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Paul Evenson

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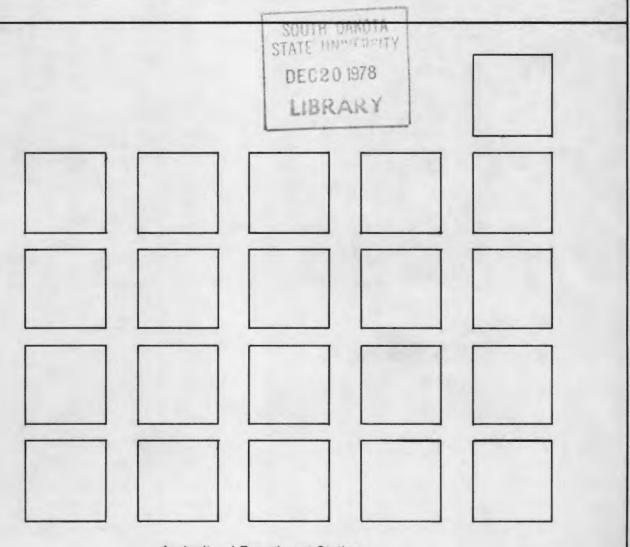
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Calculation of Multiple Regression with Three Independent Variables Using a Programable Pocket Calculator



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Agricultural Experiment Station South Dakota State University Brookings, South Dakota

Calculation of Multiple Regression with Three Independent Variables Using a Programable Pocket Calculator

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Plant Science and Statistics

Multiple regression is used to develop equations that describe relationships among several variables.

This paper describes a multiple regression program for an equation with one dependent and three independent variables, which was written for a Hewlett-Packard 97 programable "pocket" calculator.

Once each variable is entered, the program calculates sums, sums of squares, sums of cross-products and means of all variables, as well as the number of entries. It also computes the deter-

minant of the matrix, elements of the inverted matrix, and regression coefficients. The intercept is calculated after means of all variables are reentered, and a predicted value for the dependent variable can be determined for any set of independent variables.

The multiple regression equation with three independent variables has the form $\hat{Y} = a + b_1 X_1 + b_2 X_2 + b_3 X_3$ where a is the intercept; b_1 , b_2 , and b_3 are regression coefficients; Y is the dependent variable; and X_1 , X_2 , and X_3 are independent variables.

Calculation of Regression Coefficients

The normal equations for this multiple regression are:

$$x_1 : \Sigma x_1^2 b_1 + \Sigma x_1 x_2 b_2 + \Sigma x_1 x_3 b_3 = \Sigma x_1 y$$
 $x_2 : \Sigma x_1 x_2 b_1 + \Sigma x_2^2 b_2 + \Sigma x_2 x_3 b_3 = \Sigma x_2 y$
 $x_3 : \Sigma x_1 x_3 b_1 + \Sigma x_2 x_3 b_2 + \Sigma x_3^2 b_3 = \Sigma x_3 y$

where

$$\Sigma x_{i}^{2} = \Sigma X_{i}^{2} - \frac{(\Sigma X_{i})^{2}}{n}$$

$$\Sigma x_{i}y = \Sigma X_{i}Y - \frac{(\Sigma X_{i})(\Sigma Y)}{n}$$

$$\Sigma x_{i}x_{j} = \Sigma X_{i}X_{j} - \frac{(\Sigma X_{i})(\Sigma X_{j})}{n}$$

n = number of entries

The following matrices are used to solve this set of equations.

$$A = \begin{bmatrix} \sum x_1^2 & \sum x_1 x_2 & \sum x_1 x_3 \\ \sum x_1 x_2 & \sum x_2^2 & \sum x_2 x_3 \\ \sum x_1 x_3 & \sum x_2 x_3 & \sum x_3^2 \end{bmatrix}, B = \begin{bmatrix} b_1 \\ b_2 \\ b_3 \end{bmatrix}, \text{ and } C = \begin{bmatrix} \sum x_1 y \\ \sum x_2 y \\ \sum x_3 y \end{bmatrix}$$

where

$$A \cdot B = C$$

To solve for B, multiply both sides of the equation by the inverse

of A,
$$A^{-1}$$
.
 $A^{-1} \cdot A \cdot B = C \cdot A^{-1}$

Since $A^{-1} \cdot A = I$, the identity matrix, then

$$I \cdot B = C \cdot A^{-1}$$
 or $B = C \cdot A^{-1}$

$$A^{-1} \cdot C = \begin{bmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \\ a_{31} & a_{32} & a_{33} \end{bmatrix} \begin{bmatrix} \sum x_1 y \\ \sum x_2 y \\ \sum x_3 y \end{bmatrix} = B = \begin{bmatrix} b_1 \\ b_2 \\ b_3 \end{bmatrix}$$

where $a_{i,i}$'s are elements of A^{-1} .

|A| is the determinant of A and is used in calculating A^{-1} .

Calculation of the Intercept

The intercept
$$a = \overline{y} - b_1 \overline{x}_1 - b_2 \overline{x}_2 - b_3 \overline{x}_3$$

where $\overline{y} = \frac{\Sigma Y}{n}$ and $\overline{x}_i = \frac{\Sigma X_i}{n}$

USET HISTUCTIONS

Multiple Regression (Card 1)

A & C

 X_1, X_2, X_3, Y_1

Matrices _

A

OUTPUT **INPUT** STEP **INSTRUCTIONS KEYS** DATA/UNITS **DATA/UNITS** Enter card 1 Do 3 ~ 6 for each entry X_1 3. Enter X₁ X_2 Enter X2 X_2 X3 Enter X3 5. Enter Y and compute sums, sum of squares, and Y sum of cross-products Calculate statistics for A & C matrices ΣX_1 O 7. В ΣΧ2 1 ΣX₃ 2 ΣΥ 3 $\Sigma X_1^2 4$ ΣX3 5 ΣX3 6 ΣY² 7 n 9 -- A X₁ B C D Ε $\Sigma X_1 X_2 = 0$ $\Sigma X_1 X_3$ 1 ΣX₁ Y 2 $\Sigma X_2 X_3$ 3 ΣX₂Y 4 $\Sigma X_3 Y$ 5 8 9 Α В Xз D E (continued)

7

STEP	INSTRUCTIONS	INPUT DATA/UNITS	KEYS	OUTPUT DATA/UNITS
				$\Sigma x_1 x_2 = 0$
				$\Sigma x_1 x_3 = 1$
				Σx ₁ y 2
				Σx ₂ x ₃ 3
				Σx ₂ y 4
				$\Sigma x_3 y = 5$
				Σx_1^2 6
				Σx_2^2 7
				Σx ² / ₃ 8
				Σy ² 9
				A
				X ₁ B
				X ₂ C
				X ₃ D
				Y E
				I
				ΣX_1 0
				ΣX_2 1
				ΣX_3 2
				ΣΥ 3
				\overline{x}_2 5
				\overline{x}_1 4 \overline{x}_2 5 \overline{x}_3 6
				y 7
				8
				n 9
				A
				X ₁ B
				X_2 C
				X_3 D
				Y E
				I
0 0 3			C	
8. Calc	ulate determinant A			A

User Instructions



STEP	INSTRUCTIONS	INPUT DATA/UNITS	KEYS	OUTPUT DATA/UNITS
9.	Enter Card 2			
10.	Calculate elements of A-1		A	a _{]]} 0
				a ₁₂ 1
				a ₁₃ 2
				a ₂₁ 3
				a ₂₂ 4
				a ₂₃ 5
				a ₃₁ 6
				a ₃₂ 7
				a ₃₃ 8
				n 9
				A
				Х1 В
				X ₂ C
				X ₃ D
				Y E
				A I
11.	Calculate regression coefficients and store		В	T
	in R_0 ', R_1 ', and R_2 ', respectively.			b ₃ Z
				b ₂ Y
				b ₁ X
12.	Re-enter \overline{x}_1	x ₁	fa	\bar{x}_1
13.	Re-enter x ₂	$\frac{\overline{x}_2}{\overline{x}_3}$	R/S	$\frac{x_1}{\overline{x}_2}$
14.	Re-enter \overline{x}_3	x ₃	R/S	\overline{x}_3
15.	Re-enter y	y	R/S	y
16.	Calculate intercept		f b	a
17.	Calculate Ŷ			
	Enter X ₁	xı	1	
	Enter X ₂	Х2	†	
	Enter X ₃	Х3	fc	Ŷ

Example

Entry #	X ₁	x ₂	x ₃	Υ
1	0.94	4.22	1.58	8.23
2	1.13	3.48	1.28	8.26
3	0.61	2.20	0.64	9.33
4	1.17	2.20	0.08	8.92
5	0.93	2.25	0.38	8.89
6	1.94	2.45	1.45	8.34
7	2.12	2.62	2.31	8.51
8	1.03	2.97	3.60	9.15
9	0.67	2.90	2.59	9.40
10	0.78	2.64	1.62	9.01
11	1.10	2.64	3.16	8.77
12	1.78	2.39	0.23	8.11
13	1.54	2.76	0.76	8.00
14	1.77	2.23	1.42	8.68
15	2.22	3.35	1.86	8.11

	<u>Operation</u>	Output
1.	Enter Card I	0.00 ***
2.	.94	0.94 Ent +
3.	4.22	4.22 Ent ↑
4.	1.58	1.58 Ent +
5.	8.23 A	8.23 GSBA
6.	1.13	1.13 Ent ↑
7.	3.48	3.48 Ent +
8.	1.28	1.28 Ent +
9.	8.26 A	8.26 GSBA
		•

		9	
57.	2.22		Ent ↑
58.	3.35		Ent +
59.	1.86		Ent ↑
60.	8.11 A —	8.11	GSBA
61.	B —	7V 10.772	GSBB
		ΣX ₁ 19.73	
		ΣX ₂ 41.30	
		ΣX ₃ 22.96 ΣΥ 129.71	
		2	
		_	
		ΣX_3^2 50.52 ΣY^2 1124.65	
		0.00	
		n 15.00	
		0.00 used 2.22	
		used 3.35	
		used 1.86	
		used 8.11	
		0.00	1
		$\Sigma X_1 X_2$ 54.07	0
		$\Sigma X_1 X_3 \qquad 29.88$	
		ΣΧ ₁ Υ 168.21	2
		$\Sigma X_2 X_3 \qquad \qquad 66.03$	3
		ΣΧ ₂ Υ 355.72	
		ΣΧ ₃ Υ 200.34	5
		0.00	6
		0.00	7
		0.00	8
		0.00	9
		0.00	A
		used 2.22	
		used 3.35	
		used 1.86	
		used 8.11	
		0.00	

	Σ _{x1} x ₂	-0.25	0
	Σ _x 1 ^x 3	-0.32	1
	Σx ₁ y	-2.40	2
	Σx ₂ x ₃	2.82	3
	Σx ₂ y	-1.42	4
	Σx ₃ y	1.80	5
	Σ _x ² ₂ Σ _x ² ₂ Σ _x ² ₂	4.00	6
	$\Sigma_{\mathbf{X}_{2}^{2}}$	4.51	7
	$\Sigma_{\mathbf{X}}^{2}$	15.37	8
	Σy2	3.00	9
		0.00	A
	used	2.22	В
	used	3.35	С
	used	1.86	D
	used	8.11	E
		0.00	I
	ΣΧ1	19.73	0
	ΣX_2	41.30	1
	ΣΧ3	22.96	2
	ΣΥ	129.71	3
	$\frac{\overline{x}}{\overline{x}}$ $\frac{\overline{x}}{\overline{x}}$ $\frac{\overline{x}}{\overline{y}}$	1.32	4
	\overline{x}_2	2.75	5
	$\frac{1}{x_3}$	1.53	6
	y	8.65	7
		0.00	8
	n	15.00	9
		0.00	A
	used	2.22	В
	used	3.35	C
	used	1.86	D
	used	8.11	E
		0.00	I
<u> </u>		_	GSBC
	A	244.83	***

10

62. **(**

63. Enter Card 2			
64. A —	٦		GSBA
	a ₁₁ of A ⁻¹	0.25	0
	a ₁₂ of A ⁻¹	0.01	
	a ₁₃ of A ⁻¹	2.890104573-03	2
	a ₂₁ of A ⁻¹	0.01	
	a_{22}^{21} of A^{-1}	0.25	4
	a ₂₂ of A ⁻¹	-0.05	
	a ₂₁ of A ⁻¹	2.890104573-03	6
	a ₃₂ of A ⁻¹	-0.05	
	a ₃₃ of A ⁻¹	0.07	8
	n	15.00	9
		0.00	A
	used	2.22	В
	used	3.35	С
	used	1.86	D
	used	8.11	E
	A	244.83	I
65. B			GSBB
	used	-0.01	T
	b ₃	0.19	Z
	b ₂	-0.47	Y
	b ₁	-0.62	Х
	_		
66. 1.32 f a	\overline{x}_1	1.32	GSBa
67. 2.75 R/S	_	2.75	R/S
68. 1.53 R/S	$\frac{\overline{x}_2}{\overline{x}_3}$	1.53	R/S
69. 8.65 R/S -	· 😴	8.65	R/S
70. f b	•		GSBb
	a	10.46	***
71. 1.00 🕂	· X ₁	1.00	Ent +
72. 3.00 🕁	x_2	3.00	Ent +
73. 1.50 f c		1.50	GSBc
	x ₃	8.72	***

Therefore, $\hat{Y} = 10.46 - 0.62 X_1 - 0.47 X_2 + 0.19 X_3$ When $X_1 = 1.00$, $X_2 = 3.00$, and $X_3 = 1.50$; $\hat{Y} = 8.72$

Example

Card 1			Card 2
.94 ENT†	2.23 ENT†	-0.25 0	GSBA
4.22 ENT†	1.42 ENT1	-0.32 1	00211
1.58 ENT†	8.68 GSBA	-2.40 2	0.25 0
8.23 GSBA	2.22 ENT†	2.82 3	
1.13 ENT†	3.35 ENT†		
3.48 ENT†		-1.42 4	2.890104573-03 2 0.01 3
	1.86 ENT†	1.80 5	0.01 3
1.28 ENT†	8.11 GSBA	4.00 6	0.25 4
8.26 GSBA	ESBB	4.51 7	-0.05 5
.61 ENT!		15.37 8	2.890104573-03 6
2.20 ENT†	19.73 0	3.00 9	-0.0 5 7
.64 ENT†	41.30 1	0.00 A	0.0 7 8
9.33 GSBA	22 .9 6 2	2.22 B	15 .00 9
1.17 ENT†	129.71 3	3.35 C	0.00 A
2.20 ENT1	29.95 4	1.86 D	2.22 B
.08 ENT†	118.22 5	8.11 E	3.35 C
8.92 GSBA	50.5 2 6	0.00 I	1.86 D
.93 ENT†	1124.65 7		8.11 E
2.25 ENT†	0.00 8	19.73 0	244.83 I
.38 ENT†	15.00 9	41.30 1	
8.89 GSBA	0.00 A	22.96 2	GSBB
1.94 ENT†	2.22 B	129.71 3	5522
2.45 ENT+	3.35 C	1.32 4	-0.01 T
1.45 ENT+	1.86 D	2.75 5	0.19 Z
8.34 GSBA	8.11 E	1.53 6	
2.12 ENT†	0.00 I	8.65 7	
2.12 ENT1	0.00 1		-0.62 X
		0.00 8	. 70.005
2.31 ENT†	E4 07 0	15.00 9	1.32 GSBa
8.51 GSBA	54.07 0	0.00 A	2.75 R/S
1.03 ENT+	29.88 1	2.22 B	1.53 R/S
2.97 ENT+	168.21 2	3.35 C	8.€5 R/S
3.60 ENT†	66.03 3	1.86 D	€SB b
9.15 GSBA	355.72 4	8.11 E	10.46 ***
.67 ENT:	2 00.34 5	0.00 I	
2.90 ENT1	0.00 6		1.00 ENT1
2.59 ENT↑	0.00 7	€SBC	3.00 ENT1
9.40 GSBA	0.00 8	244.83 ***	1.50 GSBa
.78 ENT†	0.00 9		8.72 ***
2.64 ENT†	0.00 A		0.72 ***
1.62 ENT†	2.22 B		
9.01 GSBA	3.35 C		
1.10 ENT†	1.86 D		
2.64 ENT†	8.11 E		
3.16 ENT†	0.00 I		
8.77 GSBA	0.00 1		
1.78 ENT†			
2.39 ENT1			
.23 ENT†			
8.11 GSBA			
1.54 ENT†			
2.76 ENT†			
.76 ENT†			
8.00 GSBA			
1.77 ENT#			

					10						
			P	roc	ram	- 0	ara	1 1			
*											
. 001	*LBLA	21 11	061	RCL4	36 04	121	RCL2	36 02	181	RCL1	36 01
002	STOE	35 15	062	RCL0	36 00	122		36 09	182	X	-35
003	R4	-31	063	RCL9	36 09	123		-24	183	X	-35
004	STOD	35 14	064	÷	-24		×	-35	184	2	82
005	R↓	-31	065	ST04	35 04	125	-	-45	185	X	-35
* 006	STOC	35 13	066	XS	53	126	P≢S	16-51	186	+	-55
. 007	R4	-31	967	RCL9	36 09	127	ST01	35 01	187	RCL1	
008	STOB	35 12	068	×	-35	128	RCL2	36 02	188	X2	53
** 009	ST+0	35-55 00	069	-	-45	129	₽≢S	16-51	189	RCL7	36 07
. 010	XS	53	979	P#S	16-51	130	RCL0	36 00	190	X	-35
011	ST+4	35-55 04	071	ST06	35 06	131	RCL3	36 03	191	-	-45
▶ 812	Rt	16-31	972	P≠S	16-51	132	RCL9	36 09	192	RCLO	36 00
013	ST+1	35-55 01	073	RCL5	36 05		÷	-24	193	Xs	53
814	X2	53	074	RCL1	36 01	134	X	-35	194	RCL8	36 08
₩ 015	ST+5	35-55 05	075	RCL9	36 09	135	-	-45	195	X	-35
	Rf	16-31	076	÷	-24	136	P#S	16-51	196	-	-45
016	ST+2	35-55 02	077	ST05	35 05	137	STO2	35 02	197	RCL3	36 03
₩ 018	XS	53	078	X2	53	138	RCL3	36 03	198	X2	53
919	ST+6	35-55 06	079	RCL9	36 09	139	P#S	16-51	199	RCL6	36 06
020	Rf	16-31	080	×	-35	149	RCL1	36 01	200	X	-35
₩021	ST+3	35-55 03	081	-	-45	141	RCL2	36 02	201	-	-45
922	X2	53	082	P#S	16-51	142	RCL9	36 09	202	STOI	35 46
023	ST+7	35-55 07	083	ST07	35 07	143	÷	-24	203	PRTX	-14
- 024	RCL9	36 09	084	P#S	16-51	144	×	-35	204	RTN	24
	1	01	085	RCL6	36 06	145	-	-45	205	R/S	51
025 026	+	-55	086	RCL2	36 02	146	P#S	16-51			-
- 027	ST09	35 09	087	RCL9	36 09	147	ST03	35 03			
028	P#S	16-51	088	÷	-24	148	RCL4	36 04			
829	RCLB	36 12	089	ST06	35 06	149	P≠S	16-51			
	RCLC	36 13	090	Xs	53	150	RCL1	36 01			
036	X	-35	091	RCL9	36 09	151	RCL3	36 03			
* 032	ST+0	35-55 00	092	X	-35	152	RCL9	36 09			
	RCLB	36 12	093	_	-45	153	+	-24			
033	RCLD	36 14	894	P≠S	16-51		×	-35			
034		-35	095	STO8	35 08	155	2	-45			
035	CTAI		896	P≠S	16-51	156	PIS	16-51			
036	ST+1	35-55 01	097	RCL7	36 07			35 04			
037	RCLB	36 12		RCL3	36 03	157	STO4				
~ 038	RCLE	36 15	098		36 09	158	RCL5	36 05			
. 039	X	-35	099	RCL9		159	P#S	16-51			
040	ST+2	35-55 02	100		-24	160	RCL2	36 02			
- 041	RCLC	36 13	101	STO7	35 07	161	RCL3	36 03			
. 042	RCLD	36 14	102	XS	53	162	RCL9	36 09			
043		-35	103	RCL9	36 09	163	÷	-24			
844	ST+3	35-55 03	104	×	-35	164	X	-35			
045	RCLC	36 13	105	-	-45	165	-	-45			
046	RCLE	36 15	106	P≢S	16-51	166	P#S	16-51			
- 047	X	-35	107	ST09	35 09	167	ST05	35 05			
048	ST+4	35-55 04	108	RCL0	36 00	168	PREG	16-13			
049	RCLD	36 14	109	P ≠S	16-51	169	P#S	16-51			
DED	DOLE	76 1E	110	DCIA	76 00	170	DDEC	15-17			

- 050

052

-- 053 054

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* 058

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RCLE

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PREG

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36 15

16-51

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36 00

36 03

P	r	0	а	r	а	m	-	C	a	r	d	2
---	---	---	---	---	---	---	---	---	---	---	---	---

RCL4

×

RCL2

RCL5

ST07

PRTX

RTH

*LBLc

RCL2

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ST08

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RCL1

X

ST+8

R↓ **RCL0**

X

ST+8

RCL7

RCL8

+ PRTX

> RTN R/S

X

36 04

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35 07

36 02 -35,

35 08 -31

36 01 ...

-31 36 **00**

36 08

-55 -14

24.

51

-354

35-55 08

35-55 08 36 07

-35

24, 21 16 13

36 02. 36 05

			Pr	ogr	am	- C	ard	1 2	
001	*LBLA	21 11			16-51			36 00	181
002	RCL7	36 07	062	RCL6	36 06	122	RCLC	36 13	182
003	RCL8	36 08	06 3	RCL3	<i>36 03</i>	123	Х	-35	183
004	X	-35		X		124	RCL1	36 01	184
005	RCL3	36 0 3	065	RCL1	3€ 01	125	RCLD	36 14	
006	Χs	53 -45	966		36 00	126	X	-35	
667	_		067 068	X -	-35 -45	127 128	RCL2 RCLE	36 0 2 36 15	187 188
008 009	RCLI ÷	36 46 -24	0 69	RCLI			X	-35	
018	₽≢S	16-51		÷	-24		+	-55	
011	STO0	35 00		P≢S			+	-55	
012	₽₽S	16-51		CHS	-22	132	₽≢S	16-51	
013	RCL0	36 00	010	ST05			ST00	35 00	
014	RCL8	36 0 8		₽₽S	16-51		₽₽S	16-51	
	X		075	RCL0	36 00		RCL3	36 03	
016	RCL1	36 0 1	076 077	RCL3 ×	36 03 -35		RCLC x	3€ 13 -35	196 197
	RCL3 ×	36 03 -35	0 78	RCL7	36 0 7		RCL4	36 04	198
	_	-45	679		36 01		RCLD	36 14	
	RCLI	36 46		X	-35	140		75	
021	÷	-24		-	-45	141	RCL5	36 05	
	₽#S		082	RCLI	36 46		RCLE	36 15	202
023	CHS	-22		÷	-24		X	-35 -55	203
824	ST01	35 01		₽₽S	16-51	144	+	-55	204
025	₽≢S	16-51	085	ST06	35 06	145	+	-55	
026	RCL0	3€ 00		P#S	16-51	146	P#S CTO1	16-51	
027	RCL3	36 0 3	087 088	RCL6 RCL3	36 06 36 03	147 148	ST01 P≇S	35 01 16-51	
0 28 0 29	X RCL1	-35 36 01		X	-35	149	RCL6	36 06	200
030	RCL7	36 07	090	RCL0	36 00		RCLC	36 13	
031	X	-35	091		36 01		X	-35	
032	-	-45		X	-35		RCL7	36 07	
033	RCLI	36 46	093	-	-45		RCLD	36 14	
034	÷	-24	094		36 46	154	X	-35	
035	P≢S		695	÷	-24	155			
036	ST02	35 02			16-51		RCLE	3€ 15 -75	
037	P#S	16-51	0 97 0 98	CHS STO7	-22 35 0 7	157 158	X +	-35 -55	
038	RCL0 RCL8	36 00 36 08	099 099	9707 P#S	16-51	159	+	-55	
039 040	KULB X	-35	100	RCL6	36 0 6	160	P≢S	16-51	
041	RCL3	36 03	101	RCL7	36 07	161	ST02	35 02	
042	RCL1	36 01	102	X	-35	162	RCL1	36 01	
043	X	-35	103	RCL0	36 00	163	RCL0	36 00	
044	-	-45	104	Χs	53	164	PRST	16-14	
045	RCLI	36 4 6	105	-	-45	165	RTH	24	
046	÷	-24	106	RCLI	36 46	166	*LBLa	21 16 11	
047	₽₽S	16-51	107 108	÷ P \$S	-24 16-51	167 168	ST03 R/S	35 03 51	
048	CHS	-22 35 0 3	109	ST08	35 0 8	169	STO4	35 04	
049 050	STO3 P \$S	35 6 3 16 - 51	110	PREG	16-13	178	R/S	51	
0 51	RCL6	36 06	111	RTH	24	171	ST05	35 05	
0 52	RCL8	36 08	112	*LBLB	21 12	172	R/S	51	
053	X	-35	113	P≢S	16-51	173	ST06	35 06	
054	RCL1	36 01	114	RCL2	36 02	174	RTN	24	
055	Χz	53	115	STOC	35 13	175	*LBLb	21 16 12	
056	-	-45	116	RCL4	36 04	176	RCL0	36 0 0	
057	RCLI	36 46	117	STOD	35 14 36 85	177 178	RCL3 ×	36 0 3 -35	
058	÷ D+C	-24 16-51	118 119	RCL5 STOE	36 0 5 35 15	178	_	-35 -45	
059	P⊉S STO4	16-51 35 0 4	120	P#S	16 -5 1	180	RCL1		
060	3104	33 84	120	1 40	10 01	200			

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