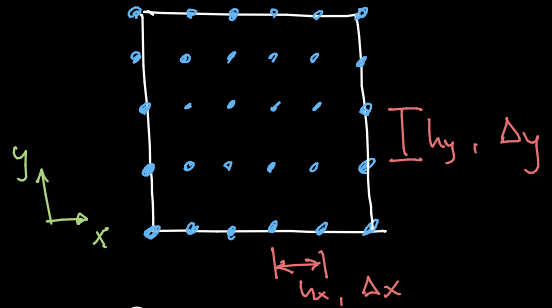
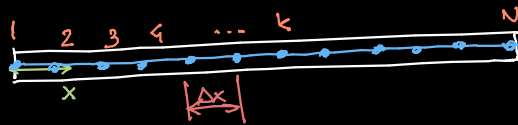


Método das diferenças finitas



Eq. de calor: $\rho c \dot{T} + \nabla \cdot (-k \nabla T) - s = 0$

CASO ESTACIONÁRIO s/
GERAÇÃO DE CALOR

$$\nabla \cdot (-k \nabla T) = 0$$

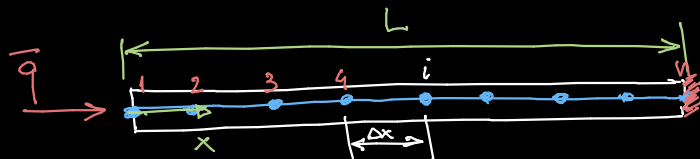
1D

$$-k \left[\frac{d^2 T}{dx^2} \right] = 0$$

2D

$$-k \left(\left[\frac{\partial^2 T}{\partial x^2} \right] + \left[\frac{\partial^2 T}{\partial y^2} \right] \right) = 0$$

Problema de transferência de calor unidimensional transiente



$$\rho c \left[\frac{\partial T}{\partial t} \right] - k \left[\frac{\partial^2 T}{\partial x^2} \right] = 0$$

C.I. $T(x, t=0) = T_0$

C.C. $\begin{cases} q(x=0, t) = \bar{q} \\ q(x=L, t) = 0 \text{ (adiabático)} \end{cases}$

Aproximações das derivadas:

$$t^k \quad \frac{\partial^2 T}{\partial x^2} \approx \frac{T_{i+1}^k - 2T_i^k + T_{i-1}^k}{\Delta x^2}$$

$$t^{k+1} \quad \frac{\partial^2 T}{\partial x^2} = \frac{T_{i+1}^{k+1} - 2T_i^{k+1} + T_{i-1}^{k+1}}{\Delta x^2}$$

$$t^k + \Delta t$$

$$\boxed{\frac{\partial T}{\partial t} = \frac{T_i^{k+1} - T_i^k}{\Delta t}}$$

$$\Delta t = t^{k+1} - t^k$$

Problema de transferência de calor unidimensional transiente

$$\rho c \left[\frac{\partial T}{\partial t} \right] - k \left[\frac{\partial^2 T}{\partial x^2} \right] = 0 \quad \Rightarrow \quad \alpha = \frac{k}{\rho c}$$

$$\frac{\partial^2 T}{\partial x^2} \approx \frac{T_{i+1}^k - 2T_i^k + T_{i-1}^k}{\Delta x^2} \quad \frac{\partial T}{\partial t} = \frac{T_i^{k+1} - T_i^k}{\Delta t}$$

$$\rho c \left(\frac{T_i^{k+1} - T_i^k}{\Delta t} \right) - k \left(\frac{T_{i+1}^k - 2T_i^k + T_{i-1}^k}{\Delta x^2} \right) = 0$$

$$T_i^{k+1} - T_i^k = \alpha \frac{\Delta t}{\Delta x^2} (T_{i+1}^k - 2T_i^k + T_{i-1}^k)$$

$$T_i^{k+1} = \frac{\alpha \Delta t}{\Delta x^2} T_{i+1}^k + \left(1 - 2\alpha \frac{\Delta t}{\Delta x^2} \right) T_i^k + \frac{\alpha \Delta t}{\Delta x^2} T_{i-1}^k$$

EXPLÍCITO

Problema de transferência de calor unidimensional transiente

$$T_i^{k+1} = \frac{\alpha \Delta t}{\Delta x^2} T_{i+1}^k + \left(1 - 2\alpha \frac{\Delta t}{\Delta x^2}\right) T_i^k + \alpha \frac{\Delta t}{\Delta x^2} T_{i-1}^k$$

Diagrama de um elemento de controle de espessura $2\Delta x$ com temperaturas T_1 e T_2 nas extremidades e fluxo de calor \bar{q} entrando na face esquerda.

Condições de contorno

$$q(x=0, t) = \bar{q}$$

$$q(x=L, t) = 0$$

EXPLÍCITO

Lei de Fourier: $q = -k \nabla T = -k \frac{\partial T}{\partial x}$

$$\left. \frac{\partial T}{\partial x} \right|_{x=0} \approx \frac{T(\Delta x, t) - T(-\Delta x, t)}{2\Delta x} = \frac{T_2^k - T_0^k}{2\Delta x}$$

Da condição de contorno:

$$-k \left(\frac{T_2^k - T_0^k}{2\Delta x} \right) = \bar{q}$$

$$T_0^k = \bar{q} \frac{2\Delta x}{k} + T_2^k$$

Problema de transferência de calor unidimensional transiente

$$\rho c \left[\frac{\partial T}{\partial t} \right] - k \left[\frac{\partial^2 T}{\partial x^2} \right] = 0$$

$$\frac{\partial^2 T}{\partial x^2} \approx \frac{T_{i+1}^{k+1} - 2T_i^{k+1} + T_{i-1}^{k+1}}{\Delta x^2} \quad \frac{\partial T}{\partial t} = \frac{T_i^{k+1} - T_i^k}{\Delta t}$$

$$\rho c \left(\frac{T_i^{k+1} - T_i^k}{\Delta t} \right) - k \left(\frac{T_{i+1}^{k+1} - 2T_i^{k+1} + T_{i-1}^{k+1}}{\Delta x^2} \right) = 0$$

$$-\alpha \frac{\Delta t}{\Delta x^2} T_{i+1}^{k+1} + \left(1 + 2\alpha \frac{\Delta t}{\Delta x^2} \right) T_i^{k+1} - \alpha \frac{\Delta t}{\Delta x^2} T_{i-1}^{k+1} = T_i^k$$



IMPLÍCITO

$$\underline{\underline{A}} \underline{\underline{I}} = \underline{\underline{b}}$$

Problema de transferência de calor unidimensional transiente

$$-\alpha \frac{\Delta t}{\Delta x^2} T_{i+1}^{k+1} + \left(1 + 2\alpha \frac{\Delta t}{\Delta x^2}\right) T_i^{k+1} - \alpha \frac{\Delta t}{\Delta x^2} T_{i-1}^{k+1} = T_i^k$$

Condições de contorno

$$q(x=0, t) = \bar{q}$$
$$q(x=L, t) = 0$$

Lei de Fourier: $q = -k \nabla T = -k \frac{\partial T}{\partial x}$

IMPLÍCITO

$$\left. \frac{\partial T}{\partial x} \right|_{x=0} \approx \frac{T(\Delta x, t) - T(-\Delta x, t)}{2\Delta x} = \frac{T_2^{k+1} - T_0^{k+1}}{2\Delta x}$$

Da condição de contorno:

$$-k \left(\frac{T_2^{k+1} - T_0^{k+1}}{2\Delta x} \right) = \bar{q}$$

$$T_0^{k+1} = \bar{q} \frac{2\Delta x}{k} + T_2^{k+1}$$

Von Neumann Stability Analysis

$$\frac{\partial u}{\partial t} - \alpha \frac{\partial^2 u}{\partial x^2} = 0$$

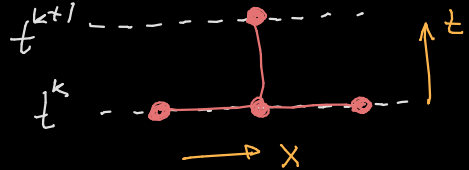
$$\alpha = \frac{k}{\rho c}$$

$$\frac{u_j^{k+1} - u_j^k}{\Delta t} = \frac{\alpha}{\Delta x^2} (u_{j+1}^k - 2u_j^k + u_{j-1}^k)$$

EXPLÍCITO

FTCS

$$\frac{\varepsilon_j^{k+1} - \varepsilon_j^k}{\Delta t} = \frac{\alpha}{\Delta x^2} (\varepsilon_{j+1}^k - 2\varepsilon_j^k + \varepsilon_{j-1}^k)$$



Fourier series : $\varepsilon(x, t) = \sum_{m=1}^M A_m e^{at} e^{i\beta_m x} = \sum_{m=1}^M \varepsilon_m$

$$\varepsilon_j^{n+1} = \sum A_m e^{a(t+\Delta t)} e^{i\beta_m x} = \varepsilon_j^n e^{a\Delta t}$$

$$\varepsilon_{j+1}^n = \sum A_m e^{at} e^{i\beta_m (x+\Delta x)} = \sum \varepsilon_m \left(\sum A_m e^{at} e^{i\beta_m \Delta x} \right)$$

...

Von Neumann Stability Analysis

$$\frac{\varepsilon_j^{k+1} - \varepsilon_j^k}{\Delta t} = \frac{\alpha}{\Delta x^2} (\varepsilon_{j+1}^k - 2\varepsilon_j^k + \varepsilon_{j-1}^k)$$

$$\varepsilon_j^{n+1} = \sum A_m e^{a(t+\Delta t)} e^{i\beta_m x} = \varepsilon_j^n e^{a\Delta t}$$

$$\varepsilon_{j+1}^n = \sum A_m e^{at} e^{i\beta_m (x+\Delta x)} = \sum \varepsilon_m \left(\sum A_m e^{at} e^{i\beta_m \Delta x} \right)$$

...

$$e^{a\Delta t} - 1 = \frac{\alpha \Delta t}{\Delta x^2} \left[e^{\beta_m \Delta x i} - 2 + e^{-\beta_m \Delta x i} \right]$$

Stability criteria

$$G = \frac{\varepsilon_j^{n+1}}{\varepsilon_j^n} \quad |G| \leq 1$$

Von Neumann Stability Analysis

$$e^{a\Delta t} - 1 = \frac{\alpha \Delta t}{\Delta x^2} \left[e^{\beta m \Delta x i} - 2 + e^{-\beta m \Delta x i} \right]$$

Stability criteria $G = \frac{\varepsilon_j^{n+1}}{\varepsilon_j^n} = e^{a\Delta t} \quad |G| \leq 1$

$$G = e^{a\Delta t} = \frac{\alpha \Delta t}{\Delta x^2} \left[e^{\beta m \Delta x i} - 2 + e^{-\beta m \Delta x i} \right] + 1$$

$$= 2 \frac{\alpha \Delta t}{\Delta x^2} \left[\cos \beta m \Delta x - 1 \right] + 1$$

$$= 1 - 4 \frac{\alpha \Delta t}{\Delta x^2} \sin^2 \left(\beta m \frac{\Delta x}{2} \right)$$

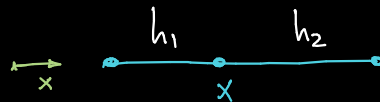
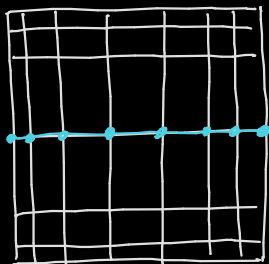
$$|G| \leq 1 \Rightarrow \begin{aligned} 1 - 4 \frac{\alpha \Delta t}{\Delta x^2} \sin^2 \left(\beta m \frac{\Delta x}{2} \right) &\leq 1 \\ -1 + 4 \frac{\alpha \Delta t}{\Delta x^2} \sin^2 \left(\beta m \frac{\Delta x}{2} \right) &\leq 1 \end{aligned}$$

$$\boxed{\frac{\alpha \Delta t}{\Delta x^2} \leq \frac{1}{2}}$$

Malhas não-uniformes

CASO 1D

CASO
2D



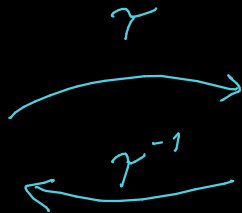
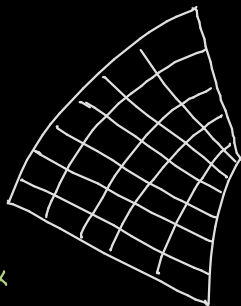
$$\begin{aligned}
 u(x+h_2) &= u(x) + h_2 u'(x) + \frac{h_2^2}{2} u''(x) + \dots & h_1^2 \\
 u(x-h_1) &= u(x) - h_1 u'(x) + \frac{h_1^2}{2} u''(x) + \dots & h_2^2
 \end{aligned}$$

$$u'(x) = \frac{h_1^2 u(x+h_2) + (h_1^2 - h_2^2) u(x) - h_2^2 u(x-h_1)}{h_1^2 h_2 + h_1 h_2^2}$$

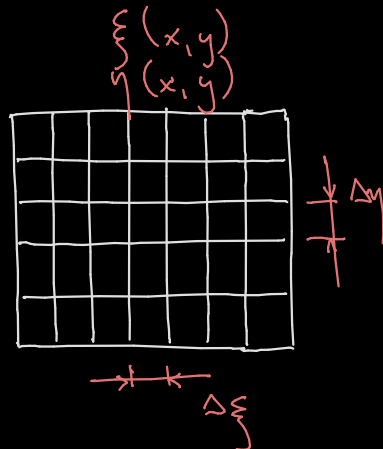
Outros domínios

$$x(\xi, \eta)$$

$$y(\xi, \eta)$$



TRANSFORMAÇÃO
CONFORME



$$\frac{\partial u}{\partial x}, \frac{\partial u}{\partial y}$$

$$\frac{\partial u}{\partial \xi}, \frac{\partial u}{\partial \eta}$$

$$\frac{\partial u}{\partial x} = \frac{\partial u}{\partial \xi} \frac{\partial \xi}{\partial x} + \frac{\partial u}{\partial \eta} \frac{\partial \eta}{\partial x} ; \quad \frac{\partial u}{\partial y} = \frac{\partial u}{\partial \xi} \frac{\partial \xi}{\partial y} + \frac{\partial u}{\partial \eta} \frac{\partial \eta}{\partial y}$$

$$\frac{\partial^2 u}{\partial x^2} = \left[\frac{\partial^2 u}{\partial \xi^2} \left(\frac{\partial \xi}{\partial x} \right)^2 \right] + \left[\frac{\partial^2 u}{\partial \eta \partial \xi} \left(\frac{\partial \xi}{\partial x} \frac{\partial \eta}{\partial x} + \frac{\partial \xi}{\partial y} \frac{\partial \eta}{\partial x} \right) \right] + \left[\frac{\partial^2 u}{\partial \eta^2} \left(\frac{\partial \eta}{\partial x} \right)^2 \right]$$