

# GooseMaterial/Metal/LinearStrain/ElastoViscoPlastic

T.W.J. de Geus

\*Contact: [tom@geus.me](mailto:tom@geus.me) – [www.geus.me](http://www.geus.me) – <https://github.com/tdegeus/GooseMaterial>

## Abstract

History dependent visco-plastic material. This corresponds to a linear relationship between the Cauchy stress  $\sigma$  and the elastic strain  $\epsilon_e$ . The elastic strain depends on the strain  $\epsilon$  (which is the symmetric part of the displacement gradient), and the history.

The model is implemented in 3-D, hence it can directly be used for either 3-D or 2-D plane strain problems.

**Keywords:** visco-plasticity; linear elasticity

## Contents

<b>1</b>	<b>Constitutive model</b>	<b>2</b>
<b>2</b>	<b>Numerical implementation: implicit</b>	<b>3</b>
2.1	Elastic predictor . . . . .	3
2.2	Return-map . . . . .	3
2.3	Actual state . . . . .	4
2.4	Consistent tangent operator . . . . .	5
<b>A</b>	<b>Nomenclature</b>	<b>6</b>
<b>B</b>	<b>Stress measures</b>	<b>6</b>

## 1 Constitutive model

The model consists of the following ingredients:

- (i) The strain,  $\boldsymbol{\varepsilon}$ , is additively split in an elastic part,  $\boldsymbol{\varepsilon}_e$ , and a plastic part,  $\boldsymbol{\varepsilon}_p$ . I.e.

$$\boldsymbol{\varepsilon} = \boldsymbol{\varepsilon}_e + \boldsymbol{\varepsilon}_p \quad (1)$$

- (ii) The stress,  $\boldsymbol{\sigma}$ , is set by the elastic strain,  $\boldsymbol{\varepsilon}_e$ , through the following linear relation:

$$\boldsymbol{\sigma} = \mathbb{C}_e : \boldsymbol{\varepsilon}_e \quad (2)$$

wherein  $\mathbb{C}_e$  is the elastic stiffness, which reads:

$$\mathbb{C}_e = K \mathbf{I} \otimes \mathbf{I} + 2G(\mathbb{I}_s - \frac{1}{3} \mathbf{I} \otimes \mathbf{I}) \quad (3)$$

$$= K \mathbf{I} \otimes \mathbf{I} + 2G \mathbb{I}_d \quad (4)$$

with  $K$  and  $G$  the bulk and shear modulus respectively. See Appendix A for nomenclature.

- (iii) Plasticity is governed by Norton's flow rule:

$$\dot{\boldsymbol{\varepsilon}}_p = \dot{\gamma} \frac{\partial \Phi}{\partial \boldsymbol{\sigma}} = \dot{\gamma} \frac{3}{2} \frac{\boldsymbol{\sigma}_d}{\sigma_{eq}} = \dot{\gamma} \mathbf{N} \quad (5)$$

wherein  $\dot{\boldsymbol{\varepsilon}}_p$  is the plastic strain rate. The ratio of the stress deviator,  $\boldsymbol{\sigma}_d$ , and its equivalent value,  $\sigma_{eq}$ , determines the direction of plastic flow (the symbol  $\mathbf{N}$  is used to emphasize that only determines a direction, not an amplitude). The evolution of the plastic multiplier,  $\dot{\gamma}$ , is finally defined as follows:

$$\dot{\gamma} = \dot{\gamma}_0 \left( \frac{\sigma_{eq}}{\sigma_0} \right)^{\frac{1}{m}} \quad (6)$$

wherein  $\dot{\gamma}_0$ ,  $\sigma_0$ , and the exponent  $m$  are material parameters.

It can furthermore be useful to define an equivalent plastic strain. Following the definition in (5), it is defined as follows:

$$\varepsilon_p = \int_0^t \dot{\gamma} \, d\tau \quad (7)$$

## 2 Numerical implementation: implicit

For the numerical implementation, first of all a numerical time integration scheme has to be selected. Here, an implicit time discretization is used, which has the favorable property of being unconditionally stable. To this end, the commonly used return-map algorithm is used. An increment in strain is first assumed fully elastic (elastic predictor). Then, if needed, a return-map is utilized to return to a physically admissible state (plastic corrector). The benefit of this scheme is that (i) the evolution of the plasticity (the state variable) can be determined by solving a single, albeit non-linear, equation; and that (ii) the linearization to obtain the consistent tangent operator is relatively straightforward.

### 2.1 Elastic predictor

Given an increment in strain

$$\boldsymbol{\varepsilon}_\Delta = \boldsymbol{\varepsilon}^{(t+\Delta t)} - \boldsymbol{\varepsilon}^{(t)} \quad (8)$$

and the state variables, the *elastic trial state* reads:

$$^*\boldsymbol{\varepsilon}_e = \boldsymbol{\varepsilon}_e^{(t)} + \boldsymbol{\varepsilon}_\Delta \quad (9)$$

$$^*\boldsymbol{\sigma} = \mathbb{C}_e : ^*\boldsymbol{\varepsilon}_e \quad (10)$$

where the notation  $^*(\cdot)$  has been used to denote a trial value for  $(\cdot)^{(t+\Delta t)}$ .

### 2.2 Return-map

A return-map is used to return the trial state back to a physically admissible state (for which the plasticity has evolved). It follows from

$$\boldsymbol{\varepsilon}_e^{(t+\Delta t)} = ^*\boldsymbol{\varepsilon}_e - \Delta\gamma \mathbf{N}^{(t+\Delta t)} \quad (11)$$

This can be reduced by using that

$$\boldsymbol{\sigma}_d^{(t+\Delta t)} = ^*\boldsymbol{\sigma}_d - 2G\Delta\gamma \mathbf{N}^{(t+\Delta t)} \quad (12)$$

$$= ^*\boldsymbol{\sigma}_d - 3G\Delta\gamma \frac{\boldsymbol{\sigma}_d^{(t+\Delta t)}}{\sigma_{eq}^{(t+\Delta t)}} \quad (13)$$

i.e. the trial and updated deviatoric stresses are *co-linear*. This implies that

$$\frac{\boldsymbol{\sigma}_d^{(t+\Delta t)}}{\sigma_{eq}^{(t+\Delta t)}} = \frac{^*\boldsymbol{\sigma}_d}{^*\sigma_{eq}} \quad \text{or} \quad \mathbf{N}^{(t+\Delta t)} = ^*\mathbf{N} \quad (14)$$

This allows the reorganization of the above to

$$\boldsymbol{\sigma}_d^{(t+\Delta t)} = \left(1 - \frac{3G\Delta\gamma}{^*\sigma_{eq}}\right) ^*\boldsymbol{\sigma}_d \quad (15)$$

from which it also follows that

$$\sigma_{eq}^{(t+\Delta t)} = ^*\sigma_{eq} - 3G\Delta\gamma \quad (16)$$

Substitution into (6) yields:

$$\Delta\gamma = \dot{\gamma}_0 \Delta t \left( \frac{^*\sigma_{eq} - 3G\Delta\gamma}{\sigma_0} \right)^{\frac{1}{m}} \quad (17)$$

which has to be solved for  $\Delta\gamma$ .

#### 2.2.1 Special case $m = 1$

For the special case that  $m = 1$ , (17) can be solved in closed form. Its solution reads

$$\Delta\gamma = ^*\sigma_{eq} / \left( 3G + \frac{\sigma_0}{\dot{\gamma}_0 \Delta t} \right) \quad (18)$$

### 2.2.2 Solution using Newton-Raphson

If  $m \neq 1$ , (17) can only be solved numerically. To this end Newton-Raphson is used. First, (17) is rewritten in residual form:

$$R(\Delta\gamma) = \Delta\gamma - \dot{\gamma}_0 \Delta t \left( \frac{{}^*\sigma_{\text{eq}} - 3G\Delta\gamma}{\sigma_0} \right)^{\frac{1}{m}} = 0 \quad (19)$$

Its derivative then trivially follows

$$\frac{\partial R}{\partial \Delta\gamma} = 1 + \frac{3G\dot{\gamma}_0 \Delta t}{m\sigma_0} \left( \frac{{}^*\sigma_{\text{eq}} - 3G\Delta\gamma}{\sigma_0} \right)^{\frac{1}{m}-1} \quad (20)$$

The iterative scheme then reads:

1. Initial guess

$$R_0 = R(\Delta\gamma = 0) \quad (21)$$

2. While  $R \neq 0$

- (a) Calculate the derivative:

$$\left. \frac{\partial R}{\partial \Delta\gamma} \right|_{\Delta\gamma_i} \quad (22)$$

- (b) Update plastic multiplier

$$\Delta\gamma_{i+1} = \Delta\gamma_i - R(\Delta\gamma_i) \left( \left. \frac{\partial R}{\partial \Delta\gamma} \right|_{\Delta\gamma_i} \right)^{-1} \quad (23)$$

- (c) Calculate new residual

$$R(\Delta\gamma_{i+1}) \quad (24)$$

### 2.3 Actual state

Finally, the trial state is updated:

- The updated stress tensor

$$\boldsymbol{\sigma}^{(t+\Delta t)} = \sigma_{\text{m}}^{(t+\Delta t)} \mathbf{I} + \boldsymbol{\sigma}_{\text{d}}^{(t+\Delta t)} \quad (25)$$

with

$$\sigma_{\text{m}}^{(t+\Delta t)} = {}^*\sigma_{\text{m}} \quad (26)$$

$$\boldsymbol{\sigma}_{\text{d}}^{(t+\Delta t)} = \left( 1 - \frac{3G\Delta\gamma}{{}^*\sigma_{\text{eq}}} \right) {}^*\boldsymbol{\sigma}_{\text{d}} \quad (27)$$

- The updated elastic strain tensor

$$\boldsymbol{\varepsilon}_{\text{e}}^{(t+\Delta t)} = \frac{1}{2G} \boldsymbol{\sigma}_{\text{d}}^{(t+\Delta t)} + \frac{1}{3} \text{tr}({}^*\boldsymbol{\varepsilon}_{\text{e}}) \mathbf{I} \quad (28)$$

- The updated equivalent plastic strain (for post-processing):

$$\varepsilon_{\text{p}}^{(t+\Delta t)} = \varepsilon_{\text{p}}^{(t)} + \Delta\gamma \quad (29)$$

## 2.4 Consistent tangent operator

The consistent constitutive tangent operator is defined as

$$\mathbb{C}_{\text{ep}} = \frac{\partial \boldsymbol{\sigma}^{(t+\Delta t)}}{\partial \boldsymbol{\varepsilon}^{(t+\Delta t)}} \quad (30)$$

For the case that the trial state coincides with the actual state (i.e.  $^*\Phi \leq 0$ ),  $\mathbb{C}_{\text{ep}} = \mathbb{C}_{\text{e}}$ . Otherwise, it can be obtained from<sup>1</sup>

$$\mathbb{C}_{\text{ep}} = \frac{\partial \boldsymbol{\sigma}^{(t+\Delta t)}}{\partial \boldsymbol{\varepsilon}^{(t+\Delta t)}} = \frac{\partial \boldsymbol{\sigma}^{(t+\Delta t)}}{\partial ^*\boldsymbol{\varepsilon}_{\text{e}}} : \frac{\partial ^*\boldsymbol{\varepsilon}_{\text{e}}}{\partial \boldsymbol{\varepsilon}^{(t+\Delta t)}} = \frac{\partial \boldsymbol{\sigma}^{(t+\Delta t)}}{\partial ^*\boldsymbol{\varepsilon}_{\text{e}}} : \mathbb{I} = \frac{\partial \boldsymbol{\sigma}^{(t+\Delta t)}}{\partial ^*\boldsymbol{\varepsilon}_{\text{e}}} \quad (31)$$

To proceed, the first step is write an explicit relation between the (actual) stress  $\boldsymbol{\sigma}^{(t+\Delta t)}$  and the trial elastic strain  $^*\boldsymbol{\varepsilon}_{\text{e}}$ :

$$\boldsymbol{\sigma}^{(t+\Delta t)} = \boldsymbol{\sigma}_{\text{m}}^{(t+\Delta t)} \mathbf{I} + \boldsymbol{\sigma}_{\text{d}}^{(t+\Delta t)} \quad (32)$$

$$= ^*\boldsymbol{\sigma}_{\text{m}} \mathbf{I} + \left(1 - \frac{3G\Delta\gamma}{^*\boldsymbol{\sigma}_{\text{eq}}}\right) ^*\boldsymbol{\sigma}_{\text{d}} \quad (33)$$

$$= ^*\boldsymbol{\sigma}_{\text{m}} \mathbf{I} + \left(1 - \frac{3G\Delta\gamma}{^*\boldsymbol{\sigma}_{\text{eq}}}\right) 2G ^*\boldsymbol{\varepsilon}_{\text{e}}^{\text{d}} \quad (34)$$

$$= \left[ \mathbb{C}_{\text{e}} - \frac{6G^2\Delta\gamma}{^*\boldsymbol{\sigma}_{\text{eq}}} \mathbb{I}_{\text{d}} \right] : ^*\boldsymbol{\varepsilon}_{\text{e}} \quad (35)$$

The tangent then follows from

$$\mathbb{C}_{\text{ep}} = \frac{\partial \boldsymbol{\sigma}^{(t+\Delta t)}}{\partial ^*\boldsymbol{\varepsilon}_{\text{e}}} = \mathbb{C}_{\text{e}} - \frac{6G^2\Delta\gamma}{^*\boldsymbol{\sigma}_{\text{eq}}} \mathbb{I}_{\text{d}} - \frac{6G^2}{^*\boldsymbol{\sigma}_{\text{eq}}} \left( \frac{\partial \Delta\gamma}{\partial ^*\boldsymbol{\varepsilon}_{\text{e}}} \right) \otimes ^*\boldsymbol{\varepsilon}_{\text{e}}^{\text{d}} + \frac{6G^2\Delta\gamma}{^*\boldsymbol{\sigma}_{\text{eq}}^2} \left( \frac{\partial ^*\boldsymbol{\sigma}_{\text{eq}}}{\partial ^*\boldsymbol{\varepsilon}_{\text{e}}} \right) \otimes ^*\boldsymbol{\varepsilon}_{\text{e}}^{\text{d}} \quad (36)$$

Now apply the following:

- Equivalent stress

$$\frac{\partial \boldsymbol{\sigma}_{\text{eq}}}{\partial \boldsymbol{\sigma}} = \frac{\partial \boldsymbol{\sigma}_{\text{eq}}}{\partial \boldsymbol{\sigma}_{\text{d}}} = \frac{\partial}{\partial \boldsymbol{\sigma}_{\text{d}}} \left( \sqrt{\frac{3}{2} \boldsymbol{\sigma}_{\text{d}} : \boldsymbol{\sigma}_{\text{d}}} \right) = \frac{1}{2 \boldsymbol{\sigma}_{\text{eq}}} \frac{\partial}{\partial \boldsymbol{\sigma}_{\text{d}}} \left( \frac{3}{2} \boldsymbol{\sigma}_{\text{d}} : \boldsymbol{\sigma}_{\text{d}} \right) = \frac{3}{2} \frac{\boldsymbol{\sigma}_{\text{d}}}{\boldsymbol{\sigma}_{\text{eq}}} = \mathbf{N} = ^*\mathbf{N} \quad (37)$$

Hence:

$$\frac{\partial ^*\boldsymbol{\sigma}_{\text{eq}}}{\partial ^*\boldsymbol{\varepsilon}_{\text{e}}} = 2G ^*\mathbf{N} \quad (38)$$

- Plastic multiplier

$$\frac{\partial \Delta\gamma}{\partial ^*\boldsymbol{\varepsilon}_{\text{e}}} = \left( \frac{\partial ^*\boldsymbol{\sigma}_{\text{eq}}}{\partial \Delta\gamma} \right)^{-1} \left( \frac{\partial ^*\boldsymbol{\sigma}_{\text{eq}}}{\partial ^*\boldsymbol{\varepsilon}_{\text{e}}} \right) \quad (39)$$

From (17), it follows that

$$\left( \frac{\Delta\gamma}{\dot{\gamma}_0 \Delta t} \right)^m = \frac{^*\boldsymbol{\sigma}_{\text{eq}} - 3G\Delta\gamma}{\sigma_0} \rightarrow ^*\boldsymbol{\sigma}_{\text{eq}} = \sigma_0 \left( \frac{\Delta\gamma}{\dot{\gamma}_0 \Delta t} \right)^m + 3G\Delta\gamma \quad (40)$$

Hence:

$$\frac{\partial ^*\boldsymbol{\sigma}_{\text{eq}}}{\partial \Delta\gamma} = 3G + \frac{m\sigma_0}{\dot{\gamma}_0 \Delta t} \left( \frac{\Delta\gamma}{\dot{\gamma}_0 \Delta t} \right)^{m-1} \quad (41)$$

The final result then reads:

$$\mathbb{C}_{\text{ep}} = \mathbb{C}_{\text{e}} - \frac{6G^2\Delta\gamma}{^*\boldsymbol{\sigma}_{\text{eq}}} \mathbb{I}_{\text{d}} + 4G^2 \left[ \frac{\Delta\gamma}{^*\boldsymbol{\sigma}_{\text{eq}}} - \left[ 3G + \frac{m\sigma_0}{\dot{\gamma}_0 \Delta t} \left( \frac{\Delta\gamma}{\dot{\gamma}_0 \Delta t} \right)^{m-1} \right]^{-1} \right] ^*\mathbf{N} \otimes ^*\mathbf{N} \quad (42)$$

<sup>1</sup>To show this one has to employ (8,9) and realize that  $\boldsymbol{\varepsilon}^{(t)}$  and  $\boldsymbol{\varepsilon}_{\text{e}}^{(t)}$  are constant during the increment. I.e.  $\frac{\partial ^*\boldsymbol{\varepsilon}_{\text{e}}}{\partial \boldsymbol{\varepsilon}^{(t+\Delta t)}} = \frac{\partial \boldsymbol{\varepsilon}^{(t+\Delta t)}}{\partial \boldsymbol{\varepsilon}^{(t+\Delta t)}} = \mathbb{I}$ .

## A Nomenclature

- Dyadic tensor product

$$\mathbb{C} = \mathbf{A} \otimes \mathbf{B} \quad (43)$$

$$C_{ijkl} = A_{ij} B_{kl} \quad (44)$$

- Double tensor contraction

$$C = \mathbf{A} : \mathbf{B} \quad (45)$$

$$= A_{ij} B_{ji} \quad (46)$$

- Deviatoric projection tensor

$$\mathbb{I}_d = \mathbb{I}_s - \frac{1}{3} \mathbf{I} \otimes \mathbf{I} \quad (47)$$

## B Stress measures

- Mean stress

$$\sigma_m = \frac{1}{3} \text{tr}(\boldsymbol{\sigma}) = \frac{1}{3} \boldsymbol{\sigma} : \mathbf{I} \quad (48)$$

- Stress deviator

$$\boldsymbol{\sigma}_d = \boldsymbol{\sigma} - \sigma_m \mathbf{I} = \mathbb{I}_d : \boldsymbol{\sigma} \quad (49)$$

- Von Mises equivalent stress

$$\sigma_{eq} = \sqrt{\frac{3}{2} \boldsymbol{\sigma}_d : \boldsymbol{\sigma}_d} = \sqrt{3 J_2(\boldsymbol{\sigma})} \quad (50)$$

where the second-stress invariant

$$J_2 = \frac{1}{2} ||\boldsymbol{\sigma}_d||^2 = \frac{1}{2} \boldsymbol{\sigma}_d : \boldsymbol{\sigma}_d \quad (51)$$