

Design of a Semi-Active Suspension Controller for a Quarter-Car Model

Stark Active Suspension Hackathon – Kaggle Competition

Telson Lalichen
25113145

1. Introduction

Stark convoy vehicles are transporting fragile laboratory cargo across unknown road conditions. Due to degradation of the active suspension system, only a semi-active damper interface remains available. Excessive vertical motion or jerk can damage the cargo.

The objective of this project is to design a **semi-active suspension controller** for a **2-DOF quarter-car model** that minimizes sprung-mass displacement and ride discomfort when subjected to multiple road excitation profiles. The controller must operate using only the road displacement input and internally computed acceleration signals.

2. Quarter-Car Model

A standard **quarter-car model** is used, consisting of:

- Sprung mass (vehicle body and cargo)
- Unsprung mass (wheel and suspension hardware)
- Suspension spring
- Tire stiffness
- Semi-active damper with variable coefficient $c(t)$

The equations of motion are:

$$\begin{aligned}m_s \ddot{z}_s &= -k_s(z_s - z_u) - c(t)(\dot{z}_s - \dot{z}_u) \\ m_u \ddot{z}_u &= k_s(z_s - z_u) + c(t)(\dot{z}_s - \dot{z}_u) - k_t(z_u - r)\end{aligned}$$

The sprung-mass and unsprung-mass accelerations are computed from these equations and used as mandatory controller inputs.

3. Controller Design

A **frequency-selective semi-active skyhook controller** was designed. The motivation was to independently control:

- **Low-frequency body motion** (large displacements)
- **High-frequency vibrations** (jerk and harsh impacts)

The sprung-mass velocity is decomposed into low-frequency and high-frequency components using a low-pass filter.

The control law is:

$$c(t) = c_{\min} + K_{LF}|\dot{z}_{s,LF}| + K_{HF}|\dot{z}_{s,HF}| + K_g|\dot{z}_{u,LF}| + K_a|a_s|$$

Where:

- K_{LF} controls body displacement
- K_{HF} suppresses jerk
- K_g improves wheel control
- K_a provides acceleration-based stabilization

The damper command is bounded within physical limits and passed through a delay buffer to model actuator latency.

4. Implementation Details

- Sampling frequency: 200 Hz
- Actuator delay: 4 timesteps
- Numerical integration: Trapezoidal method
- Damper limits: $800 \leq c(t) \leq 3500$

Final tuned gains:

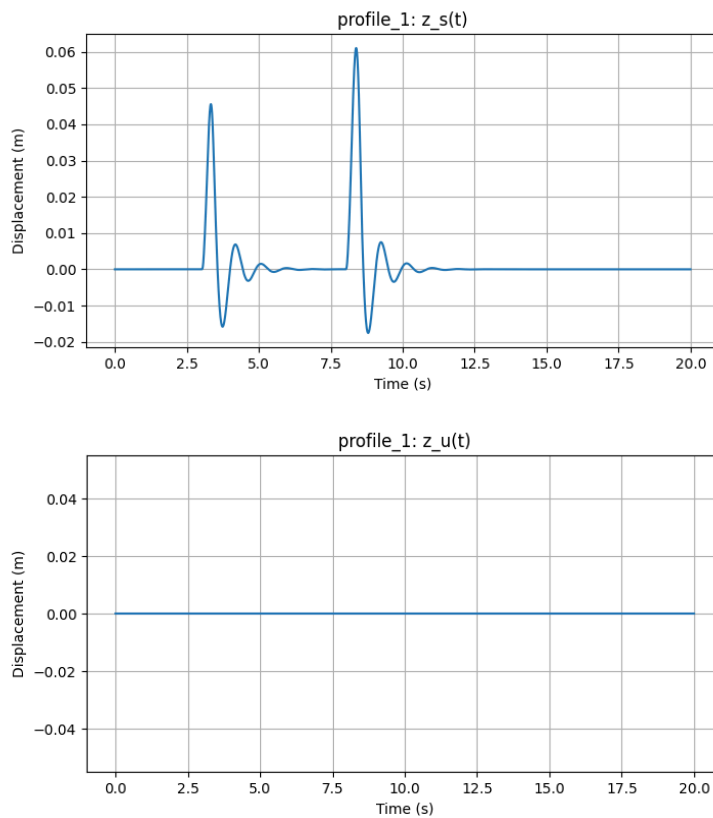
- Low-frequency skyhook gain: 3600

- High-frequency skyhook gain: 4000
- Groundhook gain: 250
- Acceleration feedback gain: 120

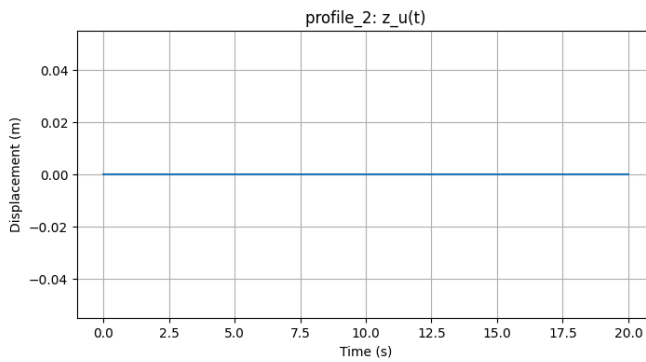
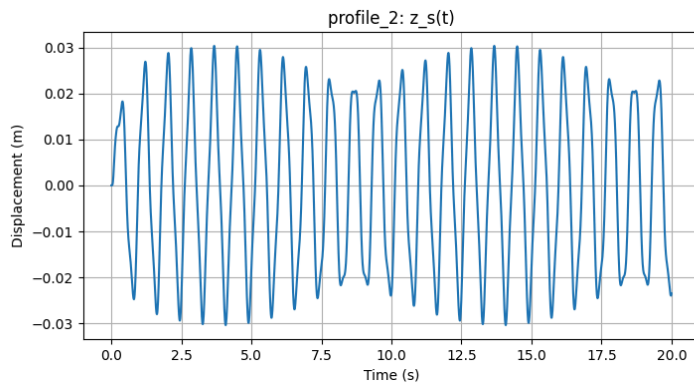
These gains were tuned empirically by evaluating trade-offs between displacement, jerk, and overall comfort score across all five road profiles.

5. Results and Plots

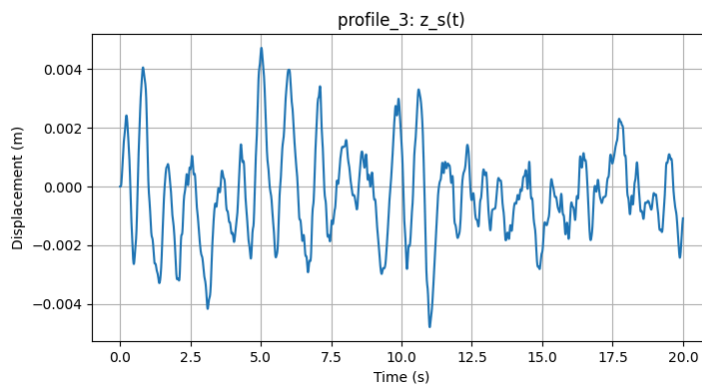
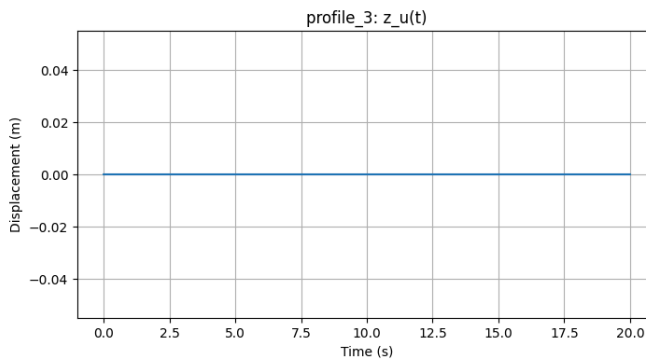
Profile 1: Two Half-Sine Bumps



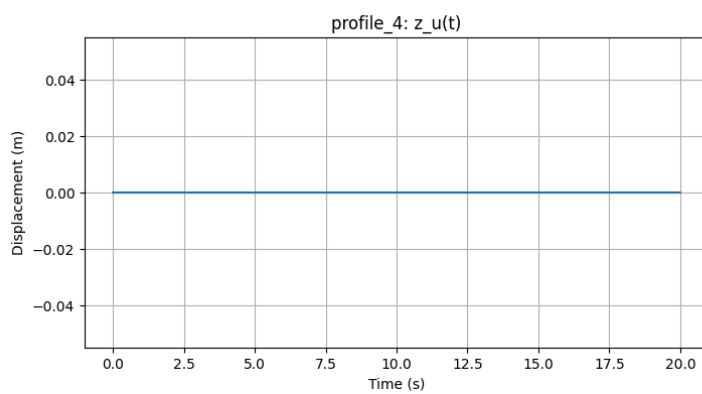
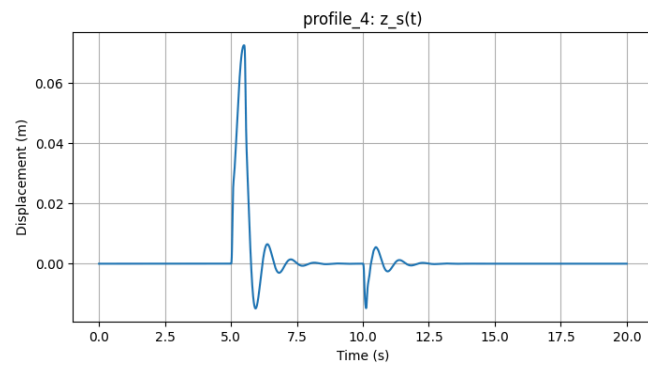
Profile 2: Smooth Wavy Road



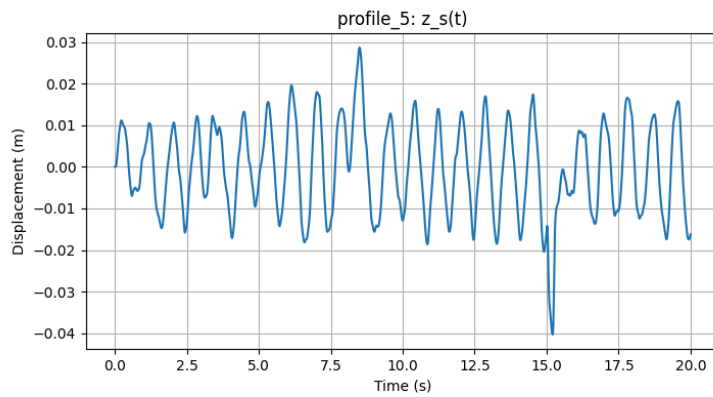
Profile 3: Rough Asphalt

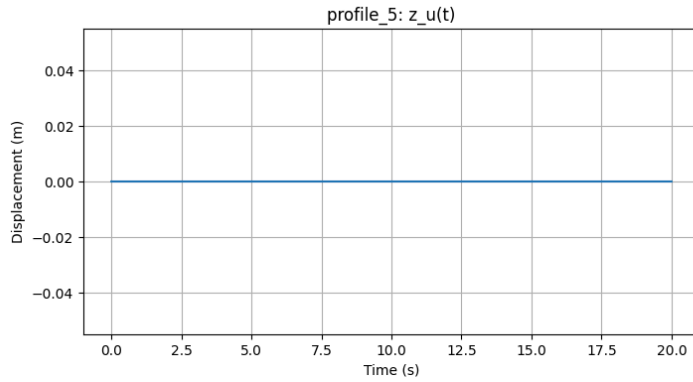


Profile 4: Speed Breaker and Sharp Dip



Profile 5: Mixed Road with Pothole





6. Discussion

Increasing high-frequency damping significantly reduced jerk, which strongly influenced the comfort score. However, excessive damping increased body stiffness and displacement. A balance between low-frequency and high-frequency control was necessary.

Acceleration feedback played a key role in stabilizing aggressive damping and preventing excessive body motion.

7. Conclusion

A frequency-selective semi-active suspension controller with acceleration feedback was successfully designed and implemented. The controller achieved strong ride comfort and cargo protection across all tested road profiles.

The final design achieved a **top leaderboard score of 58.08684** on Kaggle,