

Question 1

Calibration is done as:  $D = MV_0 + B$

$$MV_0 = D - B$$

$$V_0 = \frac{1}{M} D - \frac{B}{M}$$

In this case  $M = 1.67821 \text{ mm/V}$

$$\frac{1}{M} = 0.59587 \text{ V/mm}$$

$$B = -4.2131 \text{ mm}$$

$$\frac{B}{M} = -2.51047 \text{ V}$$

$$V_0 = 0.59587 \text{ V/mm} D + 2.51047 \text{ V}$$

① Range:

DVRT  $I_{\text{MIN}} = 0 \text{ mm}$

$I_{\text{MAX}} = 8 \text{ mm}$

DVRT  $O_{\text{MIN}} = 0 \text{ mm} \times 1 \text{ V/mm} = 0 \text{ V}$

$O_{\text{MAX}} = 8 \text{ mm} \times 1 \text{ V/mm} = 8 \text{ V}$

DEM0D-DC  $O_{\text{MIN}} = 0 \text{ V}$

$O_{\text{MAX}} = 5 \text{ V}$

② Span:

DVRT Input: 8mm

DVRT Output: 8V

DEMODO-DC output: 5V

③ Ideal Straight Line:

Ideally I'd have a straight line  
with the points

$$A(I_{\min}, O_{\min}) \Rightarrow A(0_{\text{mm}}, 0V)$$

$$B(I_{\max}, O_{\max}) \Rightarrow B(8_{\text{mm}}, 5V)$$

$$V_o = mD + c$$

$$m = \frac{5V - 0V}{8_{\text{mm}} - 0_{\text{mm}}} = 0.625 \text{ V/mm}$$

$$0 = (0.625 \text{ V/mm})(0) + c \quad \therefore c = 0$$

$$\therefore V_{\text{IDEAL}} = 0.625 \text{ V/mm} D_{\text{IDEAL}}$$

#### ④ Hysteresis

$$\text{Hysteresis \% FSD} = \frac{1 \mu\text{m}}{8 \text{ mm}} \times 100\% \\ = 0.0125\%$$

#### ⑤ Non-linearity

Accuracy  $\pm 1\%$

~~Assuming non-linearity is negligible.~~

a) Table: Static Specifications of the system

Characteristic	Value
DVRT input range	-4mm to 4mm
DVRT output range	0.12644V to 4.99395V
DEM0D-DC saturation	0V to 5V
DVRT input span	8mm
DVRT output span	8V
DEM0D-DC output span	5V
DVRT temperature range	-55°C to 175°C
System temperature range	0°C to 40°C
DEM0D-DC temperature range	-40°C to 85°C
DVRT Accuracy	$\pm 1\%$
DVRT Sensitivity	1 V/mm
DVRT Signal-to-noise (SNR)	4200
DVRT Resolution (% FSD)	0.025%
Temperature Span	0.03% / °C
Temperature Offset	0.002% / °C
Hysteresis (% FSD)	0.0125%
System Characteristics	
Input Range	-4mm to 4mm
Output Range	0V to 5V

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Input Span	8 mm
Output Span	5 V

b) @  $40^{\circ}\text{C}$        $\Delta T = 40^{\circ} - 22^{\circ}\text{C} = 18^{\circ}\text{C}$

$$\begin{aligned}\text{Temperature Span Error} &= (0.03\%/^{\circ}\text{C}) \Delta T \\ &= 0.54\%\end{aligned}$$

$$\begin{aligned}\text{Temperature Offset Error} &= (0.002\%/^{\circ}\text{C}) \Delta T \\ &= 0.036\%\end{aligned}$$

$$\text{DVRT-Demod Accuracy} = 1\%$$

$$\text{SNR error} = 0.0238\%$$

$$\text{Hysteresis} = 0.0125\%$$

$$\text{Resolution Error} = \frac{0.025\%}{2} = 0.0125\%$$

\* The specifications and errors for the DVRT are given using the DEMOD-DC system so these errors are applied to the output of the system other than the error due to the resolution.

So the error in the input is given as

$$I \pm (I) = I \left( 1 + \underset{\text{resolution}}{0.000125} \right) = I(1.000125)$$

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Now the error in the system

$$V_o(I) \Big|_{T=40^\circ\text{C}} = \left\{ (0.59587 \text{ V/mm} \overset{\text{temperature moderating}}{(1 + 0.0054)}) I_E(I) + 2.51047 \text{ V} + 5 \text{ V} \underset{\text{temperature interfering}}{(0.00036)} \right\} \left( 1 + \overset{\text{Accuracy}}{0.01} + \underset{\text{SNR}}{0.000238} + \overset{\text{Hysteresis}}{0.000125} \right)$$

$$\cancel{V_o(-4 \text{ mm}) \Big|_{T=40^\circ\text{C}} = 0.1168 \text{ V}} \quad \cancel{E(-4 \text{ mm}) = \frac{V_o(-4 \text{ mm}) \Big|_{T=60^\circ\text{C}} - V_o(-4 \text{ mm}) \Big|_{T=40^\circ\text{C}}}{V_o(-4 \text{ mm})} = 8.024\%}$$

~~NOT FULL SCALE (OPPOSITE)~~

$$V_o(4 \text{ mm}) \Big|_{T=40^\circ\text{C}} = 4.9598 \text{ V} \quad E(4 \text{ mm}) \Big|_{T=40^\circ\text{C}} = \frac{V_o(4 \text{ mm}) \Big|_{T=60^\circ\text{C}} - V_o(4 \text{ mm}) \Big|_{T=40^\circ\text{C}}}{V_o(4 \text{ mm})} = 1.346\% \text{ FSD}$$

@  $0^\circ\text{C}$        $\Delta T = -22^\circ\text{C}$

$$\text{Temperature span error} = (0.03\%/^\circ\text{C})(-22^\circ\text{C}) = -0.66\%$$

$$\text{Temperature offset error} = (0.002\%/^\circ\text{C})(-22^\circ\text{C}) = -0.044\%$$

$$V_o(I) \Big|_{T=0^\circ\text{C}} = \left\{ (0.59587 \text{ V/mm} (1 - 0.0066)) I_E(I) + 2.51047 \text{ V} + 5 \text{ V} (-0.00036) \right\} (1 + 0.01 + 0.000238 + 0.000125)$$

$$V_o(4 \text{ mm}) \Big|_{T=0^\circ\text{C}} = 4.92725 \text{ V} \quad E(4 \text{ mm}) \Big|_{T=0^\circ\text{C}} = 0.6815\%$$

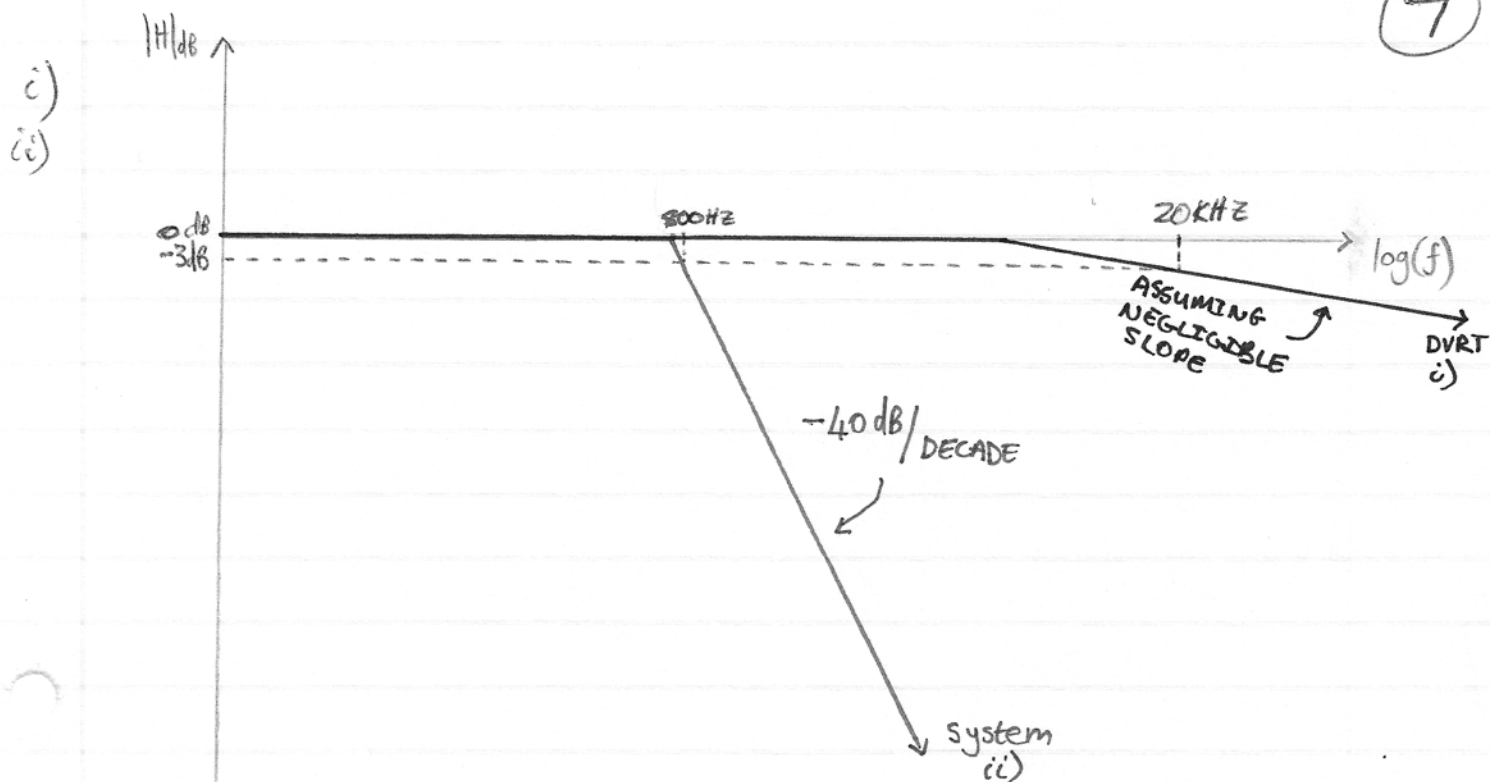
Question 2

- a) It seems that there is a conflict between the calibration results, the DVRT and the DEMOD-DC. The DVRT has a frequency response of  $800\text{ Hz}$ , this can be interpreted in two ways: 1) After  $800\text{ Hz}$  the magnitude of the transfer function starts to roll-off. 2) The sensor is guaranteed to work according to the spec sheet at frequencies lower than  $800\text{ Hz}$  but this does not imply that it won't respond to frequencies higher than that.

I am going to go with the 2<sup>nd</sup> interpretation, in other words the sensor does not act as a low pass filter at  $800\text{ Hz}$  instead I'm going to go with the worst case where the sensor does not attenuate the signal at all around the  $800\text{ Hz}$  frequency. I can argue this using the fact that a  $20\text{ kHz}$  sensor also exists so attenuation must only happen at much higher frequencies, so, let's assume the DVRT has a  $-3\text{ dB}$  gain at  $20\text{ kHz}$  and even at this point let's assume it doesn't roll-off like a first order LPF.



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\* This is a sketch of estimated Butterworth filters.

b) Assuming a Butterworth Filter

$$|H| = \frac{1}{\sqrt{1 + \left(\frac{\omega}{\omega_c}\right)^{2n}}}$$

Butterworth transfer characteristic

I know it's a second order filter  $\therefore n=2$

Also  $\omega_c$  @ 800 Hz

$$\therefore \omega_c = 2\pi(800) = 1600\pi$$

I need an aliasing error 0.1%

$$20 \log(0.001) = -60 \text{ dB}$$

The 800 Hz is insignificant because we're actually worried about the point where  $|H|_{\text{dB}} = 20 \log(0.001)$  \*THIS IS ASSUMING- @ 800 Hz the system has a  $\approx 0$  dB gain

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@  $f = 500 \text{ Hz}$   
 $\omega = 1000\pi$

$$|H(1000\pi)|_{\text{dB}} = -10 \log\left(1 + \left(\frac{1000\pi}{1600\pi}\right)^4\right)$$

$$= -0.61674 \text{ dB}$$

So I need when  $|H(\omega)|_{\text{dB}} = -60.61674 \text{ dB}$

$$-10 \log\left(1 + \left(\frac{\omega}{1600\pi}\right)^4\right) = -60.61674 \text{ dB}$$

$$\therefore \omega = 164697.98 \dots \text{ rad/sec}$$

$$\therefore f = 26212.49773 \dots \text{ Hz}$$

We need to apply Nyquist's theorem in order to find the sampling frequency:

$$f_s = 2(26212.49 \dots)$$

$$= 52424.99547 \dots \text{ Hz}$$

So use a sampling frequency of

$f_s = 53 \text{ kHz}$  to allow for an error of 0.1% or less @ 500 Hz



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c) The DVRT has a resolution of 2mm and a span of 8mm, the number of steps are, therefore:

$$\text{steps} = \frac{8\text{mm}}{2\text{mm}} = 4000$$

$$\log_2(4000) = 11.965 \dots$$

$\therefore$  A 12 bit ADC is required to match the resolution of the sensor.

### Question 3

I would choose the VI1BLT1-S24-S12-SMT 12V DC to DC converter. It meets the input range of the DEMOD-DC of 6V to 16V. I chose this over the 9V regulator because it's 1% more efficient with no effect on the circuit. Also it allows for larger drifts compared to the 9V and 15V.

Taking worst case drift into account the drift would be:

$$V_o = 12V \left( \overset{\text{accuracy}}{0.03} + \overset{\text{temperature drift}}{85^\circ\text{C}} (0.0003) + \overset{\text{regulation}}{+0.01} + 1 \right) \\ + \underset{\text{output ripple}}{20\text{mV}} + \underset{\text{output noise}}{100\text{mV}}$$

$$= 12.906\text{V} < 16\text{V}$$

This DC to DC converter can take an input of 22.8V to 25.2V.

The circuit diagram would look as follows

