## Note: Diffusion constant and solubility of helium in ULE glass at 23 $\,^{\circ}$ C

Sefer Avdiaj, Yuanchao Yang, Karl Jousten, and Tom Rubin

Citation: The Journal of Chemical Physics 148, 116101 (2018); doi: 10.1063/1.5019015

View online: https://doi.org/10.1063/1.5019015

View Table of Contents: http://aip.scitation.org/toc/jcp/148/11

Published by the American Institute of Physics





## Note: Diffusion constant and solubility of helium in ULE glass at 23 °C

Sefer Avdiaj, 1,a) Yuanchao Yang, 2,a) Karl Jousten, 3 and Tom Rubin 3,b)

<sup>1</sup>Department of Physics, University of Prishtina, Pristina 10000, Kosovo Serbia

<sup>2</sup>National Institute of Metrology (NIM), Beijing 100029, China

(Received 11 December 2017; accepted 1 March 2018; published online 20 March 2018)

https://doi.org/10.1063/1.5019015

Among other applications, ultra-low expansion (ULE) glass is commonly used as material for laser cavities. ULE glass is a trademark of Corning Incorporated and consists for the most part of SiO<sub>2</sub> with additionally about 9% TiO<sub>2</sub>. ULE cavities were recently proposed to measure helium refractivity for a new fundamental realization of the pascal. <sup>1-3</sup> In Ref. 1, it was reported that the diffusion of helium into ULE glass caused a length change of the ULE spacer. Another challenge in this application may be a pumping effect of ULE for helium or outgassing of previously absorbed helium. To estimate the impact of helium absorption, we have measured the diffusion constant and solubility of helium in ULE near 23 °C.

We received a sample of ULE glass code 7972 (charge no. 12 204 ANT1) from the Corning company and cut this sample into rectangular plates. For this investigation, we used three plates of different dimensions, as described in Fig. 1. The plates were loaded with helium in a previously evacuated load lock chamber at a pressure of  $p_{load} = 21.1$  (1) kPa. The loading and all experiments were performed at 23 (1) °C. Preliminary experiments indicated that a loading time of 170 h should be sufficient for a thickness of 2 mm and 680 h for a thickness of 4 mm to obtain a homogeneous helium concentration. The plates had been loaded for a minimum of 262 h and 771 h, respectively.

After loading with He, the plates were moved into the sample chamber to measure the outgassing rate vs. time by a quadrupole mass spectrometer (QMS), namely, Transpector from the Inficon company in our outgassing rate measurement system. The mathematics used to describe the diffusion process and calculate diffusion and permeation coefficients as well as solubility of the material has been discussed in many articles and books. Here we refer to Ref. 6 where the outgassing rate vs. time is calculated with a one-dimensional approximation for an infinite plane, i.e.,  $d \ll a$ , b. The time dependence at a temperature T is characterized by the constant

$$t_{\text{out}} = \frac{d^2}{\pi^2 \times D},\tag{1}$$

where D is the diffusion constant at T. For times  $t > t_{out}$ , the specific outgassing rate  $q_{out}$  deviates less than 1% from the

simple exponential function<sup>7</sup>

$$q_{\text{out}} = \frac{4 \times D}{d} \times c_0 \times \exp\left(-\frac{t}{t_{\text{out}}}\right),$$
 (2)

with  $c_0$  being the initial concentration of helium in the plate. Hence, the diffusion constant D can be determined from Eq. (1) and  $c_0$  can be obtained by extrapolation of the exponential curve Eq. (2) to t = 0. The measured total outgassing rate  $Q_{\text{out}}$  happens on both sides of the plate, which is

$$Q_{\text{out}} = 2 \times A \times q_{\text{out}}.$$
 (3)

Equations (2) and (3) require a traceable and absolute measurement of  $Q_{\text{out}}$  which is possible with our apparatus. We should note that the QMS was calibrated *in situ* and the interference with other gases present in the system (mainly hydrogen, water vapor, CO, and CO<sub>2</sub>) was found to be negligible at our measurement conditions. In addition, we considered the "edge effect," i.e., gave up the assumption that the plate's area is infinite. The changes of  $t_{\text{out}}$  and  $c_0$  due to this effect are in the low percent region and presented in Table I. Finally, the solubility S can be determined by using Henry's law,

$$c_0 = S \times p_{\text{load}}.\tag{4}$$

Figure 1 shows the result for the helium outgassing rate vs. time. The measurements were interrupted at some time intervals because of a limit of the recording time of the QMS software. It can be seen that deviations from the mono-exponential decay decrease quickly. After about half a time constant  $t_{\rm out}$ , they are no longer recognizable in Fig. 1. To estimate  $t_{\rm out}$ , the values between one and at least four times the expected value of  $t_{\rm out}$  were considered.

D was determined according to Eq. (1), where the uncertainty is dominated by the one of  $t_{\rm out}$ . The values determined for  $Q_{\rm out}$  (t = 0),  $c_0$ , and S for each plate were determined according to Eqs. (2)–(4), respectively, and can be found together with  $t_{\rm out}$  in Table I.

The values from the three plates agree within their uncertainties so that we calculated the following results by the weighted means:  $D = (4.22 \pm 0.06) \times 10^{-8} \text{ cm}^2/\text{s}$  and  $S = (1.82 \pm 0.14)\%$ . The permeation coefficient K was calculated from

$$K = S \times D = (7.68 \pm 0.59) \times 10^{-10} \text{cm}^2/\text{s}.$$
 (5)

<sup>&</sup>lt;sup>3</sup>Physikalisch-Technische Bundesanstalt (PTB), Abbestr. 2-12, 10587 Berlin, Germany

a)Guest researcher at Physikalisch-Technische Bundesanstalt (PTB), Abbestr. 2-12, 10587 Berlin, Germany.

b)Author to whom correspondence should be addressed: Tom.Rubin@PTB.de

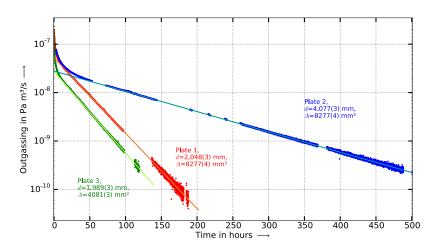


FIG. 1. Measured helium outgassing rates  $Q_{\text{out}}$  vs. time t for three different plates made from the same ULE glass. Straight lines indicate exponential decays.

TABLE I. Results for  $t_{out}$ ,  $Q_{out}$  (t = 0),  $c_0$ , and S for ULE glass at 23 (1) °C. Corrections are due to the edge effect (giving up the assumption of infinite 2-dimensional plate).<sup>8</sup>

Name	Correction for $t_{\text{out}}$ (%)	t <sub>out</sub> in h	Correction for $Q_{\text{out},(t=0)}$ (%)	$Q_{\text{out},(t=0)}$ in Pa m <sup>3</sup> /s	$c_0$ in Pa m <sup>3</sup> /m <sup>3</sup>	S in %
Plate 1	+1.2	28.3(7)	+0.1	5.15(72)	384(54)	1.82(26)
Plate 2	+2.6	108(4)	+0.2	2.63(48)	377(69)	1.79(33)
Plate 3	+2.2	26.4(6)	+0.5	2.70(34)	379(55)	1.84(26)

The values for D, S, and K are of the same order of magnitude like the results for other types of glasses obtained by permeation measurements carried out in the 1950s and 1960s.  $^{9-13}$  For example, for Lithosil (SiO<sub>2</sub>) from the Schott company, values are  $S_{\rm Lithosil} = 2.5\%$  and  $D_{\rm Lithosil(25~^{\circ}C)} = 2.4 \times 10^{-8}$  cm<sup>2</sup>/s, leading to  $K_{\rm Lithosil(25~^{\circ}C)} = 6 \times 10^{-10}$  cm<sup>2</sup>/s.  $^{14}$ 

From the values obtained in this paper, one can calculate that the initial diffusion of helium into a helium-free ULE glass causes a sink rate R (pumping speed or volume speed per area) of

$$R = 10^{-6} \times S \times \sqrt{\frac{D}{\pi \times t}} = \frac{2.13 \times 10^{-12}}{\sqrt{t/(s)}} \text{m}^3 \text{s}^{-1} \text{cm}^{-2}, \quad (6)$$

i.e.,  $1.2\times10^{-13}$  m³ s<sup>-1</sup> cm<sup>-2</sup> at 5 min,  $3.6\times10^{-14}$  m³ s<sup>-1</sup> cm<sup>-2</sup> at 1 h, and  $1.1\times10^{-14}$  m³ s<sup>-1</sup> cm<sup>-2</sup> at 10 h.

New optical pressure standards are targeting uncertainties of several ppm.<sup>1–3</sup> If He is used for a refractivity measurement in combination with ULE glass, the changes of the size of the ULE cavity spacer caused by He-absorption, but also the pumping speed of the ULE surfaces, need to be considered.

The authors thank the Corning company for providing the ULE samples and Janez Setina for valuable suggestions.

<sup>&</sup>lt;sup>1</sup>P. F. Egan, J. A. Stone, J. H. Hendricks, J. E. Ricker, G. E. Scace, and G. F. Strouse, Opt. Lett. **40**(17), 3945 (2015).

<sup>&</sup>lt;sup>2</sup>P. F. Egan, J. A. Stone, J. E. Ricker, and J. H. Hendricks, Rev. Sci. Instrum. **87**, 053113 (2016).

<sup>&</sup>lt;sup>3</sup> K. Jousten, J. H. Hendricks, D. Barker, K. Douglas, S. Eckel, P. F. Egan, J. Fedchak, J. Flügge, C. Gaiser, D. Olson, and J. E. Ricker, Metrologia 54(6), S146 (2017).

<sup>&</sup>lt;sup>4</sup>K. Jousten, S. Putzke, and J. Buthig, J. Vac. Sci. Technol., A 33, 061603 (2015)

<sup>&</sup>lt;sup>5</sup>J. Crank, *The Mathematics of Diffusion*, 2nd ed. (Oxford University Press, Oxford, 1975).

<sup>&</sup>lt;sup>6</sup>R. Calder and G. Lewin, Br. J. Appl. Phys. **18**, 1459 (1967).

<sup>&</sup>lt;sup>7</sup>K. Jousten, *Handbook of Vacuum Technology*, 2nd ed. (Wiley-VCH, Weinheim, 2016), p. 249.

<sup>&</sup>lt;sup>8</sup>Y. Yang, T. Rubin, S. Avdiaj, and K. Jousten, "The edge-effect: Outgassing rates influenced by different geometric surfaces" (to be published).

<sup>&</sup>lt;sup>9</sup>F. J. Norton, J. Am. Ceram. Soc. **36**(3), 90 (1953).

<sup>&</sup>lt;sup>10</sup>D. E. Swets, R. W. Lee, and R. C. Frank, J. Chem. Phys. **34**, 17 (1961).

<sup>&</sup>lt;sup>11</sup>W. A. Rogers, R. S. Buritz, and D. Alpert, J. Appl. Phys. **25**, 868 (1954).

 <sup>&</sup>lt;sup>12</sup>F. J. Norton, J. Appl. Phys. **28**, 34 (1957).
<sup>13</sup>V. O. Altemose, J. Appl. Phys. **32**, 1309 (1961).

<sup>&</sup>lt;sup>14</sup>M. Werner and H. Warlimont, Springer Handbook of Condensed Matter and Materials Data (Springer Science & Business Media, 2006), p. 557.