

Assignment 1 - Control Design

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2:27 PM

Remark: since we are told q_2, \dots, q_5 are directly actuated & not q_1 , then

$$B(q) = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \tau = B \tau \rightarrow \begin{matrix} B \in \mathbb{R}^{5 \times 4} \\ \tau \in \mathbb{R}^4 \end{matrix} \text{ w/ } \tau_i \text{ being the actuator for joint } q_{i+1}.$$

Goal: design τ

1. We need to pick our gains (K_p, K_d) .

Input: poles = $\{-20, -20\}$

Analytically, we can solve for K_p, K_d .

$$\lambda^2 + K_d \lambda + K_p = (\lambda + 20)^2 = \lambda^2 + 2 \cdot 20 \lambda + 20^2$$

$$\therefore \begin{bmatrix} K_p \\ K_d \end{bmatrix} = \begin{bmatrix} 400 \\ -40 \end{bmatrix}$$

Alternatively, we can use MATLAB's `acker(.)` function

$$\begin{bmatrix} K_p & K_d \end{bmatrix} = \text{acker} \left(\begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}, \begin{bmatrix} 0 \\ 1 \end{bmatrix}, [-20 \ -20] \right)$$

2. We want to show that $G = h^{-1}(\cdot)$ defines a VHC.

First, we are given the error

$$e = h(q) = \begin{bmatrix} q_2 - q_2^{\text{ref}} \\ q_3 - q_3^{\text{ref}} \\ q_4 - q_4^{\text{ref}} \\ q_5 - q_5^{\text{ref}} \end{bmatrix} = \begin{bmatrix} 0_{4 \times 1} & I_{4 \times 4} \end{bmatrix} q - q_{\text{ref}} = H q - q_{\text{ref}}$$

Then we are told to compute $B^\perp D(\sigma(\theta)) \sigma'(\theta)$

$$\textcircled{1} \sigma(\theta) = \begin{bmatrix} \theta \\ q_{\text{ref}} \end{bmatrix} \in \mathbb{R}^5 \Rightarrow \sigma'(\theta) = \begin{bmatrix} 1 \\ 0_{4 \times 1} \end{bmatrix}$$

$$\textcircled{2} B^\perp := \begin{bmatrix} 1 & 0_{1 \times 4} \end{bmatrix}, \text{ so notice that } (\sigma'(\theta))^T = B^\perp$$

$\textcircled{3}$ Since $D(q)$ is assumed positive definite $\forall q$, we have

$v^T D(q) v > 0 \quad \forall v \neq 0$. In particular, letting $v = \sigma'(\theta) \neq 0$ & $q = \sigma(\theta)$, we have:

$$0 < (\sigma'(\theta))^T D(\sigma(\theta)) \sigma'(\theta) = B^\perp D(\sigma(\theta)) \sigma'(\theta)$$

& so $B^\perp D(\sigma(\theta)) \sigma'(\theta)$ is non-zero $\forall \theta \in [\mathbb{R}]_{2\pi}$.

Moreover, since $B^\perp = \begin{bmatrix} 1 & 0_{1 \times 4} \end{bmatrix}$, we have that:

$$B^\perp D(\sigma(\theta)) \sigma'(\theta) = D_{11}(\sigma(\theta)).$$

In code, we are given the inputs:

$D \sim$ the symbolic version of the matrix $D(q)$

$B^\perp = \begin{bmatrix} 1 & 0_{1 \times 4} \end{bmatrix} \sim$ the left annihilator of B (define this in your code)

$q_{\text{ref}} \sim$ "data.qref"

Then in code we compute

`sym theta real`

`sigma = [theta; qref]`

`sigma' = (B_perp)^T`

`val = B_perp * subs(D, sigma) * sigma';` $\forall \theta \in [\mathbb{R}]_{2\pi}$

% check val is non-zero. If indeed val does not depend on θ

% (it shouldn't based on the handout) then we should be able to

% run the command:

`val_num = double(val)`

% check val_num $\neq 0$ & provide an appropriate print stmt.

3. Define the controller

From the "data" structure we need:

$H \sim$ "data.H"

$D(\cdot) \sim$ "data.D(.)"

$B \sim$ "data.B"

$C(\cdot) \sim$ "data.C(.)"

$\nabla_q P(\cdot) \sim$ "data.G(.)"

$K_p \sim$ "data.Kp"

$K_d \sim$ "data.Kd"

$q_{\text{ref}} \sim$ "data.qref"

So that the control input is computed as

$$\tau = (H(D(q))^{-1} B)^{-1} \left[H(D(q))^{-1} (C(q, \dot{q}) \dot{q} + \nabla_q P(q)) - K_p \sin(Hq - q_{\text{ref}}) - K_d H \dot{q} \right]$$