Frictional Ageing from Interfacial Bonding and the Origins of Rate and State Friction

Li et al., 2011

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Key Points

- Static friction of rocks grows logarithmically with time (ageing). The mechanism for this strengthening is explored in this paper.
- Frictional ageing arises from the formation of interfacial chemical bonds. Plastic creep cannot explain the ageing at the nm scale.
- A single contact (asperity) at the nanoscale level is isolated to investigate the physical origins of ageing process.

Key Points

- Frictional ageing is length-scale dependent: relatively larger at smaller scales.
- Logarithmic dependence is attributed to the rate of the chemical reaction slowing with time.

Methods

- Single Asperity Slide-Hold-Slide friction experiment.
- Nanoscopically sharp oxidized silicon tips and oxidized silicon wafers using Atomic Force Microscope.
- Second experiment between Silicon and Diamond/Graphite shows very contrasting results: little or no ageing.

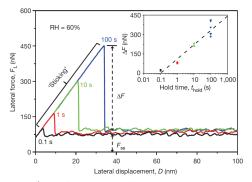


Figure 1 | Lateral force versus nominal lateral displacement data for typical SA-SHS tests after stationary holds at 60% RH. Upon lateral displacement, the tip sticks to the substrate, resulting in linear, elastic lateral loading of the AFM cantilever (Supplementary Figs 1 and 2). When the lateral force exceeds static friction, the tip slips forward, indicated by abrupt drops in lateral force (ΔF) , followed by subsequent sliding at the steady-state friction force $(F_{\rm ss})$. In the inset ΔF varies linearly with the logarithm of hold time. The dotted line is a linear fit of the averaged values.

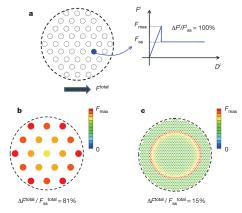


Figure 2 | The quasi-static discrete asperity model. a, An interface between a rigid top surface and an elastic half space with a circular nominal contact area encompassing identical close-packed circular asperities at fixed spacing (small circles), all with maximum static friction force $F_{\rm max}$ (with $\Delta F^i/F_{\rm sl}^i=1$). Upon lateral loading by $I^{\rm folal}$, asperities are uniformly elastically strained up to their maximum static friction, whereupon they slip (see Supplementary Information). The shear force distributions at the peak frictional force for 19 (b) and 1,459 (c) asperities result in macroscopic relative static friction ($\Delta F^{\rm total}/F^{\rm total}$) that is high (0.81) for a but much lower (0.15) for c.

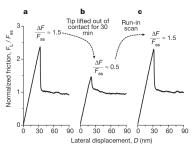


Figure 3 | Normalized friction–displacement curves from three sequential SA-SHS tests. a, Typical, strong ageing is seen immediately after a first run-in scan (cumulative displacement of \sim 1 mm); $\Delta F F_{ss} = 1.5$. b, Ageing is substantially suppressed after 30 min of exposure of the tip to the humid environment, out of contact with the sample, followed immediately by the SA-SHS test shown; $\Delta F I F_{ss} = 0.5$. c, Large ageing returned to the original value after sliding for another run-in scan; $\Delta F I F_{ss} = 1.5$. All tests used a 100-s hold time at 40% RH, with a negative lateral hold force (see Supplementary Information).

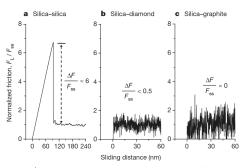


Figure 4 | Three SA-SHS tests between a silica tip and three different surfaces. a, Silica-silica; b, silica-hydrogen-terminated diamond; c, silica-graphite. The tests were all performed at 60% RH for a 100-s hold time. The normal load in each case is maintained at approximately 1 nN. The lateral forces during stationary hold are negative (see Supplementary Information).

Questions and Discussions

- Larger contacts will have lower macroscopic ageing effect: The difference is attributed to multi-asperity vs single asperity; exposure to water and other contaminants. These mechanisms are still not sufficient to explain two orders of magnitude difference in the ageing.
- Chemical bond formation should imply different rocks would have different friction properties. But they are usually considered constant across the whole earth.