

## Lecture 16

*Lecturer: Asst. Prof. M. Mert Ankarali***State-Feedback & Pole Placement**

Given a discrete-time state-evolution equation

$$x[k+1] = Gx[k] + Hu[k]$$

If direct measurements of all of the states of the system (e.g.  $y[k] = x[k]$ ) are available, the most popular control method is the linear state feedback control,

$$u[k] = -Kx[k]$$

which can be thought as a generalization of P controller to the vector form. Under this control law, without any reference signal, the system becomes an autonomous system

$$\begin{aligned} x[k+1] &= Gx[k] + H(-Kx[k]) \\ x[k+1] &= (G - HK)x[k] \end{aligned}$$

The system matrix of this new autonomous system is  $\hat{G} = G - HK$ . Important questions is how to choose  $K$ . Note that

$$\begin{aligned} K &\in \mathbb{R}^n \quad \text{Single - Input} \\ K &\in \mathbb{R}^{n \times p} \quad \text{Multi - Input} \end{aligned}$$

As in all of the control design techniques, the most critical criterion is stability, thus we want all of the eigenvalues to be strictly inside the unit-circle. However, we know that there could be different requirements on the poles/eigenvalues of the system.

The fundamental principle of “pole-placement” design is that we first define a desired closed-loop eigenvalue set  $\mathcal{E}^* = \{\lambda_1^*, \dots, \lambda_n^*\}$ , and then if possible we choose  $K^*$  such that the closed-loop eigenvalues match the desired ones.

The necessary and sufficient condition on arbitrary pole-placement is that the system should be Reachable.

In Pole-Placement, first step is computing the desired characteristic polynomial.

$$\begin{aligned} \mathcal{E}^* &= \{\lambda_1^*, \dots, \lambda_n^*\} \\ p^*(z) &= (z - \lambda_1^*) \cdots (z - \lambda_n^*) \\ &= z^n + a_1^* z^{n-1} + \cdots + a_{n-1}^* z + a_n^* \end{aligned}$$

Then we tune  $K$  such that

$$\det(zI - (G - HK)) = p^*(z)$$

## Direct Design of State-Feedback Gain

If  $n$  is small, the most efficient method could be the direct design.

**Example:** Consider the following DT system

$$x[k+1] = \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} x[k] + \begin{bmatrix} 1 \\ 1 \end{bmatrix} u[k]$$

Design a state-feedback rule such that poles are located at  $\lambda_{1,2} = 0$  (Dead-beat gain)

**Solution:** Desired characteristic equation can be computed as

$$p^*(z) = z^2$$

Let  $K = \begin{bmatrix} k_1 & k_2 \end{bmatrix}$ , then the characteristic equation of  $\hat{G}$  can be computed as

$$\begin{aligned} \det(zI - (G - HK)) &= \det\left(\begin{bmatrix} z - 1 + k_1 & k_1 \\ k_2 & z - 2 + k_2 \end{bmatrix}\right) \\ &= z^2 + z(k_1 + k_2 - 3) + (2 - 2k_1 - k_2) \end{aligned}$$

If we match the equations

$$\begin{aligned} z^2 + z(k_1 + k_2 - 3) + (2 - 2k_1 - k_2) &= z^2 \\ k_1 + k_2 &= 3 \\ 2k_1 + k_2 &= 2 \\ k_1 &= -1 \\ k_2 &= 4 \end{aligned}$$

This  $K = \begin{bmatrix} -1 & 4 \end{bmatrix}$ . Now let's compute  $\hat{G}^k$

$$\begin{aligned} \hat{G} &= \begin{bmatrix} 2 & -4 \\ 1 & -2 \end{bmatrix} \\ \hat{G}^2 &= \begin{bmatrix} 2 & -4 \\ 1 & -2 \end{bmatrix} \begin{bmatrix} 2 & -4 \\ 1 & -2 \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} \\ &\vdots \end{aligned}$$

It can be seen that closed-loop system rejects all initial condition perturbations in 2 steps.

## Design of State-Feedback Gain Using Reachable Canonical Form

Let's assume that the state-space representation is in controllable canonical form and we have access to the all states of this form

$$x[k+1] = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 \\ 0 & 0 & 1 & \cdots & 0 \\ \vdots & \vdots & \vdots & & \vdots \\ 0 & 0 & 0 & \cdots & 1 \\ -a_n & -a_{n-1} & -a_{n-2} & \cdots & -a_1 \end{bmatrix} x[k] + \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix} u[k]$$

Let  $K = [k_n \ \cdots \ k_1]$ , then autonomous system takes the form

$$x[k+1] = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 \\ 0 & 0 & 1 & \cdots & 0 \\ \vdots & \vdots & \vdots & & \vdots \\ 0 & 0 & 0 & \cdots & 1 \\ -a_n & -a_{n-1} & -a_{n-2} & \cdots & -a_1 \end{bmatrix} x[k] - \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix} [k_n \ \cdots \ k_1] x[k]$$

$$x[k+1] = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 \\ 0 & 0 & 1 & \cdots & 0 \\ \vdots & \vdots & \vdots & & \vdots \\ 0 & 0 & 0 & \cdots & 1 \\ -(a_n + k_n) & -(a_{n-1} + k_{n-1}) & -(a_{n-2} + k_{n-2}) & \cdots & -(a_1 + k_1) \end{bmatrix} x[k]$$

Let  $p^*(z) = z^2 + a_1^* z + \cdots + a_{n-1}^* z + a_n^*$ , then  $K$  can be computed as

$$K = [ (a_n^* - a_n) \ \cdots \ (a_1^* - a_1) ]$$

However, what if the system is not in Reachable canonical form. We can find a transformation which finds the Reachable canonical representation.

The reachability matrix of a state-space representation is given as

$$M = [ H \mid GH \mid \cdots \mid G^{n-1}H ]$$

Let's define a transformation matrix  $T$  as follows:

$$T = MW, \quad x[k] = T\hat{x}[k]$$

$$\hat{x}[k+1] = [T^{-1}GT] \hat{x}[k] + T^{-1}Hu[k]$$

where

$$W = \begin{bmatrix} a_{n-1} & a_{n-2} & \cdots & a_1 & 1 \\ a_{n-2} & a_{n-3} & \cdots & 1 & 0 \\ \vdots & \vdots & \ddots & & \vdots \\ a_1 & 1 & & & \\ 1 & 0 & \cdots & & 0 \end{bmatrix}$$

Then it is given that

$$T^{-1}GT = \hat{G} = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 \\ 0 & 0 & 1 & \cdots & 0 \\ \vdots & \vdots & \vdots & & \vdots \\ 0 & 0 & 0 & \cdots & 1 \\ -a_n & -a_{n-1} & -a_{n-2} & \cdots & -a_1 \end{bmatrix}$$

$$T^{-1}H = \hat{H} = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix}$$

Let's compute  $T\hat{H}$

$$\begin{aligned}
 T\hat{H} &= MW\hat{H} = M \begin{bmatrix} a_{n-1} & a_{n-2} & \cdots & a_1 & 1 \\ a_{n-2} & a_{n-3} & \cdots & 1 & 0 \\ \vdots & \vdots & \ddots & \vdots & \\ a_1 & 1 & & & \\ 1 & 0 & \cdots & & 0 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix} \\
 &= [H \mid GH \mid \cdots \mid G^{n-1}H] \begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \\ 0 \end{bmatrix} \\
 &= H
 \end{aligned}$$

A similar approach (but longer) can be used to show that  $T^{-1}GT = \hat{G}$ . We know how to design a state-feedback gain  $\hat{K}$  for the Reachable canonical form. Given  $\hat{K}$   $u[k]$  is given as

$$\begin{aligned}
 u[k] &= -\hat{K}\hat{x}[k] \\
 &= -\hat{K}T^{-1}\hat{x}[k] \\
 K &= \hat{K}T^{-1}
 \end{aligned}$$

**Example 2:** Consider the following DT system

$$x[k+1] = \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} x[k] + \begin{bmatrix} 1 \\ 1 \end{bmatrix} u[k]$$

Design a state-feedback rule using the Reachable canonical form approach, such that poles are located at  $\lambda_{1,2} = 0$  (Dead-beat gain)

**Solution:** Characteristic equation of  $G$  can be derived as

$$\det \left( \begin{bmatrix} z-1 & 0 \\ 0 & z-2 \end{bmatrix} \right) = z^2 - 3z + 2$$

The Reachability matrix can be computed as

$$M = [H \mid GH] = \begin{bmatrix} 1 & 1 \\ 1 & 2 \end{bmatrix}$$

The matrix  $W$  can be computed as

$$W = \begin{bmatrix} -3 & 1 \\ 1 & 0 \end{bmatrix}$$

Transformation matrix,  $T$  and its inverse  $T^{-1}$  can be computed as

$$\begin{aligned}
 T &= MW = \begin{bmatrix} 1 & 1 \\ 1 & 2 \end{bmatrix} \begin{bmatrix} -3 & 1 \\ 1 & 0 \end{bmatrix} = \begin{bmatrix} -2 & 1 \\ -1 & 1 \end{bmatrix} \\
 T^{-1} &= \begin{bmatrix} -1 & 1 \\ -1 & 2 \end{bmatrix}
 \end{aligned}$$

Given that desired characteristic polynomial is  $p^*(z) = z^2$ ,  $\hat{K}$  of reachable canonical form can be computed as

$$\begin{aligned}\hat{K} &= \begin{bmatrix} -a_2 & -a_1 \end{bmatrix} \\ &= \begin{bmatrix} -2 & 3 \end{bmatrix}\end{aligned}$$

Finally  $K$  can be computed as

$$\begin{aligned}K = \hat{K}T^{-1} &= \begin{bmatrix} -2 & 3 \end{bmatrix} \begin{bmatrix} -1 & 1 \\ -1 & 2 \end{bmatrix} \\ &= \begin{bmatrix} -1 & 4 \end{bmatrix}\end{aligned}$$

As expected this is the same result with the one found in Example 1 (Direct-Method).