

Experimental Characterization of Pu Separation by PUREX Process on a Low-Burnup, Pseudo-Fast-Neutron Irradiated DUO₂ for Product Decontamination Factors and Nuclear Forensics

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TEXAS A&M ENGINEERIN

AIEN 304

NUCLEAR SECURITY
SCIENCE & POLICY INSTITUTE



Outline

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Gamma Spectroscopy Results

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Motivation

- Current Events
 - Joint Comprehensive Plan of Action
 - Non-safeguarded reactors
 - Islamic State of Iraq and Syria
- Past Events
 - Septemer 11, 2001
- Limited scope of IAEA safeguards
- "the awful arithmetic of the atomic bomb" [1]
- ♦ Need for improved forensic capabilities^[2, 3, 4]

Definitions

- Special Nuclear Material (SNM)
 - ➤ Plutonium, ²³³U, or ²³⁵U
- Nuclear Forensics
 - The investiative activity that surrounds the search for attributes of undetermined radioactive specimens for the purpose of attribution.
- SNM origin attributes/indicators
 - Indicators or clues for SNM origin attribution. Examples include burnup, fluence rate, initial fuel enrichment, fuel age, and fast-to-thermal irradiation ratios
- Decontamination Factors (DF)
 - A measure of the effectiveness with which a product is decontaminated from a contaminant

$$DF_j = \frac{\frac{c_j}{c_{Pu}}|\text{initial}}{\frac{c_j}{c_{Pu}}|\text{final}}$$

National Context

"The United States has developed a nuclear forensics capability that has been demonstrated in real-world incidents of **interdicted materials** and in exercises of actions required after a nuclear detonation. The committee, however, has concerns about the program and finds that without strong leadership, careful planning, and additional funds, these capabilities will decline" [2]

Major areas of concern include:

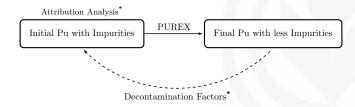
- Organization
- Sustainability
- Workforce and Infrastructure
- * Procedures and Tools

Forensic Context

- Nature of inverse problems
- Plutonium purification necessary for weapons production

$$^{238}U + n \rightarrow ^{239}U \xrightarrow{\beta^{-}} \xrightarrow{T_{1/2}=23 \text{ min}} ^{239}Np \xrightarrow{\beta^{-}} \xrightarrow{239} Pu$$

 Attribution for unpurified Pu has been previously studied [5, 6, 7]

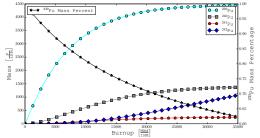






Nuclear Context

- ❖ Weapons-grade Pu can be extracted from reactor discharged fuel with a burnup of about 1 (GWD/tU)
- Pu isotopes produced in irradiated fuel can vary
- Two examples of reactors which can intentionally discharge low burned fuel for extracting weapon-grade Pu are:
 - Fast Breeder Reactor, CANDU Reactor



Chemical Context

- Plutonium Uranium Redox EXtraction (PUREX)
 - Liquid-liquid solvent extraction
 - Many stages:
- Distribution Coefficient (D): The ratio between the organic and aqueous phases (aka: D-values)

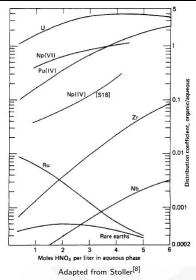
$$D = \frac{c_o}{c_{aq}}$$

- Specific element to element
- Vary widely^[8]
- The fraction of mass, f_o deposited in the organic phase, assuming a volume ratio between the aqueous and organic phases, V_R , is:

$$f_o = (1 + D^{-1}V_R^{-1})^{-1}$$

Chemical Context

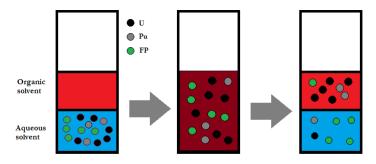
- Lack of literature on decontamination factors and distribution coefficients for useful forensic elements (Cs, Sb, Eu, Rb, Sr, Nd, Pm, and Sm)
- With a known process and D-values, DF values for individual elements can be determined





Extraction

$$\begin{array}{l} UO_{2(aq)}^{2+} + 2NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow UO_{2}(NO_{3})_{2} \cdot 2TBP_{(o)}^{[9]} \\ Pu_{(aq)}^{4+} + 4NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow Pu(NO_{3})_{4} \cdot 2TBP_{(o)} \end{array}$$

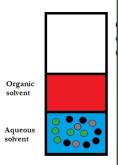


Add clean immiscible organic solvent phase Shake or stir to allow molecules to partition Phases settle and separate with gravity

Extraction

$$UO_{2(aq)}^{2+} + 2NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow UO_{2}(NO_{3})_{2} \cdot 2TBP_{(o)}^{[9]}$$

$$Pu_{(aq)}^{4+} + 4NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow Pu(NO_{3})_{4} \cdot 2TBP_{(o)}$$



Add clean immiscible organic solvent phase

Final
$$(D = \frac{c_{o,f}}{c_{A,f}})$$
:

$$M_{tot} = c_{A,f} V_A + c_{o,f} V_o \label{eq:mtot}$$

 $M_{tot} = c_{A,i}V_A$

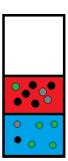
Solving for $c_{o,f}$ in terms of D:

$$c_{o,f} = \frac{M_{tot}}{\frac{V_A}{V_A} + V}$$

Solving for $\frac{c_{A,i}}{c_{o,f}}$:

$$\frac{c_{A,i}}{c_{o,f}} = \frac{\frac{V_A}{D} + V_o}{V_A} = \frac{1}{D} + \frac{V_o}{V_A} \label{eq:cases}$$

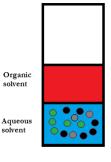
partition



Phases settle and separate with gravity

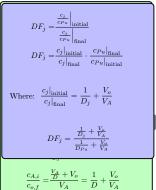
Extraction

$$\begin{array}{l} UO_{2(aq)}^{2+} + 2NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow UO_{2}(NO_{3})_{2} \cdot 2TBP_{(o)}^{[9]} \\ Pu_{(aq)}^{4+} + 4NO_{3(aq)}^{-} + 2TBP_{(o)} \leftrightarrow Pu(NO_{3})_{4} \cdot 2TBP_{(o)} \end{array}$$

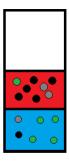


Add clean immiscible organic solvent phase

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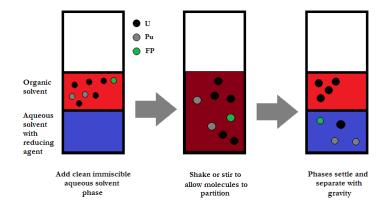


$$\frac{c_{A,i}}{c_{o,f}} = \frac{\frac{V_A}{D} + V_o}{V_A} = \frac{1}{D} + \frac{V_o}{V_A}$$

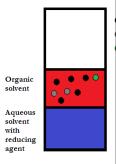


Phases settle and separate with

$$Pu(NO_3)_4(TBP)_{2(o)} + Fe^{2+}_{(aq)} \leftrightarrow Pu^{3+}_{(aq)} + 4NO^-_{3(aq)} + 2TBP_{(o)}{}^{[10]}$$



$$Pu(NO_3)_4(TBP)_{2(o)} + Fe_{(aq)}^{2+} \leftrightarrow Pu_{(aq)}^{3+} + 4NO_{3(aq)}^{-} + 2TBP_{(o)}^{[10]}$$



Add clean immiscible aqueous solvent phase

Initial:

$$M_{org} = c_{o,f}V_o$$

Final
$$(D_2 = \frac{c_{o,f2}}{c_{A2,f}})$$
:

$$M_{org} = c_{A2,f}V_{A2} + c_{o,f2}V_o$$

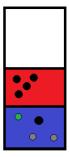
Solving for $c_{A2,f}$ in terms of D_2 :

$$c_{A2,f} = \frac{M_{org}}{V_{A2} + D_2V_2}$$

Solving for $\frac{c_{A,i}}{c_{A2,f}}$ (note: $c_{A,i}$ is from the *initial* aqueous phase):

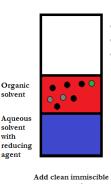
$$\frac{c_{A,i}}{c_{A2,f}} = \! \frac{1}{f_o} \frac{V_{A2} + D_2 V_o}{V_A}$$

partition

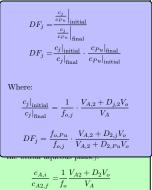


Phases settle and separate with gravity

$$Pu(NO_3)_4(TBP)_{2(o)} + Fe^{2+}_{(aq)} \leftrightarrow Pu^{3+}_{(aq)} + 4NO^-_{3(aq)} + 2TBP_{(o)}^{[10]}$$



aqueous solvent phase



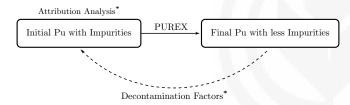
partition



Phases settle and separate with gravity

Decontamination Factors and their use

- After several cycles of Pu extraction/scrubbing/back-extraction are completed, the effectiveness of a PUREX cycle is described by the decontamination factor (DF):
- DFs are characteristic of different process cycles
- Larger values (10⁷) for industrial scale PUREX (compared to benchtop)^[8, 9]



Objectives I

Characterize a 4 extraction 3 back-extraction PUREX process

Collect D-values for each step

¹⁴⁷Pm*, ¹⁵¹Sm*, ¹⁵⁴Eu*, U*, Pu* (Mass Spec)

Collect DF-values for the process

- Prepare alpha samples for each step (triplicate)
 - Analyze alpha samples for each step
- □ Convert alpha spec + gamma spec data to DF values
- Convert Mass spec data to DF values (published)
- Mathematically connect D-values to DFs
 - Derive equations with uncertainty propagation
 - Analyze connection with uncertainty



Objectives II

Determine attribution indicators:

 Mathematically derive equations for above indicators with respect to one of the isotopes determined above

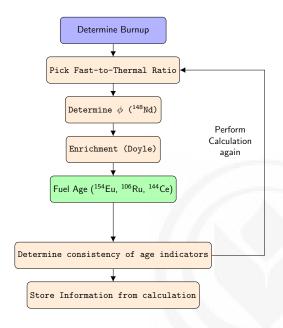


- Fast-to-thermal ratios (requires iteration)
- Program a system to iteratively solve for these parameters given heavy metal concentration ratios
 - Make a program that can read ENDF files for x-sections
 Create/Use a bateman solver with automated x-section modifications
 Create program to calculate single group x-sections from ENDF data and an assumed fast-to-thermal ratio
 - Couple all programs together in a single program
- Use above information to determine indicators for three sets of data

Present Status of the Question

- Stable noble fission gases as burnup verification^[11]
- Determine burnup, enrichment, and fuel age from used fuel in a RDD^[12]
- Analysis of purified plutonium isotopics for reactor type^[13]
- PUREX co-processing DF values for U and Pu^[14]
- PUREX D-values and DF values under numerous circumstances^[9, 15, 16, 17, 18, 8]
 - ➤ DF values for ¹⁰⁶Ru and ⁹⁵Zr^[8]
 - Compilation of D-values for U, Th, and Pu^[19]
 - ightharpoonup D-values for rare earths, Pu, Th^[17, 20, 21, 22, 23, 24, 25, 26, 27, 28]
 - ➤ Ga D-values^[28]

Procedure



Analytical Procedure

♦ 12.9±0.1 mg of DUO₂ irradiated at HFIR

$$\begin{split} \frac{dn_i}{dt} &= -\lambda_i^{eff} \, n_i + \sum_{j=1}^N b_{j \to i}^{eff} n_j \\ \lambda_i^{eff} &= \lambda_i + \phi \sum_{j=1}^N \sigma_{i \to j} \\ b_{j \to i}^{eff} &= b_{j \to i} \lambda_j + \sigma_{j \to i} \phi + \gamma_{j \to i} \sigma_{j,f} \phi \\ \frac{d\vec{n}}{dt} &= \mathbf{A} \vec{n}(t) \to \vec{n} = e^{\mathbf{A}t} \vec{n}_0 \end{split}$$

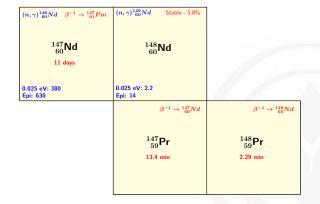
Analytical Procedure - Burnup

- Operational Parameter
- Calculated:
 - Specific heat calculation on working fluid
 - Number and isotopes that fission in the system
 - burnup isotope indicator

$$BU = \frac{\text{Power}[\text{MW}] \cdot \text{days}}{m[\text{HM}]}$$
$$= \left[\frac{N^B}{N_0^{HM}}\right] \frac{N_A E_R}{\gamma_B} \cdot \frac{1}{M_0^{HM}}$$



$(n,\gamma)^{137}_{55}Cs$ $\beta^{-1} o {}^{136}_{56}Ba$	$(n,\gamma)^{138}_{55}Cs$ $\beta^{-1} \to {}^{147}_{56}Ba$	
136 Cs 55 Cs 13 days	¹³⁷ ₅₅ Cs	
0.025 eV: 11 Epi: 57	0.025 eV: 0.2 Epi: 0.3	///
	$(n,\gamma)^{137}_{54}Xe$ Stable 8.9%	$\beta^{-1} \rightarrow {}^{137}_{55}Cs$
	¹³⁶ ₅₄ Xe	¹³⁷ Xe ^{3.8} min
	0.025 eV: 0.2 Epi: 0.1	



Analytical Procedure - Fluence Rate

- Burnup Indicator assumptions
 - Short lived precursors of same mass bin with small cross sections
 - > Small contributions from other mass bins
 - Stable

$$\phi \approx \frac{\lambda_7}{\sigma_7 \left(\frac{\gamma_7}{\gamma_8^* - \gamma_8} - 1\right)}$$

- Assumptions:
 - \triangleright Build in can be described by constant ϕ , single group x-sections
 - ightharpoonup Constant fissionable material, σ_a for 148 Nd ≈ 0
 - Cumulative yeild instantly arrives at ¹⁴⁷Nd
 - Utilizes a taylor series expansion

Analytical Procedure - Initial Enrichment and Fuel Age

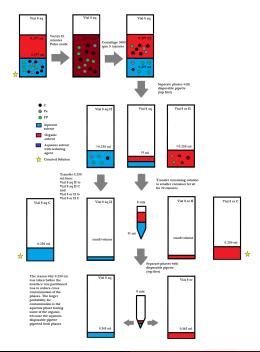
Initial Enrichment

- Heavy metal converts to heavier metal and to Fission products
- Account for in Burnup, and mass in heavy metals
- Solution assumes all higher actinides are built into the system from capture in ²³⁸U

$$\epsilon_0 = \frac{N^{U238}(T)}{N_0^U} \left[\frac{N^{U235}(T)}{N^{U238}(T)} + \frac{N^{U236}(T)}{N^{U238}(T)} \right] + \frac{M_0^U}{N_A E_R} BU(T) - G^{238} - G^{240} - G^{241}$$

Fuel Age

$$t_d = -\frac{1}{\lambda} ln \left(\frac{N_{\text{measured}}}{N_{FOI}} \right)$$



Present Status of the Question
Procedure
Current and Expected Results



Experimental Procedure - Mass Spectrometry



Experimental Procedure - Gamma Spectrometry



Experimental Procedure - Alpha Spectrometry

Current and Expected Results

Irradiation

- $12.9 \pm 0.1 \text{ mg of DUO}_2$ was irradiated
 - High Flux Isotope Reactor at Oak Ridge National Laboratory
- * Burnup was 4.43 ± 0.31 GWd/tHM^[29] from ¹³⁷Cs
- * $0.196 \pm \text{mg}$ of total Pu was produced as measured by ICP-MS





Dissolution of the spent fuel pellet





Glovebox











Experiments

- Single stage extraction and back-extraction
 - Purpose: quantify product recovery, D-values and DF values for single stage extraction and back extraction
 - Conditions:

Starting Solution Extraction Solution		Back extraction solution		
4 M nitric acid	30% vol.% TBP, 70 vol.% kerosene	0.024 M ferrous sulfamate in 0.75 M nitric acid		

- Multi-contact extraction and back-extraction
 - Purpose: Quantify DF for a process with 4 extractions, 3 back extractions
 - Conditions:

Starting Solution	Extraction Solution	Back extraction solution 0.024 M ferrous sulfamate in 4 M nitric acid		
4 M nitric acid	30% vol.% TBP, 70 vol.% kerosene			

Mass spectrometry Results

Recoveries of U and Pu						
		Pu Recovery	U Recovery			
	Single stage	(83.4±9.5)%	$(11.2\pm1.3)\%$			
	Multi-contact Cycle 1	$(99.7 \pm 4.2)\%$	$(6.8\pm0.3)\%$			
	Multi-contact Cycle 2	$(93.0\pm4.6)\%$	$(6.6\pm0.3)\%$			
	Overall Experiment 2	$(92.7\pm6.0)\%$	$(0.45\pm0.03)\%$			



Mass Spectrometry Results

Decontamination Factors

Element (Z)	SS	Error	MC Cycle 1	Error	Isotopes Used
Rb(37)	39.0	5.9	11.8	0.8	⁸⁵ Rb
Sr(38)	283	43	84.6	5.9	⁹⁰ Sr
Mo(42)	5.7	0.8	1.9	0.2	^{97,98,100} Mo
Ru(44)	59.2	6.4	16.6	2.5	^{101,102,104} Ru
Pd(46)	65	14	8.9	1.2	¹¹⁰ Pd
Cd(48)	74	17	22.1	2.5	¹¹² Cd
Cs(55)	177	28	52.9	3.9	¹³³ Cs
Ce(58)	43	16	11.5	4.9	^{140,142} Ce
Nd(60)	19.2	2.1	5.9	0.4	¹⁴³ Nd
Pm(61)	12.8	1.9	3.9	0.3	¹⁴⁷ Pm
Sm(62)	11.5	1.5	3.6	0.3	¹⁵¹ Sm
Eu(63)	10.0	1.4	3.6	0.3	¹⁵⁴ Eu
U(92)	7.4	1.2	14.7	0.9	²³⁸ U



Gamma Spectroscopy Results



Initial vs Final solutions

Subsection 5

Future Work

Objectives I

Characterize a 4 extraction 3 back-extraction PUREX process

Collect D-values for each step

Collect DF-values for the process

- Prepare alpha samples for each step (triplicate)
 - Analyze alpha samples for each step
- □ Convert alpha spec + gamma spec data to DF values
- Convert Mass spec data to DF values (published)
- Mathematically connect D-values to DFs
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Objectives II

Determine attribution indicators:

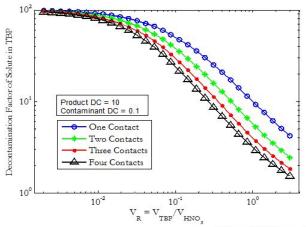
 Mathematically derive equations for above indicators with respect to one of the isotopes determined above



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- Program a system to iteratively solve for these parameters given heavy metal concentration ratios
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 Create program to calculate single group x-sections from ENDF data and an assumed fast-to-thermal ratio
 - Couple all programs together in a single program
- Use above information to determine indicators for three sets of data

Questions?

Previous Experiment Results



Decontamination Factors for multi-contact extraction.







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Mass Spec

