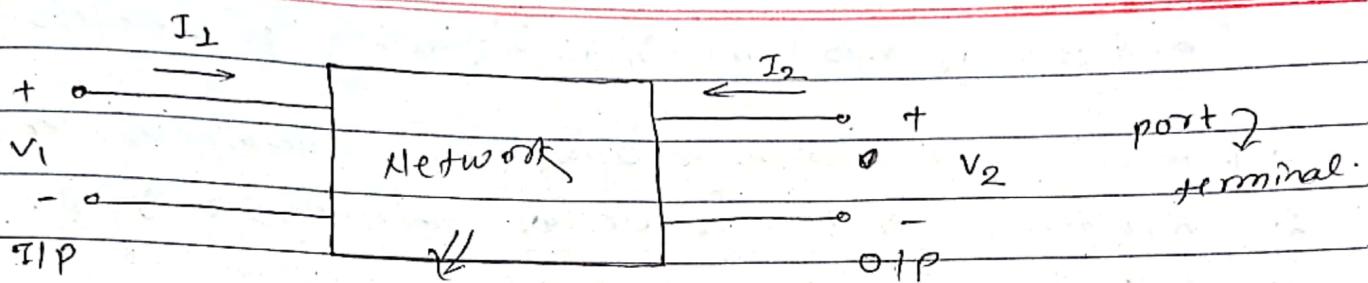


Two Port Network

Date _____
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Passive & active element

↓ ↓

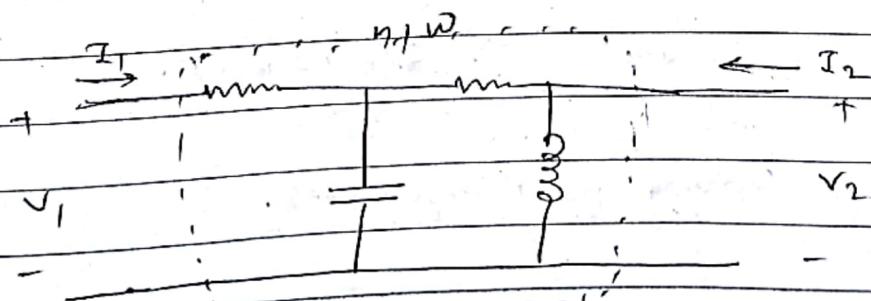
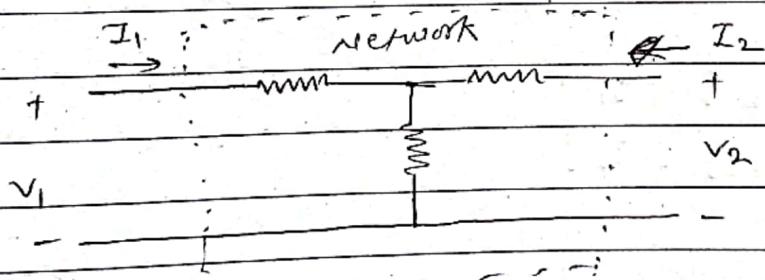
resistor
capacitor

dependent sources

port
terminal.

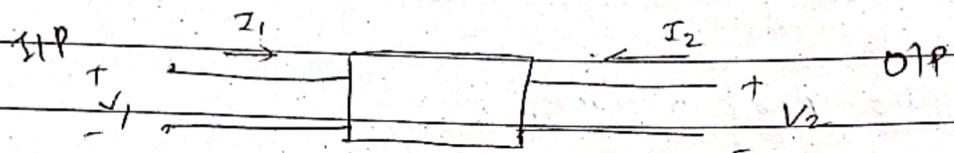
* Properties of two port network.

1. It consists of two pair of terminals
2. It has one TIP and one OIP side.
3. We can provide TIP and take OIP simultaneously.
4. The network consists of passive elements (resistor, inductor and capacitor) in relaxed state (no initial value) and active sources (dependent sources only).



* Analysis of two port network using parameters

1. Impedance parameters or open circuit parameters or Z-parameters
2. Admittance or short circuit parameters or Y-parameters
3. Hybrid or h-parameters
4. ABCD or Transmission parameters.



1. Z or Impedance or open circuit parameters.

Set of standard equations are,

$$V_1 = Z_{11} I_1 + Z_{12} I_2 \quad \text{--- (1)} \quad \text{Voltage equation.}$$

$$V_2 = Z_{21} I_1 + Z_{22} I_2 \quad \text{--- (2)}$$

$$\begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$

\uparrow
Z-parameters.

From eq¹ (1), $I_2 = 0$ (assump) \Rightarrow (OIP is opened)

$$V_1 = Z_{11} I_1$$

$$\Rightarrow Z_{11} = \frac{V_1}{I_1} \quad (\text{Driving point impedance})$$

From eq¹ (2), $I_2 = 0$

$$V_2 = Z_{21} I_1$$

$$\Rightarrow Z_{21} = \frac{V_2}{I_1} \quad (\text{Forward Impedance})$$

Assume $I_1 = 0$ (I/P is opened)

From (1)

$$V_1 = Z_{11} \cdot 0 + Z_{12} I_2$$

$$\Rightarrow Z_{12} = \frac{V_1}{I_2} \quad (\text{Backward impedance})$$

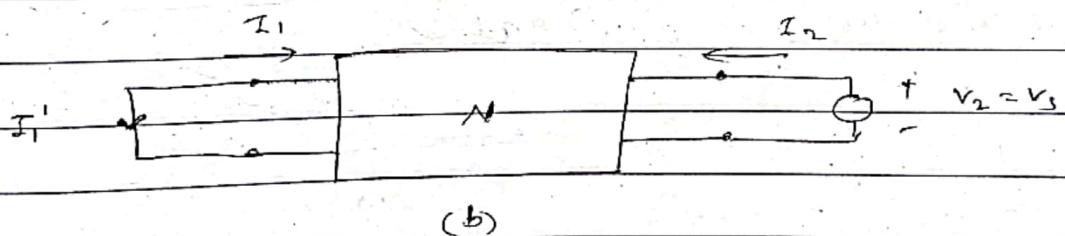
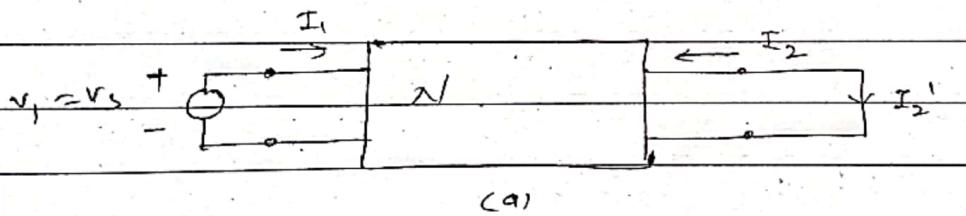
For (2)

$$V_2 = 0 + Z_{22} I_2$$

$$\Rightarrow Z_{22} = \frac{V_2}{I_2} \quad (\text{Output impedance})$$

* condition for reciprocity and symmetry.

Reciprocal :-



The network if produces the same current no matter exchanging the position of source is known as reciprocal.
In above ckt, the netw is reciprocal if

$$I_1' = I_2'$$

From fig. (a)

$$V_1 = V_s, \quad I_{2'} = -I_2, \quad V_2 = 0$$

Since, $V_1 = Z_{11} I_1 + Z_{12} I_2 \quad \text{--- (1)}$

$$V_2 = Z_{21} I_1 + Z_{22} I_2 \quad \text{--- (2)}$$

Put above conditions in eqn (1) & (2)

$$V_s = Z_{11} I_1 + Z_{12} I_2' \quad \text{--- (3)}$$

$$0 = Z_{21} I_1 + Z_{22} I_2' \quad \text{--- (4)}$$

Solving eqn (3) and (4) to get Z_{21}'

$$Z_{21}' = \frac{V_s}{Z_{11} Z_{22} - Z_{12} Z_{21}}$$

Again from fig (b),

$$V_1 = 0, \quad I_1 = -I_1', \quad \text{and} \quad V_2 = V_s.$$

Put above conditions in eqn (1) and (2).

$$0 = -Z_{11} I_1' + Z_{12} I_2 \quad \text{--- (5)}$$

$$V_s = -I_{21} I_1' + Z_{22} I_2 \quad \text{--- (6)}$$

Solving (5) and (6) to get I_1'

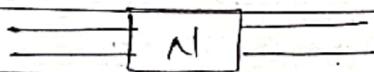
$$I_1' = \frac{V_s}{Z_{11} Z_{22} - Z_{12} Z_{21}}$$

To be reciprocal, $I_1' = I_2'$

$$\frac{V_S}{Z_{21}} - \frac{V_S}{Z_{21}} = Z_{12} Z_{21} - Z_{12} Z_{21}$$

$$\Rightarrow Z_{12} = Z_{21}$$

Symmetry :-



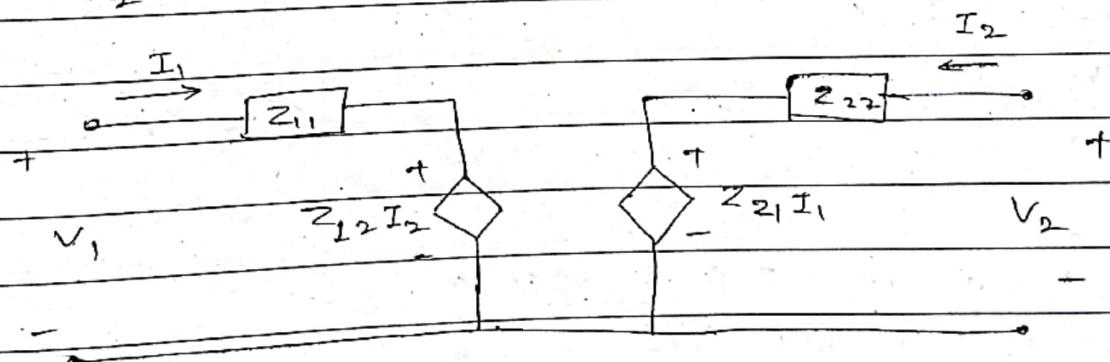
$$Z_{11} = \frac{V_1}{I_1} \quad Z_{22} = \frac{V_2}{I_2}$$

$Z_{11} = Z_{22}$, To be symmetric.

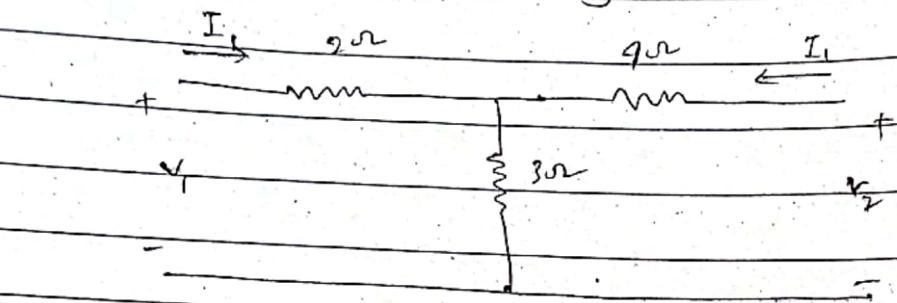
* Equivalent circuit

$$V_1 = Z_{11} I_1 + Z_{12} I_2$$

$$V_2 = Z_{21} I_1 + Z_{22} I_2$$



Q. Find the 2-parameters of the circuit. Also check for reciprocity and symmetry. Draw the equivalent circuit.



Sol:

$$V_1 = Z_{11} I_1 + Z_{12} I_2$$

$$V_2 = Z_{21} I_1 + Z_{22} I_2$$

Let $I_2 = 0$, i.e., OIP is opening

In 1st mesh, applying KVL

$$-2I_1 - 3(I_1 + I_2) + V_1 = 0$$

$$-5I_1 = V_1$$

$$Z_{11} = \frac{V_1}{I_1} = 5\Omega$$

$$\text{and, } V_2 = 3 \times I_1$$

$$Z_{21} = \frac{V_2}{I_1} = 3\Omega$$

Again

Let $I_1 = 0$ i.e., IIP is opening.

In 2nd mesh, applying KVL

$$-4I_2 - 3(I_2 + I_1) + V_2 = 0$$

$$-7I_2 + V_2 = 0$$

$$Z_{22} = \frac{V_2}{I_2} = 7\Omega$$

again, $v_1 = 3I_2$

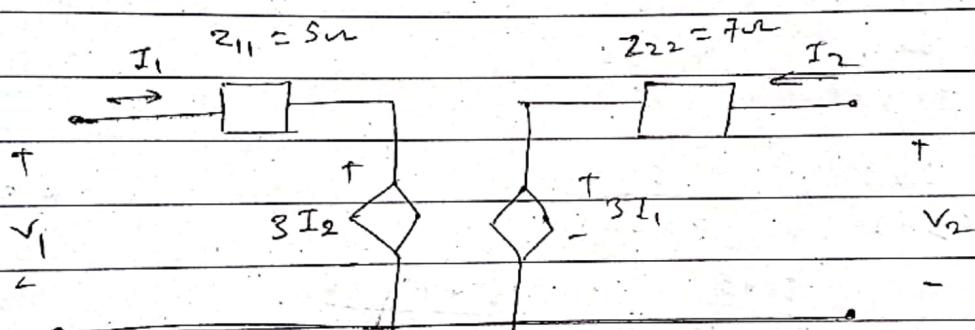
$$Z_{12} = \frac{V_1}{I_2} = 3\Omega$$

$$\left. \begin{array}{l} Z_{11} = 5\Omega \\ Z_{12} = 3\Omega \\ Z_{21} = 3\Omega \\ Z_{22} = 7\Omega \end{array} \right\}$$

since $Z_{12} = Z_{21} = 3\Omega$, the circuit is reciprocal.

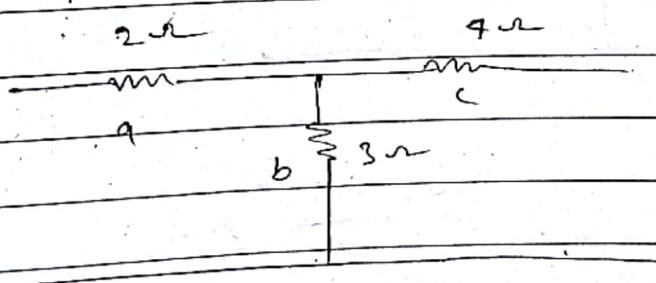
since $Z_{11} \neq Z_{22}$, the circuit is not symmetrical.

Equivalent circuit



Note:

prototype $\eta_1 w$, $T = \eta_1 w$, star. $\eta_1 w$.

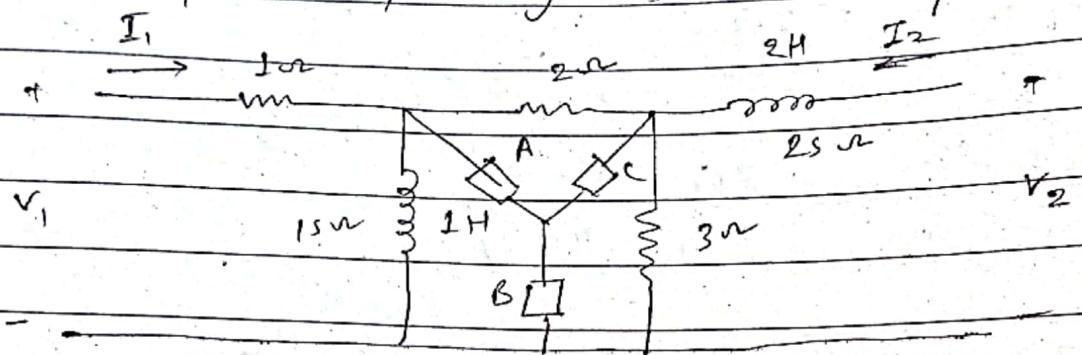


$$Z_{11} = a+b = 5\Omega$$

$$Z_{22} = b+c = 7\Omega$$

$$Z_{12} = Z_{21} = b = 3\Omega$$

Q. Find the Z -parameters of the circuit. Also check for reciprocity and symmetry. Draw the equivalent circuit.



$$A = \frac{2+15}{2+15+3} = \frac{25}{5+s}$$

$$A+1 = \frac{25}{5+s} + 1$$

$$B = \frac{3+15}{2+15+3} = \frac{18}{5+s}$$

$$C = \frac{2+3}{5+s} = \frac{5}{5+s}$$

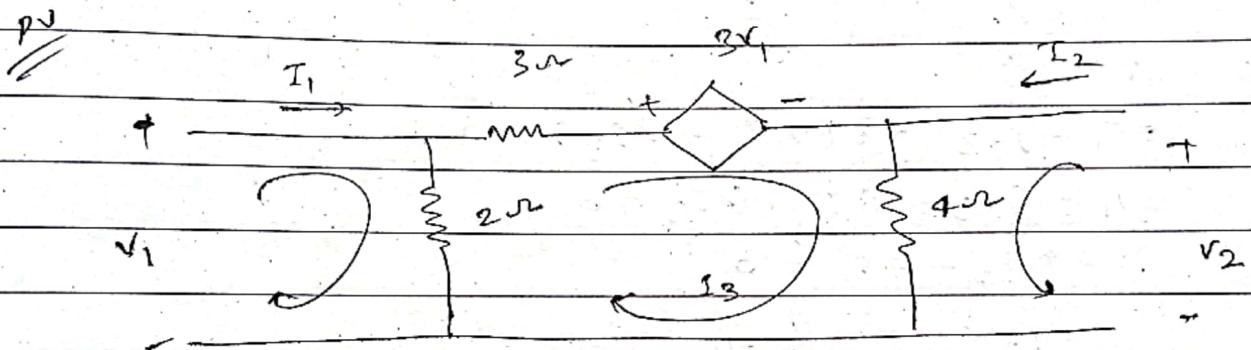
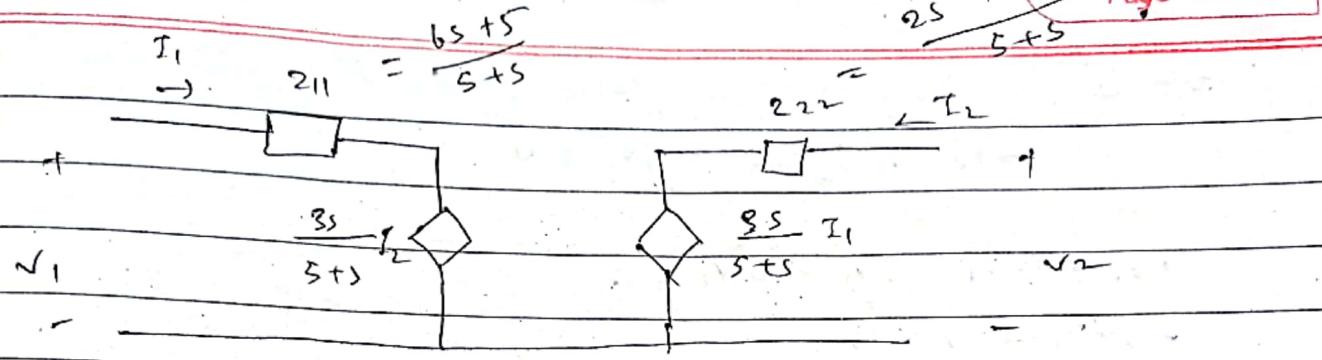
$$= \frac{G}{S+G} + \frac{2s}{S+G}$$

$$\Rightarrow G + Ls^2 + 2s$$

$$Z_{11} = \frac{3s+5}{5+s} + \frac{3s}{5+s} = \frac{6s+5}{5+s}$$

$$Z_{22} = \frac{2s^2+10s+6}{5+s} + \frac{3s}{5+s} = \frac{2s^2+13s+6}{5+s}$$

$$Z_{12} = Z_{21} = \frac{3s}{5+s}$$



Find the open circuit parameters. Also draw equivalent circuit.

(Let, $I_2 = 0$, open circuit opening)

1st mesh using KVL

$$-2(I_1 - I_3) + V_1 = 0$$

$$V_1 = 2I_1 - 2I_3 \quad \text{--- (1)}$$

In 2nd mesh, KVL

$$-3I_3 - 3V_1 - 4(I_3 + I_2) - 2(I_3 - I_1) = 0$$

$$2I_1 - 9I_3 - 3V_1 = 0 \quad \text{--- (2)}$$

Bgn,

$$-4(I_3 + I_2) + V_2 = 0$$

$$V_2 = 4I_3 \quad \text{--- (3)}$$

$$I_3 = \frac{2I_1 - V_1}{2}$$

from ②

$$2I_1 - 9 \frac{2I_1 - V_1}{2} - 3V_1 = 0$$

$$4I_1 - 18I_1 + 9V_1 - 6V_1 = 0$$

$$-14I_1 + 3V_1 = 0$$

$$3V_1 = 14I_1$$

$$\frac{V_1}{I_1} = \frac{14}{3} \Rightarrow Z_{11} = \frac{14}{3} \Omega$$

from ① 2 ②

$$2I_1 - 9I_3 - 3(2I_1 - 2I_3) = 0$$

$$2I_1 - 9I_3 - 6I_1 + 6I_3 = 0$$

$$-3I_3 - 4I_1 = 0$$

$$I_3 = -\frac{4}{3}I_1$$

from ③

$$9I_3 = V_2$$

$$V_2 = 9 \times -\frac{4}{3}I_1$$

$$\frac{V_2}{I_1} = -\frac{16}{3} \Rightarrow Z_{21} = -\frac{16}{3} \Omega$$

let $I_1 = 0$, 1/p is closing.

mesh(3).

$$V_2 - 9(I_2 + I_3) = 0$$

$$V_2 = 9I_2 + 9I_3 \quad \text{--- (4)}$$

mesh(2),

$$3I_3 - 3V_1 - 9(I_2 + I_3) - 2I_3 = 0$$

$$+ 3I_3 - 3V_1 - 4I_2 - 4I_3 - 2I_3 = 0$$

$$3V_1 + 4I_2 + 3I_3 = 0 \quad \text{--- (5)}$$

mem(1) .

$$V_1 - 2(I_1 - I_3) = 0$$

$$V_1 + 2I_3 = 0 \quad \text{--- (6)}$$

$$V_1 = -2I_3$$

$$-6I_3 + 9I_2 + 3I_3 = 0$$

$$4I_2 - 3I_3 = 0$$

$$I_3 = \frac{4I_2}{3}$$

$$\text{mem}, V_1 = -2 \times \frac{4I_2}{3} = -\frac{8}{3}I_2$$

$$\frac{V_1}{I_2} = -\frac{8}{3} n = Z_{12}$$

for (4)

$$I_3 = \frac{V_2 - 4I_2}{2}$$

$$\text{for (1) \& (4)}: I_3 = \frac{4I_2}{3}$$

for (1)

$$3V_1 + 4I_2 + 3 \frac{V_2 - 4I_2}{4} = 0$$

$$V_2 = 4I_2 + 4 \times \frac{4I_2}{3}$$

$$V_2 = 4I_2 + \frac{16I_2}{3}$$

~~$$3V_1 + 4I_2 + \frac{3V_2 - 12I_2}{4} = 0$$~~

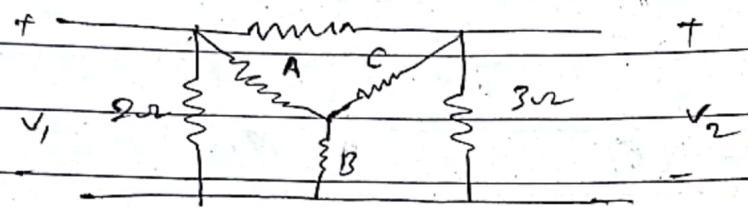
$$V_2 = \frac{12I_2 + 16I_2}{3}$$

~~$$12V_1 + 16I_2 + 3V_2 - 12I_2 = 0$$~~

$$V_2 = \frac{28I_2}{3}$$

$$\frac{V_2}{I_2} = \frac{28}{3} n = Z_{22}$$

Q. Find the equivalent T-network of the given π -network.



$$A = \frac{2 \times 4}{2+4+3} = \frac{8}{9} \Omega$$

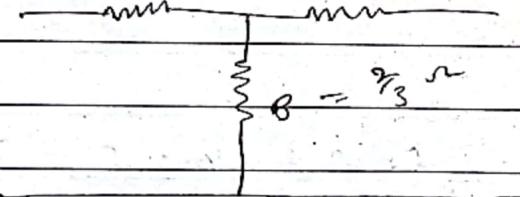
$$B = \frac{2 \times 3}{9} = \frac{6}{9} = \frac{2}{3} \Omega$$

$$Z_{11} = A+B = \left(\frac{8}{9} + \frac{2}{3}\right) \Omega$$

$$C = \frac{9 \times 3}{9} = \frac{12}{9} = \frac{4}{3} \Omega$$

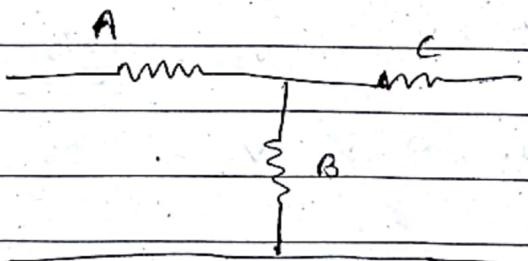
$$Z_{22} = B+C = \left(\frac{2}{3} + \frac{4}{3}\right) \Omega$$

$$A = \frac{8}{9} \Omega \quad C = \frac{4}{3} \Omega$$



$$Z_{12} = Z_{21} = B = \frac{2}{3} \Omega$$

Q. If $Z_{11} = 4 \Omega$, $Z_{22} = 6 \Omega$, $Z_{12} = Z_{21} = 1 \Omega$, then construct equivalent T-network.

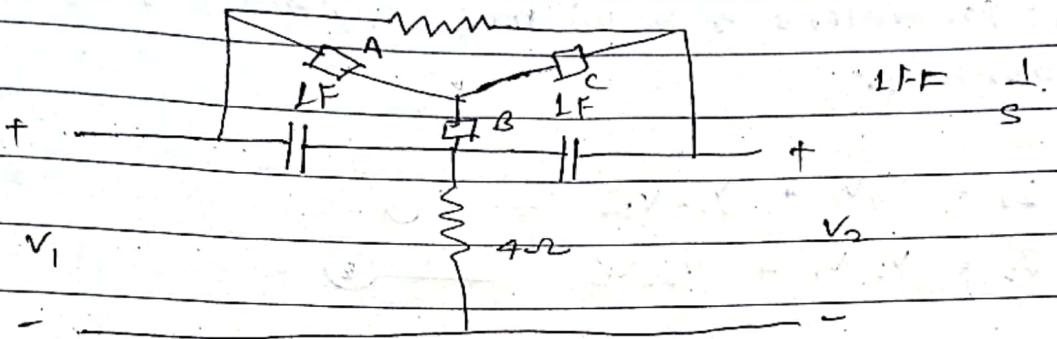


$$A+B = Z_{11} = 4 \Rightarrow A = 4 - B \Rightarrow A = 4 - 1 = 3 \Omega$$

$$B+C = Z_{22} = 6 \Rightarrow C = 6 - B \Rightarrow 5 \Omega$$

$$Z_{12} = Z_{21} = B = 1$$

8v2



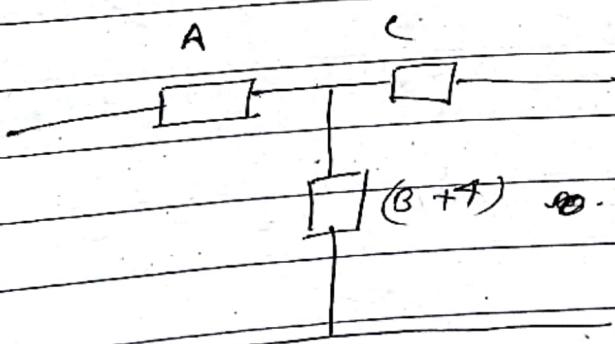
Find the equivalent T-network of the given π -network.

$$A = \frac{3 \times 1/s}{3 + 1/s + 1/s} \Rightarrow \frac{3}{3s + 2}$$

$$B = \frac{1/s \times 1/s}{3 + 1/s + 1/s} \Rightarrow \frac{1}{s(3s + 2)}$$

$$C = \frac{3 \times 1/s}{3 + 1/s + 1/s} \Rightarrow \frac{3}{3s + 2}$$

equivalent T-network,



Y-parameters or admittance parameters or short circuit parameters.

$$I_1 = Y_{11}V_1 + Y_{12}V_2 \quad \text{--- (1)}$$

$$I_2 = Y_{21}V_1 + Y_{22}V_2 \quad \text{--- (2)}$$

$$\begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

↑
Y-parameters.

Let $V_2 = 0$, i.e. output is shorted

from (1)

$$I_1 = Y_{11}V_1 + Y_{12} \times 0$$

$$Y_{11} = \frac{I_1}{V_1} \quad (\text{eq}) \quad (\text{mho})$$

from (2)

~~$I_2 = Y_{21}V_1 + Y_{22} \times 0$~~

$$Y_{21} = \frac{I_2}{V_1} \quad (\text{eq})$$

Let $V_1 = 0$, i.e. input is shorted

from (1)

$$I_1 = Y_{11} \times 0 + Y_{12} \times V_2$$

$$Y_{12} = \frac{I_1}{V_2} \quad (\text{eq})$$

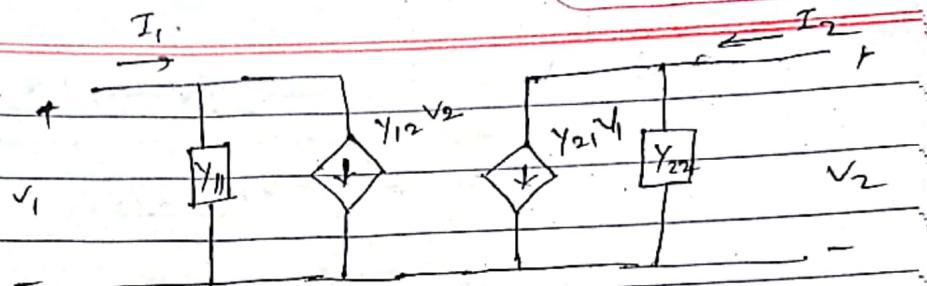
from (2)

$$I_2 = Y_{21} \times 0 + Y_{22}V_2$$

$$Y_{22} = \frac{I_2}{V_2} \quad (\text{eq})$$

Reciprocal :-

$$Y_{12} = Y_{21}$$

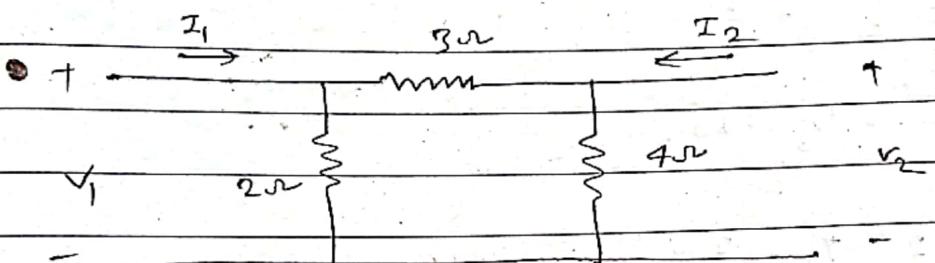


Symmetry :-

$$Y_{11} = Y_{22}$$

equivalent circuit of Y-parameters.

Q:-

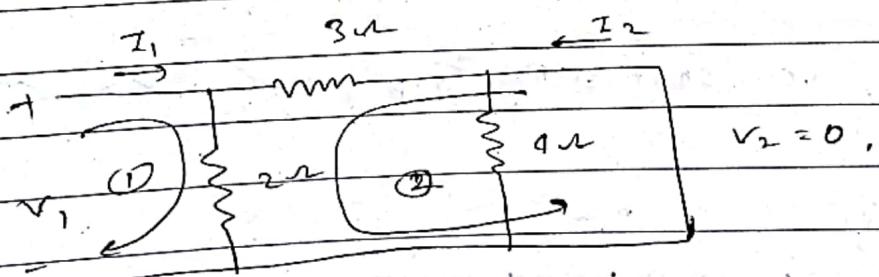


Find the Y-parameters, also check for reciprocity and symmetry - draw equivalent circuit.

$$I_1 = Y_{11} V_1 + Y_{12} V_2 \quad \text{--- (1)}$$

$$I_2 = Y_{21} V_1 + Y_{22} V_2 \quad \text{--- (2)}$$

Let, $V_2 = 0$ i.e. short circuiting output port.



In mesh 1, KVL

$$-2(I_1 + I_2) + V_1 = 0$$

$$V_1 = 2(I_1 + I_2) \quad \text{--- (1)}$$

$$-2I_1 = 5I_2$$

In mesh 2, KVL

$$-3I_2 - 2(I_1 + I_2) = 0$$

$$-2I_1 - 5I_2 = 0 \quad \text{--- (2)}$$

$$I_1 = -\frac{5}{2} I_2$$

$$\text{Ans(1)} \quad V_1 = 2 \left(-\frac{5}{2} I_2 + I_2 \right)$$

$$= 2 \left(-\frac{5}{2} I_2 + 2 I_2 \right)$$

$$= -3 I_2$$

$$Z_{12} = \frac{V_1}{I_2} = -3 \text{ mho}$$

$$\frac{I_2}{V_1} = -\frac{1}{3}$$

$$Y_{21} = -\frac{1}{3} \text{ mho.}$$

$$V_1 = 2 \left(I_1 - \frac{2}{5} I_1 \right)$$

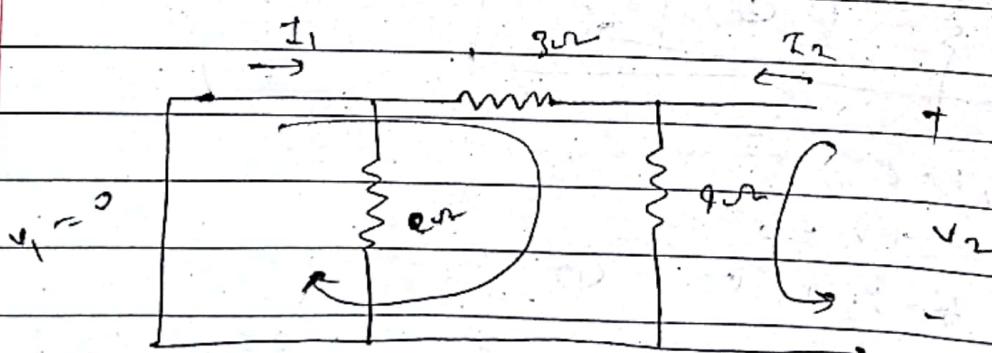
$$= 2 \left(\frac{5-2}{5} I_1 \right)$$

$$= \frac{6}{5} I_1$$

$$\frac{I_1}{V_1} = \frac{5}{6}$$

$$Y_{11} = \frac{5}{6} \text{ mho.}$$

Let $V_1 = 0$, i.e. short circuiting input port.



In first mesh, kvl

$$-3I_1 - 4(I_1 + I_2) = 0$$

$$-7I_1 - 4I_2 = 0 \quad \text{--- (3)}$$

In second mesh, kvl,

$$-4(I_2 + I_1) + V_2 = 0$$

$$V_2 = 4(I_2 + I_1) \quad \text{--- (4)}$$

$$V_2 = R(I_2 + \frac{4}{7}I_2)$$

$$= R \frac{3I_2}{7}$$

$$= \frac{12}{7}I_2$$

$$V_2 = R(\frac{7}{4}I_1 + I_1)$$

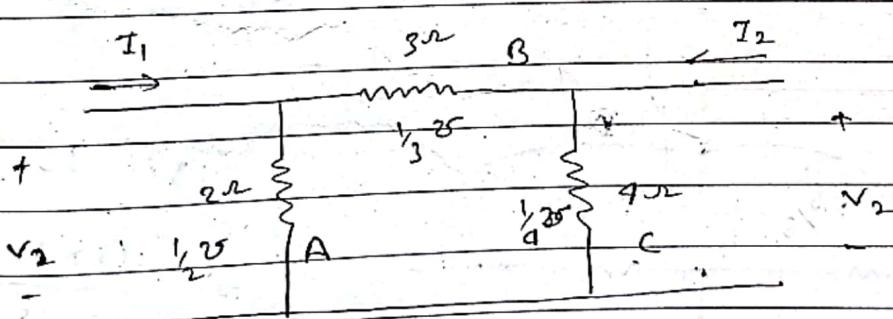
$$= R \left(-\frac{7I_1 + 4I_1}{4} \right)$$

$$= -3I_1$$

$$Y_{22} = \frac{I_2}{V_2} = \frac{7}{7I_2} \text{ mho.}$$

$$Y_{12} = \frac{I_1}{V_2} = -\frac{1}{3} \text{ mho.}$$

2-parameter mesh



γ vñ tñ sñ

(1S + 1 R) vñ

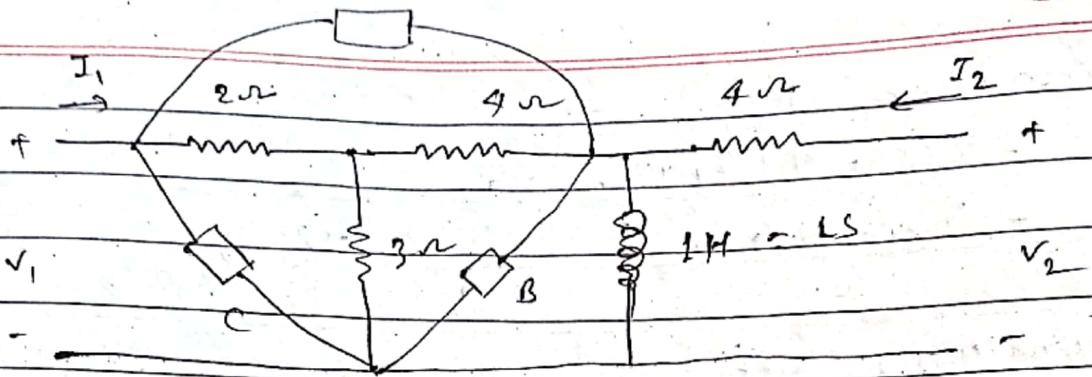
3F vñ sñ

admittance matrix 1

$$Y_{11} = A + B = \frac{1}{2} + \frac{1}{3} = \frac{5}{6} \text{ S}$$

$$Y_{22} = B + C = \frac{1}{3} + \frac{1}{4} = \frac{7}{12} \text{ S}$$

$$Y_{12} = Y_{21} = -B = -\frac{1}{3} \text{ S}$$

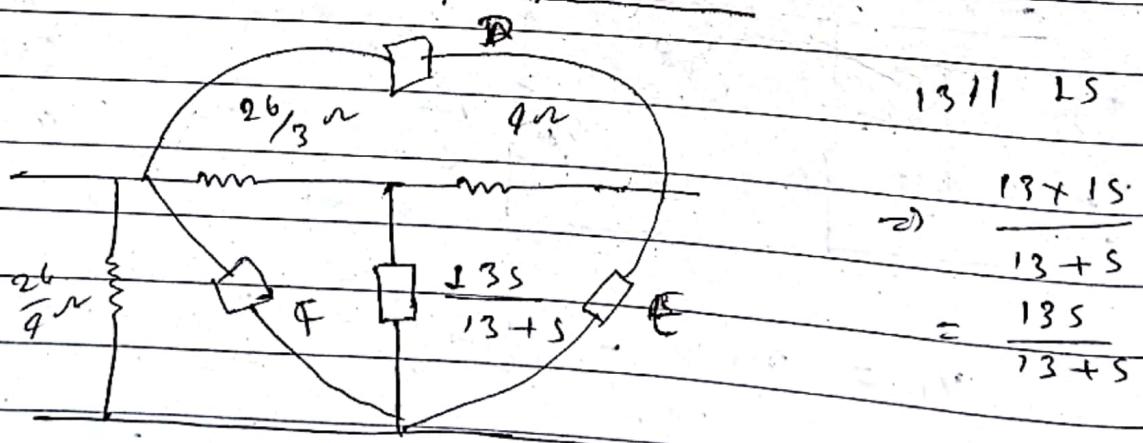
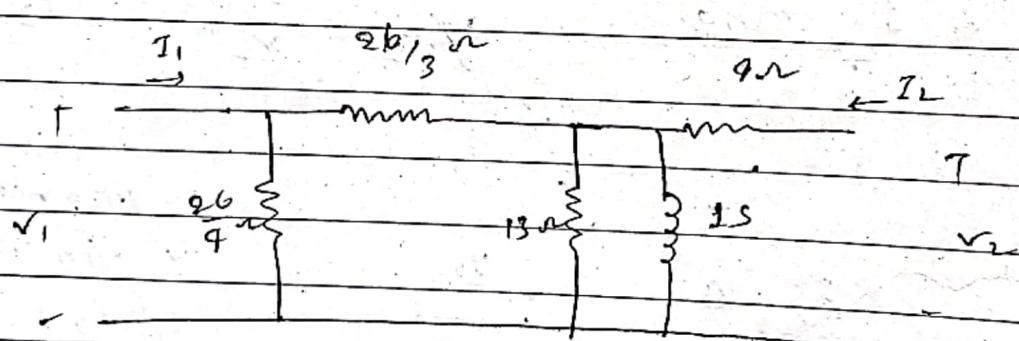


Find admittance parameters of the given network.

$$A = \frac{2 \times 4 + 4 \times 3 + 3 \times 2}{3} = \frac{8 + 12 + 6}{3} = \frac{26}{3}$$

$$B = \frac{26}{2}$$

$$C = \frac{26}{8}$$



$$\Rightarrow \frac{13 \times 13}{13 + 3} = \frac{13 \times 13}{13 + 3}$$

$$\textcircled{1} = \frac{26}{3} \times 4 + \frac{135}{13+s} \times 4 + \frac{26}{3} \times \frac{135}{13+s}$$

$$= \frac{104}{3} + \frac{525}{13+s} + \frac{3385}{3(13+s)}$$

$$= \frac{135}{13+s}$$

$$= \frac{104(13+s) + 3 \times 525 + 3385}{3 \times 135}$$

$$= \frac{1352 + 5985}{39s}$$

$$\textcircled{2} = \frac{(1352 + 5985)}{26(13+s)}$$

$$= \frac{1352 + 5985}{26(13+s)}$$

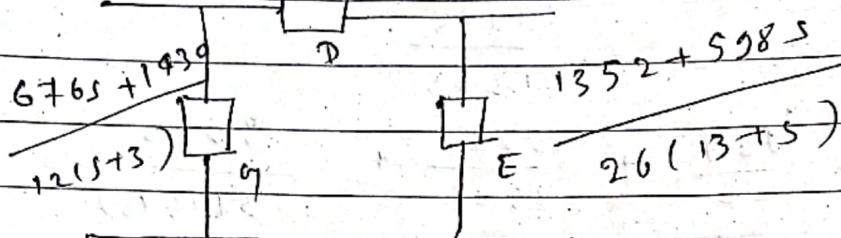
$$\textcircled{3} = \frac{1352 + 5985}{12(s+13)}$$

$$\frac{26}{4} \times \frac{1352 + 5985}{12(s+13)}$$

$$\frac{26}{4} + \frac{1352 + 5985}{12(s+13)}$$

$$\frac{26 \cancel{\times} 3(s+13) + 1352 + 5985}{12(s+13)} = \frac{676s + 1930}{12(s+13)}$$

$$\begin{array}{r} 1352 + 598S \\ \hline 39S \end{array}$$



$$Y_{11} = q + D$$

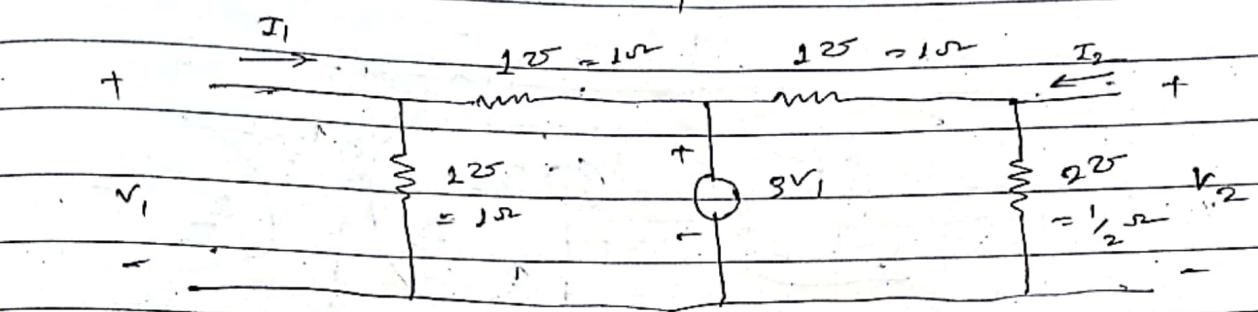
$$\begin{array}{r} 676S + 1430 \\ \hline 12(13+3) \end{array} + \begin{array}{r} 1352 + 598S \\ \hline 39S \end{array}$$

$$Y_{22} = E + D$$

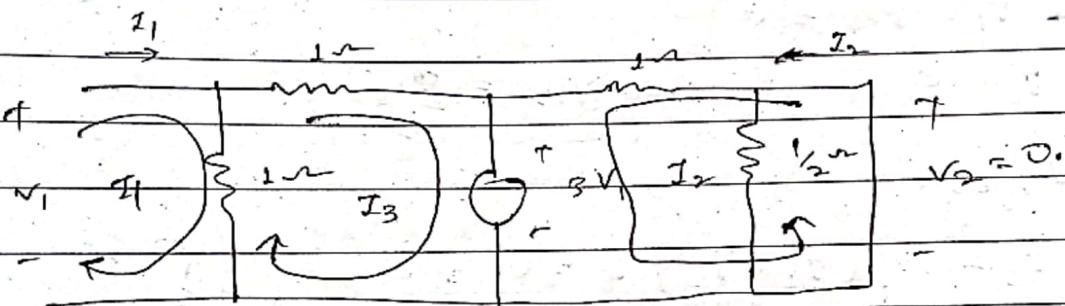
$$\begin{array}{r} 1352 + 598S \\ \hline 26(13+S) \end{array} + \begin{array}{r} 1352 + 598S \\ \hline 39S \end{array}$$

$$Y_{12} = Y_{21} = D = \frac{1352 + 598S}{39S}$$

Determine the admittance parameters of the given network.



Let $v_2 = 0$, i.e. short circuiting 2nd port.



In 1st mesh,

$$-(I_1 - I_3) + v_1 = 0$$

$$v_1 = I_1 + I_3 \quad \text{--- (1)} \quad \Rightarrow I_3 = I_1 - v_1$$

In 2nd mesh,

$$-I_3 - 3v_1 - (I_3 - I_1) = 0$$

$$3v_1 = -2I_3 + I_1 \quad \text{--- (2)}$$

$$3v_1 = -2(I_1 - v_1) + I_1$$

$$3v_1 = -2I_1 + 2v_1 + I_1$$

$$v_1 = -I_1$$

In 3rd mesh,

$$-I_2 - 3v_1 = 0$$

$$-I_2 = 3v_1$$

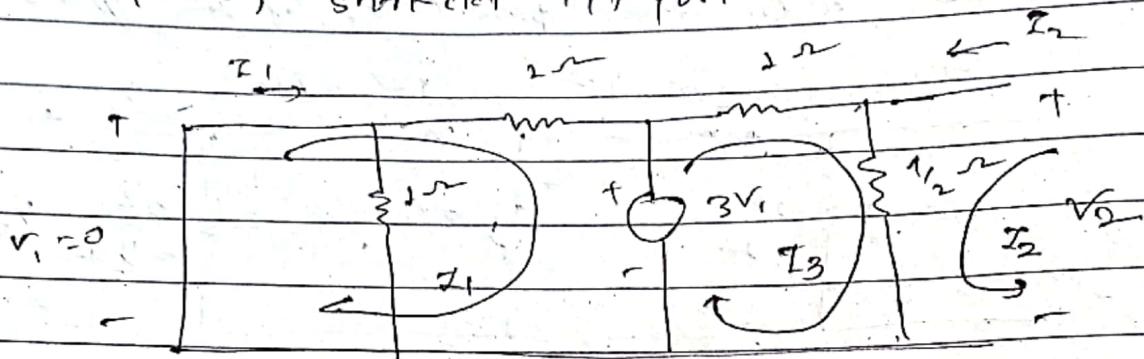
$$\frac{I_2}{v_1} = -3$$

$$\frac{I_1}{v_1} = -2$$

$$\Rightarrow Y_{11} = -1.25$$

$$\Rightarrow Y_{21} = -3.25$$

let $V_1 = 0$, short-circuit 11P port.



1st mesh,

$$-I_1 - 3V_1 = 0$$

$$I_1 = 0 \Rightarrow Y_{12} = \frac{\Phi_1}{V_2} = 0$$

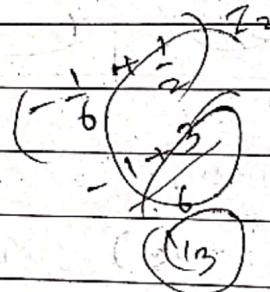
2nd mesh,

$$-I_3 - \frac{1}{2}(I_3 + I_2) + 3V_1 = 0$$

$$-I_3 - \frac{1}{2}I_3 - \frac{1}{2}I_2 = 0$$

$$-\frac{3}{2}I_3 - \frac{1}{2}I_2 = 0$$

$$3I_3 = -I_2$$



3rd mesh,

$$\frac{1}{2}(I_2 + I_3) - V_2 = 0$$

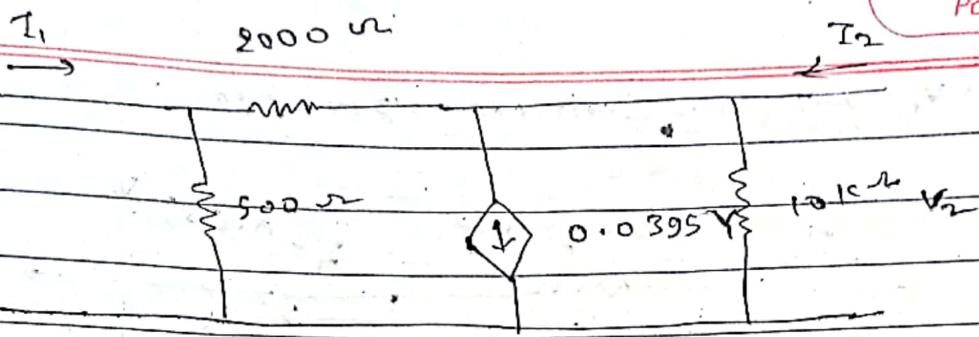
$$\frac{1}{2}I_2 + \frac{1}{2}I_3 + V_2 = 0$$

$$\frac{1}{2}I_2 - \frac{1}{2} \cdot \frac{I_2}{3} + V_2 = 0$$

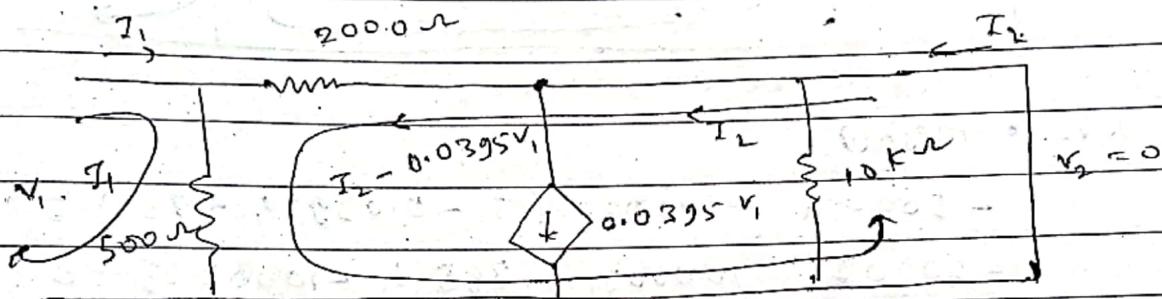
$$\frac{2I_2}{3} + V_2 = 0$$

$$+\frac{I_2}{3} = +V_2$$

$$\frac{I_2}{V_2} = +3 \Rightarrow Y_{22} = +3 \text{ S}$$



Let, $V_2 = 0$ i.e. short circuit of 1000Ω.



KVL @ mesh 1,

$$-500(I_1 + I_2 - 0.0395V_1) + V_1 = 0$$

$$-500I_1 - 500I_2 + 19.75V_1 + V_1 = 0$$

$$20.75V_1 = 500I_1 + 500I_2 \quad \text{--- (1)}$$

KVL @ mesh 2,

$$-2000(0.0395V_1) - 500(I_2 - 0.0395V_1 + I_1) = 0$$

$$-2000I_2 + 79V_1 - 500I_2 + 19.75V_1 - 500I_1 = 0$$

$$98.75V_1 = 500I_1 + 2500I_2 \quad \text{--- (2)}$$

From (1) & (2)

$$98.75V_1 = 20.75V_1 - 500I_2 + 2500I_2$$

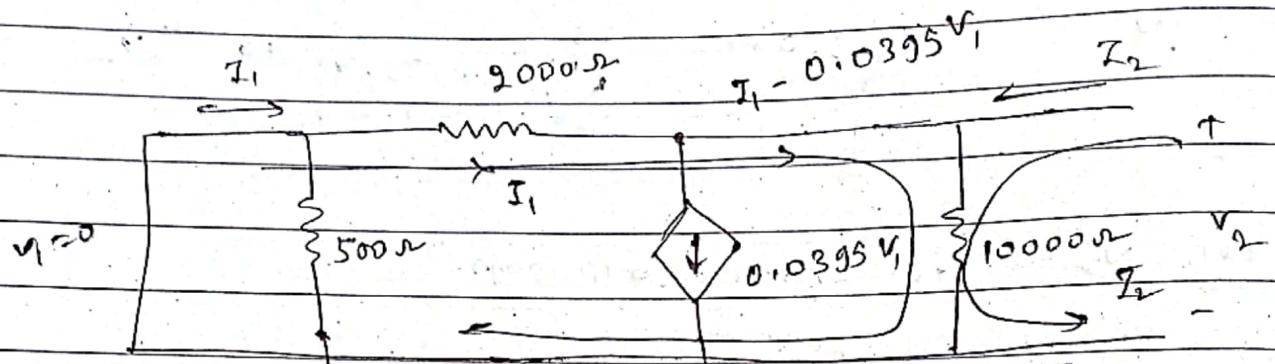
$$2000I_2 = 78V_1$$

$$\frac{I_2}{V_1} = Y_{21} = \frac{2000}{78} = 25.625$$

$$98.75V_1 = 500I_1 + 2500 \left| \frac{20.75V_1 - 500I_1}{500} \right| \quad Y_{11}$$

$$98.75V_1 = 500I_1 + 103.75V_1 - 2500I_1 \Rightarrow \frac{I_1}{V_1} = 0.002525$$

red. $v_1 = 0$ i.e. short circuit - i/p too poor.



KVL @ mesh ①

$$-2000 I_1 - 10000 (I_1 - 0.0395 V_1 + I_2) = 0$$

$$-2000 I_1 - 10000 I_1 + 395 V_1 - 10000 I_2 = 0$$

$$-12000 I_1 - 10000 I_2 + 395 V_1 = 0 \quad \text{--- (3)}$$

KVL @ mesh ②

$$-10000 (I_2 + I_1 - 0.0395 V_1) + V_2 = 0$$

$$-10000 I_2 - 10000 I_1 + 395 V_1 + V_2 = 0 \quad \text{--- (4)}$$

for (3) & (4)

$$-10000 I_2 - 10000 I_1 + 10000 I_2 + 12000 I_1 + V_2 = 0$$

$$2000 I_1 + V_2 = 0$$

$$\gamma_{12} = \frac{I_1}{V_2} = \frac{-1}{2000} = -0.0005 \text{ S}$$

$$-10000 I_2 - 10000 \left(-\frac{10000}{12000} I_2 \right) + V_2 = 0$$

$$-10000 I_2 + 100000 I_2 + V_2 = 0$$

$$90000 I_2 = -V_2$$

$$\gamma_{22} \Rightarrow \frac{I_2}{V_2} = \frac{-1}{90000} = -0.0000111 \text{ S}$$

Hybrid parameters or h-parameters:

$$v_1 = h_{11} I_1 + h_{12} v_2$$

$$I_2 = h_{21} I_1 + h_{22} v_2$$

$$\begin{bmatrix} v_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ v_2 \end{bmatrix}$$

↑
h-parameters

condition of reciprocity

$$h_{12} = h_{21}$$

$$\text{symmetry} \rightarrow h_{11} h_{22} - h_{12} h_{21} = 1.$$

Let, $v_2 = 0$ i.e. O/P short ckt

from eq ①

$$v_1 = h_{11} I_1 + h_{12} \times 0$$

$$\Rightarrow h_{11} = \frac{v_1}{I_1} \quad \text{eq ②}$$

from eq ② $I_2 = h_{21} I_1 + h_{22} \times 0$

$$\Rightarrow h_{21} = \frac{I_2}{I_1}$$

Again, let $I_1 = 0$ i.e. opening Z/P port.

for ①

$$v_1 = h_{11} \times 0 + h_{12} v_2$$

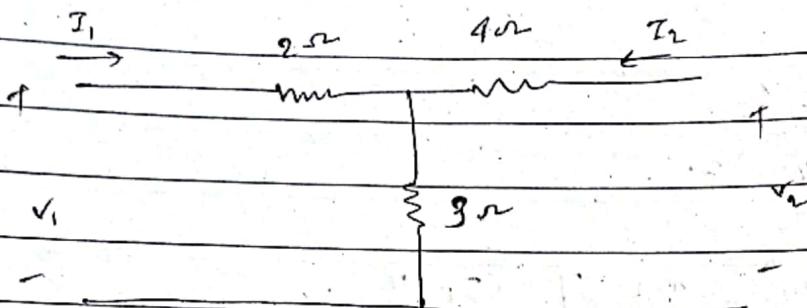
$$\Rightarrow h_{12} = \frac{v_1}{v_2}$$

for ②

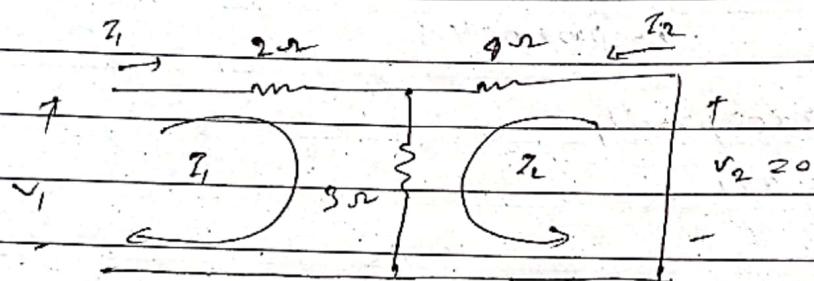
$$I_2 = h_{21} \times 0 + h_{22} v_2$$

$$\Rightarrow h_{22} = \frac{I_2}{v_2}$$

Find h-parameters,



Let $v_2 = 0$, i.e. short circuit output port.



1st mesh,

$$-2I_1 - 3(I_1 + I_2) + v_1 = 0$$

$$v_1 = 5I_1 + 3I_2 \quad \text{--- (1)}$$

2nd mesh,

$$-9I_2 - 3(I_2 + I_1) = 0$$

$$-7I_2 - 3I_1 = 0$$

$$-7I_2 = 3I_1 \quad \text{--- (2)}$$

from (1)

$$v_1 = 5I_1 + 3 \times -\frac{3}{7}I_1$$

$$= 5I_1 - \frac{9}{7}I_1$$

$$= \frac{26}{7}I_1 - 9I_1$$

from (2)

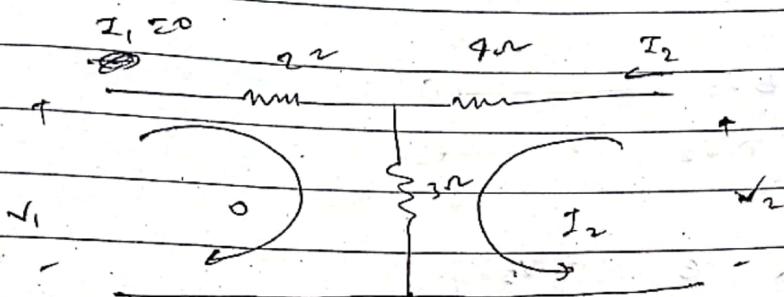
$$\frac{I_2}{I_1} = -\frac{3}{7}$$

h_{21}

$$= \frac{\frac{26}{7}I_1 - 9I_1}{I_1} = \frac{26}{7} - 9$$

$$h_{21} = \frac{-9}{I_1} = \frac{26}{7} \Omega.$$

Let, $I_2 = 0$ & open gap prob.



$$-9I_2 - 3(I_1 + I_2) + v_2 = 0 \quad (\text{meth 1})$$

$$-9I_2 - 3I_2 + v_2 = 0$$

$$v_2 = 4I_2$$

$$h_{22} = \frac{I_2}{v_2} = \frac{1}{7} \quad 25.$$

$$v_2 = 7I_2 \\ = \frac{1}{3} \cdot v_1$$

for meth ①

$$-3(0 + I_2) + v_1 = 0 \quad \Rightarrow h_{12} = \frac{v_1}{v_2} = \frac{3}{7}$$

$$-3I_2 + v_1 = 0$$

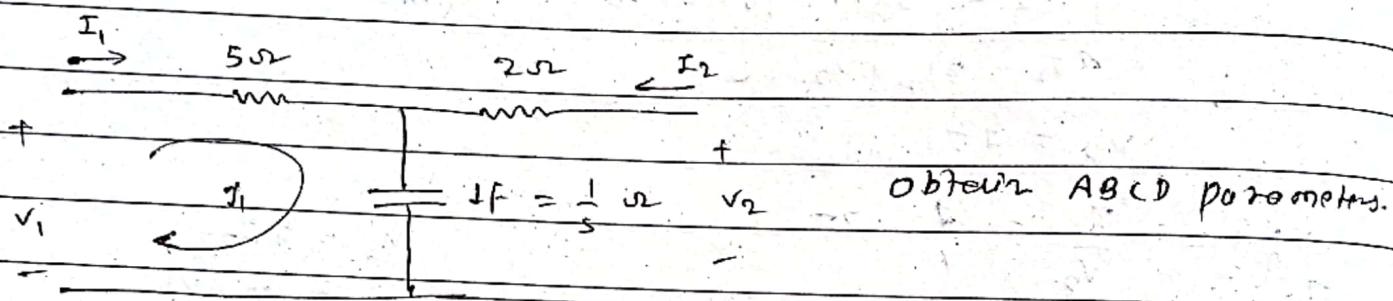
$$v_1 = 3I_2$$

ABCD (Transmission) parameters

$$v_1 = AV_2 - BI_2 \quad \text{--- (1)}$$

$$I_1 = CV_2 - DI_2 \quad \text{--- (2)}$$

$$\begin{bmatrix} v_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ -I_2 \end{bmatrix}$$



Let $I_2 = 0$ i.e. opening o/p port

In first mesh, I_2 vRL

$$-5I_1 - \frac{1}{s}(J_1 + I_2) + v_1 = 0$$

$$v_1 = 5I_1 + \frac{1}{s}J_1$$

$$v_1 = (5 + \frac{1}{s})I_1 \quad \text{--- (1)}$$

$$\text{Again, } v_2 = \frac{1}{s}I_1 \quad \text{--- (2)}$$

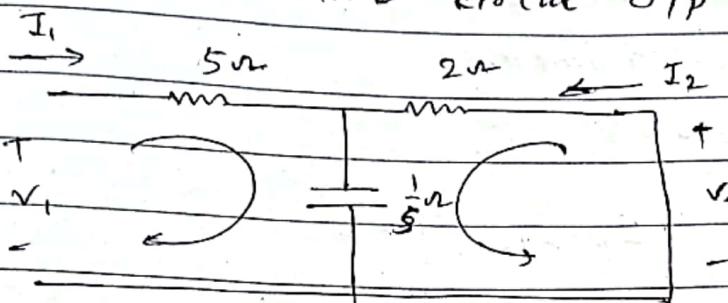
$$\Rightarrow C = \frac{I_1}{V_2} = s$$

$$\text{Also, } v_1 = (5 + \frac{1}{s}) \cdot v_2 s$$

$$= (5s + 1) \frac{v_2 s}{s}$$

$$\Rightarrow A = \frac{v_1}{v_2} = 5s + 1$$

Let $v_2 = 0$ i.e. short circuit o/p port



In first mesh, κv_2

$$-5I_1 - \frac{1}{s}(I_1 + I_2) + v_1 = 0$$

$$\begin{aligned} v_1 &= 5I_1 + \frac{1}{s}I_1 + \frac{1}{s}I_2 \\ &= \left(5 + \frac{1}{s}\right)I_1 + \frac{1}{s}I_2 \end{aligned} \quad \text{--- (3)}$$

In second mesh, κv_L

$$-2I_2 - \frac{1}{s}(I_1 + I_2) = 0$$

$$2I_2 + \frac{1}{s}I_1 + \frac{1}{s}I_2 = 0$$

$$\left(2 + \frac{1}{s}\right)I_2 = -\frac{1}{s}I_1$$

$$\Rightarrow D = -\frac{I_1}{I_2} = \left(2 + \frac{1}{s}\right)s = (2s+1)$$

Put $-I_1$ in (3) we get.

$$v_1 = \frac{5s+1}{s} \times -\frac{(2s+1)}{s} \times sI_2 + \frac{1}{s}I_2$$

$$= \frac{-(5s+1)(2s+1) + 1}{s} I_2$$

$$\Rightarrow B = -\frac{v_1}{I_2} = \frac{(5s+1)(2s+1) - 1}{s}$$

$$= \frac{10s^2 + 7s}{s}$$

$$= (10s + 7)$$

* Conversion of Parameters.

1. Z-parameters to Y-parameters

Z-parameters are known.

$$\begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix}^{-1}$$

$$= \frac{1}{\Delta Z} \begin{bmatrix} Z_{22} & -Z_{12} \\ -Z_{21} & Z_{11} \end{bmatrix}$$

$$\therefore Y_{11} = \frac{Z_{22}}{\Delta Z}, \quad Y_{12} = \frac{-Z_{12}}{\Delta Z}$$

$$Y_{21} = \frac{-Z_{21}}{\Delta Z}, \quad Y_{22} = \frac{Z_{11}}{\Delta Z}$$

$$\Delta Z = Z_{11}Z_{22} - Z_{12}Z_{21} \quad (\text{determinant of } Z\text{-parameters})$$

2. Y-parameters to Z-parameters

Y-parameters are known.

$$\begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix}^{-1} = \frac{1}{\Delta Y} \begin{bmatrix} Y_{22} & -Y_{12} \\ -Y_{21} & Y_{11} \end{bmatrix}$$

$$Z_{11} = \frac{Y_{22}}{\Delta Y}, \quad Z_{12} = \frac{-Y_{12}}{\Delta Y}$$

$$Z_{21} = \frac{-Y_{21}}{\Delta Y}, \quad Z_{22} = \frac{Y_{11}}{\Delta Y}$$

where,

$$\Delta Y = Y_{11}Y_{22} - Y_{12}Y_{21}$$

3. Z-parameters to ABCD (Transmission) parameters

Z-parameters

$$V_1 = Z_{11} I_1 + Z_{12} I_2 \quad \text{--- (1)}$$

$$V_2 = Z_{21} I_1 + Z_{22} I_2 \quad \text{--- (2)}$$

first and last

regarding (1) & (2)

not yet compare

so 1

ABCD - parameters.

$$V_1 = A V_2 - B I_2 \quad \text{--- (3)}$$

$$I_1 = C V_2 - D I_2 \quad \text{--- (4)}$$

from (2)

$$Z_{21} I_1 = V_2 - Z_{22} I_2$$

$$I_1 = \frac{V_2 - Z_{22} I_2}{Z_{21}} \quad \text{--- (5)}$$

put I_1 in (1)

$$V_1 = Z_{11} \left(\frac{V_2 - Z_{22} I_2}{Z_{21}} \right) + Z_{12} I_2$$

$$= \frac{Z_{11} V_2 - Z_{11} Z_{22} I_2 + Z_{12} I_2}{Z_{21}}$$

$$\frac{Z_{11} V_2}{Z_{21}} - \left(\frac{Z_{11} Z_{22} + Z_{12} Z_{21}}{Z_{21}} \right) I_2 \quad \text{--- (6)}$$

Comparing eq (3) & (6)

Comparing (5) & (4)

$$A = \frac{Z_{11}}{Z_{21}}$$

$$C = \frac{1}{Z_{21}}$$

$$B = \frac{Z_{11} Z_{22} - Z_{12} Z_{21}}{Z_{21}}$$

$$D = \frac{Z_{22}}{Z_{21}}$$

X. Z - parameters to h - parameters

Z - parameters,

$$V_1 = Z_{11} I_1 + Z_{12} I_2 \quad \text{--- (1)}$$

$$V_2 = Z_{21} I_1 + Z_{22} I_2 \quad \text{--- (2)}$$

h - parameters,

$$V_1 = h_{11} I_1 + h_{12} V_2 \quad \text{--- (3)}$$

$$I_2 = h_{21} I_1 + h_{22} V_2 \quad \text{--- (4)}$$

from (2)

$$I_2 Z_{22} = V_2 - Z_{21} I_1$$

$$I_2 = \frac{1}{Z_{22}} V_2 - \frac{Z_{21}}{Z_{22}} I_1 \quad \text{--- (5)}$$

from (1)

$$V_1 = Z_{11} I_1 + Z_{12} \left(\frac{1}{Z_{22}} V_2 - \frac{Z_{21}}{Z_{22}} I_1 \right)$$

$$= \left(Z_{11} - \frac{Z_{12} Z_{21}}{Z_{22}} \right) I_1 + \frac{Z_{12}}{Z_{22}} V_2$$

$$= \left(\frac{Z_{11} Z_{22} - Z_{12} Z_{21}}{Z_{22}} \right) I_1 + \frac{Z_{12}}{Z_{22}} V_2 \quad \text{--- (6)}$$

Comparing (3) & (6)

$$Z_{11} Z_{22} - Z_{12} Z_{21}$$

$$h_{11} = \frac{Z_{11} Z_{22} - Z_{12} Z_{21}}{Z_{22}}$$

Comparing (4) & (5)

$$h_{21} = -\frac{Z_{21}}{Z_{22}}$$

$$h_{12} = \frac{Z_{12}}{Z_{22}}$$

$$h_{22} = \frac{1}{Z_{22}}$$

* PU online exam.

If $Z_{11} = 30 \Omega$, $Z_{22} = 20 \Omega$, $Z_{12} = Z_{21} = 10 \Omega$. obtain transmission parameters.

Q.1

We have, transmission parameters A, B, C, D are

$$A = \frac{Z_{11}}{Z_{21}} = \frac{30}{10} = 3 \Omega$$

$$B = \frac{Z_{11}Z_{22} - Z_{12}Z_{21}}{Z_{21}} = \frac{30 \times 20 - 10 \times 10}{10} = 50 \Omega$$

$$C = \frac{1}{Z_{21}} = \frac{1}{10} \Omega$$

$$D = \frac{Z_{22}}{Z_{21}} = \frac{20}{10} = 2 \Omega$$

Interconnection of networks

When two or more networks are connected together to form bigger network, it is said that they are interconnected.

Types:

1. Cascade.

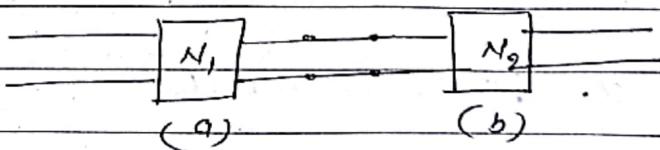
In cascade n networks, we find

$ABCD$ parameters of each

network and multiply each to

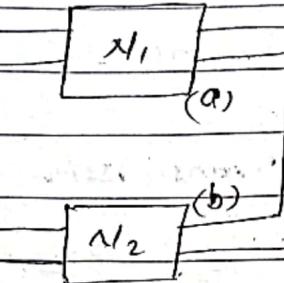
find total $ABCD$ parameters.

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix}_a \times \begin{bmatrix} A & B \\ C & D \end{bmatrix}_b$$



2. Series - Series.

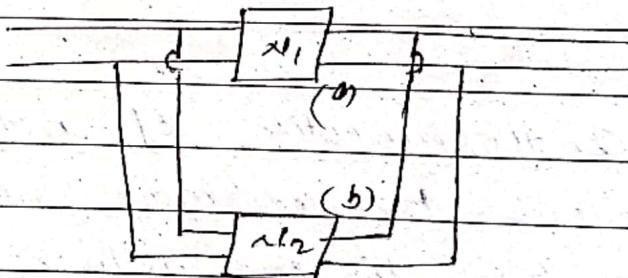
In series n_{10} , we find 2-parameters of each n_{10} and add each to find overall 2-parameters.



$$\begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix}_a + \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix}_b$$

3. Parallel - parallel

In this connection, we find y -parameters of whole circuit by adding y -parameters of each network.



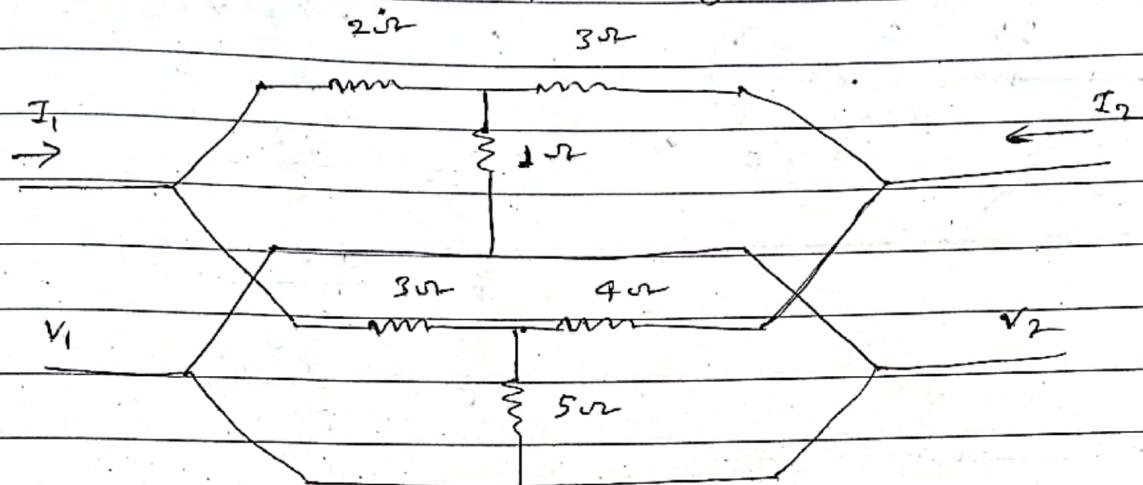
$$\begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix}_a + \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix}_b$$

4. Series - parallel.

$$\begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix}_a + \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix}_b$$

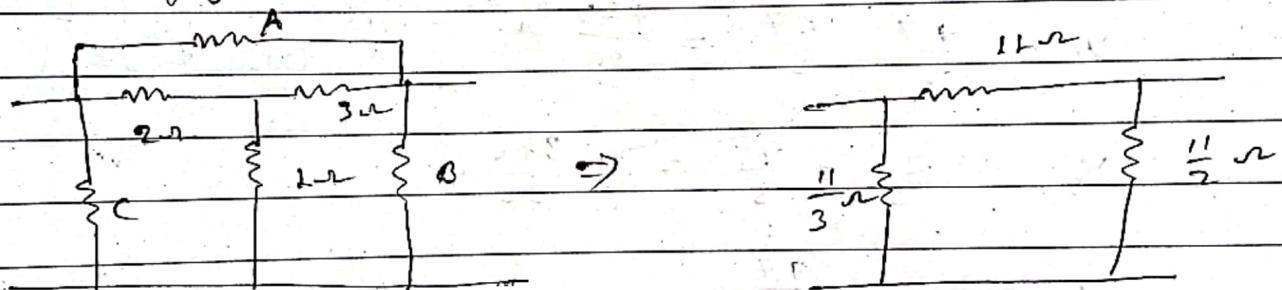


Q. Find y -parameters of the given network.



Here two nodes are connected in parallel connection so we get y -parameters.

consider first node.



$$A = \frac{2 \times 3 + 3 \times 1 + 1 \times 2}{1} = 12 \Omega$$

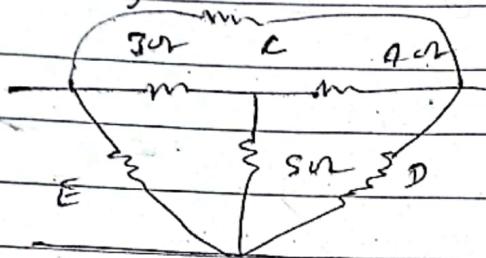
$$B = \frac{1}{2} \Omega \quad Y_{11} = \frac{11}{3} + 11 = \frac{44}{3} \Omega$$

$$C = \frac{1}{3} \Omega \quad Y_{22} = \frac{11}{2} + 11 = \frac{33}{2} \Omega$$

$$Y_{12} = Y_{21} = 11 \Omega$$

$$\therefore \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix}_q = \begin{bmatrix} 44/3 & 11 \\ 11 & 33/2 \end{bmatrix} \quad (1)$$

Considering second row.

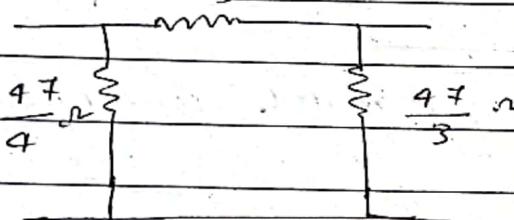


$$C = \frac{3 \times 4 + 4 \times 3 + 5 \times 3}{5}$$

$$= \frac{47}{5} \Omega$$

$$D = \frac{47}{3} \Omega$$

$$E = \frac{47}{4} \Omega$$



$$Y_1 = \frac{47}{4} + \frac{47}{5} = \frac{423}{20} \Omega$$

$$\begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix}_b = \begin{bmatrix} \frac{423}{20} & \frac{47}{5} \\ \frac{47}{5} & \frac{376}{20} \end{bmatrix}$$

$$Y_{22} = \frac{47}{3} + \frac{47}{5} = \frac{376}{20} \Omega$$

$$Y_{21} = Y_{12} = \frac{47}{5} \Omega$$

Hence, from ① & ②

$$\begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} = \begin{bmatrix} \frac{44}{3} & 11 \\ 11 & \frac{33}{2} \end{bmatrix} + \begin{bmatrix} \frac{423}{20} & \frac{47}{5} \\ \frac{47}{5} & \frac{376}{20} \end{bmatrix}$$

$$= \begin{bmatrix} \left(\frac{44}{3} + \frac{423}{20} \right) & \left(11 + \frac{47}{5} \right) \\ \left(11 + \frac{47}{5} \right) & \left(\frac{33}{2} + \frac{376}{20} \right) \end{bmatrix}$$

80