

Experimental Characterization of Pu Separation by PUREX Process on a Low-Burnup, Pseudo-Fast-Neutron Irradiated DUO₂ for Product Decontamination Factors and Nuclear Forensics

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AIEN 304



TEXAS A&M ENGINEERING EXPERIMENT STATION

NUCLEAR SECURITY
SCIENCE & POLICY INSTITUTE

Introduction Objectives Methodology Current and Expected Results



Outline

Introduction

Motivation

Context

Background

Objectives

Methodology

Mathematical methodology Experimental Procedure

Current and Expected Results

Experiment

Mass Spectrometry

Gamma Spectroscopy Results

Future Work

Motivation

- Current Events
 - > Joint Comprehensive Plan of Action
 - Non-safeguarded reactors (Example: India)
 - Islamic State of Iraq and Syria
- Past Events
 - Septemer 11, 2001
- Limited scope of IAEA safeguards
- * "the awful arithmetic of the atomic bomb" [1]
- ♦ Need for improved forensic capabilities^[2, 3, 4]

Definitions

- Special Nuclear Material (SNM)
 - ➤ Plutonium, ²³³U, or ²³⁵U
- What is Nuclear Forensics
 - Developing forensics evidence to identify the source of material and potentially the identity of the actor in a nuclear event (either using an RDD or a nuclear explosive)
- SNM origin attributes/indicators
 - Indicators or clues for SNM origin attribution. Examples include burnup, fluence rate, initial fuel enrichment, decay time, and fast-to-thermal irradiation ratios
- PUREX Decontamination Factors (DF)
 - A measure of the effectiveness with which separated Pu from irradiated fuel is decontaminated

$$DF_j = \frac{\frac{c_j}{c_{Pu}}|_{\text{initial}}}{\frac{c_j}{c_{Pu}}|_{\text{final}}}$$

National Context

"The United States has developed a nuclear forensics capability that has been demonstrated in real-world incidents of **interdicted materials** and in exercises of actions required after a nuclear detonation. The committee, however, has concerns about the program and finds that without strong leadership, careful planning, and additional funds, these capabilities will decline" [2]

Major areas of concern include:

- Organization
- Sustainability
- * Workforce and Infrastructure
- * Procedures and Tools (predetonation)

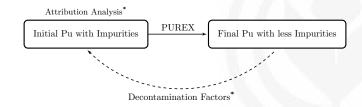


Forensic Context

- Nature of inverse problems
- Plutonium purification necessary for weapons production

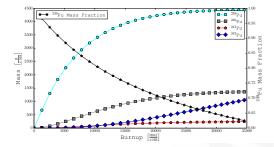
$$^{238}U + n \rightarrow ^{239}U \xrightarrow{\beta^{-}} ^{239}Np \xrightarrow{\beta^{-}} ^{239}T_{1/2} \stackrel{239}{\longrightarrow} Pu$$

 Attribution for used or spent fuel has been previously studied [5, 6, 7]



Nuclear Context

- Weapons-grade Pu can be extracted from reactor discharged fuel with a burnup of about 1 (GWD/tU)
- Pu isotopes produced in irradiated fuel can vary
- Two examples of reactors which can intentionally discharge low burned fuel for extracting weapon-grade Pu are:
 - ➤ Fast Breeder Reactor, CANDU Reactor





- HNO

Chemical Context

- Plutonium Uranium Redox EXtraction (PUREX)
 - ➤ Liquid-liquid solvent extraction
 - Many contacts:
- Distribution Coefficient (D): The ratio between the organic and aqueous phases (aka: D-values)

$$D = \frac{c_o}{c_{aq}}$$

- > Specific element to element
- ➤ Vary widely^[8]
- \succ The fraction of mass, f_o deposited in the organic phase, assuming a volume ratio between the aqueous and organic phases, V_R , is:

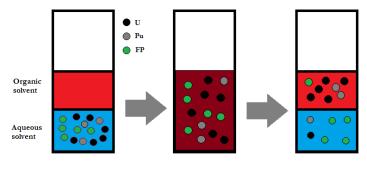
$$f_o = (1 + D^{-1}V_R^{-1})^{-1}$$





Extraction

$$\begin{array}{l} UO_{2(aq)}^{2+} + 2NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow UO_{2}(NO_{3})_{2} \cdot 2TBP_{(o)}^{[9]} \\ Pu_{(aq)}^{4+} + 4NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow Pu(NO_{3})_{4} \cdot 2TBP_{(o)} \end{array}$$



Add clean immiscible organic solvent phase Shake or stir to allow molecules to partition

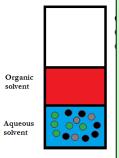




Extraction

$$UO_{2(aq)}^{2+} + 2NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow UO_{2}(NO_{3})_{2} \cdot 2TBP_{(o)}^{[9]}$$

$$Pu_{(aq)}^{4+} + 4NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow Pu(NO_{3})_{4} \cdot 2TBP_{(o)}$$



Add clean immiscible organic solvent phase

$$M_{tot} = c_{A,i}V_A$$

Final
$$(D = \frac{c_{o,f}}{c_{o,f}})$$
:

$$M_{tot} = c_{A,f}V_A + c_{o,f}V_o$$

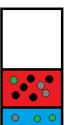
Solving for $c_{o,f}$ in terms of D:

$$c_{o,f} = \frac{M_{tot}}{\frac{V_A}{D} + V_o}$$

Solving for $\frac{c_{A,i}}{c_{o,f}}$:

$$\frac{c_{A,i}}{c_{o,f}} = \frac{\frac{V_A}{D} + V_o}{V_A} = \frac{1}{D} + \frac{V_o}{V_A}$$

partition

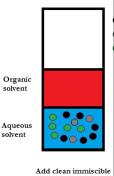




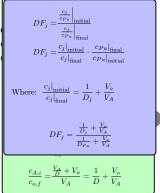
Extraction

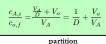
$$UO_{2(aq)}^{2+} + 2NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow UO_{2}(NO_{3})_{2} \cdot 2TBP_{(o)}^{[9]}$$

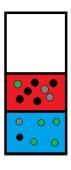
$$Pu_{(aq)}^{4+} + 4NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow Pu(NO_{3})_{4} \cdot 2TBP_{(o)}$$



organic solvent phase





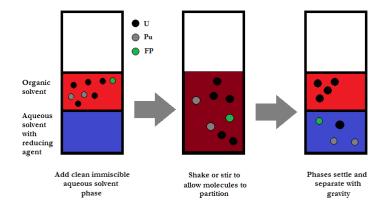






Back-Extraction

$$Pu(NO_3)_4(TBP)_{2(o)} + Fe^{2+}_{(aq)} \leftrightarrow Pu^{3+}_{(aq)} + 4NO^{-}_{3(aq)} + 2TBP_{(o)}^{[10]}$$





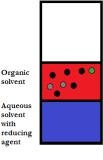


Back-Extraction

with

agent

$$Pu(NO_3)_4(TBP)_{2(o)} + Fe^{2+}_{(aq)} \leftrightarrow Pu^{3+}_{(aq)} + 4NO^-_{3(aq)} + 2TBP_{(o)}^{[10]}$$



Add clean immiscible aqueous solvent phase

Initial:

$$M_{org} = c_{o,f}V_o$$

Final
$$(D_2 = \frac{c_{o,f2}}{c_{A2,f}})$$
:

$$M_{org} = c_{A2,f} V_{A2} + c_{o,f2} V_o \label{eq:morg}$$

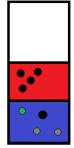
Solving for $c_{A2,f}$ in terms of D_2 :

$$c_{A2,f} = \frac{M_{org}}{V_{A2} + D_2 V_o}$$

Solving for $\frac{c_{A,i}}{c_{A2,f}}$ (note: $c_{A,i}$ is from the initial aqueous phase):

$$\frac{c_{A,i}}{c_{A2,f}} = \frac{1}{f_o} \frac{V_{A2} + D_2 V_o}{V_A}$$

partition

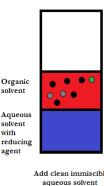




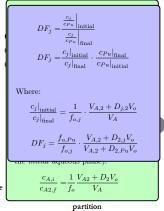


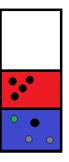
Back-Extraction

$$Pu(NO_3)_4(TBP)_{2(o)} + Fe_{(aq)}^{2+} \leftrightarrow Pu_{(aq)}^{3+} + 4NO_{3(aq)}^{-} + 2TBP_{(o)}^{[10]}$$



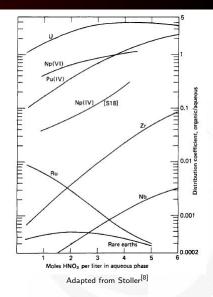
Add clean immiscible aqueous solvent phase





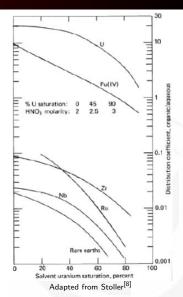
Chemical Context

- Lack of literature on decontamination factors and distribution coefficients for useful forensic elements (Cs, Sb, Eu, Rb, Sr, Nd, Pm, and Sm)
- With a known process and D-values, DF values for individual elements can be determined



Chemical Context

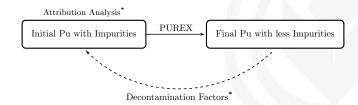
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Decontamination Factors and their use

- After several cycles of Pu extraction/scrubbing/back-extraction are completed, the effectiveness of a PUREX cycle is described by the decontamination factor (DF):
- DFs are characteristic of different process cycles
- Larger values (10⁷) for industrial scale PUREX (compared to benchtop)^[8, 9]







Objectives I

Characterize a 4 extraction 3 back-extraction PUREX process

- Collect D-values for each step
 - ¹⁴⁴Ce, ¹⁵⁵Eu*, ¹⁵⁴Eu*, ¹²⁵Sb, ¹⁰⁶Ru, ¹³⁴Cs, ¹³⁷Cs (Measured Gamma in triplicate) ^[5]
 - Convert Gamma Spectrum to D-values
 - 85Rb*, 90Sr*, 97,98,100 Mo, 101,102,104 Ru, 110 Pd, 112 Cd, 133 Cs*, 140,142 Ce, 143 Nd*,

 147 Pm*, 151 Sm*, 154 Eu*, U*, Pu* (Mass Spec)
 - Convert all mass spec data to D-values
- Collect DF-values for the process (and the two steps)
 - Prepare alpha samples for each step (triplicate)
 - Analyze alpha samples for each step

 - Convert Mass spec data to DF values (published)
- Mathematically connect D-values to DFs
 - Derive equations with uncertainty propagation
 - Analyze connection with uncertainty



Objectives II

Determine attribution indicators:

 Mathematically derive equations for above indicators with respect to one of the isotopes determined above



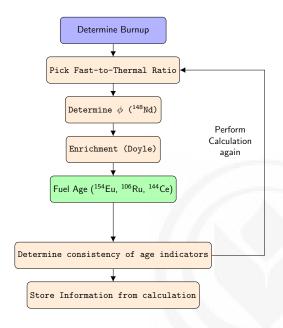
- Fast-to-thermal ratios (requires iteration)
- Program a system to iteratively solve for these parameters given heavy metal concentration ratios
 - Make a program that can read ENDF files for x-sections
 Create/Use a bateman solver with automated x-section modifications
 Create program to calculate single group x-sections from ENDF data and an assumed fast-to-thermal ratio
 - Couple all programs together in a single program
- Use above information to determine indicators for three sets of data

Present Status of the Question

- ❖ Stable noble fission gases as burnup verification^[11]
- Determine burnup, enrichment, and decay time from used fuel in a RDD^[12]
- Analysis of purified plutonium isotopics for reactor type^[13]
- PUREX co-processing DF values for U and Pu^[14]
- PUREX D-values and DF values under numerous circumstances^[9, 15, 16, 17, 18, 8]
 - ➤ DF values for ¹⁰⁶Ru and ⁹⁵Zr^[8]
 - Compilation of D-values for U, Th, and Pu^[19]
 - ightharpoonup D-values for rare earths, Pu, Th^[17, 20, 21, 22, 23, 24, 25, 26, 27, 28]
 - ➤ Gd D-values^[28]

Subsection 1

Mathematical methodology



Analytical Procedure

❖ 12.9±0.1 mg of DUO₂ irradiated at HFIR

$$\begin{split} \frac{dn_i}{dt} &= -\lambda_i^{eff} \, n_i + \sum_{j=1}^N b_{j \to i}^{eff} n_j \\ \lambda_i^{eff} &= \lambda_i + \phi \sum_{j=1}^N \sigma_{i \to j} \\ b_{j \to i}^{eff} &= b_{j \to i} \lambda_j + \sigma_{j \to i} \phi + \gamma_{j \to i} \sigma_{j,f} \phi \\ \frac{d\vec{n}}{dt} &= \mathbf{A} \vec{n}(t) \to \vec{n} = \mathrm{e}^{\mathbf{A}t} \vec{n}_0 \end{split}$$





Analytical Procedure - Burnup

- Operational Parameter
- Calculated:
 - Specific heat calculation on working fluid
 - Number and isotopes that fission in the system
 - burnup isotope indicator

$$BU = \frac{\text{Power}[\text{MW}] \cdot \text{days}}{m[\text{HM}]}$$
$$= \left[\frac{N^B}{N_0^{\text{HM}}}\right] \frac{N_A E_R}{\gamma_B} \cdot \frac{1}{M_0^{\text{HM}}}$$





Analytical Procedure - Burnup

$(n,\gamma)^{137}_{55}Cs \qquad \beta^{-1} \to {}^{136}_{56}Ba$	$(n,\gamma)^{138}_{55}Cs$ $\beta^{-1} \to {}^{147}_{56}Ba$	
136 Cs 55 Cs 13 days	¹³⁷ ₅₅ Cs	
0.025 eV: 11 Epi: 57	0.025 eV: 0.2 Epi: 0.3	1/
	$(n,\gamma)^{137}_{54}Xe$ Stable 8.9%	$\beta^{-1} \rightarrow {}^{137}_{55}Cs$
	¹³⁶ ₅₄ Xe	¹³⁷ Xe ⁵⁴ Xe ^{3.8 min}
	0.025 eV: 0.2 Epi: 0.1	





Analytical Procedure - Burnup

$(n,\gamma)^{148}_{60}Nd \beta^{-1} \to {}^{147}_{61}Pm$	$(n,\gamma)^{-1}_{60}Nd$ Stable - 5.8%	
¹⁴⁷ Nd ₆₀ Nd	¹⁴⁸ ₆₀ Nd	
0.025 eV: 380 Epi: 630	0.025 eV: 2.2 Epi: 14	1/
	$\beta^{-1} \rightarrow {}^{147}_{60} Nd$	$\beta^{-1} \rightarrow {}^{148}_{60}Nd$
	¹⁴⁷ ₅₉ Pr	¹⁴⁸ ₅₉ Pr
	13.4 min	2.29 min

(m =) 149 N/d Caphle E 00/





Analytical Procedure - Fluence Rate

- Burnup Indicator assumptions
 - Short lived precursors of same mass bin with small cross sections
 - > Small contributions from other mass bins
 - > Stable

$$\phi \approx \frac{\lambda_7}{\sigma_7 \left(\frac{\gamma_7}{\gamma_8^* - \gamma_8} - 1\right)}$$

- Assumptions:
 - \triangleright Build in can be described by constant ϕ , single group x-sections
 - ightharpoonup Constant fissionable material, σ_a for ¹⁴⁸Nd \approx 0
 - Cumulative yeild instantly arrives at ¹⁴⁷Nd
 - Utilizes a taylor series expansion





Analytical Procedure - Initial Enrichment and Decay Time

Initial Enrichment

- Heavy metal converts to heavier metal and to Fission products
- * Account for in Burnup, and mass in heavy metals
- Solution assumes all higher actinides are built into the system from capture in ²³⁸U

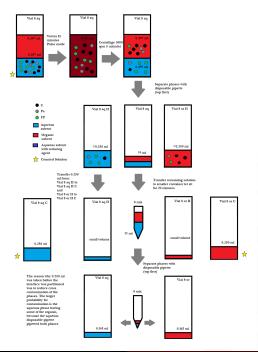
$$\epsilon_0 = \frac{N^{U238}(T)}{N_0^U} \left[\frac{N^{U235}(T)}{N^{U238}(T)} + \frac{N^{U236}(T)}{N^{U238}(T)} \right] + \frac{M_0^U}{N_A E_R} BU(T) - G^{238} - G^{240} - G^{241}$$

Decay Time

$$t_d = -\frac{1}{\lambda} ln \left(\frac{N_{\text{measured}}}{N_{FOI}} \right)$$

Subsection 2

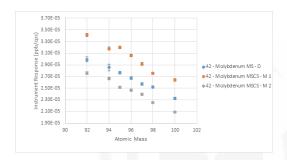
Experimental Procedure





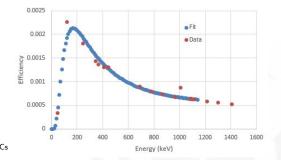
Experimental Procedure - Mass Spectrometry

- NexION 300X quadrupole
- 7 different concoction standards (including Pu and U standards)
- Two point calibration curves
- Extrapolation for radioactive species



Experimental Procedure - Gamma Spectrometry

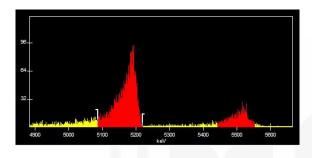
- Canberra electrode coaxial HPGe
- ¹⁵²Eu liquid calibration source
- Program written to extract and analyze
 26 gamma peaks
 155 Eu. 154 Eu. 144 Ce. 125 Sb. 106 Rb. 134 Cs. 137 Cs.





Experimental Procedure - Alpha Spectrometry

- Passivated implanted planar silicon (PIPS) detector
- 4-peak Pu, Am, Gd, and Cm source from Eckert and Ziegler
- Samples prepared by evaporating 10-20 μl on aluminm surface
 ²³⁹Pu, ²⁴⁰Pu, ²⁴¹Am



Introduction Objectives Methodology Current and Expected Results

Current and Expected Results

Irradiation

- 12.9 \pm 0.1 mg of DUO₂ was irradiated
 - High Flux Isotope Reactor at Oak Ridge National Laboratory
- * Burnup was 4.43 ± 0.31 GWd/tHM^[29] from ¹³⁷Cs
- * $0.196 \pm \text{mg}$ of total Pu was produced as measured by ICP-MS



Objectives
Methodology
Current and Expected Results



Dissolution of the spent fuel pellet



Objectives
Methodology
Current and Expected Results



Glovebox











Experiments

Conditioned solutions with sodium nitrite ($Pu^{6+} \rightarrow Pu^{4+}$)

- Single contact extraction and back-extraction
 - Purpose: quantify product recovery, D-values and DF values for single contact extraction and back extraction
 - Conditions:

Starting Solution	Extraction Solution	Back extraction solution
4 M nitric acid	30% vol.% TBP, 70 vol.% kerosene	0.024 M ferrous sulfamate in 0.75 M nitric acid

- Multi-contact extraction and back-extraction
 - Purpose: Quantify DF for a process with 4 extractions, 3 back extractions
 - Conditions:

Starting Solution	Extraction Solution	Back extraction solution	
4 M nitric acid	30% vol.% TBP, 70 vol.% kerosene	0.024 M ferrous sulfamate in 4 M nitric acid	





Mass spectrometry Results

Recoveries of U and Pu					
		Pu Recovery	U Recovery		
	Single contact	(83.4±9.5)%	$(11.2\pm1.3)\%$		
	Multi-contact Process 1	$(99.7\pm4.2)\%$	$(6.8\pm0.3)\%$		
	Multi-contact Process 2	$(93.0\pm4.6)\%$	$(6.6\pm0.3)\%$		
	Overall Experiment 2	$(92.7\pm6.0)\%$	$(0.45\pm0.03)\%$		





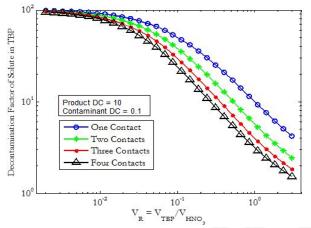
Mass Spectrometry Results

Decontamination Factors

Element (Z)	SS	Error	MC Cycle 1	Error	Isotopes Used
Rb(37)	39.0	5.9	11.8	0.8	⁸⁵ Rb
Sr(38)	283	43	84.6	5.9	⁹⁰ Sr
Mo(42)	5.7	0.8	1.9	0.2	97,98,100 Mo
Ru(44)	59.2	6.4	16.6	2.5	^{101,102,104} Ru
Pd(46)	65	14	8.9	1.2	¹¹⁰ Pd
Cd(48)	74	17	22.1	2.5	¹¹² Cd
Cs(55)	177	28	52.9	3.9	¹³³ Cs
Ce(58)	43	16	11.5	4.9	^{140,142} Ce
Nd(60)	19.2	2.1	5.9	0.4	¹⁴³ Nd
Pm(61)	12.8	1.9	3.9	0.3	¹⁴⁷ Pm
Sm(62)	11.5	1.5	3.6	0.3	¹⁵¹ Sm
Eu(63)	10.0	1.4	3.6	0.3	¹⁵⁴ Eu
U(92)	7.4	1.2	14.7	0.9	²³⁸ U



Previous Experiment Results



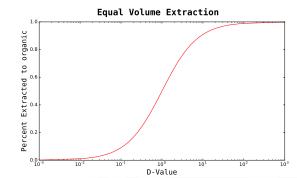
Decontamination Factors for multi-contact extraction.





Gamma Spectroscopy Results: 4M HNO₃, 2mM U, 30%vol TBP

D-Values:				
	Element (Z)	D-value	STD	
	Ce	0.04	0.01	
	Eu	0.08	0.02	
	Ru	0.04	0.02	
	Cs	3.9E-5	1.8E-5	
	Sb	0.005	0.007	
	Am	0.05	0.02	





Initial vs Final solutions (process)

$c_{A,i}/c_{A,f}$ (Fission Products)

Element (Z)	Avg	Error
¹⁴⁴ Ce (80 keV)	11	3
¹⁵⁵ Eu (105 keV)	5.5	1.1
¹⁵⁴ Eu	5.4	1
¹⁴⁴ Ce (133 keV)	11	3
¹²⁵ Sb	180	50
¹⁰⁶ Ru	13.7	0.3
¹³⁴ Cs	700	300
¹³⁷ Cs	1070	560

Subsection 4

Future Work





Objectives I

Characterize a 4 extraction 3 back-extraction PUREX process

Collect D-values for each step

Convert Gamma Spectrum to D-values

- Convert all mass spec data to D-values
- Collect DF-values for the process (and the two steps)
 - Prepare alpha samples for each step (triplicate)
 - Analyze alpha samples for each step

 - Convert Mass spec data to DF values (published)
- Mathematically connect D-values to DFs
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Objectives II

Determine attribution indicators:

 Mathematically derive equations for above indicators with respect to one of the isotopes determined above



- Fast-to-thermal ratios (requires iteration)
- Program a system to iteratively solve for these parameters given heavy metal concentration ratios
 - Make a program that can read ENDF files for x-sections
 Create/Use a bateman solver with automated x-section modifications
 Create program to calculate single group x-sections from ENDF data and an assumed fast-to-thermal ratio
 - Couple all programs together in a single program
- Use above information to determine indicators for three sets of data

Questions?

References I

- [1] Dwight D Eisenhower. Atoms for peace speech. Voices of Democracy, 1953.
- [2] Nuclear Forensics: A Capability at Risk (Abbreviated Version). The National Academies Press, Washington, DC, 2010.
- [3] AAAS/APS. Nuclear forensics: Role, state of the art and program needs. Report, AAAS/APS, 2008.
- [4] Kenton J Moody, Ian D Hutcheon, and Patrick M Grant. Nuclear forensic analysis. CRC Press, 2014.
- [5] Sunil S Chirayath, Jeremy M Osborn, and Taylor M Coles. Trace fission product ratios for nuclear forensics attribution of weapons-grade plutonium from fast and thermal reactors. *Science and Global Security*, 23(1):48–67, 2015.
- [6] Mark Robert Scott. Nuclear forensics: attributing the source of spent fuel used in an RDD event. PhD thesis, Texas A and M University, 2005.
- [7] Alexander Glaser. Isotopic signatures of weapon-grade plutonium from dedicated natural uranium-fueled production reactors and their relevance for nuclear forensic analysis. *Nuclear Science and Engineering*, 163(1):26–33, 2009.



References II

- [8] Sidney M Stoller, Walter Henry Zinn, Stuart MacLain, and Atomic Energy Commission USA. Reactor handbook. 2. Fuel reprocessing. Interscience Publ., 1961.
- [9] M Benedict, H Levi, and T Pigford. Nuclear chemical engineering. Nucl. Sci. Eng.: (United States), 82(4), 1982.
- [10] RJM Konings, LR Morss, J Fuger, LR Morss, NM Edelstein, and J Fuger. The chemistry of the actinide and transactinide elements. *Springer, Dordrecht*, 4:2113–224, 2006.
- [11] William S Charlton, Bryan L Fearey, Charles W Nakhleh, Theodore A Parish, Robert T Perry, Jane Poths, John R Quagliano, William D Stanbro, and William B Wilson. Operator declaration verification technique for spent fuel at reprocessing facilities. Nuclear Instruments and Methods in Physics Research Section B: Beam Interactions with Materials and Atoms, 168(1):98–108, 2000.
- [12] Mark Robert Scott. Nuclear forensics: attributing the source of spent fuel used in an RDD event. Thesis, 2005.
- [13] Alexander Glaser. Isotopic signatures of weapon-grade plutonium from dedicated natural uranium-fueled production reactors and their relevance for nuclear forensic analysis. *Nuclear Science and Engineering*, 163(1):26–33, 2009.

References III

- [14] Okan H Zabunoglu and Levent Ozdemir. Purex co-processing of spent lwr fuels: flow sheet. *Annals of Nuclear Energy*, 32(2):151–162, 2005.
- [15] W. B. Lanham and A. T. Gresky. Purex process laboratory development. Oak Ridge National Laboratory, USAEC Report ORNL-717, 1950.
- [16] A. J. Arker. Terminal report on purex program in kapl separations pilot plant. Knolls Atomic Power Laboratory, 1954.
- [17] D. O. Darby and J. M. Chandler. Terminal report for the ornl pilot plant investigation of the purex process. *Oak Ridge National Laboratory*, USAEC Report ORNL -1519, 1954.
- [18] E.R. Irish and Reas W.H. The purex process-a solvent extraction reprocessing method for irradiated uranium. 1957.
- [19] Thomas H. Siddall, W. E. Prout, Sidney G. Parker, U. S. Atomic Energy Commission, Laboratory Savannah River, E. I. du Pont de Nemours, and Company. Equilibrium distribution data for purex and similar extraction processes. DP; 53. E.I. du Pont de Nemours and Co., Explosives Dept., Atomic Energy Division, Technical Division, Savannah River Laboratory, 1957.





References IV

- [20] K Alcock, FC Bedford, WH Hardwick, and HAC McKay. Tri-n-butyl phosphate as an extracting solvent for inorganic nitrates-i: Zirconium nitrate. *Journal of Inorganic and Nuclear Chemistry*, 4(2):100–105, 1957.
- [21] K Alcock, FC Bedford, WH Hardwick, and HAC McKay. Tri-n-butyl phosphate as an extracting solvent for inorganic nitrates-i: Zirconium nitrate. *Journal of Inorganic and Nuclear Chemistry*, 4(2):100–105, 1957.
- [22] K Alcock, GF Best, E Hesford, and HAC McKay. Tri-n-butyl phosphate as an extracting solvent for inorganic nitrates-v: Further results for the tetra-and hexavalent actinide nitrates. *Journal of Inorganic and Nuclear Chemistry*, 6(4):328–333, 1958.
- [23] GF Best, E Hesford, and HAC McKay. Tri-n-butyl phosphate as an extracting agent for inorganic nitrates-vii: The trivalent actinide nitrates. *Journal of Inorganic and Nuclear Chemistry*, 12(1):136–140, 1959.
- [24] GF Best, HAC McKay, and PR Woodgate. Tri-n-butyl phosphate as an extracting solvent for inorganic nitrates—iii the plutonium nitrates. *Journal of Inorganic and Nuclear Chemistry*, 4(5):315–320, 1957.



References V

- [25] E Hesford, EE Jackson, and HAC McKay. Tri-n-butyl phosphate as an extracting agent for inorganic nitrates—vi further results for the rare earth nitrates. *Journal* of *Inorganic and Nuclear Chemistry*, 9(3-4):279–289, 1959.
- [26] E Hesford, HAC McKay, and D Scargill. Tri-n-butyl phosphate as an extracting solvent for inorganic nitrates—iv thorium nitrate. *Journal of Inorganic and Nuclear Chemistry*, 4(5):321–325, 1957.
- [27] D Scargill, K Alcock, JM Fletcher, E Hesford, and HAC McKay. Tri-n-butyl phosphate as an extracting solvent for inorganic nitrates-ii yttrium and the lower lanthanide nitrates. *Journal of Inorganic and Nuclear Chemistry*, 4(5):304–314, 1957.
- [28] ED Collins, DO Campbell, and LK Felker. Measurement of achievable plutonium decontamination from gallium by means of purex solvent extraction. ORNL/TM-1999/312, Oak Ridge National Laboratory, 2000.
- [29] Mathew Wayne Swinney. Experimental and Computational Assessment of Trace Nuclide Ratios in Weapons Grade Plutonium for Nuclear Forensics Analysis. PhD thesis, 2015.
- [30] Kenneth D Kok. Nuclear engineering handbook, volume 60. CRC Press, 2009.