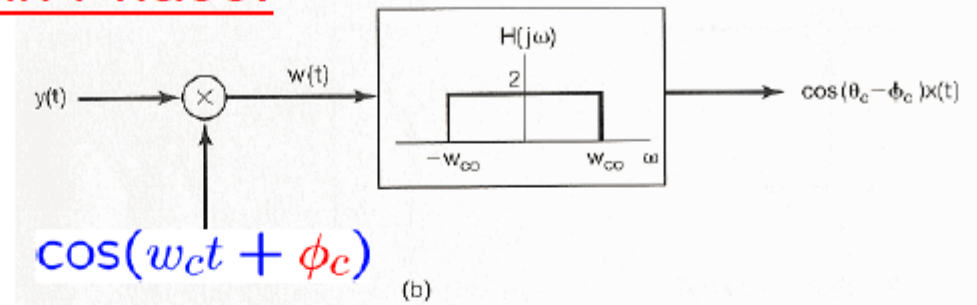
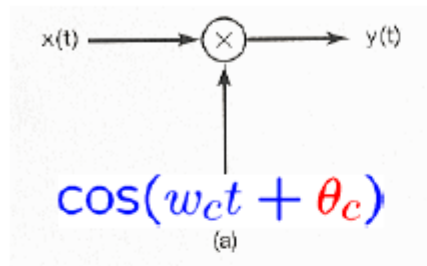
$$= y(t) e^{-j(\omega_c t + \phi_c)}$$

$$= x(t) e^{j(\theta_c - \phi_c)}$$

$$\Rightarrow \text{ONLY } |x(t)| = |w(t)|$$

AM Demodulation

- Not Synchronized in Phase:



$$y(t) = x(t) \cos(w_c t + \theta_c) \qquad w(t) = y(t) \cos(w_c t + \phi_c)$$

$$\Rightarrow w(t) = x(t) \cos(w_c t + \theta_c) \cos(w_c t + \phi_c)$$

$$= x(t) \left[\frac{1}{2} \cos(\theta_c - \phi_c) + \frac{1}{2} \cos(2w_c t + \theta_c + \phi_c) \right]$$

$$= \frac{1}{2} \cos(\theta_c - \phi_c) x(t) + \frac{1}{2} x(t) \cos(2w_c t + \theta_c + \phi_c)$$

AM Modulator for Asynchronous Modulation-Demodulation System

AM In standard AM, the carrier signal $c(t)$ has its amplitude multiplied (modulated) by the quantity $x(t) + A$

where

$$|x(t)| < A$$

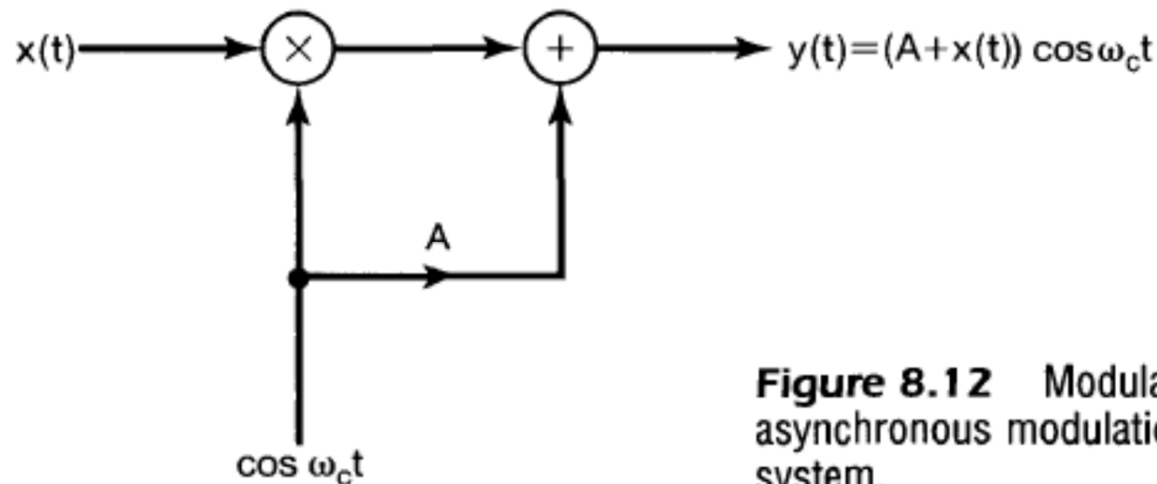
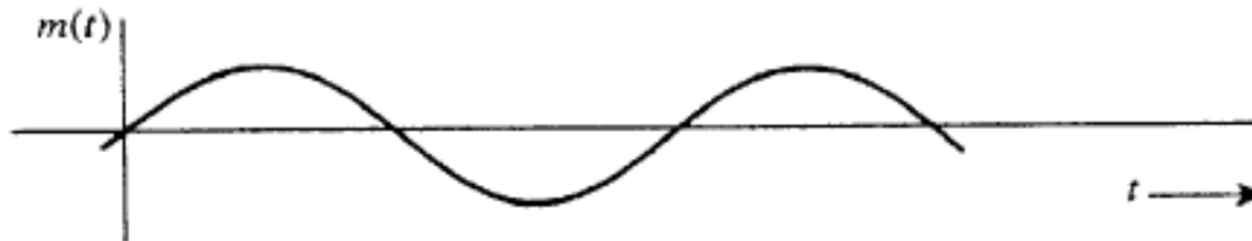
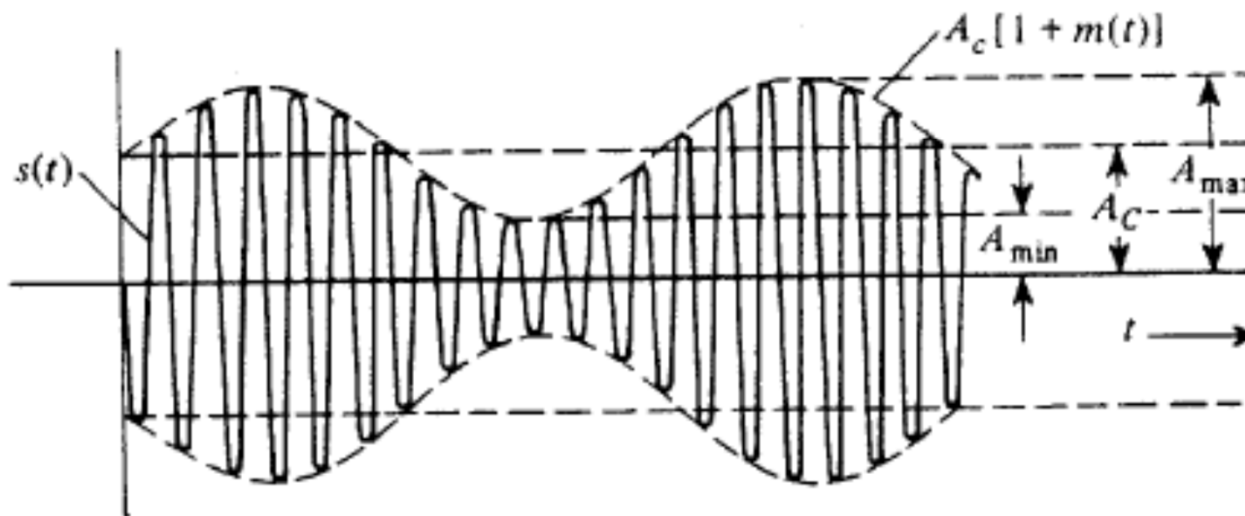


Figure 8.12 Modulator for an asynchronous modulation-demodulation system.

AM Modulator for Asynchronous Modulation-Demodulation System



(a) Sinusoidal Modulating Wave



(b) Resulting AM Signal

AM signal waveform

AM Demodulation

■ Asynchronous Demodulation:

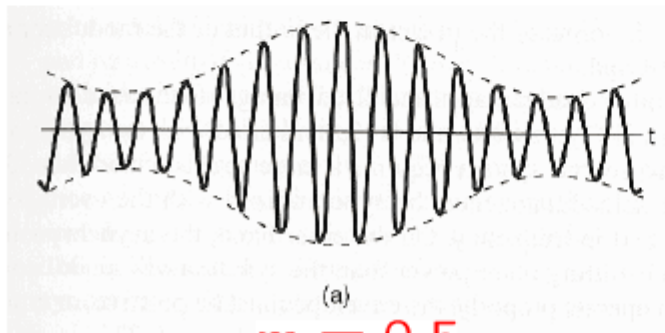
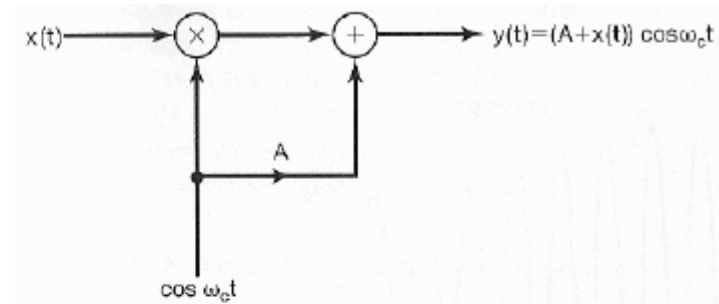
- $\omega_c \gg \omega_M$

- $x(t) > 0, \forall t$

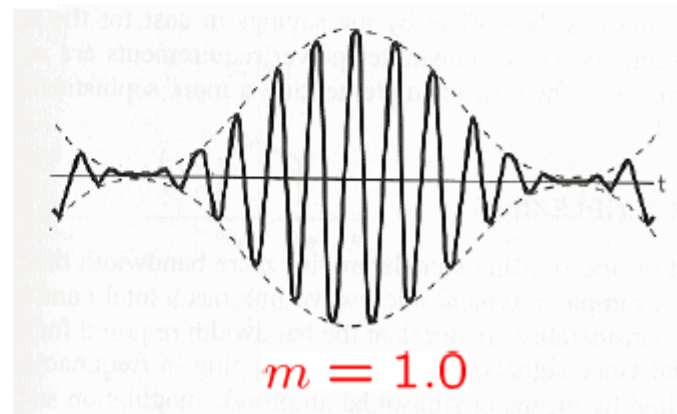
If not, $x(t) \rightarrow x(t) + A > 0$

$$A \geq K, |x(t)| \leq K$$

- $\frac{K}{A}$: modulation index m , in %



$$m = 0.5$$



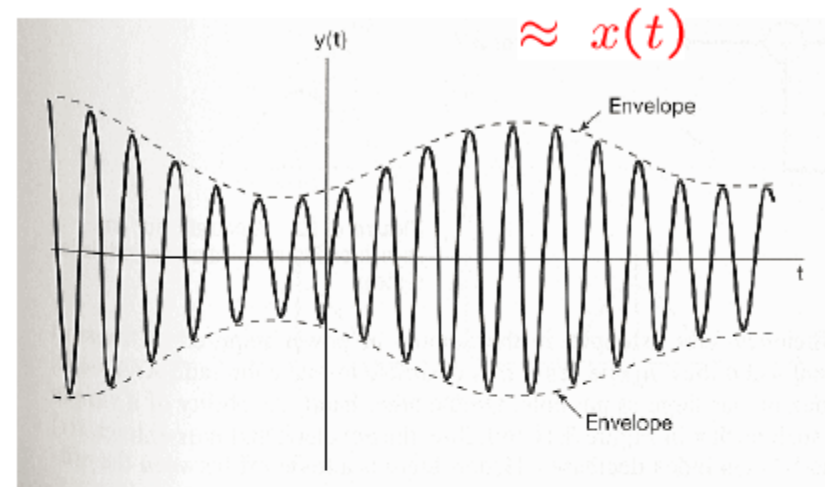
$$m = 1.0$$

AM Demodulation

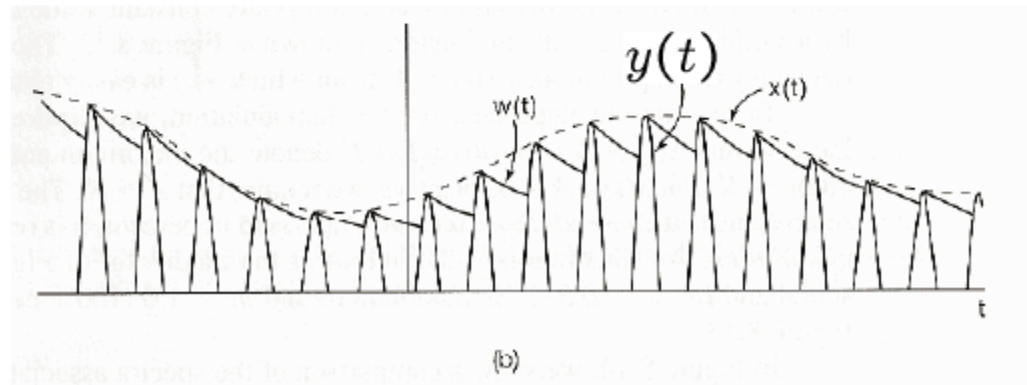
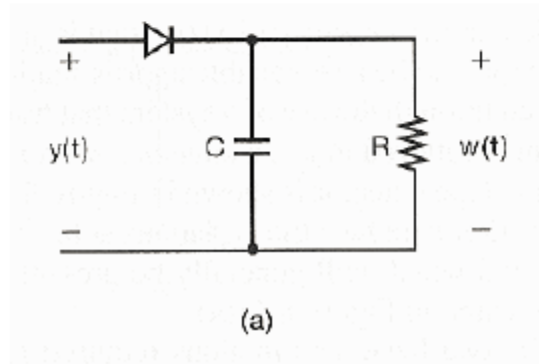
- Asynchronous Demodulation: $y(t) = x(t) \cos(\omega_c t + \theta_c)$

- $\omega_c \gg \omega_M$

- $x(t) > 0, \forall t$



- Envelope Detector:



AM Modulator for Asynchronous Modulation-Demodulation System

The modulated signal $y(t)$ has the general form illustrated in Fig. 8.10.

$$y(t) = [x(t) + A] \cos(\omega_c t) = x(t) \cos \omega_c t + A \cos \omega_c t$$

$$Y(j\omega) = \frac{1}{2} [X(j(\omega - \omega_c)) + X(j(\omega + \omega_c))] + \pi A [\delta(\omega - \omega_c) + \delta(\omega + \omega_c)]$$

In Fig. 8.14, we show a comparison of the spectra associated with the DSB-SC signal and AM signal.

AM Modulator for Asynchronous Modulation-Demodulation System

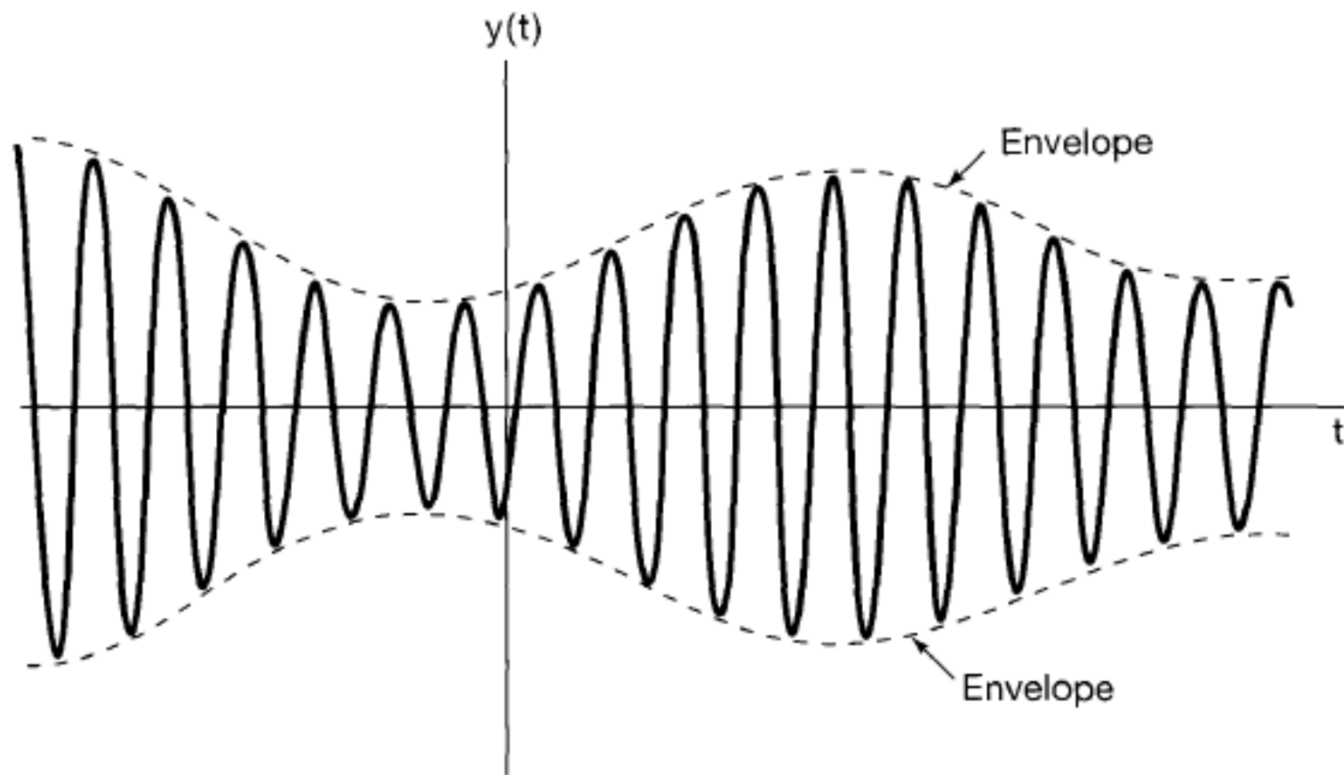


Figure 8.10 Amplitude-modulated signal.
The dashed curve represents the envelope of
the modulated signal.

AM Modulator for Asynchronous Modulation-Demodulation System

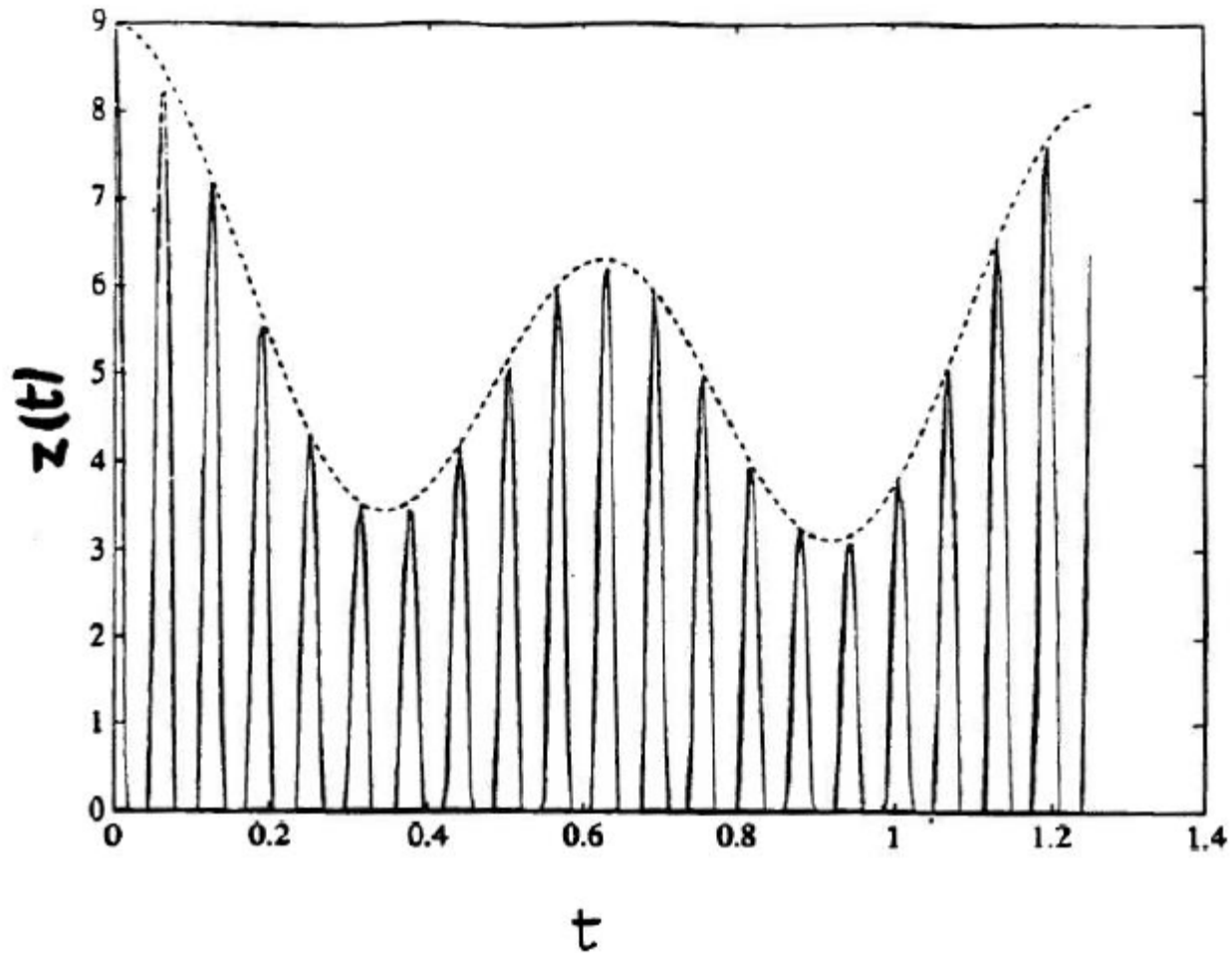
Suppose we receive the radio signal

$$y(t) = [x(t) + A] \cos(\omega_c t)$$

How can we recover $x(t)$? Lets "rectify" $y(t)$ by using a "half-wave rectifier" with the following input-output relation

$$z(t) = \begin{cases} y(t), & y(t) > 0 \\ 0, & y(t) < 0 \end{cases}$$

AM Modulator for Asynchronous Modulation-Demodulation System



AM Modulator for Asynchronous Modulation-Demodulation System

Since $[x(t) + A] > 0$, we can write

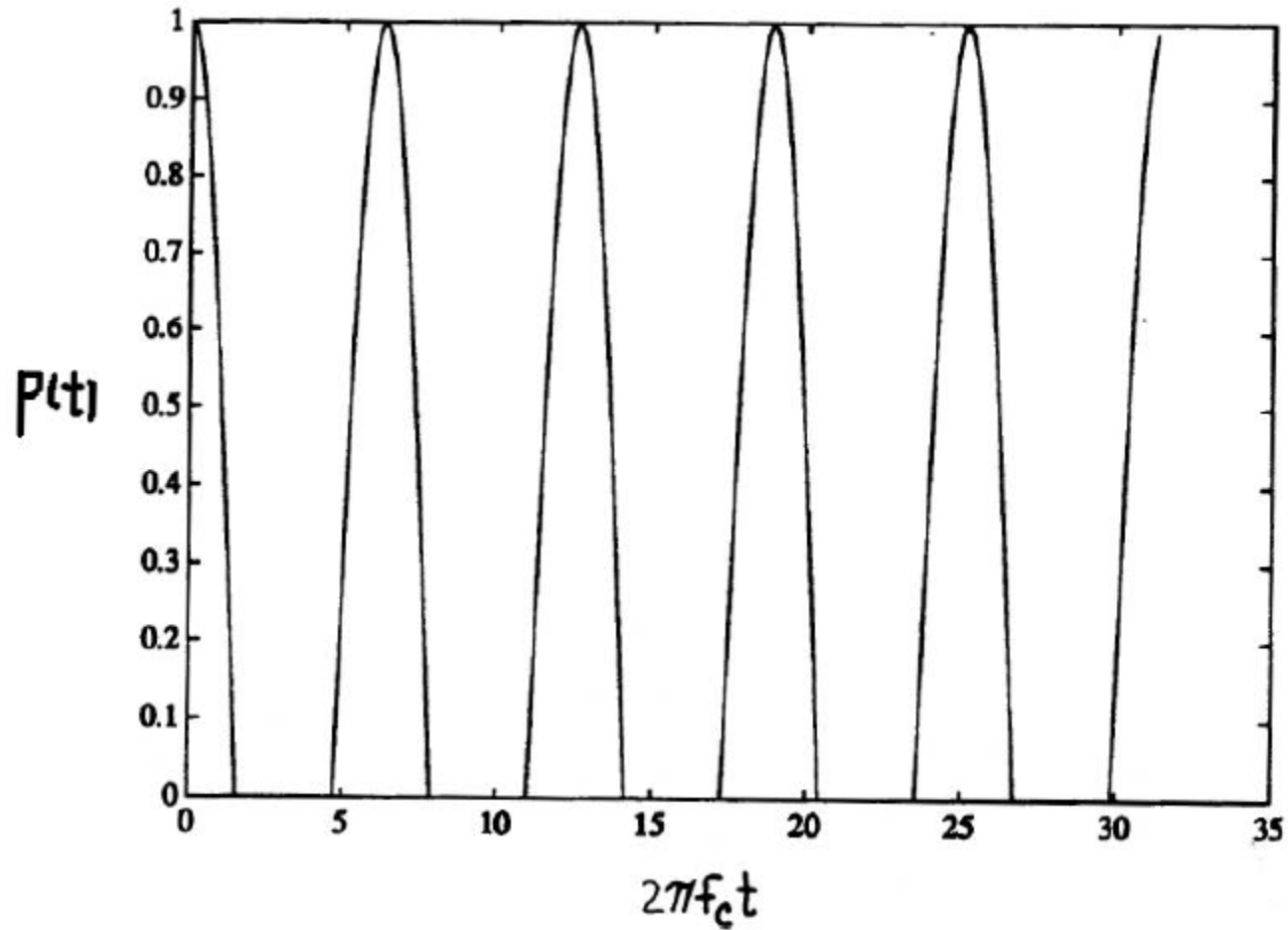
$$z(t) = \begin{cases} [x(t) + A] \cos(\omega_c t), & \cos(\omega_c t) > 0 \\ 0, & \cos(\omega_c t) < 0 \end{cases}$$

$$= [x(t) + A] p(t)$$

where

$$p(t) = \begin{cases} \cos(\omega_c t), & \cos(\omega_c t) > 0 \\ 0, & \cos(\omega_c t) < 0 \end{cases}$$

AM Modulator for Asynchronous Modulation-Demodulation System



AM Modulator for Asynchronous Modulation-Demodulation System

Note that $p(t)$ is a periodic function with

$T = 2\pi / \omega_c$. Thus $p(t)$ has an FS representation

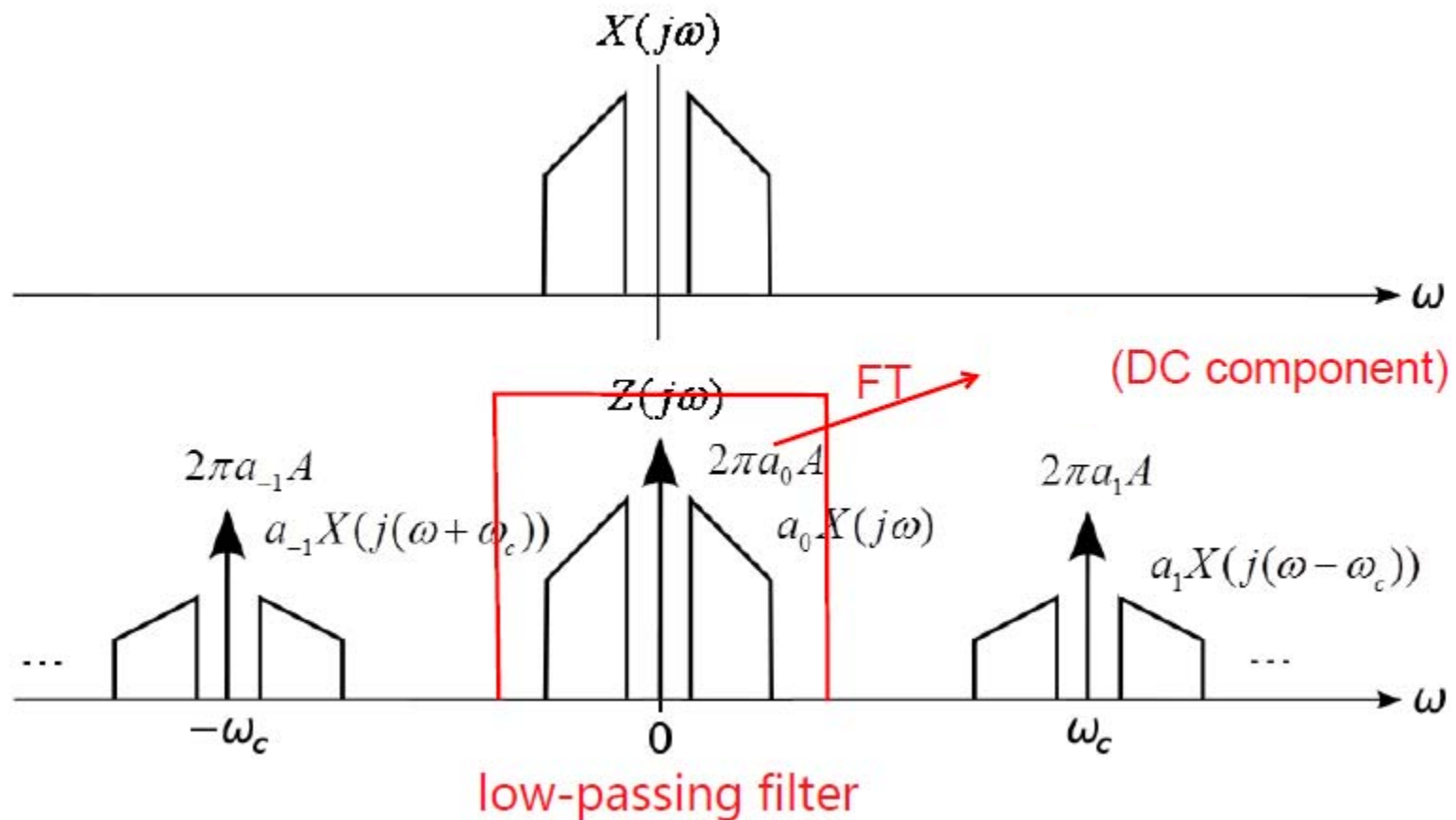
$$p(t) = \sum_{k=-\infty}^{\infty} a_k e^{jk\omega_c t}$$

$$z(t) = [x(t) + A]p(t) = \sum_{k=-\infty}^{\infty} a_k [x(t) + A] e^{jk\omega_c t}$$

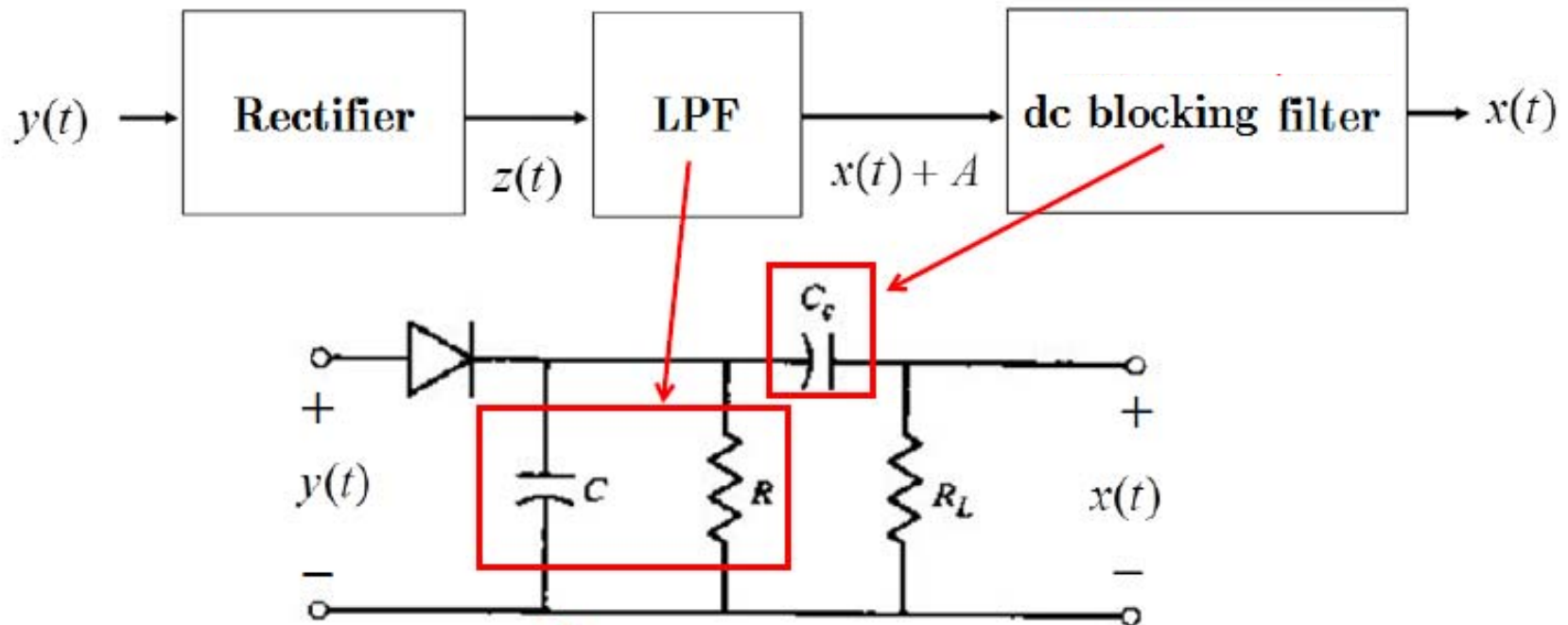
$$= \sum_{k=-\infty}^{\infty} a_k A e^{jk\omega_c t} + \sum_{k=-\infty}^{\infty} a_k x(t) e^{jk\omega_c t}$$

$$Z(j\omega) = \sum_{k=-\infty}^{\infty} 2\pi a_k A \delta(\omega - k\omega_c) + \sum_{k=-\infty}^{\infty} a_k X(j(\omega - k\omega_c))$$

AM Modulator for Asynchronous Modulation-Demodulation System



AM Modulator for Asynchronous Modulation-Demodulation System



AM Modulator for Asynchronous Modulation-Demodulation System

It follows from the above figure that we can recover $[x(t) + A]$ by lowpass filtering $z(t)$:

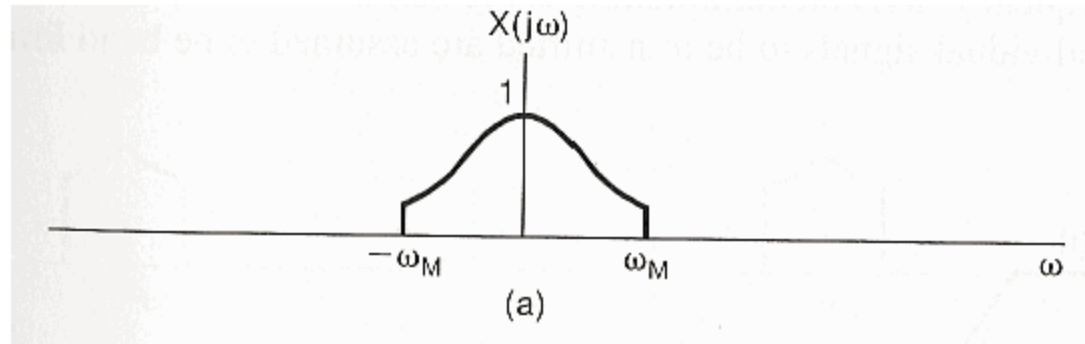
$$H(j\omega) = \begin{cases} a_0^{-1}, & |\omega| < \omega_{co} \\ 0, & |\omega| > \omega_{co} \end{cases}$$

where $\omega_M \ll \omega_{co} \ll \omega_c$.

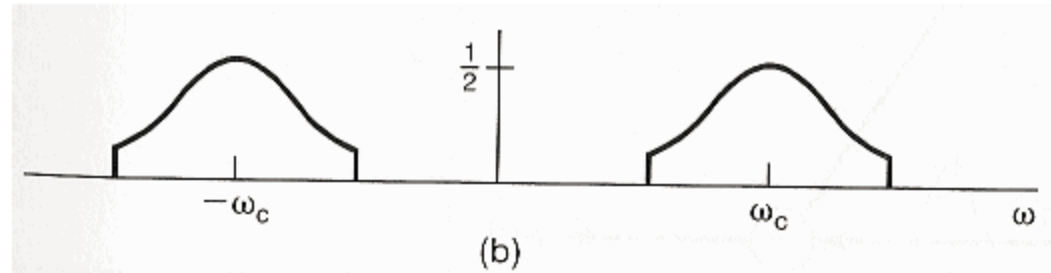
And to recover $x(t)$ from $[x(t) + A]$, we need another filter which blocks the dc component.

AM Demodulation

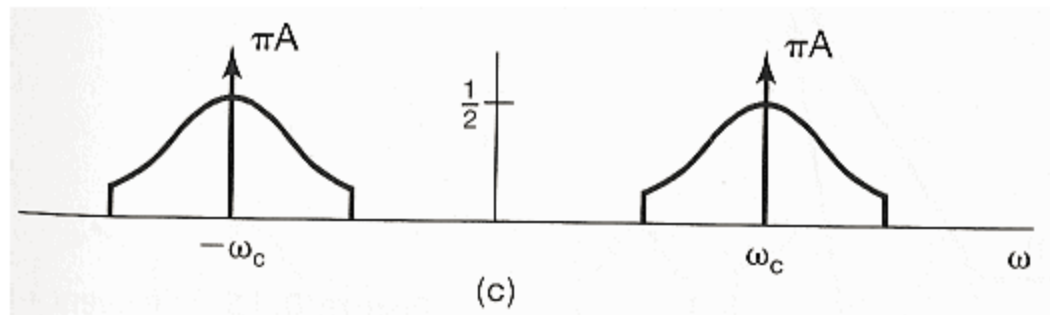
- Synchronous & Asynchronous Demodulation:



$$x(t) \cos(\omega_c t)$$



$$[x(t) + A] \cos(\omega_c t)$$

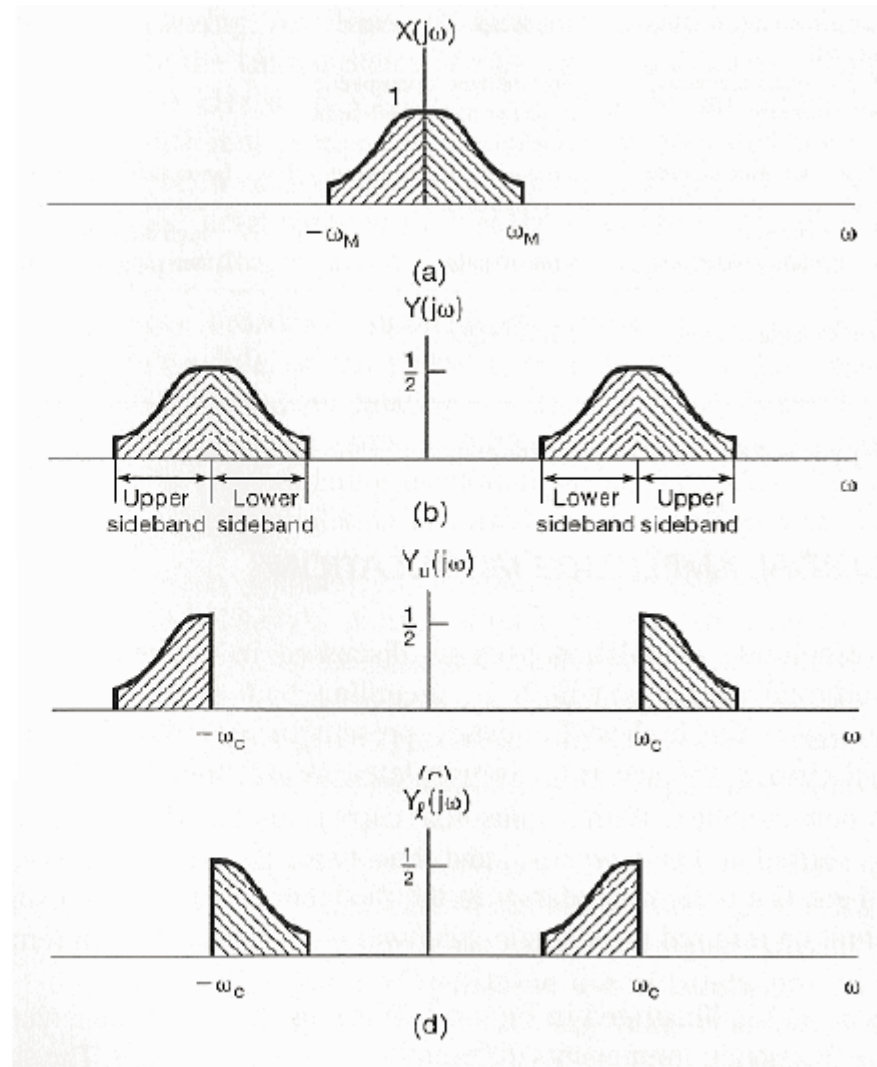


Single-Sideband Sinusoidal Amplitude Modulation

- SSB Modulation:

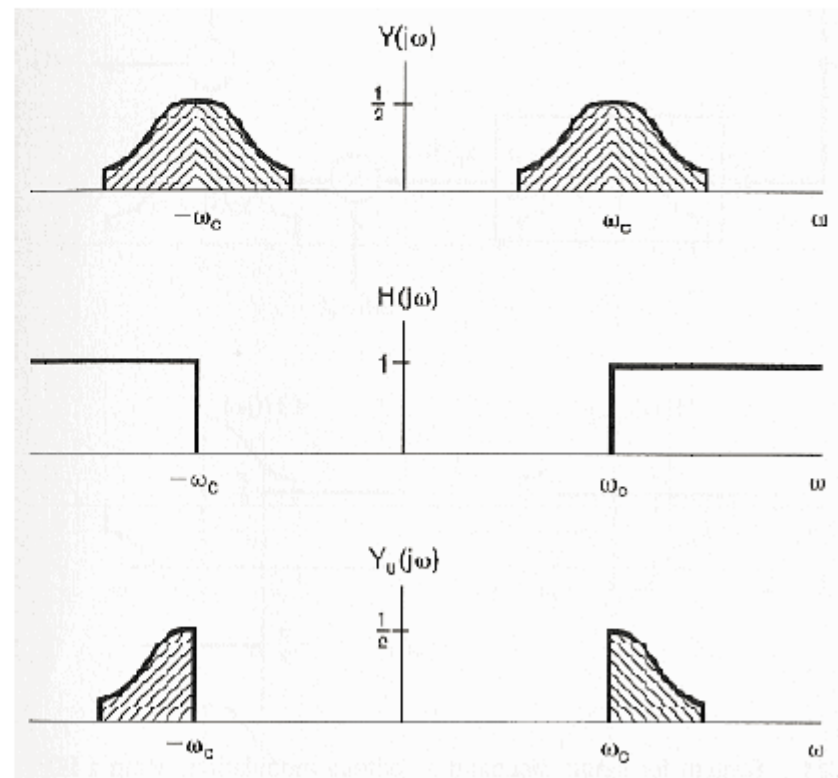
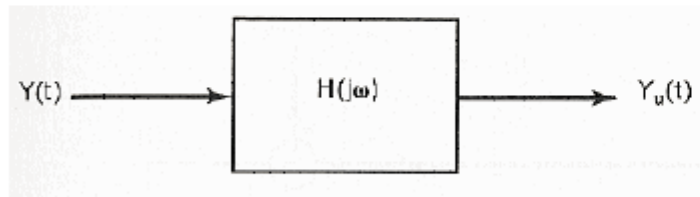
upper sidebands

lower sidebands



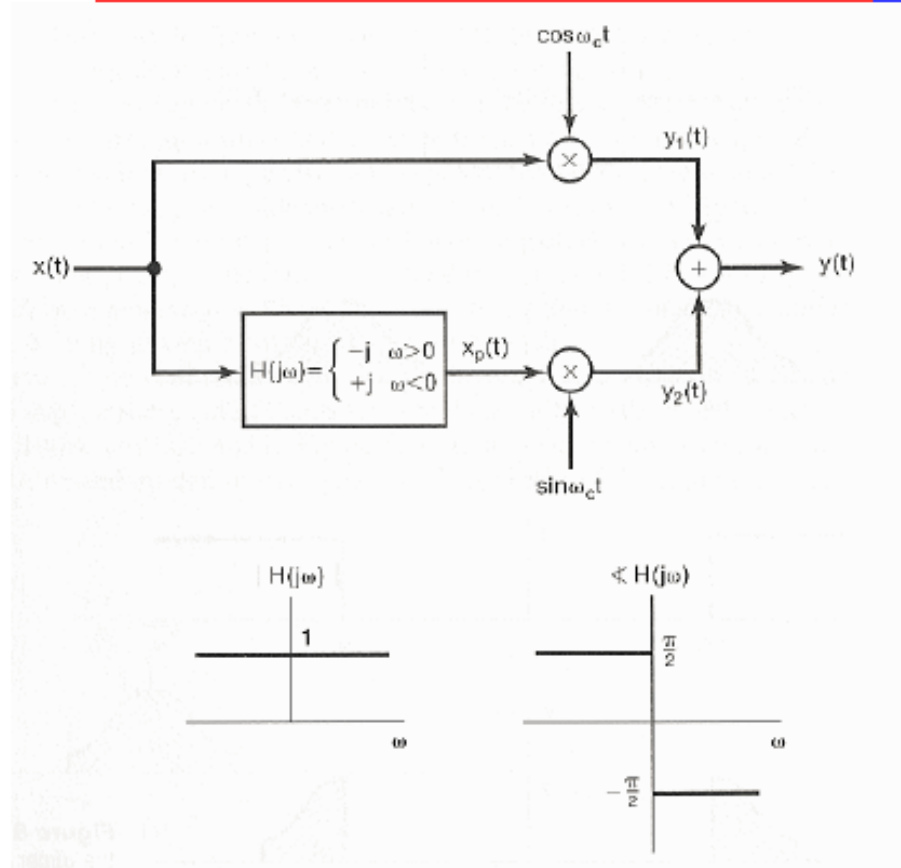
Single-Sideband Sinusoidal Amplitude Modulation

- Retain Upper Sidebands Using Ideal Highpass Filter



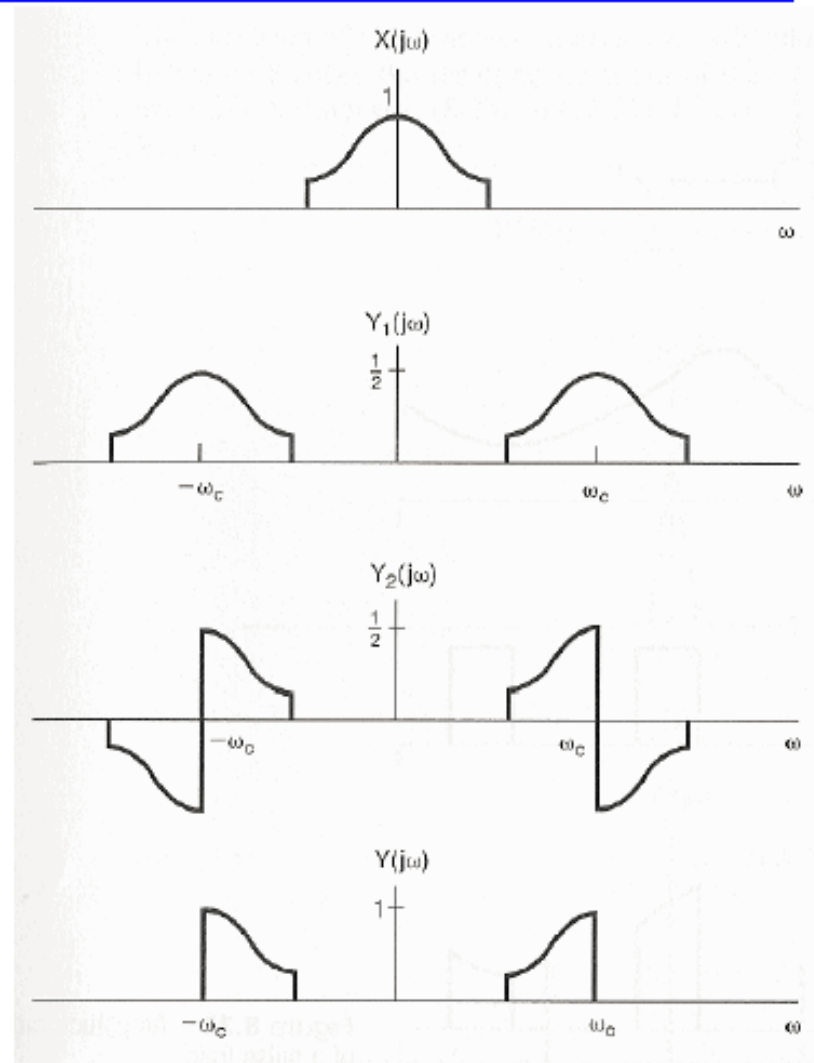
Single-Sideband Sinusoidal Amplitude Modulation

Retain Lower Sidebands Using Phase-Shift Network



Retain Upper Sidebands

$$H(j\omega) = \begin{cases} j, & \omega > 0 \\ -j, & \omega < 0 \end{cases}$$



Single-Sideband Sinusoidal Amplitude Modulation

$$X_p(j\omega) = -j \operatorname{sgn}(\omega) X(j\omega)$$

$$= -j [u(\omega) - u(-\omega)] X(j\omega)$$

$$= -jX(j\omega)u(\omega) + jX(j\omega)u(-\omega)$$

$$X_+(j\omega) \triangleq X(j\omega)u(\omega), X_-(j\omega) \triangleq X(j\omega)u(-\omega)$$

$$X(j\omega) = X_+(j\omega) + X_-(j\omega)$$

$$X_p(j\omega) = -jX_+(j\omega) + jX_-(j\omega)$$

Single-Sideband Sinusoidal Amplitude Modulation

$$y_1(t) = x(t) \cos(\omega_c t) \leftrightarrow$$

$$Y_1(j\omega) = \frac{1}{2} [X(j(\omega - \omega_c)) + X(j(\omega + \omega_c))]$$

$$= \frac{1}{2} [X_+(j(\omega - \omega_c)) + X_-(j(\omega - \omega_c))$$

$$+ X_+(j(\omega + \omega_c)) + X_-(j(\omega + \omega_c))]$$

Single-Sideband Sinusoidal Amplitude Modulation

$$y_2(t) = x_p(t) \sin(\omega_c t) \leftrightarrow$$

$$Y_2(j\omega) = \frac{1}{2j} [X_p(j(\omega - \omega_c)) - X_p(j(\omega + \omega_c))]$$

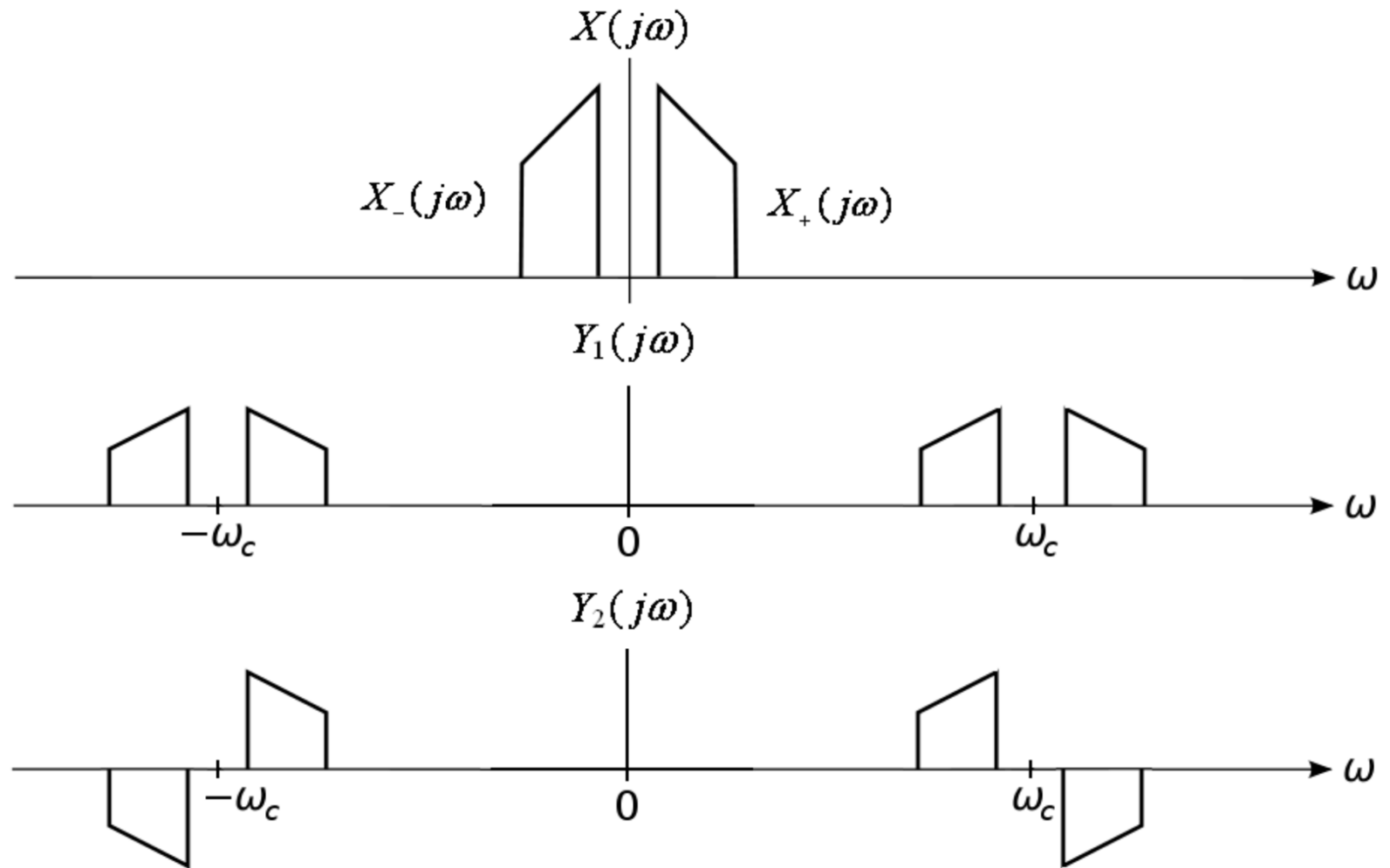
$$= \frac{1}{2j} [-jX_+(j(\omega - \omega_c)) + jX_-(j(\omega - \omega_c))$$

$$-(-jX_+(j(\omega + \omega_c)) + jX_-(j(\omega + \omega_c)))]$$

$$= \frac{1}{2} [-X_+(j(\omega - \omega_c)) + X_-(j(\omega - \omega_c))$$

$$+ X_+(j(\omega + \omega_c)) - X_-(j(\omega + \omega_c))]$$

Single-Sideband Sinusoidal Amplitude Modulation



Single-Sideband Sinusoidal Amplitude Modulation

$$y(t) = y_1(t) \pm y_2(t) \leftrightarrow$$

$$Y(j\omega) = Y_1(j\omega) \pm Y_2(j\omega)$$

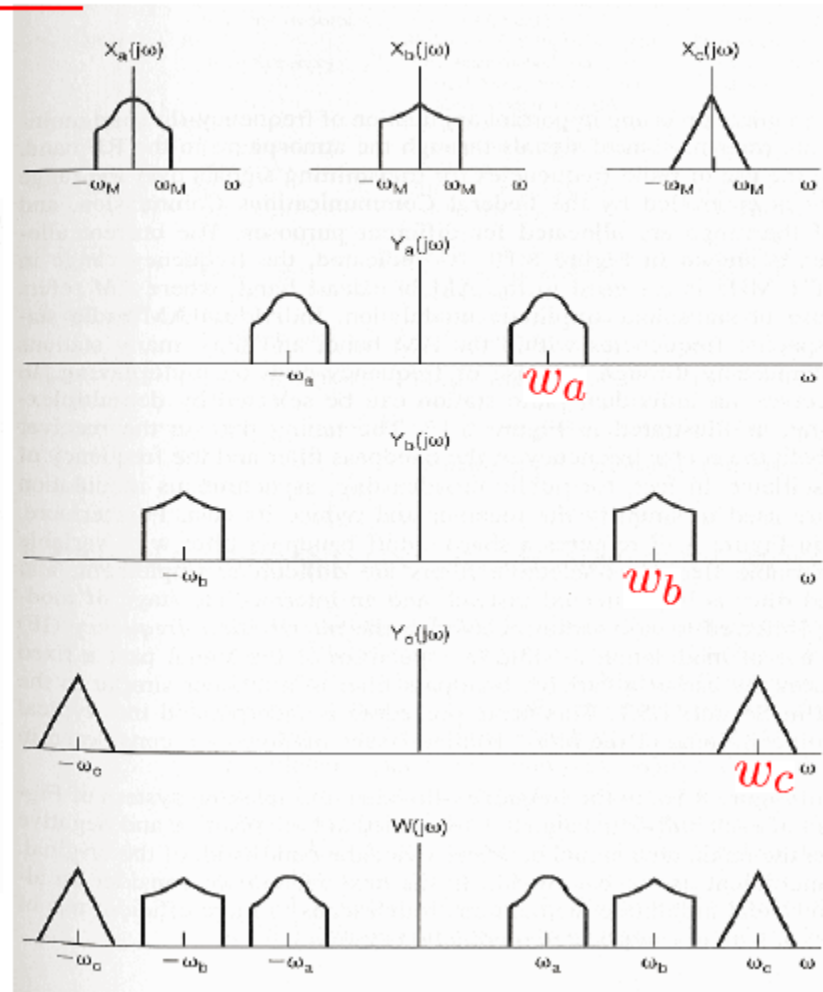
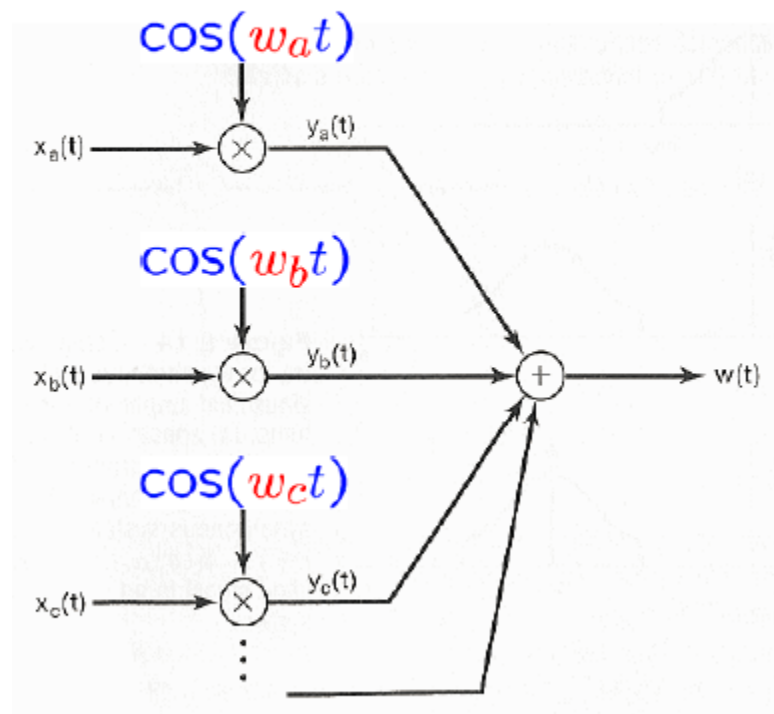
$$\begin{aligned} Y_{USB}(j\omega) &= Y_1(j\omega) + Y_2(j\omega) = \frac{1}{2}[X_+(j(\omega - \omega_c)) + \\ &X_-(j(\omega - \omega_c)) + X_+(j(\omega + \omega_c)) + X_-(j(\omega + \omega_c))] + \\ &\frac{1}{2}[-X_+(j(\omega - \omega_c)) + X_-(j(\omega - \omega_c)) + X_+(j(\omega + \omega_c)) \\ &- X_-(j(\omega + \omega_c))] \\ &= X_-(j(\omega - \omega_c)) + X_+(j(\omega + \omega_c)) \end{aligned}$$

Single-Sideband Sinusoidal Amplitude Modulation

$$\begin{aligned} Y_{LSB}(j\omega) &= Y_1(j\omega) - Y_2(j\omega) = \frac{1}{2}[X_+(j(\omega - \omega_c)) + \\ &X_-(j(\omega - \omega_c)) + X_+(j(\omega + \omega_c)) + X_-(j(\omega + \omega_c))] - \\ &\frac{1}{2}[-X_+(j(\omega - \omega_c)) + X_-(j(\omega - \omega_c)) + X_+(j(\omega + \omega_c)) \\ &- X_-(j(\omega + \omega_c))] \\ &= X_+(j(\omega - \omega_c)) + X_-(j(\omega + \omega_c)) \end{aligned}$$

FDM

■ FDM Using Sinusoidal AM:



FDM

- Demultiplexing and Demodulation:

