Characterizaiton of Pu Separation by PUREX

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Big Picture

- Pu isotopes produced in irradiated fuel can vary depending on
 - Burnup (irradiation history)
 - Reactor neutron spectrum (core design)
- Weapons-grade Pu can be extracted from reactor discharged fuel with a burnup of about 1 (GWD/tU)
- Two examples of non-safeguarded reactors which can intentionally discharge low burned fuel for extracting weapon-grade Pu are:
 - Indian Prototype Fast Breeder Reactor (PFBR-500MWe)
 - Indian Pressureized Heavy Water Reactor (PHWR-CANDU type 220 MWe)
- In accord with the Indo-US 123 agreement, these reactors were not required to be kept under IAEA safeguards



Smaller Picture

- Attribution for unpurified Pu has been previously studied [2, 6, 3]
- Intercepted Pu would likely have been processed via PUREX
- Due to a lack of literature on decontamination factors and distribution coefficients for useful forensic elements (Cs, Sb, Eu, Rb, Sr, Nd, Pm, and Sm) this research was pursued.

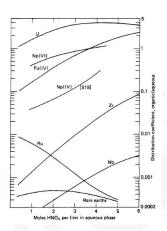


Figure 1: Effect of nitric acid concentration on distribution coefficients [7]

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Background



What is PUREX - A type of laundry detergent?

- Plutonium Uranium Redox EXtraction
 - Liquid-liquid solvent extraction
 - Many stages:
 - 1. Preparation for Dissolution
 - 2. Dissolution
 - 3. Preparation of Dissolved Feed
 - 4. Primary Decontamination Extraction to organic*
 - 5. Scrubbing
 - 6. Plutonium Partition Back-Extraction to aqueous*
 - 7. Plutonium Purification



Extraction

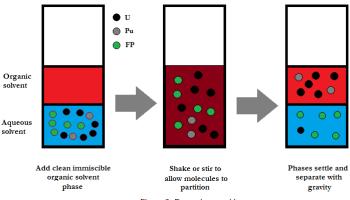


Figure 2: Extraction graphic



Back-Extraction

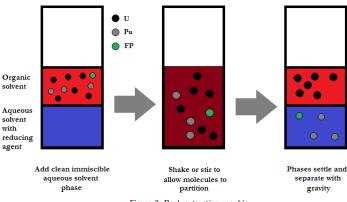


Figure 3: Back-extraction graphic



Extraction and Back-extraction

Extraction

$$UO_2^{2+}(aq) + 2NO_3^-(aq) + 2TBP(o) \leftrightarrow UO_2(NO_3)_2 \cdot 2TBP(o)^{[1]}$$
 $Pu^{4+}(aq) + 4NO_3^-(aq) + 2TBP(o) \leftrightarrow Pu(NO_3)_4 \cdot 2TBP(o)$
Most of the fission products are left in the aqueous solution at valence III and V states^[4]

Back-extraction

$$Pu(NO_3)_4(TBP)_{2_o} + Fe_{aq}^{2+} \leftrightarrow Pu_{aq}^{3+} + 4NO_{3_{aq}}^{-} + 2TBP_o$$
 [5]

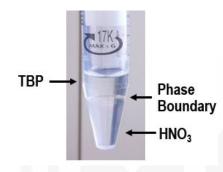


Figure 4: TBP and HNO₃



Distribution Coefficients - The Missing link

 Distribution Coefficient (DC): The ratio between the organic and aqueous phases

$$DR = \frac{c_o}{c_{aq}}$$

- Specific element to element
- Vary widely with:^[7]
 - Concentrations of solutions
 - Saturation of U and Pu in the system
 - Temperature of the solvents
- * The fraction of mass, f_o deposited in the organic phase, assuming a volume ratio between the aqueous and organic phases, V_R , is:

$$f_o = (1 + DC^{-1}V_R^{-1})^{-1}$$



Decontamination Factors - The Pot of gold

 After several cycles of Pu extraction/scrubbing/back-extraction are completed, the effectiveness of a PUREX cycle is described by the decontamination factor (DF):

$$DF_{j} = \frac{\left|\frac{c_{j}}{c_{Pu}}\right|_{initial}}{\left|\frac{c_{j}}{c_{Pu}}\right|_{final}}$$

- * DFs are characteristic of different process cycles
- Larger values (10⁷) for industrial scale PUREX (compared to benchtop)^[7, 1]



Complexity of reprocessing schemes

Worry about dependancies of of DC Worry about non equilibrium flow rates, blah blah. Show mixer settler columns, show batch. What I want to do, get some distribution coefficients develop a reasonable process for isolating a large fraction of Pu, then, based on process, calculate what the decontamination factor should be, and then actually measure it



Irradiation



Experiments

- Experiment 1
 - Purpose: quantify product recovery and DF values for single stage extraction and back extraction
 - Conditions: Latex Table
- Experiment 2
 - Purpose: recover a large fraction of Pu (4 extractions, 3 back extractions
 - Conditions Latex Table

Motivation Background Completed Work Future Work

Completed Work



Previous Experiment Results

Show the first table here



Previous Experiment Results

Calculate Compton edge for each peak

$$E_c = E_{e-}|_{(\theta=\pi)} = E_{\gamma} \left(\frac{2E_{\gamma}}{m_e c^2 + 2E_{\gamma}} \right) \tag{1}$$

Compton edges for gamma-ray sources:

Element	E_{γ} (keV)	Compton Edge (keV)
¹³³ Ba	356	207.25
¹³⁷ Cs	662	477.65
⁵⁴ Mn	835	639.36
²² Na (P.P.)	511	340.67
⁶⁰ Co	1173	963.42
²² Na	1274	1061.18
⁶⁰ Co	1332	1118.10



Previous Experiment Results

Show pretty plot

Motivation Background Completed Work Future Work

Future Work



Future Work

- Continue improving stilbene modeling parameters and capabilities in DRiFT
 - PSD using waveforms
 - Low-energy photon detection improvements

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- Begin modeling multiple stilbene detectors in different angle configurations
- Model full NEUANCE detector array
- Study detector cross-talk
- Compare MCNP6/DRiFT simulations using CGMF/FREYA against experimental measurements
 - > ²⁵²Cf: spontaneous fission
 - > ²³⁹Pu and ²³⁵U: neutron-induced fission

Questions?



References I

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