

Active Control of a Planar Offset Attaching Jet Using Synthetic Jet Actuators

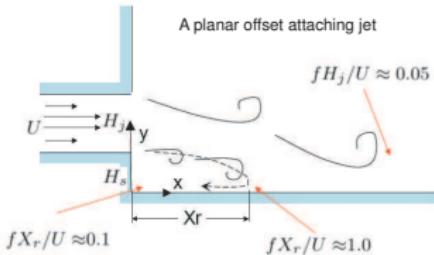


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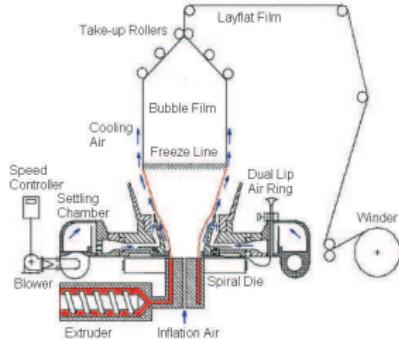
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Background: cooling flow in blown-film manufacturing process



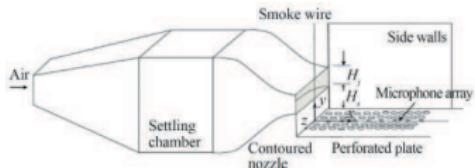
- Attaches to wall forming a re-circulation region, known as 'Coanda effect';
- Time-averaged reattachment length $X_r/H_s \approx 4$ to 6 (Gao & Ewing, 2007);
- Characteristic frequency: $fX_r/U \approx 0.1$ inside recirculation region;
 $fX_r/U \approx 1.0$ near $x = X_r$;
 $fH_j/U \approx 0.05$ away from exit.



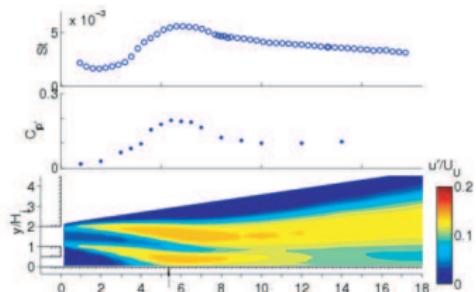
<http://www.plastictechnology.com>

Cooling jets used in blown-film process

Control of an offset attaching jet



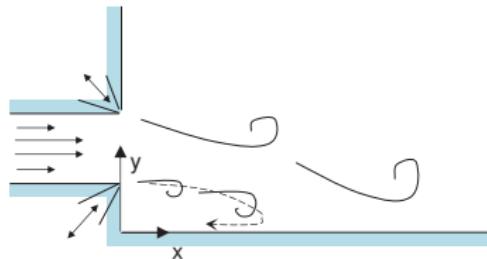
Perforated wall used by Gong *et al.*



Co-flowing wall jet used by Gao & Ewing

- Passive: Gong *et al.* (2014) used a perforated bottom wall, they found the low frequency flapping motion ($fX_r/U \approx 0.1$) was removed;
- Active: Gao & Ewing (2007,2008,2014,2015) examined a constant flow rate co-flowing wall jet, they found
 - fluctuations along the inner shear layer modified when low flow rate jet added,
 - wake type of structures emerged when large velocity co-flowing jet added; local heat transfer rate near the reattachment point enhanced.

Objectives



Offset jet forced using synthetic jet actuators

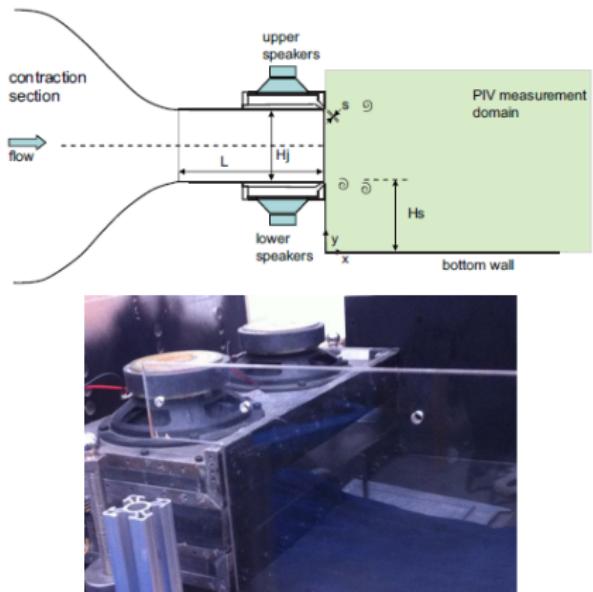
- To examine effect of synthetic jet on the development of a planar wall jet with an offset ratio of $H_s/H_j = 1.0$, including

- time-averaged re-attachment location X_r ;
- time-averaged velocity U , Reynolds stresses $\overline{u^2}$, $\overline{v^2}$ and \overline{uv} ;
- flow structures.

- Test parameters:

- synthetic jet at the upper and lower edge of the jet;
- forcing frequencies $f^* = 0.08$ to 0.45 ,
 $f^* = fH_j/U_o$

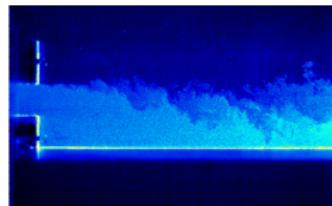
Experiment facility



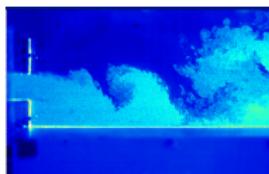
- Blow down jet facility, 0.75kW blower, settling chamber, contoured nozzle, 2D contraction 10:1;
- Jet height $H_j = 30mm$, aspect ratio (W/H_j) 10, offset ratio $H_s/H_j = 1.0$, mass flow averaged exit velocity $U_o = 8.0m/s$, Reynolds number 15300;
- Two zero-net-mass-flux actuators used, each has two 8cm diameter, 4Ω , 40W speakers, jet width $s = 1mm$, forcing strength $u'/U_o=0.3$, u' is root-mean-square of the jet velocity during the 'exhalation' portion of the cycle;
- A LaVision 2D PIV system was used to measure the velocity one the $z = 0$ plane, $100\mu s$ time interval, 2000 image pairs acquired at 25Hz.

Schematics and a picture of the test rig

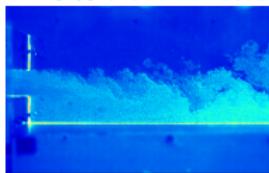
Laser-smoke visualization using PIV



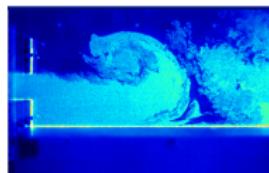
(a) No Control



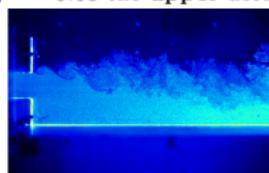
(b) $f^* = 0.08$ the **lower** actuator



6 of 17 (d) $f^* = 0.45$ the **lower** actuator

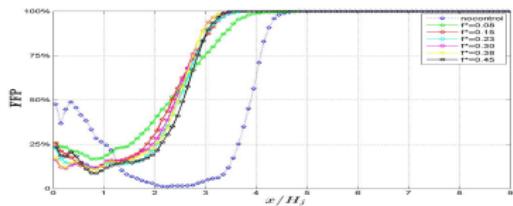


(c) $f^* = 0.08$ the **upper** actuator

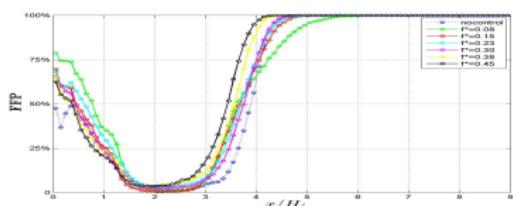


(e) $f^* = 0.45$ the **upper** actuator

Time-averaged reattachment location, X_r

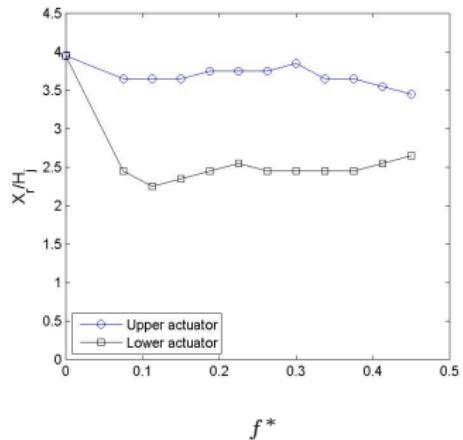


lower actuator



upper actuator

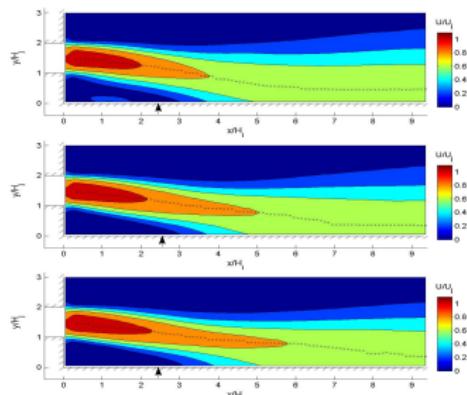
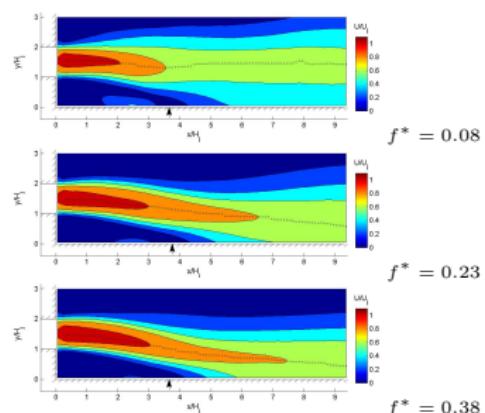
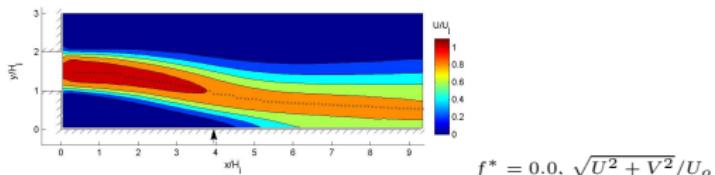
Distributions of the forward flow percentage (FFP) near wall ($y/H_j = 0.1$)
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f^*
Time-averaged reattachment Location

Distributions of the time-averaged re-attachment location where forward flow ratio was 50% (Spazzini *et al.* 2001)

Effect of actuation on the mean flow

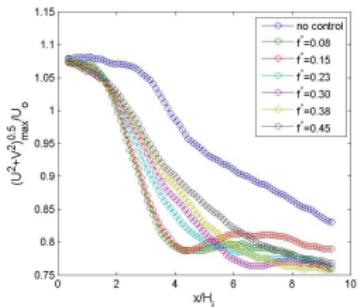


lower actuator

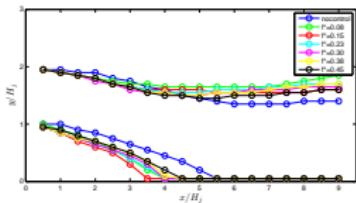
upper actuator

Maximum local velocity and jet half width

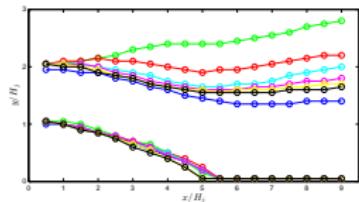
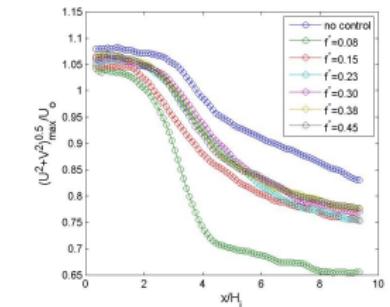
Max. local velocity



Jet half width

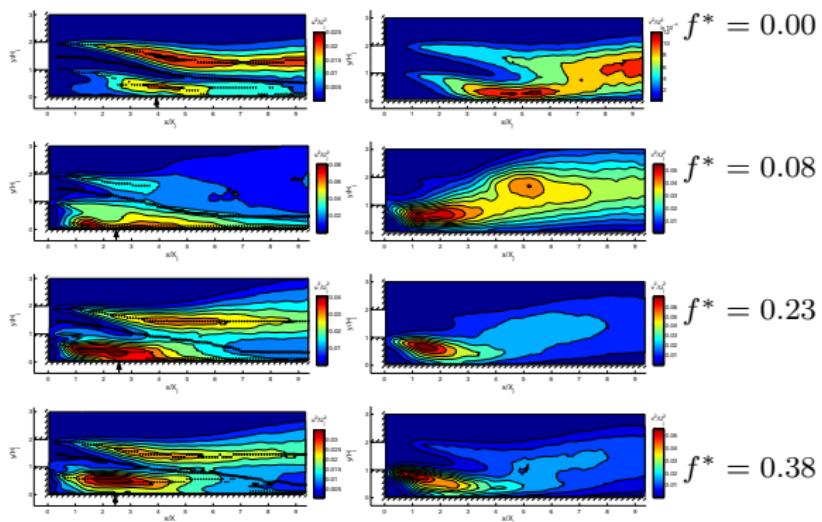


Lower actuator



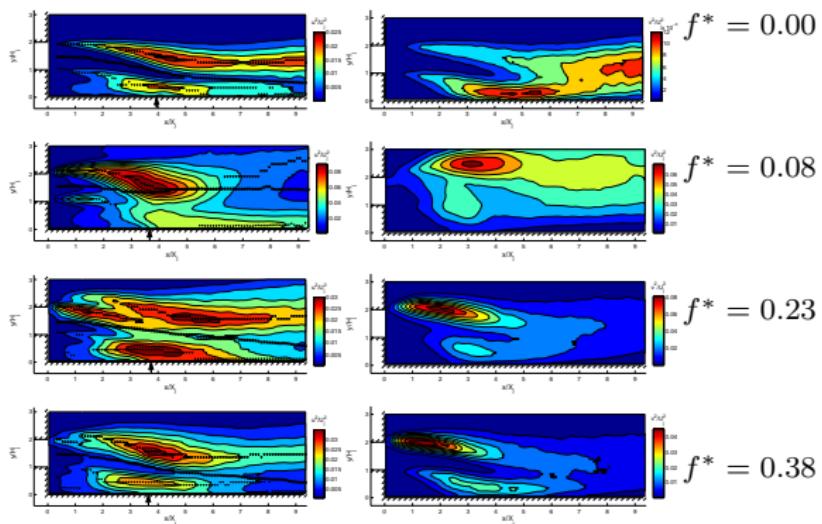
Upper actuator

Effect of actuation on the shear layers lower actuator

 $\overline{u^2}$ $\overline{v^2}$

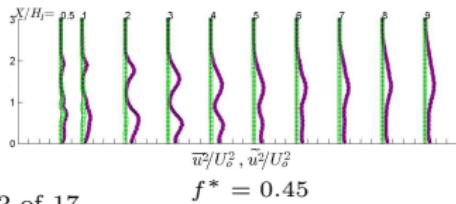
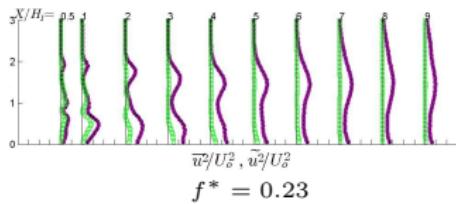
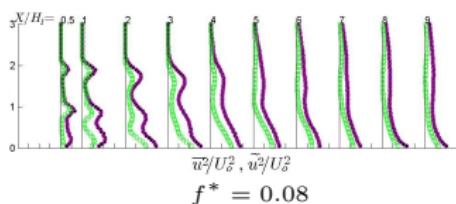
Effect of actuation on the shear layers

upper actuator

 $\overline{u^2}$ $\overline{v^2}$

Phase-averaged and time-averaged Reynolds normal stresses

$\overline{\tilde{u}^2}$, $\overline{u^2}$, lower actuator



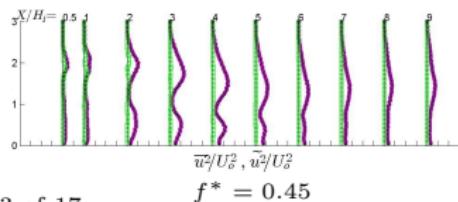
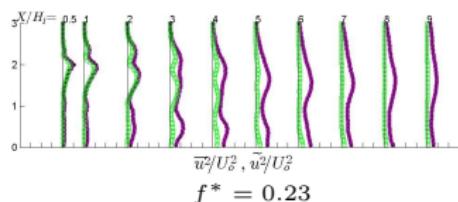
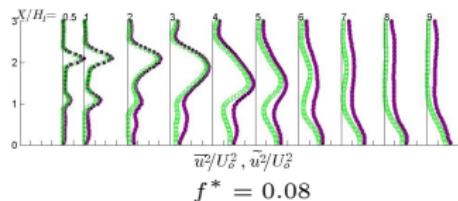
- Velocity measurements were phase averaged, 2000 realizations were separated into 50 groups according to the phase of the actuation, phase angle within $\pm 3.6^\circ$ in each group, velocity for group k is

$$\tilde{u}_k = \frac{1}{N} \sum_{j=1}^N u_{k,j}.$$

- when forced at $f^* = 0.08$, phase-averaged stress $\overline{\tilde{u}^2}$ was similar to time-averaged stress $\overline{u^2}$;
- when forced at $f^* \geq 0.23$, contributions from $\overline{\tilde{u}^2}$ to $\overline{u^2}$ were small, due to the changes in the shear layer frequencies.

Phase-averaged and time-averaged Reynolds normal stresses

$\overline{\tilde{u}^2}$, $\overline{u^2}$, upper actuator



- when forced at $f^* = 0.08$, phase-averaged stress $\overline{\tilde{u}^2}$ similar to time-averaged stress $\overline{u^2}$, larger than forcing the inner shear layer;
- when forced at $f^* \geq 0.23$, contributions from $\overline{\tilde{u}^2}$ to $\overline{u^2}$ were small.



Phase-averaged vorticity ($\tilde{\omega}_z$), lower actuator

$$f^* = 0.08$$

$$f^* = 0.45$$



Phase-averaged vorticity ($\tilde{\omega}_z$), upper actuator

$$f^* = 0.08$$

$$f^* = 0.45$$



Conclusions and future work

Conclusions:

- Experiments were performed to investigate the affect of synthetic jets forcing location and frequency on the development of a planar offset attaching jet with $H_s/H_j = 1.0$ and $Re = 15\,300$;
- Low frequency forcing at $f^* = 0.08$ enhanced a flapping motion of the jet, especially when applied at the upper edge of the planar jet, spreading rate of the jet increased significantly;
- Time-averaged re-attachment length decreased when forced at all the frequencies examined, at either location.

Future work:

- Effect of the forcing amplitude $u'/U_o = 0.1, 0.2$ and 0.4 will be examined;
 - Combinations of the two synthetic jets will be examined, in-phased and anti-phased actuation;
 - Effect of actuation on the convective heat transfer rate will be investigated.
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Thank you!