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Second order gradient ascent pulse engineering

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ABSTRACT

We report some improvements to the gradient ascent pulse engineering (GRAPE) algorithm for optimal control of spin ensembles and other quantum systems. These include more accurate gradients, convergence acceleration using the Broyden–Fletcher–Goldfarb–Shanno (BFGS) quasi-Newton algorithm as well as faster control derivative calculation algorithms. In all test systems, the wall clock time and the convergence rates show a considerable improvement over the approximate gradient ascent.

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1. Introduction

An optimal control problem consists in bringing a dynamic system from one state to another to a given accuracy with minimum expenditure of effort [1-3]. Such tasks are encountered in optical spectroscopy [4-6], magnetic resonance [7-12], spin dynamics [13,14] and the emerging field of quantum information processing [15–19]. While many variations exist in practice [20–22], depending on the desired outcome and the constraints placed on the solution by instrumental limitations [1,23,24], they can all be broadly classified into gate design problems [11,25], where a specific unitary transformation of the entire state space is sought, and state control problems [10,26–28], where the population is to be moved from one specific state to another without conditions on the dynamics of other states. Because any gate design problem can be represented as a state control problem in a space of higher dimension [23,25], we will only consider the state control formulation below.

The state of a quantum system can be described by a density operator $\hat{\rho}(t)$, whose evolution is governed by the quantum Liouville equation [29]:

$$\frac{\partial}{\partial t}\hat{\rho}(t) = -i\left[\hat{H}(t), \hat{\rho}(t)\right] + \hat{R}\hat{\rho}(t) \tag{1}$$

where $\hat{H}(t)$ is a possibly-time dependent Hamiltonian and \hat{R} is the relaxation superoperator. It is often convenient to carry out the calculations in Liouville space by replacing a matrix representation of

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 $\hat{
ho}(t)$ with a vector $|\hat{
ho}(t)\rangle$ obtained by stacking the columns of $\hat{
ho}(t)$. In this representation, the equation acquires the following form:

$$\frac{\partial}{\partial t}|\hat{\rho}(t)\rangle = -i\hat{\hat{L}}(t)|\hat{\rho}(t)\rangle, \quad \hat{\hat{L}}(t) = \hat{E}\otimes\hat{H}(t) - \hat{H}(t)^{T}\otimes\hat{E} + i\hat{\hat{R}}$$
 (2)

where \hat{E} is the unit matrix of the same dimension as \hat{H} [29] and \hat{R} is the Liouville space representation of the relaxation superoperator. The general solution may be formally written as:

$$|\hat{\rho}(t)\rangle = \exp_{(0)}\left(-i\int_{0}^{t}\hat{\hat{L}}(t)dt\right)|\hat{\rho}(t)\rangle \tag{3}$$

where $\exp_{(O)}$ indicates Dyson's time-ordered exponential [30]. Given a fixed grid of points $\{t_1, \dots, t_N\}$, the density matrix at a particular grid point n is then given by:

$$|\hat{\rho}(t_n)\rangle=\hat{\hat{P}}_n...\hat{\hat{P}}_2\hat{\hat{P}}_1|\hat{\rho}(0)\rangle,\quad \hat{\hat{P}}_n=exp_{(0)}\biggl(-i\int_{t_{n-1}}^{t_n}\hat{\hat{L}}(t)dt\biggr) \eqno(4)$$

A state control problem consists in finding such $\hat{H}(t)$ as would maximize the population of a given target density matrix $|\hat{\sigma}\rangle$ after evolution from a given initial state $|\hat{\rho}(0)\rangle$ under the total Liouvillian $\hat{L}(t)$ [23,28]:

$$\hat{H}_{\text{opt}}(t) \in \underset{\hat{H}(t)}{\text{arg max}} (\langle \hat{\sigma} | \hat{\rho}(t_N) \rangle) \tag{5}$$

where the maximum is sought in the class of square-integrable Hermitian matrix valued functions of time. From the experimental perspective, not every part of $\hat{H}(t)$ can be modified at will, and it is common to separate it into the "drift" and the "control" parts:

$$\hat{H}(t) = \hat{H}_0 + \sum_{k} c^{(k)}(t) \hat{H}_k \Rightarrow \hat{\hat{L}}(t) = \hat{\hat{L}}_0 + \sum_{k} c^{(k)}(t) \hat{\hat{L}}_k
\hat{\hat{L}}_0 = \hat{E} \otimes \hat{H}_0 - \hat{H}_0^T \otimes \hat{E} + i\hat{\hat{R}}, \quad \hat{\hat{L}}_k = \hat{E} \otimes \hat{H}_k - \hat{H}_k^T \otimes \hat{E}$$
(6)

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 \hat{L}_0 being the "drift" component deemed to be beyond our direct influence and \hat{L}_k are the "control" components, whose contributions may be varied experimentally [13]. Various constraints are often placed on the control functions $c^{(k)}(t)$, mostly to enforce the instrumental limitations [20,21]. The optimization problem in Eq. (5) is difficult to solve in full generality, and it is common to simplify the description of $\hat{H}(t)$ by assuming the control functions to be piecewise-constant with fixed switching times [9,12]:

$$c^{(k)}(t) = c_n^{(k)}, \quad t_{n-1} < t < t_n$$
 (7)

This makes the problem finite-dimensional and facilitates numerical solutions. In practice this is often not an approximation, since the actual output of many hardware devices, *e.g.* waveform generators in NMR spectroscopy, can be made piecewise-constant. Under this assumption, the time-ordered exponential (a notoriously complicated object from the numerical calculation perspective) in Eq. (4) simplifies into a simple matrix exponential:

$$\hat{\hat{P}}_n = \exp_{(0)} \left[-i \int_{t_{n-1}}^{t_n} \hat{\hat{L}}(t) dt \right] = \exp \left[-i \left(\hat{\hat{L}}_0 + \sum_k c_n^{(k)} \hat{\hat{L}}_k \right) \Delta t \right]$$
(8)

where Δt is the time grid spacing. Progress can then be made with the optimization problem in Eq. (5), because the gradient of the error functional $1 - \langle \hat{\sigma} | \hat{\rho}(t_N) \rangle$ with respect to the amplitude of control k at time step n is now easily computed:

$$\begin{split} \frac{\partial}{\partial c_{n}^{(k)}} \langle \hat{\sigma} | \hat{\rho}(t_{N}) \rangle &= \frac{\partial}{\partial c_{n}^{(k)}} \left\langle \hat{\sigma} \Big| \hat{\hat{P}}_{N} \dots \hat{\hat{P}}_{n} \dots \hat{\hat{P}}_{1} \Big| \hat{\rho}(\mathbf{0}) \right\rangle \\ &= \left\langle \hat{\sigma} \Bigg| \hat{\hat{P}}_{N} \dots \hat{\hat{P}}_{n+1} \frac{\partial \hat{\hat{P}}_{n}}{\partial c_{n}^{(k)}} \hat{\hat{P}}_{n-1} \dots \hat{\hat{P}}_{1} \Bigg| \hat{\rho}(\mathbf{0}) \right\rangle \\ &= \left(\hat{\hat{P}}_{n+1}^{\dagger} \dots \hat{\hat{P}}_{N}^{\dagger} | \hat{\sigma} \rangle \right)^{\dagger} \frac{\partial \hat{\hat{P}}_{n}}{\partial c_{n}^{(k)}} \left(\hat{\hat{P}}_{n-1} \dots \hat{\hat{P}}_{1} | \hat{\rho}(\mathbf{0}) \rangle \right) \end{split} \tag{9}$$

This effectively means that the destination state has to be propagated *backward* to time point t_n , the source state has to be propagated *forward* to time point t_{n-1} and the scalar product with the derivative of the propagator for the time step n has to be taken. In practice [7,9,12,28], the entire forward trajectory is computed from $\hat{\rho}(0)$, the entire backward trajectory is computed from $\hat{\sigma}$ and then the two are folded in each step with the propagator derivatives as prescribed by Eq. (9).

2. Calculation of control derivatives

The expression for the propagator derivative suggested in the paper introducing the GRAPE method [9] reasonably assumes that the control sequence discretization step is small:

$$\begin{split} \frac{\partial}{\partial c_{n}^{(k)}} \hat{\hat{P}}_{n} &= \frac{\partial}{\partial c_{n}^{(k)}} \exp \left[-i \left(\hat{\hat{L}}_{0} + \sum_{k} c_{n}^{(k)} \hat{\hat{L}}_{k} \right) \Delta t \right] \\ &= \exp \left[-i \left(\hat{\hat{L}}_{0} + \sum_{k} c_{n}^{(k)} \hat{\hat{L}}_{k} \right) \Delta t \right] \left(-i \hat{\hat{L}}_{k} \Delta t + O(\Delta t^{2}) \right) \\ &= \hat{\hat{P}}_{n} \left(-i \hat{\hat{L}}_{k} \Delta t \right) + O(\Delta t^{2}) \end{split} \tag{10}$$

this assumption makes the evaluation of control gradient very computationally affordable – it introduces no new matrix–matrix multiplications beyond those used to compute the propagators, because $-i\hat{L}_k\Delta t$ and \hat{P}_n can be multiplied sequentially into the vectors on either side of the derivative in Eq. (9). The cost of the control gradient is therefore approximately equal to the cost of the trajectory calculation. From Eq. (9), we have:

$$\frac{\partial}{\partial c_n^{(k)}} \langle \hat{\sigma} | \hat{\rho}(t_N) \rangle = \left(\hat{\hat{P}}_n^{\dagger} \dots \hat{\hat{P}}_N^{\dagger} | \hat{\sigma} \rangle \right)^{\dagger} \left(-i \hat{\hat{L}}_k \Delta t \right) \left(\hat{\hat{P}}_{n-1} \dots \hat{\hat{P}}_1 | \hat{\rho}(0) \rangle \right) \\
+ O(\Delta t^2) \tag{11}$$

While the gradient ascent using this equation does in most cases yield acceptable accuracy solutions, it has been recognized for some time that the $O(\Delta t^2)$ residual tends to limit both the convergence rate and the final accuracy achievable. As the gradient becomes smaller during the minimization, it is the first term in Eq. (11) that gets reduced, and the situation eventually emerges where the approximation error dominates the gradient. This leads to the often observed and much lamented "slowdown" of the GRAPE algorithm as it approaches high transfer fidelities. It also scrambles the approximate Hessians used by quasi-Newton methods, essentially preventing their use. This may be seen directly by following the $O(\Delta t^2)$ residual through Newton's method:

$$f(\vec{x} + \Delta \vec{x}) = f(\vec{x}) + (\nabla f(\vec{x})^{\mathsf{T}} + O(\Delta t^{2}))\Delta \vec{x} + \frac{1}{2}\Delta \vec{x} \mathbf{H} \Delta \vec{x} + O(|\Delta \vec{x}|^{3})$$

$$= f(\vec{x}) + \nabla f(\vec{x})^{\mathsf{T}} \Delta \vec{x} + \frac{1}{2}\Delta \vec{x} \mathbf{H} \Delta \vec{x} + O(\Delta t^{2}|\Delta \vec{x}|) + O(|\Delta \vec{x}|^{3})$$
(12)

Unless the time step Δt is chosen to be extremely small, the $O(\Delta t^2 |\Delta \vec{x}|)$ error term, which is linear in $|\Delta \vec{x}|$, completely obscures the Hessian term, which is quadratic in $|\Delta \vec{x}|$. For typical NMR systems, this accuracy constraint places Δt into nanosecond range, which makes the number of steps very large and causes difficulties on the instrumental side.

In our experience, these problems can be removed at a reasonable computational cost, if the *exact* propagator gradient is used, rather than the first order approximation. The most straightforward avenue is to differentiate the Taylor or Chebyshev expansion for the exponential directly [31]. In the case of the Taylor series, this yields:

$$\frac{\partial}{\partial c_n^{(k)}} \exp\left[-i\hat{\hat{L}}\Delta t\right] = \sum_{p=1}^{\infty} \frac{(-i\Delta t)^p}{p!} \sum_{q=0}^{p-1} \hat{\hat{L}}^q \hat{\hat{L}}_k \hat{\hat{L}}^{p-q-1},$$

$$\hat{\hat{L}} = \hat{\hat{L}}_0 + \sum_k c_n^{(k)} \hat{\hat{L}}_k \tag{13}$$

The second sum appears because \hat{L} and \hat{L}_k do not necessarily commute. This formulation is computationally about as expensive as the original exponential because matrices involved (particularly \hat{L}_k) are often very sparse [32,33], but it is rather inconvenient because it involves double summation. A more computer-friendly version is given by a commutator series, which is the direct extension of Eq. (10):

$$\begin{split} \frac{\partial}{\partial c_{n}^{(k)}} \hat{\hat{P}}_{n} &= \frac{\partial}{\partial c_{n}^{(k)}} \exp\left[-i\hat{\hat{L}}\Delta t\right] = \exp\left[-i\hat{\hat{L}}\Delta t\right] \left(-i\hat{\hat{L}}_{k}\Delta t + \frac{\Delta t^{2}}{2} \left[\hat{\hat{L}}, \hat{\hat{L}}_{k}\right] \right. \\ &\left. + \frac{i\Delta t^{3}}{6} \left[\hat{\hat{L}}, \left[\hat{\hat{L}}, \hat{\hat{L}}_{k}\right]\right] - \frac{\Delta t^{4}}{24} \left[\hat{\hat{L}}, \left[\hat{\hat{L}}, \left[\hat{\hat{L}}, \hat{\hat{L}}_{k}\right]\right]\right] + \cdots\right) \end{split} \tag{14}$$

This expression can be obtained by rotating summation indices in $Fa_{(13)}$:

$$\sum_{p=1}^{\infty} \frac{(-i\Delta t)^p}{p!} \sum_{q=0}^{p-1} \hat{L}^q \hat{L}_k \hat{L}^{p-q-1} = \sum_{p=0}^{\infty} \sum_{q=0}^{\infty} \frac{A^p B A^q}{(p+q+1)!},$$

$$A = -i\hat{L}\Delta t, \quad B = -i\hat{L}_k \Delta t, \tag{15}$$

splitting the factorial in the denominator, then summing the series into matrix exponentials

$$\frac{1}{(p+q+1)!} = \frac{1}{p!q!} \int_{0}^{1} (1-\alpha)^{p} \alpha^{q} d\alpha \Rightarrow
\sum_{p=0}^{\infty} \sum_{q=0}^{\infty} \frac{A^{p} B A^{q}}{(p+q+1)!} = e^{A} \int_{0}^{1} e^{-\alpha A} B e^{\alpha A} d\alpha, \tag{16}$$

evaluating the integral

$$\int_{0}^{1} e^{-\alpha A} B e^{\alpha A} d\alpha = \int_{0}^{1} e^{-a d_A \alpha} B d\alpha = \gamma [-a d_A] B,$$

$$\gamma(z) = \frac{e^z - 1}{z} = \sum_{n=0}^{\infty} \frac{z^n}{(n+1)!}, \quad a d_x y = [x, y]$$

$$(17)$$

and expressing powers of ad_A as nested commutators with A:

$$\sum_{m=0}^{\infty} \frac{(-ad_A)^m}{(m+1)!} B = \sum_{m=0}^{\infty} \frac{(-1)^m}{(m+1)!} [A, B]_m,$$

$$[A, B]_m = [A, [A, B]_{m-1}], \quad [A, B]_0 = B$$
(18)

With Eqs. (14)–(18) in place, the expression for the control gradient becomes:

$$\begin{split} &\frac{\partial}{\partial c_{n}^{(k)}} \langle \hat{\sigma} | \hat{\rho}(t_{N}) \rangle = - \left(\hat{\hat{P}}_{n}^{\dagger} \dots \hat{\hat{P}}_{N}^{\dagger} | \hat{\sigma} \rangle \right)^{\dagger} \\ &\left(\sum_{m=0}^{\infty} \frac{\left(\mathbf{i} \Delta t \right)^{m+1}}{(m+1)!} \left[\hat{\hat{L}}_{0} + \sum_{k} c_{n}^{(k)} \hat{\hat{L}}_{k}, \hat{\hat{L}}_{k} \right]_{m} \right) \left(\hat{\hat{P}}_{n-1} \dots \hat{\hat{P}}_{1} | \hat{\rho}(0) \rangle \right) \end{split} \tag{19}$$

where the summation of the series is to be continued until the desired accuracy (as indicated by the residual norm) is achieved. A few initial orders of accuracy in the Taylor expansion of $\gamma(z)$ are plotted in Fig. 1.

The numerical accuracy of Eq. (19) in finite-precision arithmetic merits further discussion. As with all power series, the perfect scenario from the numerical point of view is to have the norm of the argument $-i\hat{L}\Delta t$ scaled into the unit interval – this avoids the "hump" in the convergence and keeps the terms well within the accuracy limits imposed by 64-bit floating-point arithmetic. As Fig. 2 demonstrates, adequate numerical accuracy is maintained for $\|-i\hat{L}\Delta t\|<30$, but deteriorates rapidly thereafter. The standard technique used to resolve this issue is known as "scaling and squaring" [31,34]:

$$\exp\left(-i\hat{\hat{L}}\Delta t\right) = \exp\left(\frac{-i\hat{\hat{L}}\Delta t}{2}\right)^{2} \tag{20}$$

The product rule for the derivative makes the scaling and squaring procedure for the derivative propagator slightly different:

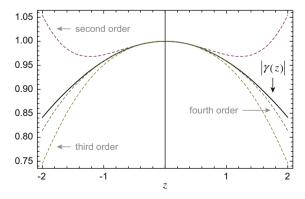


Fig. 1. Taylor approximation accuracy for $|\gamma(z)|$ as a function of approximation order and matrix norm. It should be noted that only power series are in practice affordable in Eq. (17) – any rational approximation would require computationally expensive matrix inversions.

$$\begin{split} \frac{\partial}{\partial c_{n}^{(k)}} \exp\left(-i\hat{\hat{L}}\Delta t\right) &= \exp\left(\frac{-i\hat{\hat{L}}\Delta t}{2}\right) \left[\frac{\partial}{\partial c_{n}^{(k)}} \exp\left(\frac{-i\hat{\hat{L}}\Delta t}{2}\right)\right] \\ &+ \left[\frac{\partial}{\partial c_{n}^{(k)}} \exp\left(\frac{-i\hat{\hat{L}}\Delta t}{2}\right)\right] \exp\left(\frac{-i\hat{\hat{L}}\Delta t}{2}\right) \end{split} \tag{21}$$

Because the exponential propagator itself is computed elsewhere in the GRAPE procedure [9], the cost of the squaring step is modest – two sparse matrix multiplications. Our experience with this procedure has been very positive, it tolerates scaling factors in excess of 10⁶, thus encompassing all practically encountered GRAPE algorithm application situations.

If relaxation is negligible and the Hamiltonian dimension is small enough to permit numerical diagonalization, the series in Eq. (19) may be avoided because we can evaluate $\gamma[\mathrm{ad}(\mathrm{i}\hat{H}\Delta t)](-\mathrm{i}\hat{H}_k\Delta t)$ directly by diagonalizing \hat{H} [8,22,31]. Let $\hat{H}=\hat{V}\hat{\Lambda}\hat{V}^{\dagger}$, where \hat{V} is a unitary matrix whose columns are eigenvectors of \hat{H} and $\hat{\Lambda}$ is a diagonal matrix with the corresponding eigenvalues λ_r along the diagonal. We then have:

$$\begin{split} \hat{D}^{(k)} &= \gamma \Big[\text{ad}(i\hat{H}\Delta t) \Big] \Big(-i\hat{H}_k \Delta t \Big) = \hat{V} \Big(\hat{G} \odot \hat{B} \Big) \hat{V}^{\dagger} \\ G_{rs} &= \gamma [i(\lambda_r - \lambda_s) \Delta t], \quad \hat{B} = \hat{V}^{\dagger} \Big(-i\hat{H}_k \Delta t \Big) \hat{V} \end{split} \tag{22}$$

where \odot denotes element-wise (Hadamard) matrix multiplication. Using this formula, we have:

$$\frac{\partial}{\partial c_n^{(k)}} \langle \hat{\sigma} | \hat{\rho}(t_N) \rangle = \left(\hat{\hat{P}}_n^{\dagger} \dots \hat{\hat{P}}_N^{\dagger} | \hat{\sigma} \rangle \right)^{\dagger} \hat{\hat{D}}^{(k)} \left(\hat{\hat{P}}_{n-1} \dots \hat{\hat{P}}_1 | \hat{\rho}(0) \rangle \right)$$

$$\hat{\hat{D}}^{(k)} = \hat{D}^{(k)} \otimes \hat{E} - \hat{E} \otimes \hat{D}^{(k)T}$$
(23)

This method is the adaptation of the diagonalization method for matrix functions – the matrix is transformed into its eigenframe, the function is applied to the eigenvalues and the result is transformed back into the original frame. It is not applicable to Hamiltonians with dimensions in excess of 10^4 , because the eigenvector array \hat{V} is often dense even for sparse Hamiltonians and overflows the computer memory.

Eqs. (13)–(23) present an analytical formalism for the calculation of the control derivatives. A popular numerical alternative is to use finite-difference approximations, e.g.:

$$\frac{\partial \hat{\hat{P}}_n}{\partial c_n^{(k)}} = \frac{\hat{\hat{P}}_n(\dots, c_n^{(k)} + h, \dots) - \hat{\hat{P}}_n(\dots, c_n^{(k)}, \dots)}{h} + O(h)$$
(24)

$$\frac{\partial \hat{\hat{P}}_n}{\partial c_n^{(k)}} = \frac{\hat{\hat{P}}_n \left(\dots, c_n^{(k)} + h, \dots \right) - \hat{\hat{P}}_n \left(\dots, c_n^{(k)} - h, \dots \right)}{2h} + O(h^2)$$
 (25)

where the amplitude of the kth control at the nth time point is varied by a finite amount h. Eqs. (24) and (25) are indicative – they are the simplest examples of a large class of numerical finite-difference approximations for the derivative [35]. The primary balance to be maintained in this approach is between the approximation accuracy, the numerical accuracy and the computational cost of the derivative.

The forward finite difference approximation in Eq. (24) has the advantage of being computationally affordable – it only requires the calculation of one extra $\exp\left(-\mathrm{i}\hat{L}\Delta t\right)\hat{\rho}$ product per step, which may be carried out using Krylov subspace techniques, thus avoiding matrix multiplications. From Eq. (9):

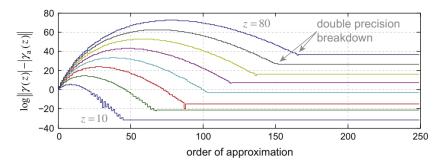


Fig. 2. Numerical convergence profiles in double precision for the Taylor approximation of $\gamma(z)$ as functions of approximation order and matrix norm. The *Y* axis shows the norm of the difference between the value of $\gamma(z)$ evaluated directly and using the series expansion $\gamma_a(z)$ to a given order. Due to the presence of numerical round-off errors, the scaling and squaring procedure is mandatory for z > 30.

$$\begin{split} \frac{\partial}{\partial c_{n}^{(k)}} \langle \hat{\sigma} | \hat{\rho}(t_{N}) \rangle &= \left(\hat{\hat{P}}_{n+1}^{\dagger} \dots \hat{\hat{P}}_{N}^{\dagger} | \sigma \rangle \right) \frac{\partial \hat{\hat{P}}_{n}}{\partial c_{n}^{(k)}} \left(\hat{\hat{P}}_{n-1} \dots \hat{\hat{P}}_{1} | \hat{\rho}(0) \rangle \right) \\ &= \left(\hat{\hat{P}}_{n+1}^{\dagger} \dots \hat{\hat{P}}_{N}^{\dagger} | \sigma \rangle \right) \frac{\hat{\hat{P}}_{n} \left(c_{n}^{(k)} + h \right) - \hat{\hat{P}}_{n} \left(c_{n}^{(k)} \right)}{h} \\ &\times \left(\hat{\hat{P}}_{n-1} \dots \hat{\hat{P}}_{1} | \hat{\rho}(0) \rangle \right) + O(h) \end{split} \tag{26}$$

Approximations with a higher order of accuracy may be used at the expense of having to calculate further $\exp\left(-i\hat{L}\Delta t\right)\hat{\rho}$ products for the extra stencil points. In common with the commutator series approach in Eq. (19), the finite difference method is applicable to dissipative quantum systems, where anti-Hermitian terms may be present in the Liouvillian. It should be noted that Eq. (26) only involves a finite difference with respect to the step propagator – the rest of the trajectory does not need to be recomputed. This is a much more efficient arrangement as compared to the brute-force finite-differencing of $\langle \hat{\sigma} | \hat{\rho}(t_N) \rangle$.

The accuracy of finite difference methods depends on the step size h. In practical situations, the choice is constrained in two ways: if the step is too large, the finite difference would not be a good approximation to the derivative, and if the step is too small, the number of accurate digits in the floating point representation of the difference would reduce to none. In general, we do not have sufficient information to make an a priori estimate for the finite difference approximation error (it requires the knowledge of higher derivatives), but the numerical round-off error is a somewhat more straightforward quantity. A reasonable strategy therefore is to choose the smallest h for which the round-off error is guaranteed to be below a given threshold. Assuming the approximation error is indeed small for that choice of h, we can approximate a function f(x) with a linear polynomial f(x + h) = f(x) + f'(x)h for the purpose of obtaining the required round-off error bound.

The evaluation of matrix exponentials is accurate up to a fixed purely absolute error ε_A , which is a few orders of magnitude larger than the machine precision ε_M (equal to 2.22×10^{-16} in 64-bit arithmetic), because the norm of exponential time propagators in quantum mechanics is less than or equal 1. The error incurred in computing f(x+h)-f(x) is then $2\varepsilon_A$ plus at most $\varepsilon_M(|f(x)|+|f'(x)|h)$ from truncating their difference. The finite difference approximation $|h^{-1}[f(x+h)-f(x)]-f'(x)|$ then carries an absolute error bounded by:

$$\frac{1}{|h|}(2\varepsilon_{\mathsf{A}} + \varepsilon_{\mathsf{M}}|f(x)|) + \varepsilon_{\mathsf{M}}|f'(x)|. \tag{27}$$

This expression may be equated to the chosen error threshold and solved for h, assuming that an order of magnitude estimate of |f'(x)| is available. Even if the norm of f'(x) cannot be estimated a priori, Eq. (27) can still be used to validate the choice of step a posteriori, using the finite difference approximation to f'(x).

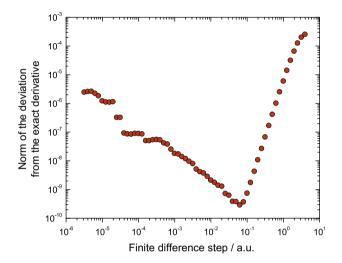


Fig. 3. Norm of the deviation of the finite difference derivative (fourth order central finite difference approximation) from the limit of the commutator series in Eq. (19) as a function of the differentiation parameter step.

The dependence of the approximation accuracy on the finite difference step size is illustrated in Fig. 3 – for large steps the error is dominated by the approximation error of the finite difference, which drops smoothly when the step is reduced. For small steps the error is dominated by the numerical round-off errors, which increase erratically as the numerical accuracy decreases.

The choice of the differentiation algorithm is ultimately left to user's discretion. The considerable improvement that better gradient accuracy brings to the asymptotic convergence rate is illustrated in Fig. 4 – for the spin chain in question, a pulse with 100 nanosecond time stepping is clearly outside the validity range of the first-order approximation in Eq. (11), and further terms in Eq. (19) are necessary to prevent the minimization process from halting when the insufficiently accurate gradient effectively sends the system uphill.

3. GRAPE with quasi-Newton optimizers

The close relationship between optimal control and numerical optimization methods is well researched [36–38] and the emerging numerical optimization methods (such as SQP [39]) have been specialized to optimal control and successfully applied, for example, to controlling fluid flow [40] or biological processes [41]. In the magnetic resonance context, the above noted fact that the control gradient of the objective function is relatively cheap to compute means that it is almost always advantageous to use the

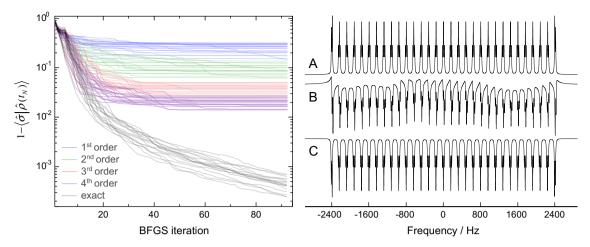


Fig. 4. (*Left Panel*) Quality of state transfer as a function of iteration number of the BFGS algorithm (as implemented in the interior-point algorithm used by Matlab's *fmincon* function [46,47]). The fidelity parameter refers to the quality of magnetization inversion under a 50-point shaped radiofrequency pulse applied to a chain of 31 protons with chemical shifts spread at regular intervals over the range of 8 ppm with strong nearest neighbor *J*-couplings of 20 Hz in a 600 MHz magnet. Pulse duration 5 ms (100 μs per waveform step), pulse amplitude capped at 2500 Hz. State space restriction to three-spin orders involving adjacent spins was used to reduce the matrix dimension involved in the simulation. The starting points in the optimization were set to sequences of uniformly distributed random numbers from the ±1000 Hz interval. The "kth order" labels refer to the number of commutator series terms in Eq. (19), "exact" refers to the series that has been summed to machine precision. (*Right Panel*) **A:** pulse-acquire NMR spectrum of the spin system described above; **B:** magnetization inversion profile under the pulse waveform obtained after 100 iterations with the first-order approximation to the gradient; **C:** magnetization inversion profile obtained after 100 iterations with the "exact" gradient computed using Eq. (19).

gradient history to build an approximation to the Hessian matrix, which can then be used in quasi-Newton optimization algorithms, which can exhibit super-linear convergence [42]. Because GRAPE is a concurrent update algorithm [9], the standard quasi-Newton methods may be used directly.

Several schemes exist for generating approximate Hessians from the gradient history, the most notable being DFP [43] and BFGS [42]:

$$\mathbf{H}_{k+1}^{\mathrm{DFP}} = \left(\mathbf{E} - \frac{\vec{g}_{k} \vec{s}_{k}^{\mathrm{T}}}{\vec{g}_{k}^{\mathrm{T}} \vec{s}_{k}}\right) \mathbf{H}_{k} \left(\mathbf{E} - \frac{\vec{s}_{k} \vec{g}_{k}^{\mathrm{T}}}{\vec{g}_{k}^{\mathrm{T}} \vec{s}_{k}}\right) + \frac{\vec{g}_{k} \vec{g}_{k}^{\mathrm{T}}}{\vec{g}_{k}^{\mathrm{T}} \vec{s}_{k}},$$

$$\mathbf{H}_{k+1}^{\mathrm{BFGS}} = \mathbf{H}_{k} + \frac{\vec{g}_{k} \vec{g}_{k}^{\mathrm{T}}}{\vec{g}_{k}^{\mathrm{T}} \vec{s}_{k}} - \frac{(\mathbf{H}_{k} \vec{s}_{k})(\mathbf{H}_{k} \vec{s}_{k})^{\mathrm{T}}}{\vec{s}_{k}^{\mathrm{T}} \mathbf{H}_{k} \vec{s}_{k}},$$

$$\vec{g}_{k} = \nabla f(\vec{x}_{k+1}) - \nabla f(\vec{x}_{k}), \quad \vec{s}_{k} = \vec{x}_{k+1} - \vec{x}_{k}$$
(28)

These pseudo-Hessians are constructed to satisfy the natural finite difference condition:

$$\nabla f(\vec{\mathbf{x}}_k) = \nabla f(\vec{\mathbf{x}}_{k+1}) - \mathbf{H}_{k+1}(\vec{\mathbf{x}}_{k+1} - \vec{\mathbf{x}}_k) \tag{29}$$

A necessary condition for \mathbf{H}_{k+1} to be negative definite is therefore that

$$(\vec{x}_{k+1} - \vec{x}_k)^T \boldsymbol{H}_{k+1} (\vec{x}_{k+1} - \vec{x}_k) = (\vec{x}_{k+1} - \vec{x}_k)^T (\nabla f(\vec{x}_{k+1}) - \nabla f(\vec{x}_k)) < 0 \tag{30}$$

but a useful property of BFGS and DFP update rules is that it is also a sufficient condition, assuming that \mathbf{H}_0 was chosen to be negative definite [42]. The iteration step (with optional line search) is then performed as:

$$\vec{\mathbf{x}}_{k+1} = \vec{\mathbf{x}}_k - \alpha_k H_k^{-1} \nabla f(\vec{\mathbf{x}}_k), \quad \alpha_k > 0$$
(31)

where α_k is the line search parameter (α_k = 1 corresponds to Newton iteration).

Because matrix inversions are expensive, it is in practice necessary to use the corresponding update schemes for the inverse of the Hessian:

$$(\mathbf{H}^{-1})_{k+1}^{\mathrm{BFGS}} = \left(\mathbf{E} - \frac{\vec{\mathbf{S}}_{k} \vec{\mathbf{g}}_{k}^{\mathrm{T}}}{\vec{\mathbf{g}}_{k}^{\mathrm{T}} \vec{\mathbf{S}}_{k}}\right)^{\mathrm{T}} \mathbf{H}_{k}^{-1} \left(\mathbf{E} - \frac{\vec{\mathbf{S}}_{k} \vec{\mathbf{g}}_{k}^{\mathrm{T}}}{\vec{\mathbf{g}}_{k}^{\mathrm{T}} \vec{\mathbf{S}}_{k}}\right) + \frac{\vec{\mathbf{S}}_{k} \vec{\mathbf{S}}_{k}^{\mathrm{T}}}{\vec{\mathbf{g}}_{k}^{\mathrm{T}} \vec{\mathbf{S}}_{k}}$$

$$(\mathbf{H}^{-1})_{k+1}^{\mathrm{DFP}} = \mathbf{H}_{k}^{-1} + \frac{\vec{\mathbf{S}}_{k} \vec{\mathbf{S}}_{k}^{\mathrm{T}}}{\vec{\mathbf{g}}_{k}^{\mathrm{T}} \vec{\mathbf{S}}_{k}} - \frac{\left(\mathbf{H}_{k}^{-1} \vec{\mathbf{g}}_{k}\right) \left(\mathbf{H}_{k}^{-1} \vec{\mathbf{g}}_{k}\right)^{\mathrm{T}}}{\vec{\mathbf{g}}_{k}^{\mathrm{T}} \mathbf{H}_{k}^{-1} \vec{\mathbf{g}}_{k}}$$

$$(32)$$

In the case of BFGS, a very memory-efficient procedure is available for generating the next step vector directly from the past gradient history, requiring no matrix storage. It is known as memory-limited BFGS, or L-BFGS [44,45]. In the context of optimal control, the number of variables often exceeds 10⁴, and L-BFGS is the only quasi-Newton method that is capable of handling such problems. The performance of DFP, BFGS and L-BFGS for the optimization of

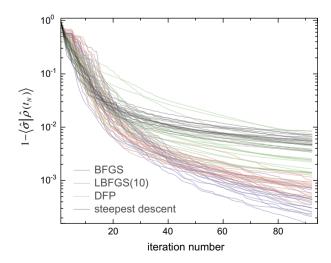


Fig. 5. Quality of state transfer as a function of iteration number for three Hessian update schemes as compared to cubic line search steepest descent. DFP stands for Davidon–Fletcher–Powell method. The fidelity parameter refers to the quality of magnetization inversion pulse in a 31-spin system as described in the caption to Fig. 3. It should be noted that the steepest descent minimization requires 5–10 function evaluations per iteration (line search) and is therefore considerably slower on the wall clock, as well as iteration count, than the three quasi-Newton methods.

a broadband magnetization inversion pulse in NMR spectroscopy is illustrated in Fig. 5.

4. Conclusions and outlook

The GRAPE algorithm for control sequence optimization has the benefit of computationally affordable gradients. Using the equations reported in this paper, their accuracy may be improved beyond the first order approximation and the result used to generate approximate Hessians for quasi-Newton optimization. In all test systems, the wall clock time and the convergence rates show a considerable improvement over the approximate gradient ascent – the "slowdown" problem disappears. The BFGS-GRAPE procedure reported in this paper is implemented in the *Spinach* software library [33].

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