Classical Density Functional Theory for Thermopack - Radial distribution function at contact from fundamental measure theory.

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1 Introduction

From statistical mechanics the compressibility in a hard sphere system is known from the virial theorem,

$$\frac{\beta P}{\rho} = 1 + \frac{2\pi}{3} \rho \sigma^3 g^{c}(\sigma), \qquad (1)$$

where $g^{c}(\sigma)$ is the radial distribution function (RDF) at contact. For additive mixtures, the virial theorem extends to a double sum over the contributions form all pairs, ij,

$$\frac{\beta P}{\rho} = 1 + \frac{2\pi}{3} \rho \sum_{i} \sum_{j} x_{i} x_{j} \sigma_{ij}^{3} g^{c} \left(\sigma_{ij}\right), \tag{2}$$

where x_i is the mole fraction of component i [2, Eq. 5.14]. The excess pressure is then related to the RDF at contact through the algebraic relation,

$$\beta P_{\rm ex} = \frac{2\pi}{3} \sum_{i} \sum_{j} \rho_i \rho_j \sigma_{ij}^3 g^{\rm c} \left(\sigma_{ij} \right). \tag{3}$$

In a classical density functional theory (DFT) formulation, the Helmholtz free energy density can be calculated from fundamental measure theory (FMT). In FMT, the Helmholtz energy is a function of weighted densities, **n**, ie.

$$\Phi = \Phi(\mathbf{n}). \tag{4}$$

The weighted densities are given as convolution integrals,

$$n_{\alpha} = \int d\mathbf{r}' \rho(\mathbf{r}') w_{\alpha}(\mathbf{r} - \mathbf{r}') = \rho(\mathbf{r}) \otimes w_{\alpha}(\mathbf{r}), \qquad (5)$$

where w_{α} is the a weight function.

The excess pressure is given from,

$$\beta P_{\rm ex} = -\Phi + \sum_{i} \rho_i \frac{\partial \Phi}{\partial \rho_i}.$$
 (6)

Here,

$$\frac{\partial \Phi}{\partial \rho_i} = \sum_{\alpha} \frac{\partial \Phi}{\partial n_{\alpha}} \frac{\partial n_{\alpha}}{\partial \rho_i}.$$
 (7)

For mixtures, the RDF at contact are related to the Helmholtz energy [2, Eq. 5.29], [1] through the differentials,

$$g^{c}(\sigma_{ij}) = \frac{1}{2\pi (2 - \delta_{ij}) \rho_{i} \rho_{j} \sigma_{ij}^{2}} \frac{\partial \Phi}{\partial \sigma_{ij}}$$
(8)

The equation require the differential

$$\frac{\partial \Phi}{\partial \sigma_{ij}} = \sum_{\alpha} \frac{\partial \Phi}{\partial n_{\alpha}} \frac{\partial n_{\alpha}}{\partial \sigma_{ij}}.$$
(9)

The differential $\frac{\partial n_{\alpha}}{\partial \sigma_{ij}}$ requires integrals of the weight function differentials with respect to σ_{ij} and it is therefore not possible to derive a analytical relation for the RDF at contact. New weighted functions, similar to the weight functions used for the calculation of entropy are required to model the $g^{c}(\sigma_{ij})$.

The component densities, ρ_i , in Eq. 8 is in the FMT context can be either $n_{0,i}$ or simply the local density, $\rho_i(\mathbf{r})$. This must be investigated.

2 The PCP-SAFT hard-chain functional

The hard-chain functional used in PCP-SAFT [3] is,

$$\beta F^{\text{hc}}\left[\rho_{k}\right] = \sum_{i} \left(m_{i} - 1\right) \int \rho_{i}\left(\mathbf{r}\right) \left(\ln \rho_{i}\left(\mathbf{r}\right) - 1\right) d\mathbf{r}$$

$$-\sum_{i} \left(m_{i} - 1\right) \int \rho_{i}\left(\mathbf{r}\right) \left(\ln \left[y_{ii}^{\text{dd}}\left(\bar{\rho}_{k}^{\text{hc}}\left(\mathbf{r}\right)\right) \lambda_{i}\left(\mathbf{r}\right)\right] - 1\right) d\mathbf{r},$$
(10)

where λ_i is a weighted density based on a normalized weight function and $\bar{\rho}_k^{\text{hc}}$ are a dirac weighted density, both of width $2d_i$,

$$\bar{\rho}_k^{\text{hc}}(\mathbf{r}) = \frac{3}{4\pi d_i^3} \int \rho_i(\mathbf{r}_2) \Theta(d_i - |\mathbf{r}_2 - \mathbf{r}_1|) d\mathbf{r}_2$$
 (11)

$$\lambda_i(\mathbf{r}) = \frac{1}{4\pi d_i^2} \int \rho_i(\mathbf{r}_2) \,\delta(d_i - |\mathbf{r}_2 - \mathbf{r}_1|) \,d\mathbf{r}_2 \tag{12}$$

Show entropy profile using the above functional.....

3 The association hard chain term used for PCP-SAFT

The associative attraction functional require a description of the ij RDF at contact. To describe RDF at contact for heterogeneous systems, Sauer and Gross used the term proposed by Yu and Wu [4]:

$$g_{ij}^{c}(\{n_{\alpha}(\mathbf{r})\}) = \frac{1}{1 - n_{3}} + \frac{d_{ii}d_{jj}}{d_{ii} + d_{jj}} \frac{\xi n_{2}}{2(1 - n_{3})^{2}} + \left(\frac{d_{ii}d_{jj}}{d_{ii} + d_{jj}}\right)^{2} \frac{\xi^{2}n_{2}^{2}}{18(1 - n_{3})^{3}},$$
(13)

where $\xi = 1 - \vec{\mathbf{n}}_2 \cdot \vec{\mathbf{n}}_2 / n_2^2$.

4 Test

Use equation Eq. 8 to test:

- Is $g_{ij} = g_{ji}$?
- Resulting g_{ij} compared to the model version of both PCP-SAFT [3] and Yu and Wu [4].
- Effect on entropy

References

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