


# Mobile robotic fabrication at 1:1 scale: the In situ Fabricator

## System, experiences and current developments

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Received: 30 December 2016 / Accepted: 24 May 2017 / Published online: 12 June 2017  
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**Abstract** This paper presents the concept of an In situ Fabricator, a mobile robot intended for on-site manufacturing, assembly and digital fabrication. We present an overview of a prototype system, its capabilities, and highlight the importance of high-performance control, estimation and planning algorithms for achieving desired construction goals. Next, we detail on two architectural application scenarios: first, building a full-size undulating brick wall, which required a number of repositioning and autonomous localisation manoeuvres. Second, the mesh mould concrete process, which shows that an In situ Fabricator in combination with an innovative digital

fabrication tool can be used to enable completely novel building technologies. Subsequently, important limitations of our approach are discussed. Based on that, we identify the need for a new type of robotic actuator, which facilitates the design of novel full-scale construction robots. We provide brief insight into the development of this actuator and conclude the paper with an outlook on the next-generation In situ Fabricator, which is currently under development.

**Keywords** Construction robotics · Digital fabrication · Mobile manipulation · In situ fabrication

This research was supported by the Swiss National Science Foundation through the National Centre of Competence in Research (NCCR) Digital Fabrication (Agreement #51NF40\_141853), a Professorship Award to Jonas Buchli (Agreement #PP00P2\_138920) and the Research Equipment Grant #206021\_150856. The authors would like to thank Norman Hack, Nitish Kumar and Alexander N. Walzer for providing details on the Mesh Mould process. Special thanks also go to the NCCR technicians Michael Lyrenmann and Philippe Fleischmann for their technical support on IF1.

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## 1 Introduction

### 1.1 Motivation

In the past decades, there has been significant effort to raise the degree of automation in building construction

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and architecture. Digital fabrication promises a revolution in the construction industry and exhibits a great potential for novel architectural approaches and alternative tectonics. The tight integration of planning and construction allows the architect to optimise processes on multiple levels. During planning, shapes can be optimised to create highly differentiated forms which minimise the usage of material. For construction, novel processes are enabled which minimise material waste, increase efficiency and improve working conditions. To handle the high level of geometric- and fabrication-informed complexity in an efficient manner, using digitally controlled machinery for the construction of computer-generated forms is essential. Furthermore, by tightly integrating digital design and fabrication, the performance and aesthetics of the structures being built can be improved through continuous adaptation of the design and process in real time.

To date, digital fabrication has had the most impact on the area of off-site prefabrication in which smaller components of a building are made in a dedicated factory and then transported to the building site for final assembly (an example is the roof presented in Willmann et al. 2016). Directly on building sites, however, the level of automation is still comparably low. The final assembly of building components is heavily dominated by manual labour, which breaks the digital process chain between design and making.

Motivated by this insight, recent research goes in the direction of on-site digital fabrication, the autonomous fabrication of buildings (or building components) on the spot, generally referred to as *in situ* fabrication. Within this field, one approach addresses on-site additive manufacturing with large-scale gantry systems (Khoshnevis 2004; Bosscher et al. 2007). However, the most striking disadvantage of this approach is the fact that the size of the employed machine constrains the size of the object being built. Therefore, using mobile, autonomous robots can be considered a more versatile option as it allows for the fabrication of structures significantly larger than the tool employed.

A number of attempts have already been made to develop mobile robots for on-site robotic construction. Early exploratory setups deserving explicit mentioning were the robots “Rocco” (Andres et al. 1994) and “Bronco” (Pritschow et al. 1996). However, these systems were designed for relatively standardised and strictly organised production processes. “Dimrob” was presented in Helm et al. (2012), but several factors restricted the platform’s usefulness for a wide range of building scenarios. It could only be repositioned manually and did not make use of advanced sensing and control concepts, therefore requiring the use of static support legs and

effectively rendering it as a movable fixed-base robot. In Keating (2016), a full-scale mobile system was shown to be capable of printing a large-scale foam structure, however also using a quasi fixed-base setup and without strict accuracy requirements. In Jokic et al. (2015), a self-supporting 3d printing system which can move on the printed structure was presented. For a recent, more complete survey of mobile robots in construction, we refer the reader to Ardiny et al. (2015).

To the best of our knowledge, to date, there is no robotic platform which fully satisfies the requirements for autonomous, mobile robotic construction at 1:1 scale. While there has been a number of research projects aiming at enabling mobile robots for on-site robotic construction, we believe that the key challenge which has prevented significant breakthroughs so far is that such machines must be able to robustly handle the unstructured nature of the building construction site. Because construction sites are constantly changing and relatively dirty and cluttered environments, it is not possible to apply classical industrial automation approaches in controlling such systems.

This challenge poses design, engineering and research questions at many different levels. While environmental and hardware requirements (e.g., payload requirements) determine the design, shape and physical realisation of the mobile robot itself, the role of state estimation, control and planning algorithms, as well as their proper implementations, should be considered in the design of the overall system such that it can be effectively operated by a non-expert user. Finally, the system needs to be integrated into layouting systems and architectural design software in such a way that there can be a seamless interaction between design and construction.

## 1.2 Contributions and structure of this paper

In this paper, we present the “*In situ Fabricator*” concept: a class of mobile robots specially designed for on-site digital fabrication. First, we propose a list of basic requirements for an *In situ Fabricator* in Sect. 2. Second, we present a systematic overview of the IF1, a first prototype built from off-the-shelf components, in Sect. 3. Next, we introduce the fully integrated digital tool-chain developed for the system, spanning from digital design to the planning and control for the mobile system. In Sect. 4, we present the planning, state estimation and control algorithms methods used for achieving the required capabilities for digital fabrication on IF1. In Sect. 5, we explain the IF1’s integration into architectural design and planning Software. We highlight the capabilities of this fully integrated system through two architectural demonstrators, in Sect. 6. First is a dry brick wall, which demonstrates the IF1’s ability to

build geometrically complex shaped structures at full scale. Second, we showcase the Mesh Mould project, which shows the IF1's potential to enable completely new building processes.

Reliable, dedicated hardware plays an important role in the construction sector. The characteristics of tasks appearing in building construction differ significantly from the task spectrum that classical industrial robotics can cover today. Therefore, in Sect. 7 we outline the inherent limitations of IF1 and related concepts based on commercially available industrial robotics. We list important conclusions drawn from those limitations, and highlight the development of a novel type of actuation designed specifically for the needs of full-scale robotic construction, in Sect. 8. Based on that, we introduce the concept of the future In situ Fabricator (IF2), which is currently under development.

## 2 Requirements and definition of an In situ Fabricator

Looking at a typical construction site today, one will often find a variety of machines of different sizes and with different specialised purposes. It is likely that we will see a similarly broad spectrum of different robots for specialised tasks in building construction in the future. In our research we have decided to first consider an intermediately sized class of mobile robots dedicated to a broad variety of fabrication tasks, referred to as In situ Fabricators. We believe that such a machine could have a significant impact on building construction in the near future and would effectively demonstrate the capabilities of on-site robotic digital fabrication. In situ Fabricators are defined through the following set of requirements:

### *Control and state estimation:*

- provide 1–5 mm positioning accuracy at the end effector.
- can operate within a local portion of the construction site. Moving obstacles, humans, and changing scenes outside of this area should not impact performance.
- is mobile in non-flat terrain with obstacles and challenges as found on a typical construction site.
- can operate with limited human intervention. The machine alone should offer the modality for achieving the overall accuracy of the building task.

### *Size and workspace constraints:*

- can reach the height of a standard wall.
- can fit through a standard door (in our case defined as a 80 cm wide Swiss standard door).
- can be loaded on a pallet/van.

### *Versatility and customisation:*

- can be equipped with different tools or end effectors to perform a wide range of building tasks.
- have sufficient payload to handle heavy and highly customised digital fabrication end effectors.
- can work in confined non-ventilated spaces.
- are protected against dust and water ingress.

### *Power supply:*

- can be plugged into standard mains power.
- have sufficient on-board power for phases of construction where no external power supply is available (e.g. during transportation to and from the construction site)

### *Usability and integration:*

- can provide required information to the architectural planning and control environments, e.g. current robot location, building state, etc.
- provide interfaces for interaction with an operator who is not a robotics expert.

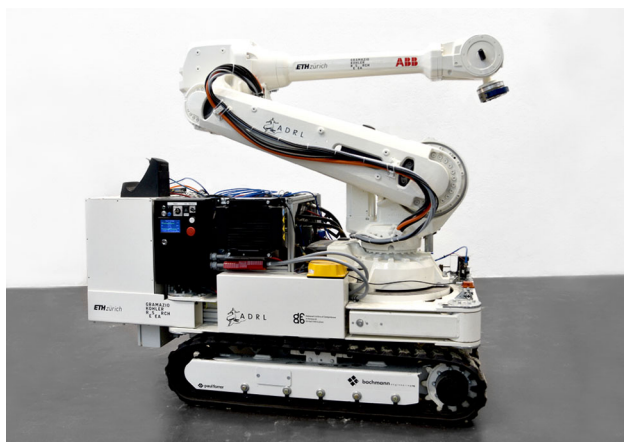
Note that we are not addressing the whole building production process chain, which would also include logistics and supply management. While this domain offers great opportunities for automation and optimisation, our work focuses on a machine intended solely for the production of the desired structure. As such, special attention is put on creating the possibility to close the feedback loop between design and the building process through in-the-loop sensing and control.

## 3 In situ Fabricator 1

In 2014, the first prototype machine was realised, the IF1, which is shown in Fig. 1. It is partially based on existing parts from the Dimrob project Helm et al. (2012) and mostly consists of commercially available off-the-shelf components. A brief overview of the robot hardware is given in the following section.

IF1 is equipped with an ABB IRB 4600 robot arm with 2.55 m reach and 40 kg payload. The decision to use an industrial robot arm for the first prototype allowed for quick progress in providing a fully sized mobile robot for initial research, although its limitations were already known at this point. All required industrial robot controller electronics from an ABB IRC5 controller unit were fit to the robot base in a custom, more compact form. The arm is position-controlled, and a commercial control interface provided by the manufacturer allows to send reference position and velocity commands at 250 Hz rate.

IF1 is electrically powered. It carries four packs of Li-Ion batteries with capacity for 3–4 h of autonomous operation at average machine load without being



**Fig. 1** The In situ Fabricator 1 (without end effector)

plugged into mains power. The robot features an on-board charging system and a power conversion system offering currents between 5–48 V DC and 230–400 V AC at 50 Hz.

The robot also carries a custom on-board hydraulic system, which is used to power its tracks through hydraulic motors, but can also provide hydraulic power to the tool mounted at the end effector. Its core components are a compact AGNI DC electric motor attached to a pump delivering hydraulic pressure at 150 bar. The hydraulic system is designed such that the tracks can be driven both with manual levers or through automatic operation, in which case the flow to the tracks' hydraulic motors is controlled by proportional valves. The IF1 can achieve a maximum driving speed of 5 km/h at a total weight of 1.4 tons. It is physically capable of manoeuvring on non-flat or soft ground as prevalent on construction sites.

Depending on the desired task, IF1 can be equipped with additional exteroceptive sensors. All sensors and actuators are driven by an on-board computer system which runs a hard real-time-enabled version of Linux with the Xenomai kernel-patch (Xenomai 2016). The main on-board computer unit features an Intel i3-3220T processor with 2.8 GHz and 4 GB RAM, which is sufficient to run basic state estimation, planning and control algorithms. Computationally more intensive tasks are run externally, with wireless communication provided through ROS (Quigley et al. 2009) or a custom real-time enabled TCP/IP implementation.

The standard mounting flange of the industrial arm and a general set of power and data connections are provided at the end effector to allow for the attachment of a wide range of tools. IF1 also provides various mounting points for temporary (complementary) equipment such as vacuum pumps or welding equipment.

## 4 State estimation, planning and control

For enabling autonomous localisation, driving and building, we have implemented a mix of well-established as well as novel algorithms for state estimation, planning and control. The methods described in the following sections have proven to reach high positioning accuracies over the course of long building processes and many robot repositioning manoeuvres without reliance on external reference systems.

### 4.1 Sensing and state estimation

In order for a robot to build structures on the construction site with high accuracy, it needs to be able to track the position of the tool it is using with respect to some fixed reference frame. This section describes the sensing system developed for IF1. These developments are broken up into three main functional parts: robot localisation within the construction site, alignment between the sensing reference frame and the CAD model, and feedback of the building accuracy during construction.

While there is an extensive body of research from the robotics community in localisation (Bonin-Font et al. 2008), motion tracking (Scaramuzza and Fraundorfer 2011), and mapping (Thrun 2002) for mobile robots, these systems do not directly translate to the construction site. In the active research area of simultaneous localization and mapping (SLAM), the main design driver is achieving bounded estimator accuracy over very long trajectories in unknown environments (Leutenegger et al. 2015; Fuentes-Pacheco et al. 2015). This performance criteria is very appropriate for use in autonomous navigation, but not for on-site building construction, where robots need to achieve millimetre-scale positioning accuracy relative to their workpiece in a limited workspace. Additionally, most state-of-the-art robotic sensing methodologies can not easily incorporate prior information about the robot's environment into the sensing system. We believe that the abundant prior information available for building construction, in the form of the CAD model or other plan data, is very valuable in achieving the demanding accuracy requirement for this application. Our work in sensing for IF has, therefore, focused on tailoring existing sensing solutions from the robotics community to the application of on-site building construction.

#### 4.1.1 Localisation

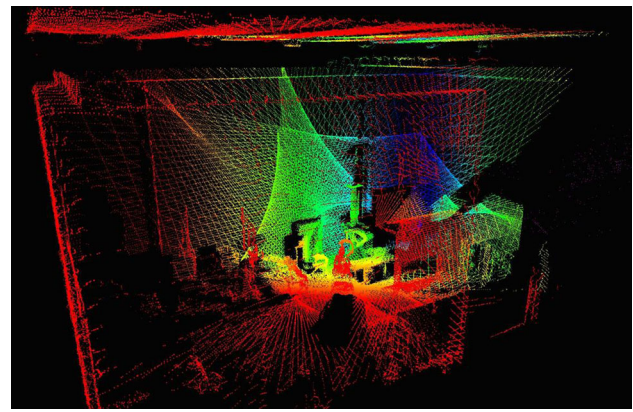
The most basic function of an In situ Fabricator's sensing system is to localise the end effector of the robot with respect to a fixed reference frame. In conventional



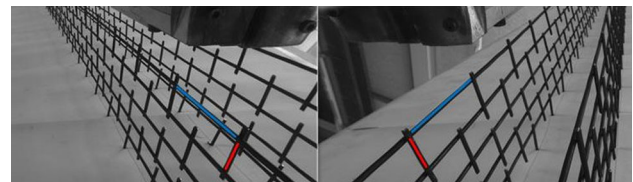
industrial robots, this is easily achieved using the rotary encoders in the robot's joints since the robot is sufficiently stiff and rigidly attached to the ground. For a mobile robot, however, exteroceptive sensing is required to ensure zero-drift pose estimates. A strategy typically used for such a system is to track a known point on the robot with respect to a static sensor system (e.g., a Vicon motion tracking system or a Hilti Total Station). While these systems can provide high-accuracy positioning data with minimal integration effort, they can be prohibitively expensive and take considerable initial setup time and effort. Furthermore, the measurement frequency and delay is often not optimized for mobile applications. Alternatively, sensors can be mounted directly on the robot and used to locate visual references in the robot's workspace. While these solutions are much lower cost, they typically require significantly more integration effort, as the sensor information must be heavily processed to extract the information required for localisation (e.g., image processing to extract the local visual features). This strategy is pursued for IF as to avoid the presence of visibility constraints from an external measurement system and because we believe this sensing modality can be more easily expanded to feed back additional pieces of information to inform the remainder of the building process (as in Sect. 4.1.3).

We have developed two separate sensing systems for use on IF1, each supporting one of the application examples presented in Sect. 6. For the brick-laying experiments, we mounted an off-the-shelf laser range finder (LRF) on the end effector of IF1. By executing sweeping motions with the wrist of the arm, we could build 3D point clouds of the robot's surroundings (Fig. 2). These point clouds were then registered versus an initial point cloud to infer the robot's relative motion (see Dörfler et al. 2016 for implementation details). The main shortcoming of this method is that it assumes that the majority of the robot's environment remains unchanged during construction, which is a bad assumption since construction sites are constantly changing environments. Subsequent efforts therefore focused on sensing modalities which allow the robot to localise considering only measurements in vicinity of its workpiece. In Sandy et al. (2016) we use the same scanning system to build point clouds of the workpiece and then register a geometric model of the workpiece to the scan to determine the robot's pose.

One of the disadvantages of using LRFs is that their depth sensing accuracy and angular resolution are fixed by the sensor's internal hardware. This means that a sensor used for mapping the robot's environment is not well suited for detecting small components of the workpiece. For the Mesh Mould project (see Sect. 6.2) we therefore switched to using camera-based sensing. Two camera systems are used: one for global localization and one for local detection



**Fig. 2** Point cloud of our lab captured by IF1



**Fig. 3** Stereo image pair taken with the cameras on the Mesh Mould toolhead during fabrication. The two detected wire segments are highlighted in *blue* and *red* in each image. The next segment of the mesh was welded to these segments

of the wire mesh being built. We use the same model of camera for both sensing tasks, but change the lens and positioning of the cameras to address the different requirements of the two sensing systems. For localisation, two cameras fixed to the base of the robot observe AprilTag (Olson and AprilTag 2011) fiducial markers to localise relative to a calibrated map of the tag positions in the workspace. With this system, we can achieve a global positioning accuracy of less than 5 mm. This system alone is not sufficient for construction of the mesh, though, since the mesh deforms during construction due to internal tension in the wires. A second sensing system is therefore required to measure the position of the wire used for the next construction step so that the tool can clamp to it without unexpected collisions. A stereo pair of cameras mounted on the tool-head generates images of the mesh. We then use line detection and matching, along with our CAD model of the mesh, to locate the target wire. Figure 3 shows a stereo image pair from this system with the detected wires highlighted. By coupling these two sensing systems, we additionally obtain information as to how well the measured mesh agrees with the original design.

#### 4.1.2 Alignment with the CAD model

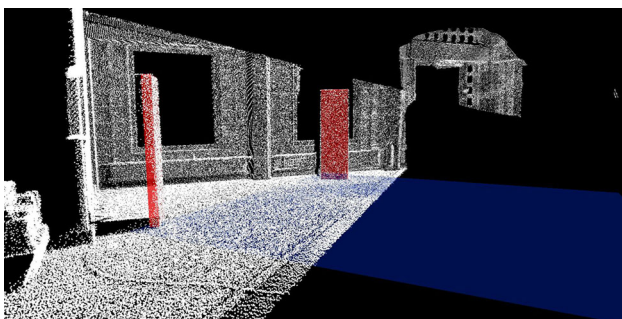
In most architectural applications, localising the tool with respect to some general fixed global reference frame is not

enough. Any structure built needs to be attached to an existing element of the construction site and must be located with sufficient precision that the overall accuracy of the construction is ensured. For in situ fabrication, this can be achieved by aligning the sensing reference frame with the reference frame of the CAD model of the structure being built. This requires determining the position of either the external sensing system or the visual features used for localisation in the CAD model. This alignment step can typically be done just once before building. During this alignment step, key interfaces on the construction site, to which the structure being build must attach, can be identified and their positions fed back to update the design of the structure to accommodate any inaccuracies which may be present on the construction site.

In the IF1 brick laying work (Sect. 6.1), localisation is performed relative to a reference scan of the construction site taken before starting to build. The reference scan is aligned with the CAD model of the structure by registering features of the constructions site to which the wall was anchored (Fig. 4). In this way, the robot is not only able to localise relative to the CAD model, but also we are able to adjust the parametric design of the wall to match the true positions of the pillars within the construction site. For the Mesh Mould project (Sect. 6.2) we need to align our map of the visual fiducial poses to the CAD model of the wall. This is done by aligning the position of several reference tags to their known positions in the CAD model.

#### 4.1.3 Feedback of building accuracy

We believe that, to realise the full potential of robotic on-site construction technology, the robot used should be able to feed back data about the progress of the building project during construction. In this way, building inaccuracies and changing conditions in the construction site can be compensated for during construction. This is especially crucial in building processes where material does not behave predictably after processing. This is the case in the Mesh



**Fig. 4** Point cloud of the building site, showing the registered positions of geometric models of the attachments pillars (red) and floor (blue) of the CAD model

Mould project. As the wire mesh is constructed, internal tension between the wires tends to pull the mesh away from the position in which it was welded. The direction and amount of deflection are difficult to model; therefore, real-time feedback of the material behaviour is required to ensure accurate construction. Using the two coupled measurement systems described, however, IF can determine the shape of the last wire welded to the mesh in the global reference frame, therefore observing how well it matches the initial design. In the presence of significant errors in the wire contour, the building plan for the next layers of the mesh can be adjusted to compensate for the error and effectively pull the mesh back into alignment with the CAD model. It should be noted that this functionality is a natural extension of the camera sensing system since various custom features can be extracted from images relatively easily. It would be very difficult, however, to do this compensation if a commercial off-board sensing systems was used, since it would not be capable of detecting the contour of the wire mesh.

## 4.2 Planning and control

Generally speaking, we approach the planning and control problem for In situ Fabricators through optimal control. Optimal control solves the problem of finding a control policy for a dynamic system such that a predefined criterion of optimality is achieved. It can be used to compute either open-loop trajectories, which is the domain of trajectory optimisation, to compute feedback laws which stabilise given trajectories, which is pure feedback control, or both at the same time. By solving a corresponding mathematical optimisation problem, we find optimal trajectories and/or control laws that steer the system to a desired pose while minimising some cost function and respecting constraints at the same time. Difficulties arising in planning and control for mobile construction robots are obstacles, inherent motion constraints (for example non-holonomic constraints due to wheels or tracks), motion with contact and interaction forces and accumulated model uncertainties. The latter is an important issue for IF1, as tracked locomotion on imperfect ground can not be modelled with high accuracy. In contrast to classical, sampling based planning algorithms like Rapidly exploring random trees and probabilistic roadmap methods (see LaValle 2006 for an overview), or the integrated kinematic planners typically supplied with industrial robots, many optimal control algorithms can handle some of these difficulties with reasonable complexity.

For IF1, we have integrated different control and planning approaches, which allow us to consider base- and arm motion either separately or jointly as a whole-body problem. Coordinated whole-body motions with non-holonomic

base constraints and holonomic operational-space constraints (e.g. tool position constraints) are generated using constrained sequential linear quadratic (SLQ) optimal control. Although being an iterative optimal control algorithm, it is computationally highly efficient, as it features linear time complexity  $O(n)$ . Feedforward trajectories and feedback are optimised simultaneously, which generalises the control policy in the vicinity of the nominal, optimal trajectory. The resulting feedback gains are compliant with non-holonomic constraints. On IF1, we run this algorithm in a model predictive control (MPC) fashion at up to 100 Hz update rate, where the feedback loop is closed through an on-board visual-inertial state estimator. This allows us to achieve robust positioning despite the presence of model uncertainties and external perturbations. In particular, this allows for rejecting uncertainty from the tracked locomotion from the end effector motion. Figure 5 shows snapshots from a motion sequence with an end effector position constraint executed on IF1 using Constrained SLQ in an MPC fashion. More details about SLQ MPC on IF1 and experimental results are provided in Gifftaler et al. (2017).

When performing sequential building tasks, as for example demonstrated in Sandy et al. (2016), or when more obstacles are present, we separate the base- and arm control problem and move base and arm sequentially. In this case, we use a constrained version of the stochastic planner STOMP Kalakrishnan et al. (2011, 2013) for trajectory optimisation and a simple trajectory following strategy as presented in Sarkar et al. (1993).

For manipulation, we combine individually planned sequences of arm/base motion with a library of task-specific, pre-programmed manipulation primitives (e.g., picking up a brick from the brick feeder or moving a joint at constant velocity). This combination has proven sufficient for a number of building tasks.

Note that our approach can typically handle a moderate number of convex obstacles easily and reliably. However, at the current stage, we cannot handle cluttered or fragmented environments with a large number of non-convex, possibly intersecting or dynamically changing obstacles. Besides requiring a system for real-time obstacle perception and classification, which is currently not implemented,

this would lead to strongly non-convex and ill-posed optimisation problems which cannot be treated in a classical optimal control setting. The combination of our optimal control framework with higher-level planners which are able to negotiate cluttered environments is part of our future research.

## 5 Integration into architectural design and planning software

A major interest in the development of the In situ Fabricator is to tightly integrate its functions and capabilities into an architectural planning framework, to make its features directly available for architects and designers. Eventually we are aiming to see the generation and rationalisation of shapes to be directly influenced by the specific logic of making—in this case, next to the choice of a material and assembly system, this is the feature of mobility and the extended workspace of the mobile robot.

To fully exploit the design-related potentials of using such a robot for fabrication, it is essential to make use not only of the manipulation skills of this robot, but to also use the possibility to feed back its sensing data into the design environment. This allows the system to guide and inform a running fabrication process such as to be able to detect and react upon unforeseen assembly tolerances and process-related uncertainties. Furthermore, the system can base immediate design decisions on the information extracted from sensors, allowing a high level of flexibility, autonomy and control in fabricating an architectural artifact.

Motivated by this, the high level planning of fabrication tasks, such as the sequencing of the mobile robot's positions and fabrication procedures and computing the arm, base and end effector positioning commands, is implemented within an architectural planning tool, in our case Grasshopper Rhinoceros (Rhinoceros 2016). A TCP/IP plugin allows for the online control the robot's arm and base, and gives access to the robot's state estimator, planning routines and movement primitives. This approach is also detailed in Dörfler et al. (2016) and Kumar et al. (2017). Generally speaking, the robot's setup is designed to allow for feedback loops at multiple levels of the system:



**Fig. 5** Snapshots from a motion sequence with an end effector position constraint executed on IF1 using Constrained sequential linear quadratic optimal control in a model predictive control fashion.

The task is to reposition and reorient the base while keeping the end effector at a constant position



all time-sensitive tasks are executed by control loops running on the robot's low-level computer while the control loop over the overall building process is closed via the architectural planning tool.

## 6 Architectural demonstrators and examples

The main drivers for the development of the IF1's functionality and software framework were the architectural demonstrators shown in this section. The challenge of fabricating multiple architectural prototypes with an increasing level of complexity was specifically chosen to gradually advance the generic features of the robot. The realisation of these demonstrators was significant for evaluating chosen methods and to learn what is necessary—from both the robotics and the architecture point of view—to enable automated material deposition and assembly processes in an unstructured, cluttered, and ever changing environment such as a construction site. At the current stage of development, this enables us to build customised, geometrically complex structures accurately over the course of the entire building space. While the presented experiments are still performed on flat ground, a generalization onto non-flat surfaces would be possible.

### 6.1 Undulating brick wall

The first architectural scale demonstration with IF1 was the semi-autonomous fabrication of a continuous dry-stacked, undulating brick wall (Fig. 6) in a laboratory environment which was set-up to mimic a construction site. The material system—consisting of discrete building elements and a simple assembly logic—allowed us to subdivide the sequential building process of the entire wall into discrete production steps from subsequent robot locations (Fig. 7).

In this experiment, it played a key role to align the CAD model of the building site with the true positions of key



**Fig. 6** IF1 building the undulating brick wall



**Fig. 7** Visualisation of a possible building sequence for the double-leaf brick wall shown in Fig. 6. The wall is 6.5 m long and 2 m high, consists of 1600 bricks and is fabricated from 15 different base positions

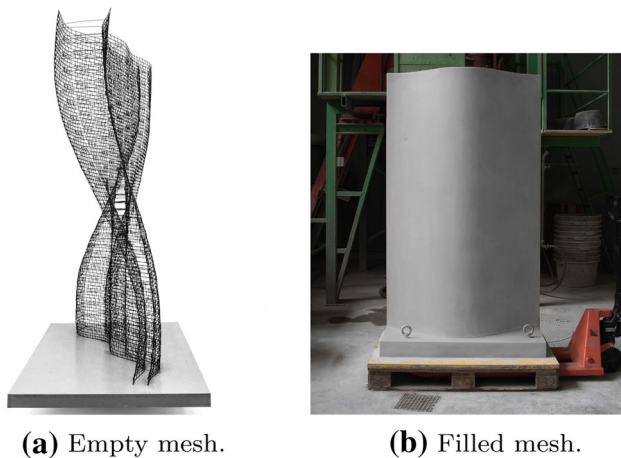
features of the working environment, extrapolated from the initial 3D scan of the surrounding captured by the robot's sensor system. This allowed us to adapt the ideal dimensions of the wall's parametric geometry model to the true dimensions of the construction site before actually starting the fabrication.

The building process itself consisted of iterative steps of moving the robot to positions along the wall, localising the robot's base pose and building a patch of bricks reachable within the workspace of the robot. The global localisation and brick placement errors did not accumulate over the course of the building process, first because of the initial alignment of the true positions of the attachment points to the building plan, and second, every point cloud for localisation captured from a new location was always registered against the same initial reference scan. Therefore, the designed double-leaf brick wall—requiring the robot to be repositioned 14 times—was successfully constructed semi-autonomously with a maximal assembly error of 7 mm over the entire workpiece. While the bricklaying was done autonomously, feeding the robot with bricks was accomplished manually.

### 6.2 Mesh mould

The second demonstrator combines the novel construction technique Mesh Mould (Hack et al. 2015; Kumar et al. 2017) with the use of IF1. The main objective of Mesh Mould is the bespoke fabrication of free-form steel meshes which form both mould and reinforcement to enable a waste-free production of customised reinforced concrete wall structures (see Fig. 8). This fabrication method is an ideal test-bed for showing the possibility of a continuous construction process fabricated by a mobile robot. The possibility to bend and weld these meshes directly on site offers a multitude of advantages: the integrated vision feedback system allows to react to material tolerances during fabrication on the spot. It allows to negotiate





**Fig. 8** Mesh Mould demonstrators built by IF1

between true measurements of the structure during build-up and a required target shape based on the planning data right when it is needed. Production sequences can radically be redefined: Structures to be built do not have to be discretised into separate building components due to size limits for transportation, but can rather be redefined in accordance with the fabrication logics of the chosen material system and the mobile machinery.

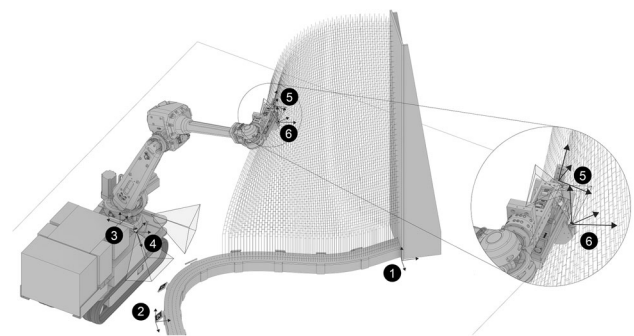
The integration of the robotised Mesh Mould end effector for bending and welding steel wires into the architectural control and simulation framework of IF1 constituted a major part of the efforts in implementation. Once completed, the whole system was tested for the first time on a floor slab of NEST<sup>1</sup>—an exploratory construction site at EMPA in Zürich. The fabrication of an undulated, curved Mesh Mould element directly on the construction site served to test the system’s robustness under realistic working conditions and helped to understand the logistics requirements of performing the fabrication process in situ (see Fig. 9). For more details, the interested reader may also refer to Hack et al. (2017).

For the Mesh Mould project, IF1 was equipped with both a global and local state estimator (see Fig. 10). The global pose estimation of the robot’s origin using artificial landmarks enables automated localisation during repositioning procedures. Further, the integration of perception at the end effector is required for correcting its pose in case of detecting accumulative fabrication errors and mesh deformations.

Currently IF1 and Mesh Mould are integrated into a larger building project: a fully load bearing 14 m long steel reinforced concrete wall is being fabricated at the ground



**Fig. 9** IF1 building a small doubly curved metal mesh at the exploratory construction site NEST



**Fig. 10** Vision system and frame definition for the Mesh Mould wall fabrication process: 1 world frame, 2 tag frame, 3 robot frame, 4 base camera frame, 5 end effector frame, 6 end effector camera frame

level of the NEST unit realized by the Swiss National Competence Center of Research in Digital Fabrication.<sup>2</sup>

## 7 Limitations and lessons learned from IF1: why classical industrial arms are a poor choice for mobile building construction robots

IF1 by design exhibits a number of drawbacks. Importantly, these shortcomings are not specific to this particular robot, but are rather inherent to the relevant off-the-shelf technology existing to date and being available to research in our field. Some of the predominant issues are summarised in the following section.

Standard serial-chain industrial manipulators often make use of heavy-duty electric motors and gearboxes. The joints and links are designed for maximising stiffness, which is essential for reaching high positioning accuracy using traditional robot control approaches. A consequence resulting from that design strategy is a relatively low payload to

<sup>1</sup> <https://www.empa.ch/web/nest>.

<sup>2</sup> <http://www.dfab.ch>

weight ratio (PWR). For example, our ABB IRB 4600 arm offers a PWR of 40:440 kg. Additional downsides to the weight of industrial robots are the need for a heavy base to ensure that the robot cannot tip over, the difficulty transporting the robot, and the added safety risks of operating such a large system. At 1.4 tons, IF1 is already too heavy to access some standard building environments.

Purely position-controlled robotic arms are by design ill-suited for many construction tasks. For advanced manipulation tasks taking place beyond perfect conditions, such as on-site assembly of structures, drilling, coring or chiseling, being able to control the interaction forces between tool and workpiece is essential. While adding a multi-DoF force–torque sensor at the end effector appears to be a workaround and certainly gives more flexibility to the setup, it remains a sub-optimal design choice. While a detailed discussion of this issue is beyond the scope of this paper, it is a well established result that such an arrangement (non-collocated sensing and control) has non-ideal control theoretical stability properties. This practically restricts the system to slow, conservative motions, and imposes strong limitations on the dynamics of processes that can be controlled by the end effector. For a detailed treatment of the drawbacks of non-collocated force control, we refer to Eppinger and Seering (1986, 1987), Howard (1990).

Moreover, for many of the aforementioned tasks, classical, electrically actuated robot arms without compliant, vibration-damping mechanical elements will not be suited for long runtimes and everyday application. Bad load cases can rapidly damage sensitive mechanical elements such as gearboxes and will cause them to wear out rapidly. In robotics, common solutions are to consider series-elastic or hydraulic actuators.

Consequently, the next-generation In situ Fabricator needed to be thoroughly rethought to provide a concept which resolves these problems. It's worth mentioning that sufficiently sized platforms with full force–torque control at joint level, and access to low-level control loops (for implementing dynamically capable control methods) are commercially not available today.

## 8 Developing the next-generation In situ Fabricator

From the experience gained with IF1 and the Mesh Mould project, it is clear that the next-generation In situ Fabricator (IF2) has to fulfil an additional set of requirements:

- *Agility* Able to perform a specified set of manoeuvres typical of operating in a representative building, for example traverse a narrow doorway from a corridor.

- *Payload* Capable of operating with a 60 kg payload.
- *System weight* Maximum of 440 kg overall system weight (500 kg including payload), which corresponds to a typical maximum load for a standard floor.
- *Arm(s)* at least one 7 DOF robotic arm with at least 2.5 m reach.
- *Safety* Capable of reverting to safe or passive modes on detection of an unsafe situation.
- *Robust in construction site* Minimise or eliminate external components that may be subject to damage, e.g. external hoses and wires. Maximise reliability and on-site maintainability.
- *Control* Capable of high bandwidth (>1 kHz) force and position control.

Through straight-forward calculations, it can be shown that using conventional electrical or hydraulic robot joint actuators, it would be impossible to achieve the required 440 kg overall mass limit and the desired PWR at the same time. An assessment of the other system requirements suggests that a completely novel actuator design is required to achieve the desired performance, weight and force control properties.

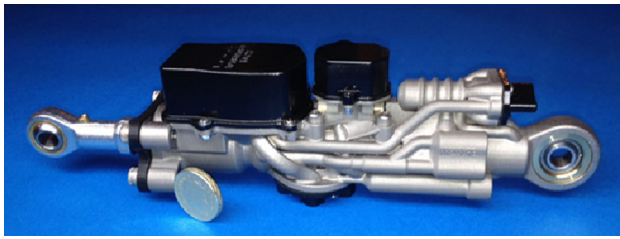
### 8.1 Intermediate result: development of a novel type of hydraulic actuator

To meet the demanding requirements for IF2, a highly feature dense, structurally capable, lightweight actuator design is required. In cooperation with Moog Inc and Renishaw PLC, we are developing a novel, integrated hydraulic actuator offering superior power density. Building on previous work in the field of integrated actuation (Fig. 11), a novel titanium fully integrated vane actuator is developed (see Fig. 12). The actuator is constructed around a conventional limited angle rotary vane actuator and includes all hydraulic controls, safety valves, sensors, electronic controls, local processing, data bus as well as hydraulic and electrical slip rings. To provide the required degree of integration in a compact, structurally efficient package, additive manufacturing using the laser powder bed principle was chosen for the major components.

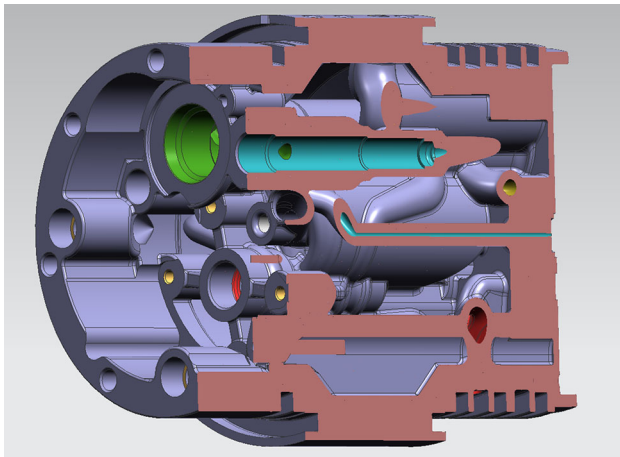
The actuator is capable of mounting for joint rotation around and perpendicular to the major axis. It is designed in three different sizes, which for example allows for a lightweight realisation of different manipulator segments such as arms or legs.

### 8.2 Outlook on IF2

Hydraulic actuation in conjunction with advanced additive manufacturing technology is particularly well suited



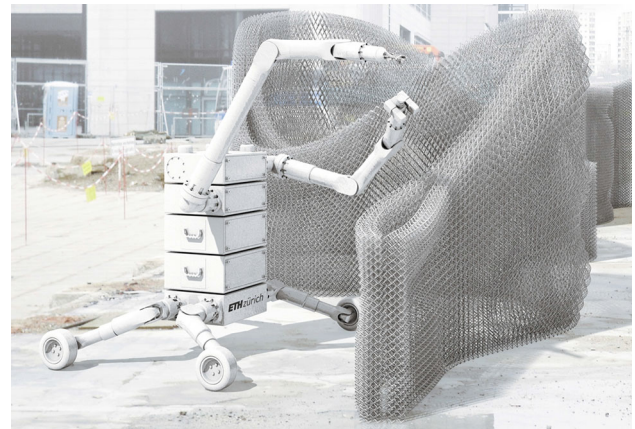
**Fig. 11** Linear integrated actuator, see Semini et al. (2016) for details



**Fig. 12** Section through a fully integrated vane actuator as described in Sect. 8. It includes all hydraulic controls, sensors, electronics, local processing, data bus and slip rings

to construction robots. It features superior power density, even on compact, mobile systems with on-board pumps. At the same time, hydraulic systems can be scaled up to dimensions relevant for construction machinery more easily than electrically actuated systems and are typically highly robust—one of the reasons why a majority of heavy-duty machinery on today's construction site is hydraulically driven.

Based on our experience with IF1 and the novel hydraulic actuators, a preliminary design of IF2 has been created, which is shown in Fig. 13. To achieve the desired manoeuvrability, it is equipped with legs and wheels, which allows for multiple modes of locomotion: walking, driving, or hybrid modes. A main design goal of IF2 is modularity, such that the robot's morphology can be adapted to different requirements of different architectural tasks with comparably low effort. IF2 is currently under development. The overall design shown in Fig. 13 represents the current concept, its feasibility is pending on how further tests with the novel actuators evolve. Prototypes of the hydraulic actuators, a first arm prototype, as well as first experimental results are expected by the end of 2017.



**Fig. 13** Concept of the In situ Fabricator 2, which is currently under development

## 9 Summary and conclusion

In this paper, motivated by the need for digitally controlled mobile robots for on-site manufacturing, assembly and digital fabrication, we have presented an overview of a class of machine that we call 'In situ Fabricators'. We have listed the core requirements defining that class of robot. We have presented a compact overview of the IF1, which is a prototype system based on classical industrial off-the-shelf components, and its capabilities. To meet the desired accuracy and performance, we have implemented a number of state-of-the-art algorithms for motion planning, state estimation and control. The development and implementation of the IF1's software framework was strongly inspired by the needs of two full-scale application demonstrators, which are showcased in this paper: First, a full-size undulating brick wall, which required a number of repositioning manoeuvres during the building process, in which we achieved mm-scale positioning accuracy. Second, the Mesh Mould process, which shows that an In situ Fabricator in combination with an innovative toolhead can be used to enable completely novel building processes. IF1 successfully built a number of metal mesh segments, which were also filled with concrete and underwent structural load tests. In a next step, IF1 will be deployed to an exploratory construction site to build the ground floor of a demonstrator living unit.

We also emphasised the limitations of our approach. As the general interest in construction robotics and digital fabrication is currently increasing in both academia and industry, one of our core aims is to raise the awareness amongst other researchers in the field, that the classical industrial robotics approach is bound to a number of significant disadvantages. In our case, these limitations provided the motivation for the development of an innovative, compact, force-controlled rotary hydraulic actuator.



Thanks to very recent developments in AM technology we are enabled to use highly integrated compact actuators in conjunction with very efficient additively manufactured structural components. We concluded this work by introducing the concept for IF2, the next-generation In situ Fabricator. We expect that this development is going to be a major step towards facilitating advances in full-scale construction robots.

## References

- Andres J, Bock T, Gebhart F (1994) First results of the development of the masonry robot system ROCCO. In: Proceedings of the 11th ISARC in Brighton (international symposium on automation and robotics in construction), pp 87–93
- Ardiny H, Witwicki SJ, Mondada F (2015) Are autonomous mobile robots able to take over construction? A review. *Int J Robot* 4(3):10–21
- Bonin-Font F, Ortiz A, Oliver G (2008) Visual navigation for mobile robots: a survey. *J Intell Robot Syst* 53(3):263–296
- Boscher P, Williams RL, Bryson LS, Castro-Lacouture D (2007) Cable-suspended robotic contour crafting system. *Autom Constr* 17(1):45–55
- Dörfler K, Sandy T, Gifftthaler M, Gramazio F, Kohler M, Buchli J (2016) Mobile robotic brickwork—automation of a discrete robotic fabrication process using an autonomous mobile robot. In: Robotic fabrication in architecture, art and design, pp 205–217
- Eppinger S, Seering W (1986) On dynamic models of robot force control. In: IEEE international conference on robotics and automation (ICRA), vol 3, pp 29–34
- Eppinger S, Seering W (1987) Understanding bandwidth limitations in robot force control. In: IEEE international conference on robotics and automation (ICRA), vol 4, pp 904–909
- Fuentes-Pacheco J, Ruiz-Ascencio J, Rendón-Mancha JM (2015) Visual simultaneous localization and mapping: a survey. *Artif Intell Rev* 43:55–81
- Gifftthaler M, Farshidian F, Sandy T, Stadelmann L, Buchli J (2017) Efficient kinematic planning for mobile manipulators with non-holonomic constraints using optimal control. In: IEEE international conference on robotics and automation (ICRA)
- Hack N, Lauer WV, Gramazio F, Kohler M (2015) Mesh Mould: robotically fabricated metal meshes as concrete formwork and reinforcement. In: FERRO-11: proceedings of the 11th international symposium on ferrocement and 3rd ICTRC international conference on textile reinforced concrete. RILEM Publications SARL, Bagneux, pp 347–359
- Hack N, Wangler T, Mata-Falcón J, Dörfler K, Kumar N, Walzer A, Graser K, Reiter L, Richner H, Buchli J, Kaufmann W, Flatt RJ, Gramazio F, Kohler M (2017) Mesh Mould: an on site, robotically fabricated, functional formwork. In: Concrete innovation conference HPC/CIC. Tromsø
- Helm V, Ercan S, Gramazio F, Kohler M (2012) Mobile robotic fabrication on construction sites: Dimrob. In: 2012 IEEE/RSJ international conference on intelligent robots and systems (IROS)
- Howard RD (1990) Joint and actuator design for enhanced stability in robotic force control. Ph.D. thesis, Massachusetts Institute of Technology
- Jokic S, Novikov P, Maggs S, Sadan D, Jin S, Nan C (2015) Minibuilders. In: Architectural principles, tools, and processes. Digital Vernaclar, pp 259–265
- Kalakrishnan M, Chitta S, Theodorou E, Pastor P, Schaal S (2011) Stomp: stochastic trajectory optimization for motion planning. In: IEEE international conference on robotics and automation (ICRA), pp 4569–4574
- Kalakrishnan M, Herzog A, Righetti L, Schaal S (2013) Markov random fields for stochastic trajectory optimization and learning with constraints. In: Robotics: science and systems, workshop on hierarchical and structured learning for robotics, Berlin
- Keating S (2016) From bacteria to buildings: additive manufacturing outside the box. Ph.D. thesis, Massachusetts Institute of Technology
- Khoshnevis B (2004) Automated construction by contour crafting-related robotics and information technologies. *Autom Constr* 13(1):5–19
- Kumar N, Hack N, Dörfler K, Walzer A, Rey G, Gramazio F, Kohler M, Buchli J (2017) Design, development and experimental assessment of a robotic end-effector for non-standard concrete applications. In: IEEE international conference on robotics and automation (ICRA) (**submitted**)
- LaValle SM (2006) Planning algorithms. Cambridge University Press, Cambridge
- Leutenegger S, Lynen S, Bosse M, Siegwart R, Furgale P (2015) Keyframe-based visual-inertial odometry using nonlinear optimization. *Int J Robot Res* 34(3):314–334
- Olson E (2011) AprilTag: a robust and flexible visual fiducial system. In: Proceedings of the IEEE international conference on robotics and automation (ICRA). IEEE, pp 3400–3407
- Pritschow G, Dalacker M, Kurz J, Gaenssle M (1996) Technological aspects in the development of a mobile bricklaying robot. *Autom Constr* 5(1):3–13
- Quigley M, Conley K, Gerkey BP, Faust J, Foote T, Leibs J, Wheeler R, Ng AY (2009) Ros: an open-source robot operating system. In: ICRA workshop on open source software
- Rhinoceros G (2016) Grasshopper Rhinoceros. <http://www.grasshopper3d.com/>. Accessed 06 Nov 2016 (**Online**)
- Sandy T, Gifftthaler M, Dörfler K, Kohler M, Buchli J (2016) Autonomous repositioning and localization of an in situ fabricator. In: IEEE international conference on robotics and automation (ICRA), pp 2852–2858
- Sarkar N, Yun X, Kumar V (1993) Dynamic path following: a new control algorithm for mobile robots. In: Decision and control, 1993. Proceedings of the 32nd IEEE conference, vol 3, pp 2670–2675. doi:10.1109/CDC.1993.325681
- Scaramuzza D, Fraundorfer F (2011) Visual odometry [tutorial]. *IEEE Robot Autom Mag* 18(4):80–92
- Semini C, Baker M, Laxman K, Chandan V, Maruthiram T, Robert Morgan R, Frigerio M, Barasuol V, Caldwell DG, Rey G (2016) A brief overview of a novel, highly-integrated hydraulic servo actuator with additive-manufactured titanium body. In: IEEE/RSJ IROS workshop on force/torque controlled actuation
- Thrun S et al (2002) Robotic mapping: a survey. Exploring artificial intelligence in the new millennium, vol 1, pp 1–35
- Willmann J, Knauss M, Bonwetsch T, Apolinarska AA, Gramazio F, Kohler M (2016) Robotic timber construction expanding additive fabrication to new dimensions. *Autom Constr* 61:16–23
- Xenomai (2016) Xenomai: real-time framework for Linux. <http://www.xenomai.org>. Accessed 06 Nov 2016 (**Online**)