

Experimental Characterization of Pu Separation by PUREX Process on a Low-Burnup, Pseudo-Fast-Neutron Irradiated DUO<sub>2</sub> for Product Decontamination Factors and Nuclear Forensics

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Monday, February 27, 2017, 10:00 am

**AIEN 304** 



TEXAS A&M ENGINEERING EXPERIMENT STATION

NUCLEAR SECURITY
SCIENCE & POLICY INSTITUTE



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Gamma Spectroscopy Results

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### Motivation

- Current Events
  - Joint Comprehensive Plan of Action
  - Non-safeguarded reactors (Example: India)
  - Islamic State of Iraq and Syria
- Past Events
  - Septemer 11, 2001
- Limited scope of IAEA safeguards
- "the awful arithmetic of the atomic bomb" [1]
- ♦ Need for improved forensic capabilities<sup>[2, 3, 4]</sup>



### **Definitions**

- Special Nuclear Material (SNM)
  - ➤ Plutonium, <sup>233</sup>U, or <sup>235</sup>U
- What is Nuclear Forensics
  - Developing forensics evidence to identify the source of material and potentially the identity of the actor in a nuclear event (either using an RDD or a nuclear explosive)
- SNM origin attributes/indicators
  - Indicators or clues for SNM origin attribution. Examples include burnup, fluence rate, initial fuel enrichment, decay time, and fast-to-thermal irradiation ratios
- PUREX Decontamination Factors (DF)
  - A measure of the effectiveness with which separated Pu from irradiated fuel is decontaminated

$$DF_j = \frac{\frac{c_j}{c_{Pu}}|_{\text{initial}}}{\frac{c_j}{c_{Pu}}|_{\text{final}}}$$





## **National Context**

"The United States has developed a nuclear forensics capability that has been demonstrated in real-world incidents of **interdicted materials** and in exercises of actions required after a nuclear detonation. The committee, however, has concerns about the program and finds that without strong leadership, careful planning, and additional funds, these capabilities will decline" [2]

## Major areas of concern include:

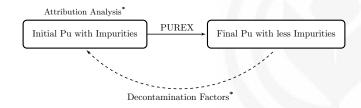
- Organization
- Sustainability
- \* Workforce and Infrastructure
- \* Procedures and Tools (predetonation)

### Forensic Context

- Nature of inverse problems
- Plutonium purification necessary for weapons production

$$^{238}U + n \rightarrow ^{239}U \xrightarrow{\beta^{-}} \xrightarrow{T_{1/2}=23 \text{ min}} Np \xrightarrow{\beta^{-}} \xrightarrow{7_{1/2}=2 \text{ d}} Pu$$

 Attribution for used or spent fuel has been previously studied [5, 6, 7]

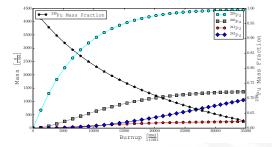






### **Nuclear Context**

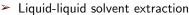
- Weapons-grade Pu can be extracted from reactor discharged fuel with a burnup of about 1 (GWD/tU)
- Pu isotopes produced in irradiated fuel can vary
- Two examples of reactors which can intentionally discharge low burned fuel for extracting weapon-grade Pu are:
  - > Fast Breeder Reactor, CANDU Reactor





### Chemical Context





- Many contacts:
- Distribution Coefficient (D): The ratio between the organic and aqueous phases (aka: D-values)

$$D = \frac{c_o}{c_{aq}}$$

- Specific element to element
- Vary widely<sup>[8]</sup>
- The fraction of mass,  $f_o$  deposited in the organic phase, assuming a volume ratio between the aqueous and organic phases,  $V_R$ , is:

$$f_o = (1 + D^{-1}V_R^{-1})^{-1}$$

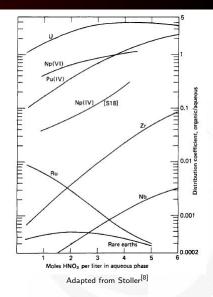


Boundary



### Chemical Context

- Lack of literature on decontamination factors and distribution coefficients for useful forensic elements (Cs, Sb, Eu, Rb, Sr, Nd, Pm, and Sm)
- With a known process and D-values, DF values for individual elements can be determined



organic solvent

phase

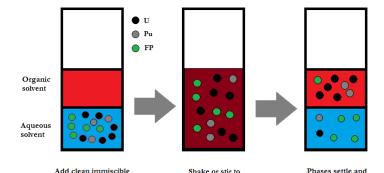


separate with

gravity

### Extraction

$$\begin{array}{l} UO_{2(aq)}^{2+} + 2NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow UO_{2}(NO_{3})_{2} \cdot 2TBP_{(o)}^{[9]} \\ Pu_{(aq)}^{4+} + 4NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow Pu(NO_{3})_{4} \cdot 2TBP_{(o)} \end{array}$$



allow molecules to

partition

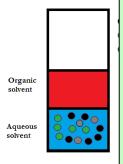




### Extraction

$$UO_{2(aq)}^{2+} + 2NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow UO_{2}(NO_{3})_{2} \cdot 2TBP_{(o)}^{[9]}$$

$$Pu_{(aq)}^{4+} + 4NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow Pu(NO_{3})_{4} \cdot 2TBP_{(o)}$$



Add clean immiscible organic solvent phase

$$M_{tot} = c_{A,i}V_A$$

Final 
$$(D = \frac{c_{o,f}}{c_{A,f}})$$
:

$$M_{tot} = c_{A,f} V_A + c_{o,f} V_o \label{eq:mtot}$$

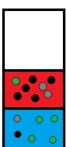
Solving for  $c_{o,f}$  in terms of D:

$$c_{o,f} = \frac{M_{tot}}{\frac{V_A}{D} + V_o}$$

Solving for  $\frac{c_{A,i}}{c_{o,f}}$ :

$$\frac{c_{A,i}}{c_{o,f}} = \frac{\frac{V_A}{D} + V_o}{V_A} = \frac{1}{D} + \frac{V_o}{V_A}$$

partition



Phases settle and separate with gravity

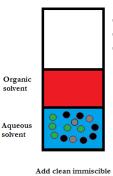




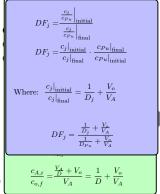
### Extraction

$$UO_{2(aq)}^{2+} + 2NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow UO_{2}(NO_{3})_{2} \cdot 2TBP_{(o)}^{[9]}$$

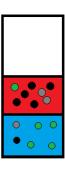
$$Pu_{(aq)}^{4+} + 4NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow Pu(NO_{3})_{4} \cdot 2TBP_{(o)}$$



Add clean immiscible organic solvent phase



partition

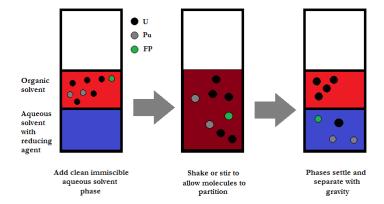


Phases settle and separate with gravity



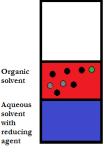


$$Pu(NO_3)_4(TBP)_{2(o)} + Fe^{2+}_{(aq)} \leftrightarrow Pu^{3+}_{(aq)} + 4NO^-_{3(aq)} + 2TBP_{(o)}^{[10]}$$





$$Pu(NO_3)_4(TBP)_{2(o)} + Fe^{2+}_{(aq)} \leftrightarrow Pu^{3+}_{(aq)} + 4NO^-_{3(aq)} + 2TBP_{(o)}^{[10]}$$



Add clean immiscible aqueous solvent phase Initial:

$$M_{org} = c_{o,f}V_o$$

Final 
$$(D_2 = \frac{c_{o,f2}}{c_{A2,f}})$$
:

$$M_{org} = c_{A2,f}V_{A2} + c_{o,f2}V_o \label{eq:morg}$$

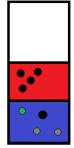
Solving for  $c_{A2,f}$  in terms of  $D_2$ :

$$c_{A2,f} = \frac{M_{org}}{V_{A2} + D_2V_o}$$

Solving for  $\frac{c_{A,i}}{c_{A2,f}}$  (note:  $c_{A,i}$  is from the *initial* aqueous phase):

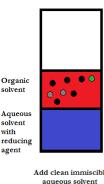
$$\frac{c_{A,i}}{c_{A2,f}} = \frac{1}{f_o} \frac{V_{A2} + D_2 V_o}{V_A}$$

partition

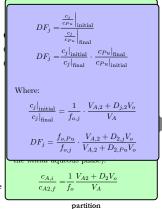


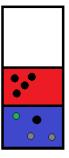
Phases settle and separate with gravity

$$Pu(NO_3)_4(TBP)_{2(o)} + Fe^{2+}_{(aq)} \leftrightarrow Pu^{3+}_{(aq)} + 4NO^-_{3(aq)} + 2TBP_{(o)}^{[10]}$$



Add clean immiscible aqueous solvent phase





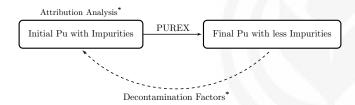
Phases settle and separate with gravity





### Decontamination Factors and their use

- After several cycles of Pu extraction/scrubbing/back-extraction are completed, the effectiveness of a PUREX cycle is described by the decontamination factor (DF):
- DFs are characteristic of different process cycles
- Larger values (10<sup>7</sup>) for industrial scale PUREX (compared to benchtop)<sup>[8, 9]</sup>





## Objectives I

### Characterize a 4 extraction 3 back-extraction PUREX process

Collect D-values for each step

Convert Gamma Spectrum to D-values

- Convert all mass spec data to D-values
- Collect DF-values for the process
  - Prepare alpha samples for each step (triplicate)
    - Analyze alpha samples for each step
  - □ Convert alpha spec + gamma spec data to DF values
  - Convert Mass spec data to DF values (published)
- Mathematically connect D-values to DFs
  - Derive equations with uncertainty propagation
  - Analyze connection with uncertainty





# Objectives II

#### **Determine attribution indicators:**

 Mathematically derive equations for above indicators with respect to one of the isotopes determined above

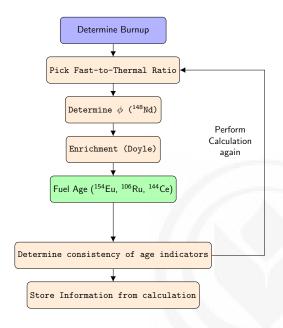


- Fast-to-thermal ratios (requires iteration)
- Program a system to iteratively solve for these parameters given heavy metal concentration ratios
  - Make a program that can read ENDF files for x-sections
     Create/Use a bateman solver with automated x-section modifications
     Create program to calculate single group x-sections from ENDF data and an assumed fast-to-thermal ratio
  - Couple all programs together in a single program
- Use above information to determine indicators for three sets of data

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# Present Status of the Question

- \* Stable noble fission gases as burnup verification<sup>[11]</sup>
- Determine burnup, enrichment, and fuel age from used fuel in a RDD<sup>[12]</sup>
- Analysis of purified plutonium isotopics for reactor type<sup>[13]</sup>
- PUREX co-processing DF values for U and Pu<sup>[14]</sup>
- PUREX D-values and DF values under numerous circumstances<sup>[9, 15, 16, 17, 18, 8]</sup>
  - ➤ DF values for <sup>106</sup>Ru and <sup>95</sup>Zr<sup>[8]</sup>
  - Compilation of D-values for U, Th, and Pu<sup>[19]</sup>
  - ightharpoonup D-values for rare earths, Pu, Th<sup>[17, 20, 21, 22, 23, 24, 25, 26, 27, 28]</sup>
  - ➤ Ga D-values<sup>[28]</sup>





## **Analytical Procedure**

❖ 12.9±0.1 mg of DUO<sub>2</sub> irradiated at HFIR

$$\begin{split} \frac{dn_i}{dt} &= -\lambda_i^{eff} \, n_i + \sum_{j=1}^N b_{j \to i}^{eff} n_j \\ \lambda_i^{eff} &= \lambda_i + \phi \sum_{j=1}^N \sigma_{i \to j} \\ b_{j \to i}^{eff} &= b_{j \to i} \lambda_j + \sigma_{j \to i} \phi + \gamma_{j \to i} \sigma_{j,f} \phi \\ \frac{d\vec{n}}{dt} &= \mathbf{A} \vec{n}(t) \to \vec{n} = \mathrm{e}^{\mathbf{A}t} \vec{n}_0 \end{split}$$





## Analytical Procedure - Burnup

- Operational Parameter
- Calculated:
  - Specific heat calculation on working fluid
  - Number and isotopes that fission in the system
  - burnup isotope indicator

$$BU = \frac{\text{Power}[\text{MW}] \cdot \text{days}}{m[\text{HM}]}$$
$$= \left[\frac{N^B}{N_0^{HM}}\right] \frac{N_A E_R}{\gamma_B} \cdot \frac{1}{M_0^{HM}}$$

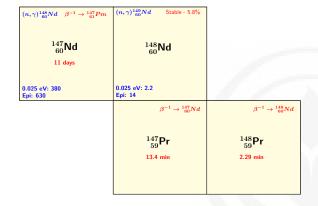




$(n,\gamma)^{137}_{55}Cs \qquad \beta^{-1} \to {}^{136}_{56}Ba$	$(n,\gamma)^{138}_{55}Cs$ $\beta^{-1} \to {}^{147}_{56}Ba$	
<sup>136</sup> Cs <sub>55</sub> Cs	<sup>137</sup> <sub>55</sub> Cs	
0.025 eV: 11 Epi: 57	0.025 eV: 0.2 Epi: 0.3	
	$(n,\gamma)^{137}_{54}Xe$ Stable 8.9%	$eta^{-1} ightarrow {}^{137}_{55}Cs$
	<sup>136</sup> <sub>54</sub> Xe	<sup>137</sup> Xe <sup>54</sup> Xe <sup>3.8 min</sup>
	0.025 eV: 0.2 Epi: 0.1	









## Analytical Procedure - Fluence Rate

- Burnup Indicator assumptions
  - Short lived precursors of same mass bin with small cross sections
  - Small contributions from other mass bins
  - > Stable

$$\phi pprox rac{\lambda_7}{\sigma_7 \left(rac{\gamma_7}{\gamma_8^* - \gamma_8} - 1
ight)}$$

- Assumptions:
  - $\triangleright$  Build in can be described by constant  $\phi$ , single group x-sections
  - ightharpoonup Constant fissionable material,  $\sigma_a$  for <sup>148</sup>Nd $\approx 0$
  - Cumulative yeild instantly arrives at <sup>147</sup>Nd
  - Utilizes a taylor series expansion



# Analytical Procedure - Initial Enrichment and Fuel Age

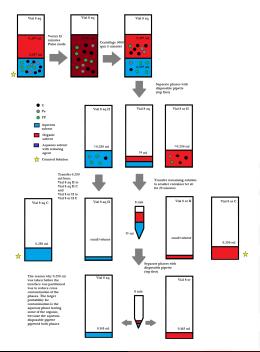
#### Initial Enrichment

- Heavy metal converts to heavier metal and to Fission products
- \* Account for in Burnup, and mass in heavy metals
- Solution assumes all higher actinides are built into the system from capture in <sup>238</sup>U

$$\epsilon_0 = \frac{N^{U238}(T)}{N_0^U} \left[ \frac{N^{U235}(T)}{N^{U238}(T)} + \frac{N^{U236}(T)}{N^{U238}(T)} \right] + \frac{M_0^U}{N_A E_R} BU(T) - G^{238} - G^{240} - G^{241}$$

### Fuel Age

$$t_d = -\frac{1}{\lambda} ln \left( \frac{N_{\text{measured}}}{N_{FOI}} \right)$$

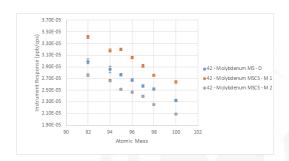






# Experimental Procedure - Mass Spectrometry

- NexION 300X quadrupole
- 7 different concoction standards (including Pu and U standards)
- Two point calibration curves
- Extrapolation for radioactive species

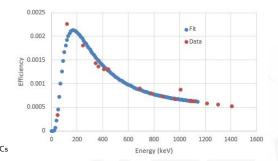






# Experimental Procedure - Gamma Spectrometry

- Canberra electrode coaxial HPGe
- <sup>152</sup>Eu liquid calibration source
- Program written to extract and analyze
   26 gamma peaks
   155 Eu, 154 Eu, 144 Ce, 125 Sb, 106 Rh, 134 Cs, 137 Cs

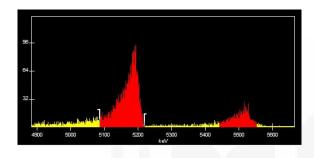






## Experimental Procedure - Alpha Spectrometry

- Passivated implanted planar silicon (PIPS) detector
- 4-peak Pu, Am, Gd, and Cm source from Eckert and Ziegler
- Samples prepared by evaporating 10-20 μl on aluminm surface
   <sup>239</sup>Pu, <sup>240</sup>Pu, <sup>241</sup>Am



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# Current and Expected Results





### Irradiation

- $12.9 \pm 0.1 \text{ mg of DUO}_2$  was irradiated
  - High Flux Isotope Reactor at Oak Ridge National Laboratory
- \* Burnup was  $4.43 \pm 0.31$  GWd/tHM<sup>[29]</sup> from <sup>137</sup>Cs
- \*  $0.196 \pm \text{mg}$  of total Pu was produced as measured by ICP-MS







# Dissolution of the spent fuel pellet



Objectives
Present Status of the Question
Current and Expected Results



### Glovebox











## **Experiments**

- Single stage extraction and back-extraction
  - Purpose: quantify product recovery, D-values and DF values for single stage extraction and back extraction
  - Conditions:

Starting Solution	Extraction Solution	Back extraction solution
4 M nitric acid	30% vol.% TBP, 70 vol.% kerosene	0.024 M ferrous sulfamate in 0.75 M nitric acid

- Multi-contact extraction and back-extraction
  - Purpose: Quantify DF for a process with 4 extractions, 3 back extractions
  - Conditions:

Starting Solution	Extraction Solution	Back extraction solution
4 M nitric acid	30% vol.% TBP, 70 vol.% kerosene	0.024 M ferrous sulfamate in 4 M nitric acid



# Mass spectrometry Results

Recoveries of U and Pu						
		Pu Recovery	U Recovery			
	Single stage	(83.4±9.5)%	(11.2±1.3)%			
	Multi-contact Cycle 1	$(99.7 \pm 4.2)\%$	$(6.8\pm0.3)\%$			
	Multi-contact Cycle 2	$(93.0\pm4.6)\%$	$(6.6\pm0.3)\%$			
	Overall Experiment 2	$(92.7\pm6.0)\%$	$(0.45\pm0.03)\%$			

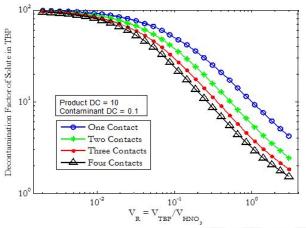


# Mass Spectrometry Results

## **Decontamination Factors**

Element (Z)	SS	Error	MC Cycle 1	Error	Isotopes Used
Rb(37)	39.0	5.9	11.8	0.8	<sup>85</sup> Rb
Sr(38)	283	43	84.6	5.9	<sup>90</sup> Sr
Mo(42)	5.7	0.8	1.9	0.2	<sup>97,98,100</sup> Mo
Ru(44)	59.2	6.4	16.6	2.5	<sup>101,102,104</sup> Ru
Pd(46)	65	14	8.9	1.2	<sup>110</sup> Pd
Cd(48)	74	17	22.1	2.5	<sup>112</sup> Cd
Cs(55)	177	28	52.9	3.9	<sup>133</sup> Cs
Ce(58)	43	16	11.5	4.9	<sup>140,142</sup> Ce
Nd(60)	19.2	2.1	5.9	0.4	<sup>143</sup> Nd
Pm(61)	12.8	1.9	3.9	0.3	<sup>147</sup> Pm
Sm(62)	11.5	1.5	3.6	0.3	<sup>151</sup> Sm
Eu(63)	10.0	1.4	3.6	0.3	<sup>154</sup> Eu
U(92)	7.4	1.2	14.7	0.9	<sup>238</sup> U

# Previous Experiment Results

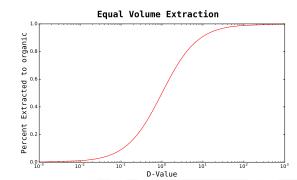


Decontamination Factors for multi-contact extraction.



### Gamma Spectroscopy Results: 4M HNO<sub>3</sub>, 2mM U, 30%vol.

D-Values:							
	Element (Z)	D-value	Error				
	Ce	0.04	0.01				
	Eu	0.08	0.02				
	Ru	0.04	0.02				
	Cs	3.9E-5	1.8E-5				
	Sb	0.005	0.007				
	Am	0.05	0.02				



#### Initial vs Final solutions (process)

# $c_{A,i}/c_{A,f}$ (Fission Products)

Avg	Error
11	3
5.5	1.1
5.4	1
11	3
180	50
13.7	0.3
700	300
1070	560
	11 5.5 5.4 11 180 13.7 700

#### Subsection 5

Future Work



# Objectives I

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# Objectives II

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  - Couple all programs together in a single program
- Use above information to determine indicators for three sets of data

# Questions?

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