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Automated Weld Path Generation Using Random Sample Consensus and Iterative Closest Point Workpiece Localization

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ABSTRACT

Jobs performed by small to medium enterprises (SMEs) are infrequently automated due to high setup costs and lack of technical expertise needed for robot training, however productivity and worker safety can be improved in SMEs with the use automated tooling. In a traditional automated manufacturing environment, tasks such a welding or painting are accomplished through execution of pre-programmed tool motions which rely on the location and orientation of the workpiece to be fixed and known. The lack of this spatial information is typically treated through positioning of the workpiece with respect to the robot arm using jigs or fixtures which are costly in initial setup and not easily modified. Further, the resulting toolpath associated with a desired task is typically defined through manual teaching resulting in a path appropriate for an individual job. For this reason, SMEs requiring variation in part geometry or arrangement are not commonly automated. This work presents a method for automated weld path generation for a 6DOF co-bot arm using random sample consensus (RANSAC) and iterative closest point (ICP) workpiece localization from LiDAR point clouds. Scans from a low cost 2D LiDAR mounted to the co-bot arm are used to generate 3D point clouds of the workspace scene with the Robot Operating System (ROS). The Point Cloud Library (PCL) is used to compare the generated point cloud with a CAD model to produce a rigid transformation to localize the workpiece. The estimated pose of the workpiece with respect to a fixed frame is used offline to generate a weld path as series of tool poses. An example welding processes in which two square tubes are joined through weldment are investigated and a physical implementation of the method is demonstrated using a 2D LiDAR mounted to a 6DOF co-bot arm.

Keywords: robotics, automation, welding, ROS, PCL

1. INTRODUCTION

Small to medium enterprises perform manufacturing tasks associated with relatively low part volume and increased variation in assembly geometry as compared to jobs performed in large scale manufacturing environments. This type of manufacturing operation is infrequently automated due to high setup costs. However, productivity and worker safety can be improved in small to medium enterprises with automation such as robotic tooling.

In a traditional automated manufacturing environment, a task such a welding or painting is accomplished through the execution of pre-programmed tool motions which rely on the location and orientation of the workpiece to be fixed and known with respect to a global coordinate system. The need for spatial information is typically treated through positioning of the workpiece with respect to the robot arm using jigs or fixtures which are costly in initial setup and are not easily modified. In large scale production environments, this can be accomplished with dedicated infrastructure built into the environment such as moving jigs on assembly lines and other features available in a highly structured environment. Further, the resulting toolpath associated with a desired task is typically defined through manual teaching resulting in a path appropriate for an individual job. For this reason, operations performed by SMEs requiring lower volume manufacturing with variation in part geometry or arrangement are not commonly automated.

A method is presented in this paper is for automated weld path generation with a 6DOF co-bot arm using random sample consensus (RANSAC) and iterative closest point (ICP) workpiece localization implemented using the Robot Operating System (ROS) and the Point Cloud Library (PCL). In the process, the welding robot will perform a lidar scan of the workpiece located within the robot workspace and represent this data in a point cloud format. Then, using a solid model of the workpiece, an algorithm combining filters and ICP is performed to provide a homogenous transformation that describes the

position and orientation of the workpiece in a coordinate frame attached to the point cloud data. This homogenous transformation is then used to map a desired weld tool path described also in the solid – model format. This leads to a method to automatically generate weld paths from sensor information. This method builds on the current techniques, for example those demonstrated in Kuss, Schneider and Keith [29] and Gao et al [33] in the following manner. The existing works assume a relatively clean match between the workpiece model and the scanned space of the robot. However, in manufacturing practice, the workpiece is cluttered with other objects such as clamps, jigs or fixtures. Further, it may not be practical to include these objects with the workpiece in the solid model representation. This paper will suggest and demonstrate a range of strategies to remove from the scan data set, information that is not part of the actual workpiece to yield better accuracy in the homogenous transformation. The method is demonstrated on two examples.

a. Literature Review

Automated path planning for welding robots has been studied for decades [36] and is an area of increasing interest as the use [9] and availability of robotics and sensing technology increases. Seam tracking is a pre-dominate [31],[35],[36],[37] approach to the automation of welding. A vision system or other non-contact sensor detects and measures the location of seam to be welded, and this spatial information provides feedback for a control strategy to guide the tool through the required process. The detection and tracking of weld seams have been demonstrated through use of optical cameras with structured light [24],[35], stereo vision [23], and 3D LiDAR [33]. Shah et al provide a review of vision-based examples of weld seam identification, detection, and tracking [31].

Automation of the welding process has been shown using various feature detection techniques which inform the controller of spatial information of the weld seam without exposing the full pose of the workpiece with respect to the robot. In practice, the starting weld point (SWP) must be known for a weld to be successfully completed through seam tracking or other automatic controller. Autonomous determination of the start welding position (SWP) has been presented by Chen [32]. This is also shown in [38].

Alternatively, the problem can be framed as a search for the location and orientation of the workpiece in a global sense. This information can be compared to a model to localize the weld seam with respect to the workpiece and robot. At a minimum, this requires the location of three points of the workpiece to be known [24],[28],[29] and an accurate three-dimensional model of the working environment and workpiece must be available. A process of extracting the geometry of a weld seam on flat parts lying on a 2D surface from stereo vision imagery is shown in [23]. Similarly, the discovery and localization of workpieces to be joined by welding from 3D point cloud data is described by Rajaraman, et al. [28]. This paper will follow a similar process from pose sensing to path planning.

Gao et al present a method for extraction of seam geometry in D-type weld based on point clouds [33]. This work presents a similar approach to weld seam localization through processing of point cloud data.

Schleth, Kuss, and Kraus provide an overview of the available literature related to workpiece registration in robot manufacturing processes [20]. Kuss et al. present the problem of workpiece localization and detection of part alignment and shape variation in preparation for a manufacturing application such as welding or deburring. [20],[21],[22]. Part alignment and its effect on the welding model used for automated process planning is investigated in [29].

The work presented in the current paper follows [29],[33] in the sense that the iterative closest point method is used to determine the rigid transformation representing the workpiece in a welding operation to be completed by a 6DOF robotic arm designed for automated manufacturing processes. The Pass-Through filter and Voxel down sampling used by Gao [33] is similar to the prefiltering routine used in this paper with the addition of the statistical filter to remove outliers in the point clouds. This paper will present examples of weld operations incorporating fillet-type welds on non-flat bodies.

The strategy presented in this work differs from that of Kuss et al in that the localization process is performed using global images of the entire scanned area including the table and clamps instead of isolated scans of the workpiece itself. A strategy for outlier detection and removal with RANSAC segmentation is implemented prior to image registration which improves the performance of the process.

A process combining multiple algorithms is used to locate, or register, a point cloud representing the workpiece in a point cloud of the working environment collected by a LiDAR scanner located on the robot. Once the known part is located with respect to a fixed frame, an automated weld path generation routine is used to plan a weld toolpath offline. Two example welding applications are presented. In the first, a square tube is joined to a flat plate through weldment. In the second, two square tubes are joined orthogonally to each other to form a tee. Simulations of both applications are investigated, and a physical implementation of the method is demonstrated using a 2D LiDAR mounted to a 6DOF co-bot carrying a MIG welding torch which can be seen below in Figure 1.

The primary algorithms used in the approach presented are well known and accepted [2],[12],[6]. Random sample consensus (RANSAC) and iterative closest point (ICP) have been thoroughly tested and documented. However, the iterative closet point method is limited by local minima convergence issues associated with poor initial search conditions [4],[7]. Although there are many improvements and variations available, this paper will use classical point-to-point ICP as available with PCL [5],[6],[16]. The known issues associated with point cloud outliers and poor initial conditions are addressed in this paper by pre filtering and segmentation of the input point clouds prior to the use of ICP.

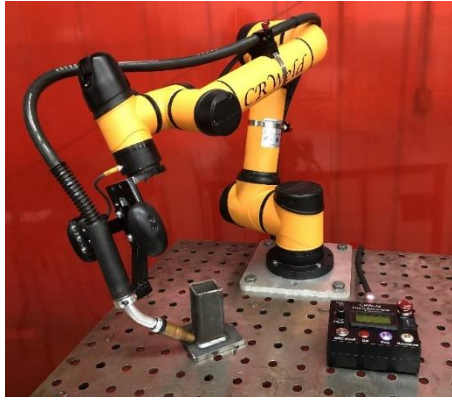


FIGURE 1: CO-BOT WITH TORCH

2. OVERVIEW OF APPROACH

The proposed approach to automated weld path generation shown in figure 2 consists of a model preparation stage, a workspace sensing stage, a workpiece localization stage, followed by an offline robot path generation stage. The resulting path can be used to automate a welding process on the component in the workspace with a 6-DOF co-bot carrying a welding torch.

a. Model Preparation Stage

In the model preparation stage, the geometry of the workspace and the workpiece is defined based on the prescribed application. An ideal model of the workpiece is generated using CAD. Part models are first generated of the individual workpiece components which are then assembled to represent the workpiece. The CAD assembly representing the workpiece is converted into a point cloud through a uniform sampling technique to be used for workpiece registration. The point cloud associated with the CAD model is known as the source point cloud.

A simplified model of the workspace and environment including the welding table and the robot base is also created for simulation purposes. This environment model is also converted into a point cloud file. The 3D models are generated using standard CAD software from which they can be exported as .ply files or other standard file formats.

b. Workspace Sensing Stage

Prior to the sensing stage, the workpiece is placed in the robot workspace by the operator in the proper relative orientation to be joined by a weldment. The relative orientation of the parts must match that of the model to an extent and the global location of the workpieces is restricted to the usable workspace of the robot. In the sensing stage a sweeping motion of the arm is performed, and the workpiece and environment are scanned with the 2D LiDAR mounted on link 5 of the robot. Multiple 2D lidar scans are measured along with corresponding sensor poses. As the scanning stage continues, the data are transformed from the sensor frame link 5 to the base frame link 0 through the known robot kinematics and accumulated into a 3D point cloud with respect to the base frame. This process produces sparse data sets with redundant points. Therefore, the scans are filtered and downsampled using a voxel grid to improve results and reduce

the resource requirements of storage and processing. The resulting point cloud contains an image of the workpiece and fixtures as well as the top of the welding table and the background. The point cloud associated with the LiDAR scan is known as the reference or target cloud. The sensing stage along with the methods of filtering and downsampling can be seen below in figure 3.

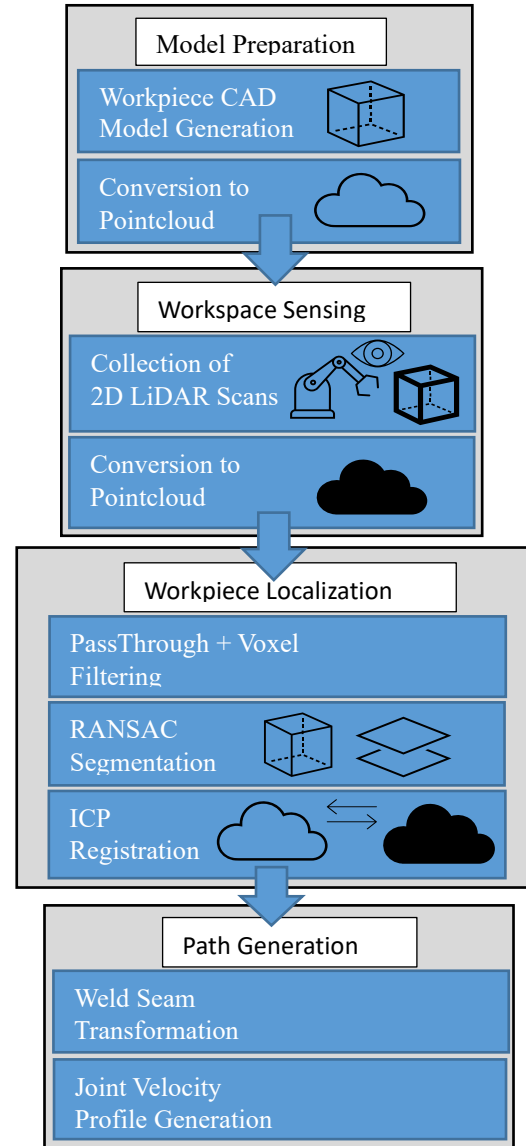


FIGURE 2: - AUTOMATED WELD PATH GENERATION

c. Workspace Localization Stage

In the workpiece localization stage, the source point cloud derived from the CAD model is compared to the reduced reference cloud acquired from lidar in the sensing stage. The relative transformation between clouds is found using the iterative closest point algorithm (ICP). The pose of the workpiece can be used to determine the required location of the weld seam in a global sense.

The reference cloud, collected from LiDAR, contains a larger volume of points, but not necessarily more points, than the source cloud. Also, the percentage of the workpiece represented in the LiDAR cloud depends on the sweeping motion used in the scanning stage and the amount of interference caused by the clamps or other obstructions. In the best-case scenario, approximately half of the points associated with the external faces of the workpiece are available in the LiDAR cloud.

The LiDAR cloud is first reduced to the usable workspace of the robot using a 3D bounding box or PassThrough filter [33] which removes points from the surrounding walls and extents of the table. Next, the point cloud is downsampled with a voxel filter [15] to ensure uniform density of points in the reference point cloud and reduce computational requirements of the localization algorithms. The remaining image contains points from the workpiece, the clamps holding the workpiece, and the table. The robot arm may also be included in the remaining point cloud. At this point, RANSAC based segmentation is used to compare geometrical information such as the planar nature of the table or the orthogonality of the workpiece to the LiDAR cloud to separate, or segment, the points associated with the workpiece. The results of a cascaded RANSAC segmentation are stored as the reference point cloud. Finally, the rigid transformation between the reference and source point cloud is found with the iterative closest point (ICP) cloud registration algorithm. This transformation matrix represents the location and orientation of the workpiece with respect to a fixed origin attached to the base link.

d. Path Generation Stage

The weld seam is defined by the geometry of the workpiece and the desired weld. In the examples provided the seam is described as a collection of linear segments with defined torch angles. The required tool path which lies along the weld seam is transformed into global coordinates using the transformation resulting from the workpiece localization stage.

3. Automated Weld Path Generation Approach

a. Model Preparation Stage

The source point cloud generated from CAD is defined as $S_1 = \{s_1, s_2, \dots, s_n\}$, with $s_i = (x_i, y_i, z_i)$ a triplet of a specific point in the cloud with respect to an origin of the CAD model for a total of n data points resulting from the conversion from CAD.

b. Workspace Sensing

The reference point cloud generated from a LiDAR scan is defined as $R_1 = \{r_1, r_2, \dots, r_m\}$ with $r_i = (x_i, y_i, z_i)$ a triplet of a specific point in the cloud with respect to a global origin fixed to the base of the robot for a total of m data points in the original 3D scan.

c. Workpiece Localization

i. Filtering with PassThrough and Voxel

Due to the nature of the LiDAR scanner, the reference cloud typically contains a large number of points not belonging to the workpiece. A PassThrough filter [33],[5] removes points outside of prescribed limits which is used to eliminate data outside of the expected location of the workpiece. This reduces the computational requirements of the algorithms used in the following workpiece localization process by reducing the number of elements in the point clouds.

The point cloud R is restricted to the defined coordinate bounds $X_{min}, X_{max}, Y_{min}, Y_{max}, Z_{min}$, and Z_{max} subset of the reference cloud which is contained inside the prescribed bounds. The results of the PassThrough filter may still contain a large number of redundant points, and voxel grid downsampling is used to reduce the number of points in the reference and source clouds. The process is described in detail in [33],[39] and is shown below for convenience.

The coordinate system is divided into a uniform three-dimensional grid of cells referred to as voxels. The input cloud points are sorted into the grid by location, and then the centroid of the points in each voxel is added to the filtered point cloud [15]. This reduces redundant data points and allows for the resolution to be set using the voxel grid size as a parameter. The maximum and minimum values in all three coordinates of the input cloud $x_{min}, x_{max}, y_{min}, y_{max}, z_{min}$, and z_{max} are found. The cloud length l_x , width l_y , and height l_z based on the maximum and minimum values can be calculated.

$$l_x = x_{max} - x_{min} \quad (1)$$

$$l_y = y_{max} - y_{min} \quad (2)$$

$$l_z = z_{max} - z_{min} \quad (3)$$

Then, define the voxel grid unit side length $cell$, and calculate M , N , and L as the number of cells in each coordinate of the $M \times N \times L$ grid. The total number of cells is given as the sum of the three dimensions. The number of points m in the reference cloud is updated.

$$m = M * N * L \quad (4)$$

$$M = \left\lceil \frac{l_x}{cell} \right\rceil, N = \left\lceil \frac{l_y}{cell} \right\rceil, L = \left\lceil \frac{l_z}{cell} \right\rceil \quad (5)$$

Next, sort each cloud point into the appropriate voxel.

$$i = \frac{(x_i - x_{min})}{cell}, j = \frac{(y_i - y_{min})}{cell}, k = \frac{(z_i - z_{min})}{cell} \quad (6)$$

Finally, replace the cloud points in each voxel with the center of gravity of the voxel c_{ijk} from m points p_i which results a reduced reference cloud R_2 .

$$c_{ijk} = \frac{1}{m} \sum_{i=1}^m p_i \quad (7)$$

The filtering process is primarily for removing data from the reference cloud R_1 that does not represent the workpiece. Voxel grid downsampling is also useful for preparing the source cloud S_1 exported from the CAD model. This allows for the resolution of the model data to be defined programmatically to reduce computational requirements. The voxel grid downsampling process described for the reference cloud is repeated for the source cloud S_1 resulting in a reduced cloud S_2 .

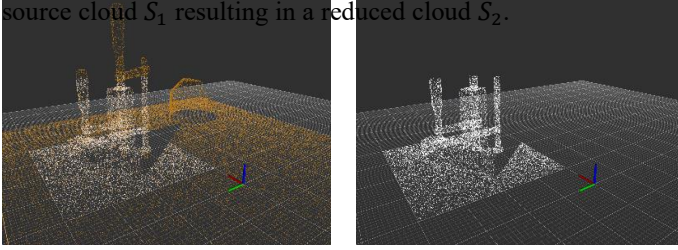


FIGURE 3: BOUNDING BOX

ii. Segmentation with RANSAC

The filtered reference cloud R_2 now mostly contains points representing the workpiece. A portion of the table and the clamps used to hold the workpiece exist in bounding box therefore remain in the reference cloud R_2 . In the examples shown in this paper, a planar model is used with RANSAC multiple time to capture the faces of the workpiece and the inliers of this segmentation are kept as the filtered reference cloud R_3 which is subset of R_2 containing mostly points representing the planar faces of the workpiece with few outliers. The number of points in the source cloud n is updated.

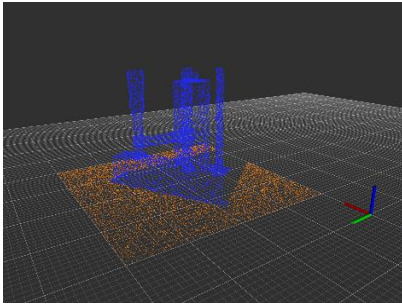


FIGURE 4A: INPUT CLOUD WORKPIECE TABLE AND CLAMPS

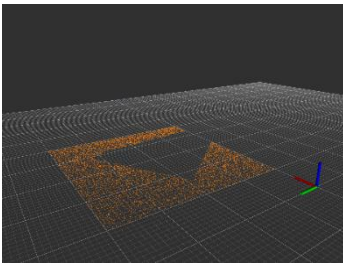


FIGURE 4B: PLANE INLIERS:

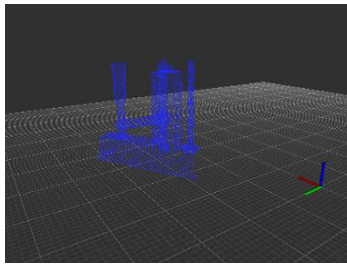


FIGURE 4C: PLANE OUTLIERS WORKPIECE AND CLAMPS

FIGURE 4: SEGMENTATION TO REMOVE TABLE

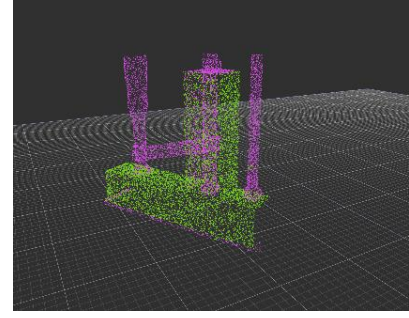


FIGURE 5A: INPUT CLOUD WORKPIECE AND CLAMPS

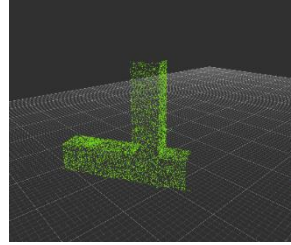


FIGURE 5B: PLANE INLIERS - WORKPIECE

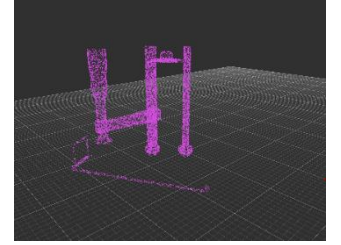


FIGURE 5C: PLANE OUTLIERS - CLAMPS

FIGURE 5: SEGMENTATION TO REMOVE CLAMPS

iii. Iterative Closest Point Registration

The ICP method as described in [12], [4] is summarized here. As defined above, a source and reference point cloud are available after filtering as S_2 and R_3 . The mean square objective function using the point-to-point error metric (or point-to-plane [4][6]) to be minimized is,

$$E(R, t) = \frac{1}{n} \sum_{i=1}^n \|r_i - R s_i - t\|^2 \quad (8)$$

where $R \in \mathbb{R}^{3 \times 3}$ is an $so(3)$ array that projects S onto R_p and $t \in \mathbb{R}^3$ that translates S_2 onto R_3 . If the correct correspondences are known, the correct relative rotation/translation can be calculated in closed form. A closed form implementation that can be found in the PCL library [16] is briefly described. The center of mass μ_{R_3}, μ_{S_2} for the reference point cloud set and source point cloud set respectively is calculated for each set as,

$$\mu_{R_3} = \frac{1}{m} \sum_{i=1}^m r_i, \quad \mu_{S_2} = \frac{1}{n} \sum_{i=1}^n s_i \quad (9)$$

The reference point cloud set and source point cloud set are shifted by their center mass such that they are distributed around zero as,

$$R_3' = \{r_i - \mu_r\} = \{r_i'\} \quad (10)$$

$$S_3' = \{s_i - \mu_s\} = \{s_i'\} \quad (11)$$

A cross-covariance matrix, $W \in \mathbb{R}^{3 \times 3}$ is defined as

$$W = \sum_{i=1}^m r'_i s'^T_i \quad (12)$$

A singular value decomposition (SVD) of W is given as

$$W = UDV^T \quad (13)$$

where D is a diagonal matrix containing the singular values, $\sigma_i, i = 1:3$, ordered such that $\sigma_1 \geq \sigma_2 \geq \sigma_3$ and $U \in R^{3 \times 3}$, $V \in R^{3 \times 3}$ are the left and right singular vectors of W . When the $rank(W) = 3$, the rotation R and translation t minimizing $E(R, t)$ are unique and given by:

$$R = UV^T \quad (14)$$

$$t = \mu_r - R\mu_s \quad (15)$$

The correspondence between points assumed in equation (1) is unknown at the start. Therefore, this process is performed iteratively [4]. Correspondence between the reference and source point cloud set is based on a minimum distance between points. The source is updated with the resulting transformation, and the process repeats until convergence of the source and reference point cloud set occurs as given in the error $E(R, t)$.

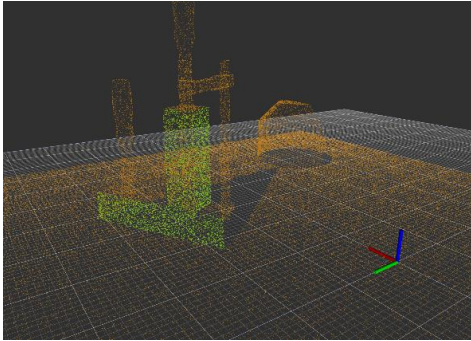


FIGURE 6A: SOURCE AND REFERENCE CLOUDS

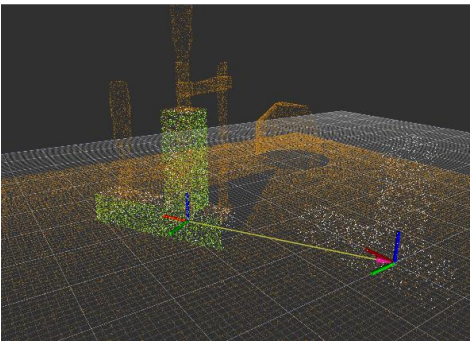


FIGURE 6B: RESULTING TRANSFORMATION

FIGURE 6: WORKPIECE REGISTRATION WITH ICP

d. PATH GENERATION

The weld path is constructed from the information encoded in a solid model or similar representation of the manufactured part. This work will consider that the welds required for manufacturing are a collection of linear segments with defined work and travel angles for the torch, where the work angle is an angle measured about the weld seam from a reference plane and the travel angle is a rotation about an axis perpendicular to the weld seam and the torch axis. Finally, the torch can be rotated about the torch axis without affecting the weld so this angle (torch angle) can be freely chosen. The pose of the torch at any point will be contained in the pair of triplets (P_i, O_i) where P_i contains the x, y, z positions of the torch tip and O_i contains the three angles, work angle, travel angle and torch angle following a defined rotation operation (see the section, defining torch orientation). Thus, the weld path is defined as a set of points and orientations:

$$WP = [P_1, P_2, \dots, P_l], WO = [O_1, O_2, \dots, O_l] \quad (16)$$

with WP the set of weld points, WO the set of weld orientations for a total of l defining the weld path. The weld path is series spline of linear segments connecting all points and orientations contained in the sets, WP and WO (see Figure 7 Sample Manufactured part). The weld path then consists of intersecting line segments, $\overline{P_i P_{i+1}}$ for all weld paths $i=1 \dots l$ with orientations $O_{i,i+1}$ defined over each weld path between P_i and P_{i+1} . The trajectory is defined as a Linear segment with appropriate blends for the full robot pose. Parabolic blends are used in this work, but could be replaced with a blend that would limit the magnitude of higher derivatives of joint motion. The weld specifications defines the travel speed along each line segment, and finally a nominal blend time for the end of the paths is selected as 2.5% of the total path time. The LSPB applied to each segment yields a function $q: [t_i, t_f] \rightarrow C$ with q the function yielding robot configuration C at any time over the interval t_i, t_f the initial and final times determined from the linear segment speed and blend percentage, time. Note that required torch orientations are not continuous at the line intersection. In practice, one way of handling this discontinuity is by inserting an additional path segments between line segments $\overline{P_i P_{i+1}}$ and $\overline{P_{i+1} P_{i+2}}$, with end points $P_{i+1} - \epsilon_i, P_{i+1} + \epsilon_{i+2}$, with $\epsilon_i, \epsilon_{i+2}$, a small displacement along the along the weld seam toward point i or $i+2$ and orientations at the endpoints, $O_{i,i+1}, O_{i+1,i+2}$.

In order to complete the path generation, the key weld path information extracted from the solid model representation of the part is mapped to the reference frame using the transformation resulting from workpiece localization. The original weld path is derived from the key points and orientations in the manufactured part solid model: (P_i, O_i) . The points are updated through multiplication with the transformation from ICP t . The

orientations are updated from updates to the workpiece frame, $\{x_{wp}, y_{wp}, z_{wp}\}$.

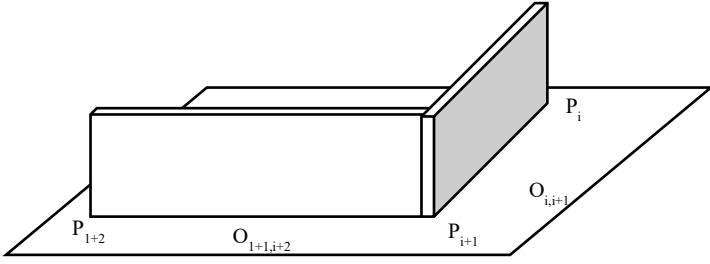


FIGURE 7: SAMPLE MANUFACTURED PART

Defining the torch orientation: The fixed reference frame is $\{x_0, y_0, z_0\}$ while the workpiece frame is $\{x_{wp}, y_{wp}, z_{wp}\}$ where z_{wp} lies along the weld seam and x_{wp} lies in the reference plane of the workpiece and is orthogonal to z_{wp} (see Figure 9). Note that the weld seams are assumed linear and defined by end point pairs, $\overline{P_i P_{i+1}}$. The rotation operator projecting the workpiece frame onto the fixed frame is

$$R_{wp}^0 = [\hat{r}_{wp,x}^0, \hat{r}_{wp,y}^0, \hat{r}_{wp,z}^0] \quad (17)$$

with $\hat{r}_{wp,x}^0$ a unit vector defined by the projection of x_{wp} onto frame $\{0\}$, $\hat{r}_{wp,z}^0$ a unit vector defined by the projection of z_{wp} onto frame $\{0\}$ and $\hat{r}_{wp,y}^0$ completes the SO(3) operator. The torch frame orientation is aligned to the workpiece according to the so-called travel angle and work angle (and if desired the torch angle) which are called out in the weld specifications. The rotation operator projecting the torch frame $\{x_T, y_T, z_T\}$ onto the workpiece frame is $\{x_{wp}, y_{wp}, z_{wp}\}$ consists of the three rotations, work angle (θ_w) about z_{wp} , travel angle (θ_T) about the new y axis and torch roll angle, (θ_R) about the new x axis. The rotation operator projecting the torch frame onto the fixed frame is,

$$R_T^0 = R_{WP}^0 R_T^{WP} \quad (18)$$

$$R_T^{WP} = R_{z,\theta_w} * R_{y,\theta_T} * R_{x,\theta_R} \quad (19)$$

The orientation of the torch with respect to the fixed frame at position i will be represented as the triplet, $0_i = \{\theta_{w_i}, \theta_{T_i}, \theta_{R_i}\}$ using the definitions provide above.

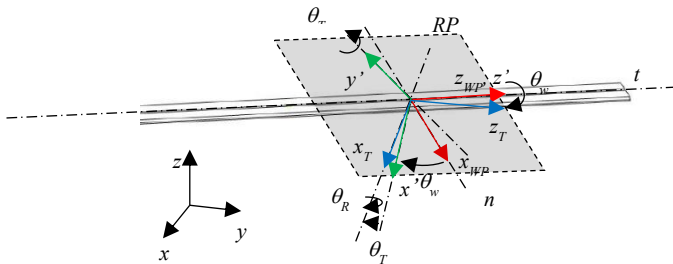


FIGURE 8: PATH PLANNING FRAMES

4. IMPLEMENTATION USING ROS AND PCL

This research has been implemented in ROS on Ubuntu Linux which provides a multi-threaded and distributed software framework for robotics applications. The combination of 2D LiDAR scans into 3D point clouds was done using a custom ROS package *scan2cloud* that is based on *ROS laser_geometry*. The rigid transformation from the sensor frame to the base of the robot is programmed with *ROS tf* so that individual 2D scans collected using *ROS rplidar* can be processed and saved as a .pcd file with respect to a global origin. The robot and sensor are operated simultaneously using ROS, and the resulting point cloud is saved as a .pcd file which can be processed using the Point Cloud Library or converted to a .ply polygon file.

5. MANUFACTURING APPLICATION

A manufacturing task is considered, in which a weldment is performed on a workpiece resting on a welding table. The workpiece in this task consists of multiple components to be joined through weldment. The relative alignment of the multiple components of the workpiece is assumed to be correct within the physical constraints of the designed part prior to the automated process. In practice, this alignment is set by the operator and secured using clamps or other fixtures.

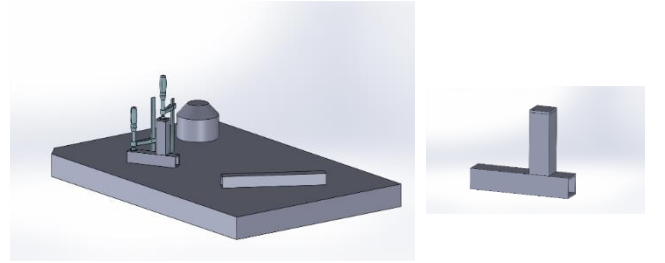


FIGURE 9: SIMULATED EXAMPLE APPLICATION

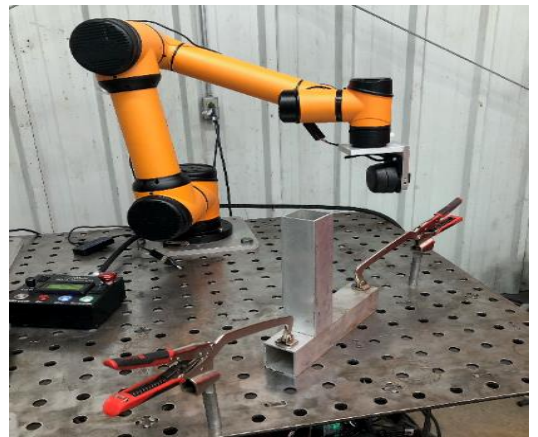


FIGURE 10: EXPERIMENTAL EXAMPLE APPLICATION

An example application is considered in which, two square tubes are joined perpendicular to one another with a fillet weld along two of the shared edges to be joined by weldment so that the tubes are perpendicular and form a tee. In this example, the assembly is temporarily joined together by clamps which will be included in the lidar scan. Prior to the alignment process, these clamps will be removed from the point cloud data via segmentation with RANSAC.

6. SIMULATION RESULTS

Example application A and B were performed for testing and validation of the proposed approach using synthetic data generated from CAD models of the workspace including the table and clamps as shown in the figure above. The models of the scene were converted to point clouds using the uniform sampling process described for the conversion of the source cloud. The localization process was performed, and the resulting position and orientation of workpiece was determined from the resulting transformation as shown in Table 1. The XYZ position is found as the fourth column of the transformation and the orientation is contained in the first three columns. This conversion from transformation matrix to Cartesian position and orientation is not presented, as it is assumed to be common practice.

TABLE 1: SIMULATION RESULTS – EXAMPLE APPLICATION

	X	Y	Z
Expected Translation	0.25	0.2	0.025
Measured Translation	0.251347	0.19923	0.02436
Difference	-0.00134	0.00077	0.00064

	Roll	Pitch	Yaw
Expected Rotation	0.0	0.0	0.52360
Measured Rotation	-0.00918	-0.00681	0.52759
Difference	0.00918	0.00680	-0.00399

7. EXPERIMENTAL RESULTS

Example Application A was performed with an Aubo i5 on a welding table with a RP-LiDAR A2 mounted to the end effector for generating 3D point clouds shown in figure 11. In the scanning stage the arm performed a sweeping motion while collecting a point cloud containing approximately half of the workpiece, a large portion of the table, and a small portion of the arm itself. The recorded points are restricted to those that fall in a selected region of the usable workspace of the robot. This collection process produces redundant data points representing the objects and the cloud data can become large. The approach presented is applied to the raw projected LiDAR points as described with respect to the base frame of the robot.

The 3D point cloud is generated through transforming 2D scans into the global frame from the sensor frame based on the known kinematics of the robot arm. The known kinematic chain for the robot used in point cloud generation contained minor

discrepancies associated with the mounting alignment and drivetrain backlash. This is expressed as a static offset in the collected point cloud with respect the robot origin. This offset was measured using known locations on the welding table provided by the clamping grid. The calibration offsets are shown in table 2. Table 3 shows the results of the workpiece localization routine for example application A after the calibration offset is removed.

TABLE 2: EXPERIMENTAL RESULTS – LIDAR CALIBRATION

	X (m)	Y (m)	Z (m)
Expected Translation	0.0	-0.60960	0.02540
Measured Translation	0.00893	-0.60874	0.02003
Difference	-0.00893	-0.00086	0.00537

	Roll (rad)	Pitch (rad)	Yaw (rad)
Expected Rotation	0.0	0.0	0.0
Measured Rotation	-0.00493	-0.00071	0.019938
Difference	0.00493	0.00071	-0.00071

TABLE 3: EXPERIMENTAL RESULTS - EXAMPLE APPLICATION

	X (m)	Y (m)	Z (m)
Expected Translation	0.10160	-0.60960	0.02540
Measured Translation	0.10840	-0.61096	0.02034
Difference	-0.00680	0.00136	0.00506

	Roll (rad)	Pitch (rad)	Yaw (rad)
Expected Rotation	0.0	0.0	0.785
Measured Rotation	-0.00457	0.02186	0.79461
Difference	0.00457	-0.02186	-0.00921293

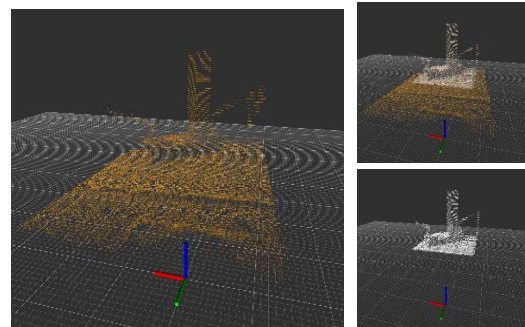


FIGURE 11: EXAMPLE APPLICATION - FILTERING

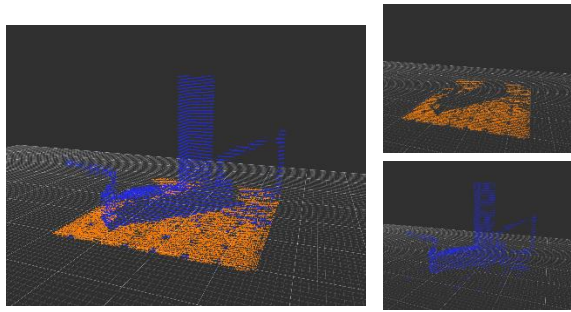


FIGURE 12: EXAMPLE APPLICATION – SEGMENTATION OF TABLE

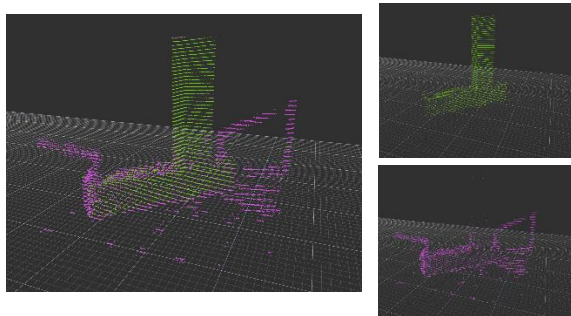


FIGURE 12: EXAMPLE APPLICATION – SEGMENTATION OF CLAMPS

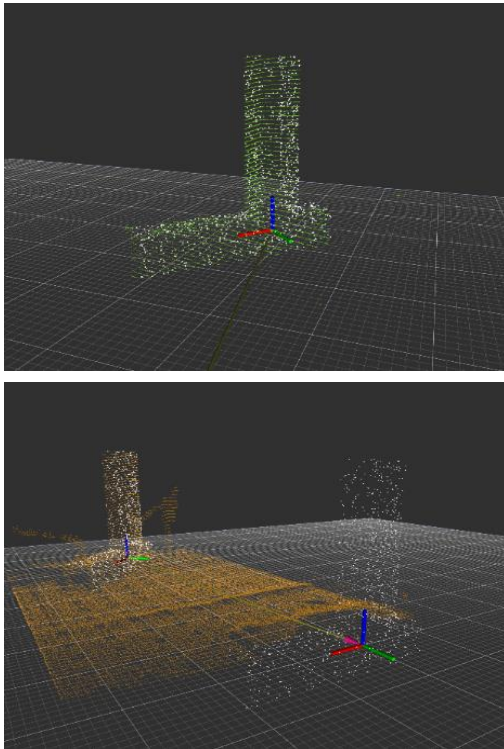


FIGURE 13: EXAMPLE APPLICATION – WORKPIECE REGISTRATION

8. RESULTS AND DISCUSSION

The results show that the proposed method of automated weld path generation using RANSAC and ICP algorithms is viable for workpiece localization. The alignment achieved in the simulated examples is strong as shown in the simulation and experimental results and proved that these algorithms can be implemented even in the case of increased noise in the target point cloud due to clamping mechanisms or miscellaneous items on the weld surface. The accuracy of the simulated tests is to be expected given that the simulated scene contained geometric features designed in CAD which closely resembled the target point cloud features. The physical experiment shows that this approach can be applied to a welding application using physical data in a realistic environment given that proper calibration is completed. The 3D LiDAR scans require calibration to accurately transform the source cloud to the target cloud. The implementation of passthrough filtering and voxel downsampling is an essential step prior to the segmentation algorithm with RANSAC. Furthermore, outlier rejection is a required step when there are features such as clamps included in the target point cloud set. Correspondence matching and alignment with ICP is shown to be effective when sufficient outliers have been removed and a reasonable initial guess is provided by RANSAC. Utilization of cascaded RANSAC segmentation provides an effective means for sufficient outlier removal such that workpiece alignment is sufficient [24] to be applied to a physical welding process.

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