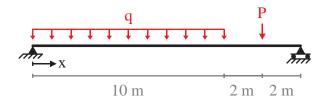
Homework 6 Due: Friday, November 20, 2015 @ 5:00:00 PM in E218

For each problem:

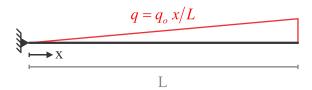
- i) Find the exact solution for the deflection, w(x).
- ii) Define and apply Boundary Conditions to solve for d_1 and d_0 :

$$\overline{w}(x) = d_3 x^3 + d_2 x^2 + d_1 x + d_0$$

- iii) Solve for the remaining unknown coefficients using:
 - a. The Variational Principle
 - b. The Method of Weighted Residuals
- iv) Plot your three solutions on one graph and discuss how they compare.
- **1.** Beam: q = 2 kN/m and P = 10 kN. E = 200,000 MPa, $I = 1 \times 10^9$ mm⁴. Note that the exact solution will be piecewise. The approximate solution, while not piecewise, will require piecewise integration. **25 pts.**



2. Truss: $A = 100 \text{ mm}^2$, E = 200,000 MPa, L = 10 m, $q_o = 2 \text{ kN/m}$. **15 pts.**



Note: The axial deformation, w, of a truss element loaded by a distributed axial load, q, is governed by the differential equation:

$$q = -EA \frac{d^2w}{dx^2}$$

The total potential energy for a truss element can be expressed as:

$$\Pi = \frac{1}{2} EA \int_{L} \left(\frac{dw}{dx} \right)^{2} dx - \int_{L} (qw) dx$$

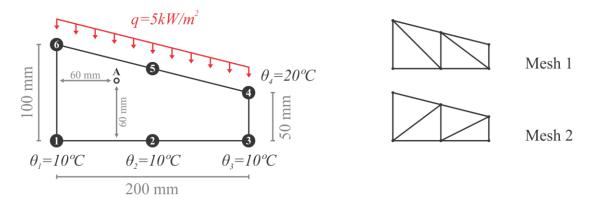
Homework 7 Due: Monday, December 7, 2015 @ 5:00:00 PM in E218

Solve **Question 1** by hand:

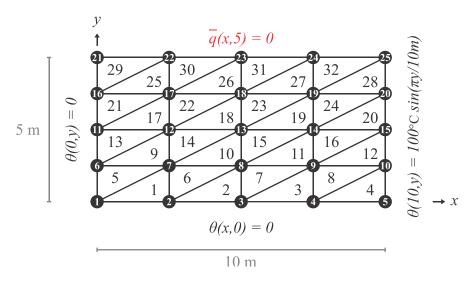
- i) Redraw the diagram and label your elements & degrees of freedom.
- ii) Generate the force vector as well as the element <u>and</u> global stiffness matrices.
- iii) Solve for the nodal temperature values and the temperature at point A.

Code in the heat triangle element into MATLAB and perform an analysis for Questions 1 and 2:

- iv) Provide labeled images of your input geometry and a plot of your temperature distribution.
- v) Compare (tabulate and discuss) your hand calculations with your MATLAB results.
- vi) Provide a short description of your code changes and attach a printout <u>only</u> of the parts of the code that you changed.
- 1. 2D heat: Perform all analyses for both meshes. t = 10 mm. $k_x = k_y = 50$ W/m°C. Q = 0. 25 pts



2. 2D heat: Instead of hand calculations, compare your answer to the exact solution. Q = 0. **15 pts**



Exact solution:
$$\theta(x, y) = \frac{100^{\circ}C}{\sinh(\pi)} \sin\left(\frac{\pi y}{10m}\right) \sinh\left(\frac{\pi x}{10m}\right)$$

FEM – HWs 6-10 2 S. Bagrianski & J.H. Prévost Princeton University

Homework 8 Due: Monday, December 7, 2015 @ 5:00:00 PM in E218

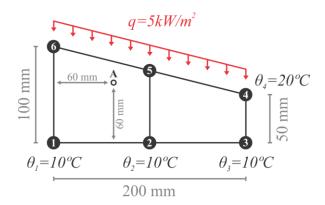
Solve **Question 1** by hand:

- i) Redraw the diagram and label your elements & degrees of freedom.
- ii) Generate the force vector as well as the element <u>and</u> global stiffness matrices.
- iii) Solve for the nodal temperature values and the temperature at point A.

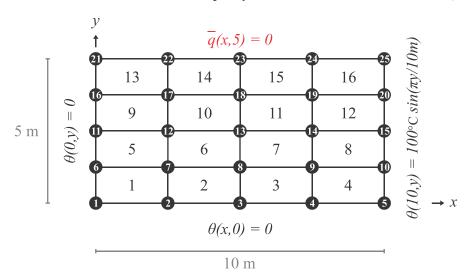
Code in the heat quad element into MATLAB and perform an analysis for **Questions 1 and 2**:

- iv) Provide labeled images of your input geometry and a plot of your temperature distribution.
- v) Compare (tabulate and discuss) your hand calculations with your MATLAB results as well as your calculations from Homework 7.
- vi) Provide a short description of your cod changes and attach a printout <u>only</u> of the parts of the code that you changed.

1. 2D heat: t = 10 mm. $k_x = k_y = 50$ W/m°C. Q = 0. **25 pts**



2. 2D heat: Instead of hand calculations, compare your answer to the exact solution. Q = 0. **15 pts**



Exact solution:
$$\theta(x, y) = \frac{100^{\circ}C}{\sinh(\pi)} \sin\left(\frac{\pi y}{10m}\right) \sinh\left(\frac{\pi x}{10m}\right)$$

FEM – HWs 6-10

S. Bagrianski & J.H. Prévost

Princeton University

Homework 9 Due: Friday, December 11, 2015 @ 5:00:00 PM in E218

For both **Question 1 and 2**:

- i) Redraw the diagram and label your elements & degrees of freedom.
- ii) State whether the problem is Plane Stress or Plane Strain (and why).
- iii) Calculate the applied force vector.

Solve **Question 1** by hand:

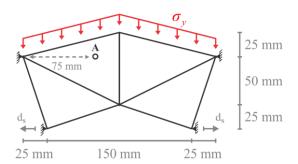
- iv) Generate all element stiffness matrices as well as [K_{UU}] and [K_{US}] without generating [K_G].
- v) Solve for the nodal displacements.
- vi) Find the displacements, $\{\epsilon\}$, $\{\sigma\}$, σ_1 , σ_2 , and θ_p at point A.

Code the elastic triangle into MATLAB and perform an analysis for Questions 1 and 2:

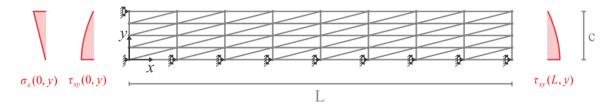
- vii) Provide images of the input and deformed geometry as well as plots of σ_x , σ_y , τ_{xy} , σ_1 & σ_2 .
- viii) Provide a description of your code changes and <u>only</u> the modified parts of your code.

Perform an analysis with SAP2000 for **Questions 1 and 2**:

- ix) Provide images of the input and deformed geometry as well as plots of σ_x , σ_y , τ_{xy} , σ_1 & σ_2 . Finally, for both **Questions 1 and 2**:
- x) Tabulate the displacements from your MATLAB, SAP2000, and hand calculations.
- xi) Compare and discuss your results based on the tabulated displacements and the stress plots.
- **1.** 2D Elasticity: t = 10 m, $E = 200\,000$ MPa, v = 0.3, $d_s = 0.1$ mm, and $\sigma_y = 50$ MPa down. **35 pts**



2. 2D Elasticity: L = 16 m, c = 2 m, t = 10 mm, $E = 10\,000 \text{ MPa}$, v = 0.3, and P = -10 kN. **25 pts**



The non-zero applied surface tractions are defined in global coordinates as:

$$\sigma_x(0,y) = -\frac{3PL}{2tc^3}y$$
 $\tau_{xy}(0,y) = \tau_{xy}(L,y) = \frac{3P}{4tc^3}(c^2 - y^2)$

Use the exact solution, instead of hand calculations, for your comparison:

$$\begin{cases} u_x \\ u_y \end{cases} = \frac{P}{4Etc^3} \begin{cases} y(3x^2 - 6Lx + 2.3c^2 - 2.3y^2) \\ (L - x)^3 - L^3 + x(5.5c^2 + 3L^2) + 0.9(L - x)y^2 \end{cases} \qquad \sigma_x = -3P(L - x)y/2tc^3$$

$$\sigma_y = 0$$

$$\tau_{xy} = 3P(c^2 - y^2)/4tc^3$$

FEM – HWs 6-10 S. Bagrianski & J.H. Prévost

Homework 10 Due: Friday, December 18, 2015 @ 5:00:00 PM in E218

For both Question 1 and 2:

i) Redraw the diagram and label your elements & degrees of freedom.

Solve **Question 1** by hand:

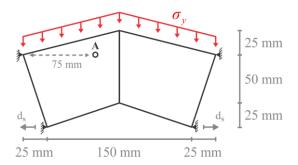
- ii) Generate all required element matrices. For your first integration point, find [D], [J $_{e,1}$], [J $_{e,1}$], [B $_{e,1}$], and [K $_{e,1}$]. Then find [K $_{e,2}$], [K $_{e,3}$], and [K $_{e,4}$] as well as the final [K $_{e}$].
- iii) Find [K_{UU}] and [K_{US}] without solving for [K_G]. Then, solve for the nodal displacements.
- iv) Find the displacements, $\{\varepsilon\}$, $\{\sigma\}$, σ_1 , σ_2 , and θ_p at point A.

Code the elastic quad into MATLAB and perform an analysis for Questions 1 and 2:

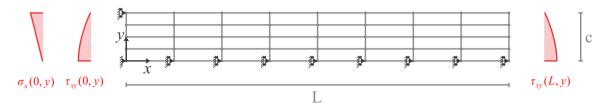
- v) Provide images of the input and deformed geometry as well as plots of σ_x , σ_y , τ_{xy} , σ_1 & σ_2 .
- vi) Provide a description of your code changes and <u>only</u> the modified parts of your code.

Perform an analysis with SAP2000 for **Questions 1 and 2**:

- vii) Provide images of the input and deformed geometry as well as plots of σ_x , σ_y , τ_{xy} , σ_1 & σ_2 . Finally, for both **Questions 1 and 2** (incorporating results from HW9):
- viii) Tabulate the displacements from your MATLAB, SAP2000, and hand calculations.
- ix) Compare and discuss your results based on the tabulated displacements and the stress plots.
- **1.** 2D Elasticity: t = 10 m, $E = 200\,000$ MPa, v = 0.3, $d_s = 0.1$ mm, and $\sigma_v = 50$ MPa down. **35 pts**



2. 2D Elasticity: L = 16 m, c = 2 m, t = 10 mm, $E = 10\,000 \text{ MPa}$, v = 0.3, and P = -10 kN. **20 pts**



The non-zero applied surface tractions are defined in global coordinates as:

$$\sigma_x(0,y) = -\frac{3PL}{2tc^3}y$$
 $\tau_{xy}(0,y) = \tau_{xy}(L,y) = \frac{3P}{4tc^3}(c^2 - y^2)$

Use the exact solution, instead of hand calculations, for your comparison:

$$\begin{cases} u_x \\ u_y \end{cases} = \frac{P}{4Etc^3} \begin{cases} y(3x^2 - 6Lx + 2.3c^2 - 2.3y^2) \\ (L - x)^3 - L^3 + x(5.5c^2 + 3L^2) + 0.9(L - x)y^2 \end{cases} \qquad \sigma_x = -3P(L - x)y/2tc^3$$

$$\sigma_y = 0$$

$$\tau_{xy} = 3P(c^2 - y^2)/4tc^3$$

FEM – HWs 6-10 5 S. Bagrianski & J.H. Prévost Princeton University