

Embedded systems 2

# Report Cosy Cafeteria

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# 1 Intro

To improve the experience of the students in the cafeteria, an embedded system will be developed to gather a variety of data. This data will then be display to the students through an online medium such as a website. The main focus will be to gather information about the amount of people that are in the cafeteria. There are two main goals. The first goal is to display the estimated waiting time to get a meal to the students. Secondly the amount of available seats will be tracked and displayed to the students. Next to this some additional information will be gathered. The temperature, air-quality and sound level will be monitored to give the student a general idea about the conditions in the cafeteria. This way the student can gauge if the cafeteria is suitable to study in at a certain moment. An overview of the envisioned system is displayed in figure 1. All the developed hardware and software is displayed at: [https://github.com/thomasf10/cosy\\_cafeteria](https://github.com/thomasf10/cosy_cafeteria).

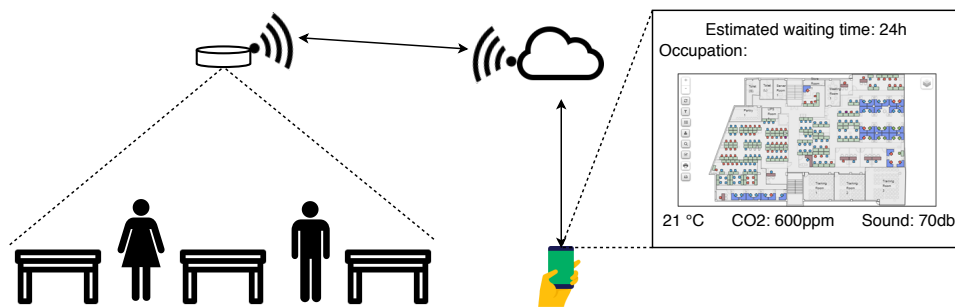


Figure 1: Situation sketch

## 2 Specifications

### 2.1 Functional specifications

- Monitor the available seats
- Monitor the queue to get a meal
- Display the data to the students
- Energy provision for 1 semester (4-5 months)
- Wireless coverage over the entire campus
- Measure new data every 10 minutes
- Send the data to the online medium every hour
- If the data changes with a large amount (needs to be specified) update the online medium sooner

## 2.2 Other technical specifications

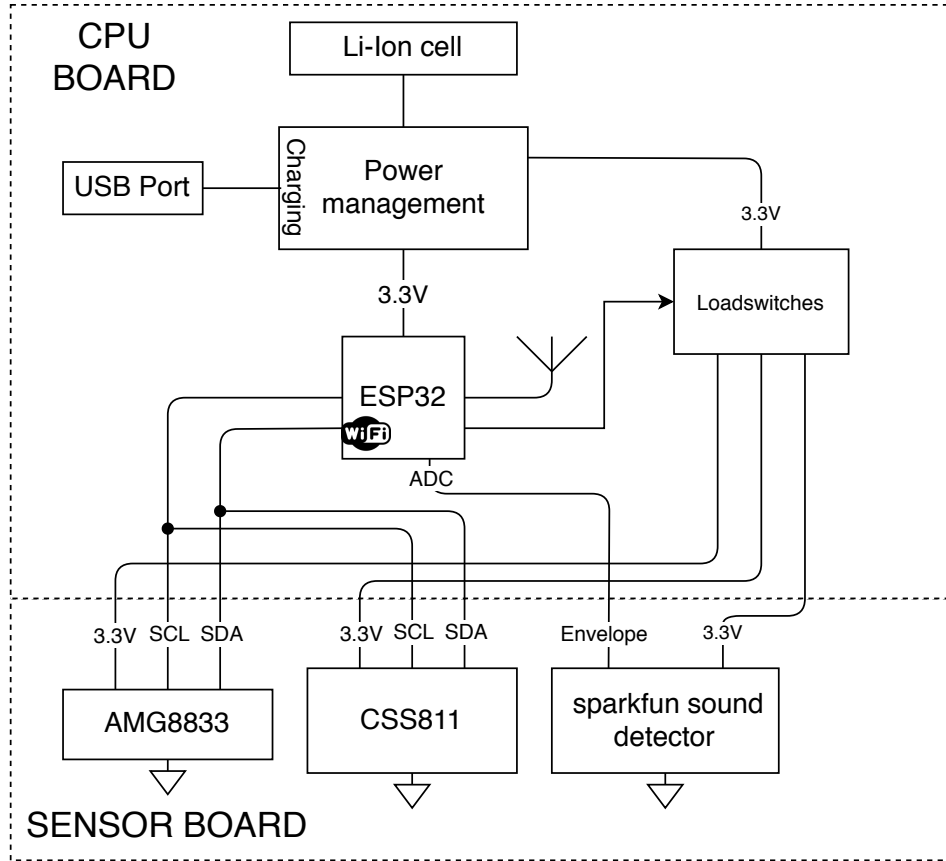
- Enclosure: 10 x 10 cm
- Easy deployment: the node must be easy to attach and detach from the sealing
- Must be easy to recharge (Wireless or via USB)
- Light weight: 300 g (so it wont detach from the sealing)

## 2.3 Non-technical specifications

- Cost: €??
- The data should be easy accessible to the students

## 3 System architecture

systeem wat uitleggen ...!!**EENS CHECKEN OF DE ARCHITECTUUR IN GROTE LIJNEN KLOPT** An overview of the full system is displayed in figure 2.



**Figure 2:** System architecture

The developed system uses three sensors:

- AMG8833: IR grid sensor
- CSS811: air quality sensors
- Sparkfun sound detector: microphone

By incorporating these sensors in to the system, a variety of sensor data is gathered, namely: ambient temperature [°C],  $CO_2$ -level [ppm], TVOC-level (total volatile organic compounds) [ppb] and sound level [db]. Next to this the AMG8833 captures the temperature af a two dimensional area in 8 by 8 pixels.

The 'brain' of the system is an ESP32, this microcontroller has an integrated Wi-Fi module, which will be used to transmit the data. The gathered data is sent to a server, which stores the received data in a database.

Alongside the reception of data from the ESP32, the server hosts a website which is used to display the data to the students. The website uses the pixel data to generate a heatmap of the cafeteria, this allows the students to see how many people are present in the cafeteria. Unfortunately one module cannot cover the entire cafeteria, to generate the heatmap. In order to do this, several modules have to be deployed in the cafeteria. In this project only one module will be constructed as a proof of concept. Next to the heatmap, the other sensor data is displayed on the website this includes: ambient temperature,  $CO_2$ -level, TVOC-level and the sound-level. Based on these parameters the students can gauge if the cafeteria is currently suitable as a study-location.

## 4 Power management design

This section explains the different trade-off's which were made in designing the power management part of the system. The first part in designing the power management is choosing a way to supply the circuit. In our case, the device needs to be deployed at the ceiling of a cafeteria. You can't just tap off the electricity cable at any point here, so our device will need a battery to supply the power. Our first aim was to supply the device as long as one semester. Another aspect was the ability to recharge the battery for environmental reasons. This excludes standard cell batteries that have a much lower energy density and are not rechargeable. Our choice was quickly made for the type of battery, namely a Lithium-Ion (Li-Ion) battery which will be discussed in section 4.1.

### 4.1 Lithium-Ion battery

Lithium-Ion batteries are now a commonly used battery in consumer electronics. Li-Ion batteries is the most commonly used battery in phones, MP3 players and other portable equipment. The voltage of a single Li-Ion battery cell is usually fixed at 3.6 V or 3.7 V. We call this the nominal voltage. However, the actual voltage during use can vary from 2.4 V to 4.2 V. When the voltage drops below 2.4 V, the cell is discharged too deeply and damaged beyond repair. Therefore, a safety voltage of 3 V is often maintained. If the cell is discharged to this voltage, nothing is wrong. Charging a Li-Ion battery usually takes 3 hours. Don't be blinded by fast chargers for these batteries, practical tests have shown that it takes 3 hours until a battery is fully charged [1]. A few benefits of a Li-Ion battery are:

- Very high energy density
- Minor self-discharge
- No memory effect

- High power, long service life

Some disadvantages are:

- Relatively expensive to purchase
- Dangerous if used incorrectly, can explode/combust
- Need a protection circuit to not drop below the 2.4 V threshold value
- Charging and discharging process needed

The most common Li-Ion battery is the 18650 cylindrical cell which is 18mm wide, 65mm long and the '0' stands for its cylindrical shape. Another common type of Lithium-Ion battery is the Lithium-Ion Polymer (Li-Po) battery. Li-Po's are preferred over standard Li-Ion batteries in application where weight reduction is important, fast charge opportunity is needed and which need a very high current during discharge time. Li-Po's are more used for drones (where lightweight is a requirement) and electric cars (fast charging requirement). Li-Po's are also less likely to combust or explode and are more expensive. Therefor a Li-Po would be overkill in our application [? 2? ].

#### 4.1.1 Selected battery

The reason we chose a single cell Li-Ion battery was:

- Voltage range: our microcontroller needs 3.3 V supply voltage, which is only a low dropout voltage of 0.4 V in comparison with the 3.7 V nominal voltage of a single cell Li-Ion battery. This results in less power dissipation in the voltage regulator.
- Rechargeable: for environmental aspects
- High capacity: around 3000 mAh, to last a semester

The specifications of the chosen NCR18650B are:

- Size/package: 18650
- Rated capacity: 3200 mAh
- Nominal voltage: 3.6 V
- Maximum voltage: 4.2 V
- Maximum charge current: 1625 mA
- Maximum discharge current: 6400 mA<sup>1</sup>

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<sup>1</sup>Maximum discharge rate is 2C. This means discharging the battery capacity in 0.5 hours  $\frac{3200mAh}{0.5h} = 6400mA$ .



- Maximum discharge voltage: 2.5 V
- Charge time: 4 hours
- No protection circuit

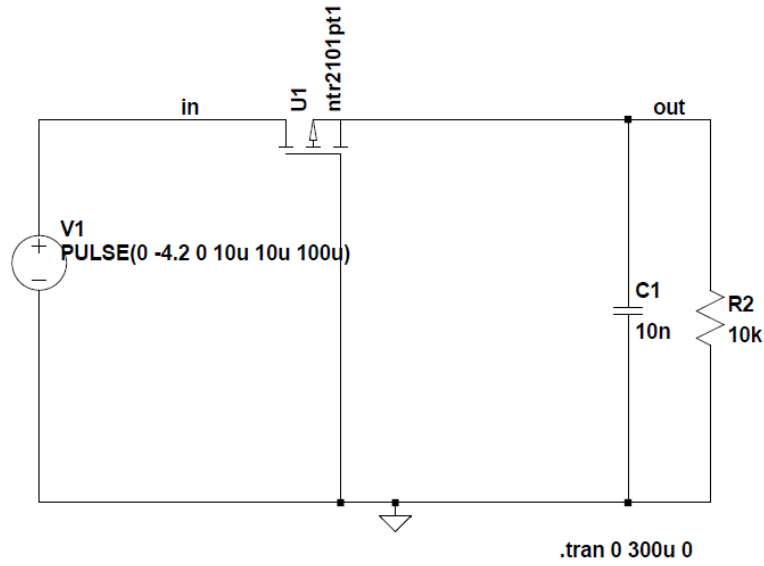
To charge the Li-Ion we had to include a charge circuit in our design. We found a high frequently used breakout board to charge a single cell Li-Ion battery via USB with battery protection here. Such a charge circuit would be perfect for our application. Due the reason we couldn't use a breakout board we had to integrate the components on one PCB. Unfortunately the components which were used on the breakout board were not available on the websites we're using to order components like Mouser, Digi-Key, Farnell, etc. After some research and a recommendation of a fellow student who had experience with battery charging applications in his master thesis, he advised to go for Texas Instruments IC's for charging Li-Ion batteries. The charger IC didn't had a protection circuit on it, so we also needed a circuit for this. Eventually we also went for a protection IC and voltage regulator of Texas Instruments. To protect the circuit for reverse polarity of the battery we also included an own-designed protection circuit which was first evaluated in LT Spice. All named components will be discussed in the following sections.

## 4.2 Reverse polarity protection

Reverse polarity protection is a nice feature to have to protect a circuit against polarity mismatches of the battery. For the design of this circuit we based us on a design found on the internet here. Before implementing this circuit in our design we first evaluated it's correct functioning using LT Spice in section 4.2.1.

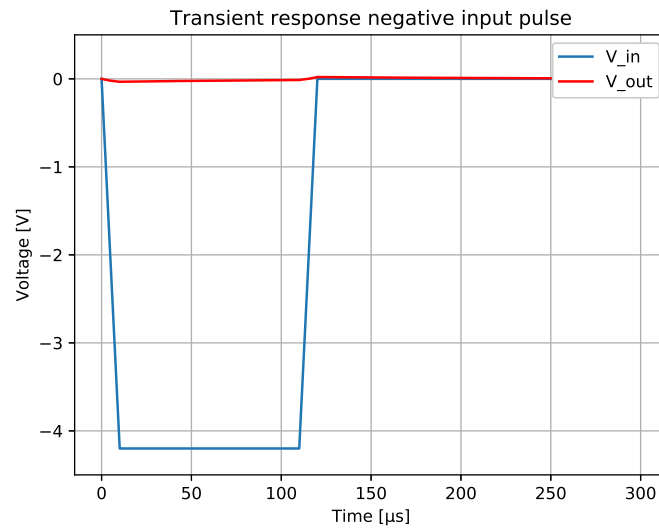
### 4.2.1 Simulation

Reverse polarity protection is simple done by including a P type MOSFET as shown in figure 3. Since the maximum voltage is limited to 4.2 V of the battery, there is no need for high drain-to-source voltage  $V_{DS}$  requirements for the MOSFET. A suitable MOSFET was found [3]. Normally there should be a zener diode placed between gate and source to protect the maximum gate-to-source voltage  $V_{GS}$ . Since the selected MOSFET's  $V_{DS} = V_{GS} = 8$  V there is no need for a zener diode to clamp the voltage.



**Figure 3:** Simulation reverse polarity protection circuit

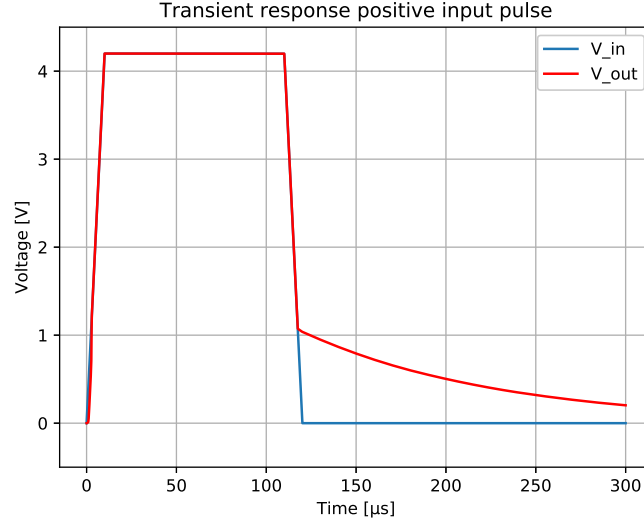
Figure 4 shows the transient response when applying a negative pulse at the input. As can be seen in the figure, the negative pulse doesn't come through the rest of the circuit. The voltage at the output is 0 V.



**Figure 4:** Transient response negative input pulse

When applying a positive pulse at the input, it can be seen in figure 5 the output follows the input. We can evaluate the circuit works properly to protect against reverse polarity protection. Now it can be implemented in

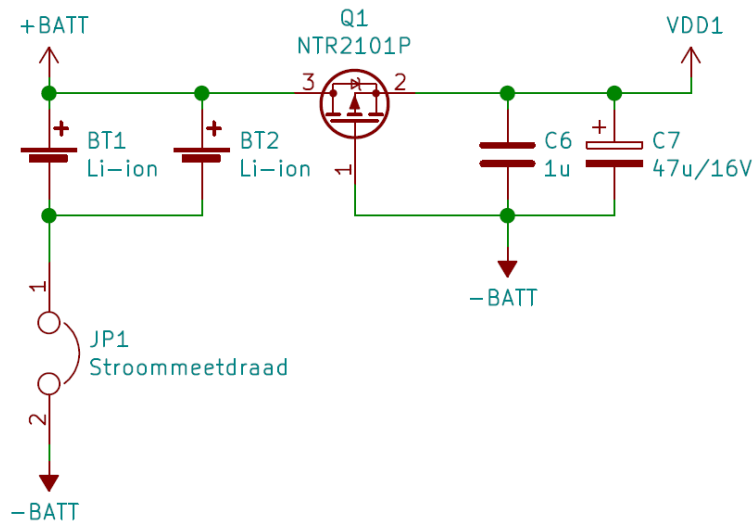
our design discussed in section 5.



**Figure 5:** Transient response positive input pulse

#### 4.2.2 Implementation

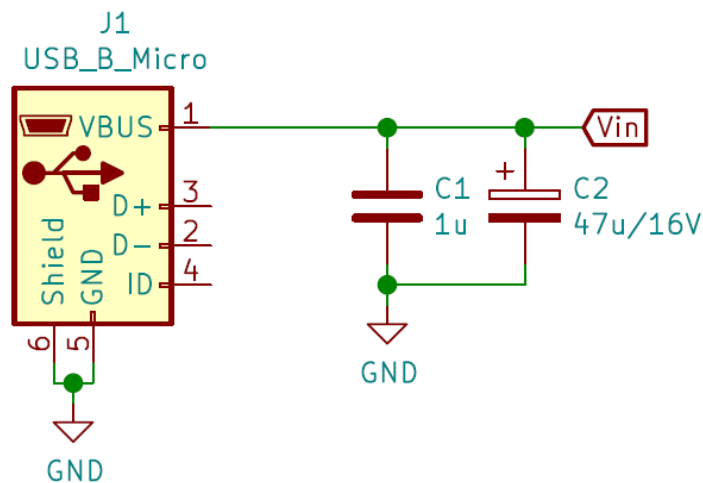
As a precaution we included two batteries in the first version of our design. This was done for debugging reasons: in case our real current consumption would be too high after trying every possibility to reduce it in software, we had an extra battery to meet our lifetime goal. It was possible to include an extra battery because the PCB dimensions were still lesser than 100 x 100 mm. JP1 is a footprint to solder a wire so we are able to measure the current using a current probe. When the battery is correct polarity of the battery is applied, +BATT is connected to VDD1.



**Figure 6:** Reverse polarity protection circuit

### 4.3 Charging choice

For charging you're free to choose at which voltage and current you charge. Eventually a Li-Ion charger IC will step down the voltage to the maximum 4.2 V for a cell. For charging you could design your own AC-DC converter, we went for the ability to charge the device using USB. Here for we rely on a power adapter which transforms 240 VAC to 5 VDC, or the ability to charge our device using a USB port on a computer. Figure 7 shows the input connector micro USB type B with two decoupling capacitors  $C_1$  and  $C_2$ . The charging voltage source is labeled as  $V_{in}$ .



**Figure 7:** Micro USB type B input

## 4.4 Battery charging circuit

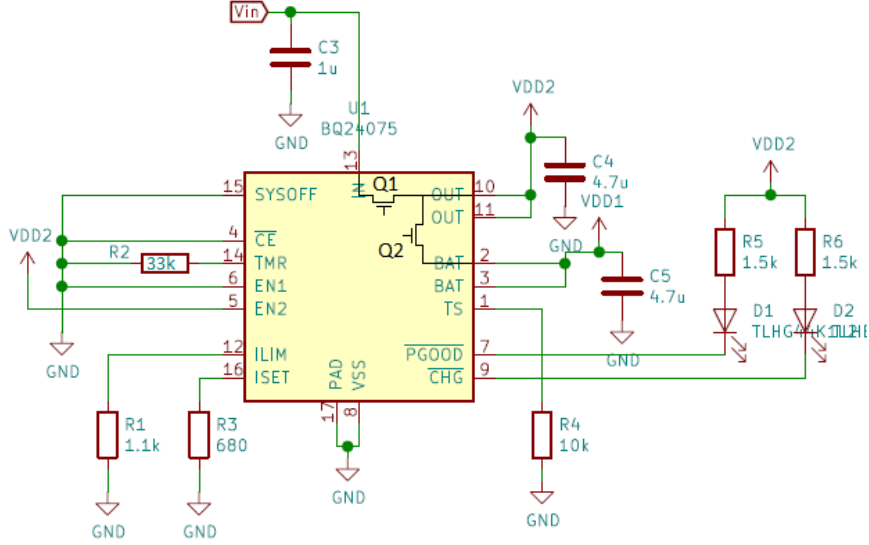
We considered many chips from different kind of manufacturers. As previously said a TP4056 IC charger is commonly used for single cell Li-Ion batteries, but it's not available on Digi-Key, Farnell, etc. Eventually we went with the BQ24075 IC from Texas Instruments. It's a great choice because it's made to charge a single cell Li-Ion battery, and it's perfectly fit to charge using a USB port. The IC operate from either a USB port or an AC adapter and support charge currents up to 1.5 A. The input voltage range with input overvoltage protection supports unregulated adapters. The USB input current limit accuracy and start up sequence allow the BQ24075 to meet USB-IF inrush current specifications<sup>2</sup>. Additionally, the input dynamic power management (VIN-DPM) prevents the charger from crashing incorrectly configured USB sources. An additional specification that was decisive in the choice of charger IC was the availability of 2 pins for status indication:

1. **power good indication:** if the input voltage  $V_{in}$  is in specified range.
2. **charge indication:** if the charger is charging (bright up LED) and when the charge cycle is complete (quench LED)

Figure 8 shows the BQ24075 IC implemented in our design. A green LED D1 indicates the power good signal, and blue LED D2 indicates the charging stage. When no voltage is applied at the input  $V_{in}$ , the internal transistor Q1 is opened and Q2 is closed. Therefore VDD1 is connected to VDD2. During charge cycle both transistors Q1 and Q2 are closed allowing the battery to charge. The BQ24075 feature a SYSOFF input that allows the user to turn Q2 off and disconnect the battery from the OUT pin. This is useful for disconnecting the system load from the battery, factory programming where the battery is not installed or for host side impedance track fuel gauging, where the battery open circuit voltage level must be detected before the battery charges or discharges. We don't use this feature so we connect SYSOFF to GND to close Q2 for normal operating mode [4]. The other features of BQ24075 and schematic components will be discussed in sections 4.4.1 to 4.4.6.

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<sup>2</sup>[http://www.testusb.com/inrush\\_issue.htm](http://www.testusb.com/inrush_issue.htm)



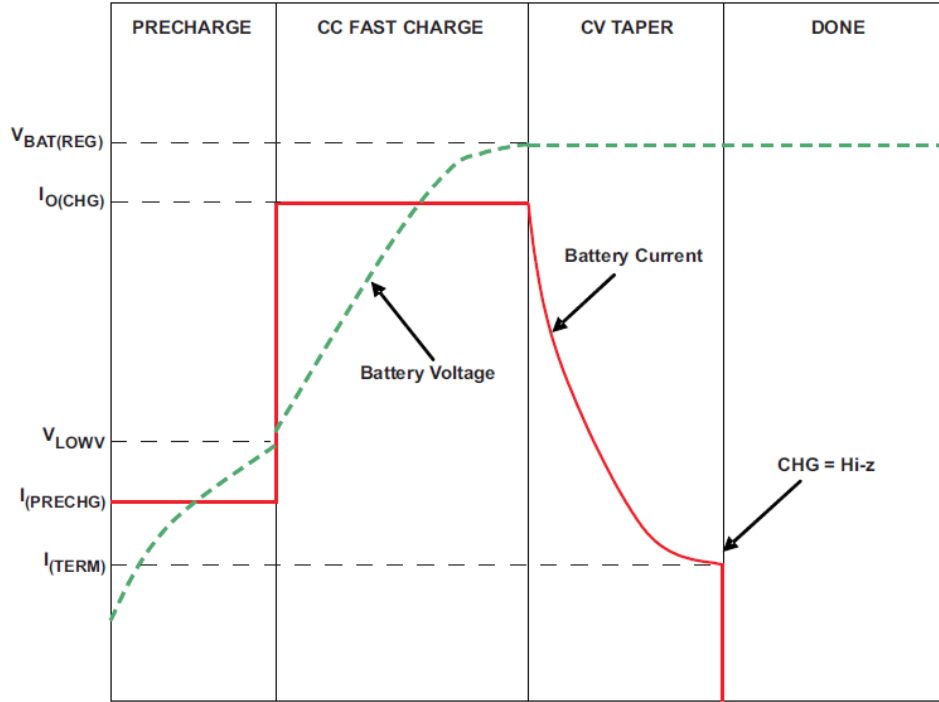
**Figure 8:** Typical application circuit BQ24075

#### 4.4.1 Charging phases

Set  $\overline{CE}$  low to initiate battery charging. The battery is charged in three phases:

1. Conditioning pre-charge
2. Constant current (CC) fast charge (current regulation)
3. Constant voltage (CV) tapering (voltage regulation)

Figure 9 illustrates the three charging phases. In the pre-charge phase, the battery is charged at with the pre-charge current  $I_{PRECHG}$ . Once the battery voltage crosses the  $V_{LOWV}$  threshold, the battery is charged with the fast-charge current  $I_{CHG}$ . As the battery voltage reaches  $V_{BAT(REG)}$ , the battery is held at a constant voltage of  $V_{BAT(REG)}$  and the charge current tapers off as the battery approaches full charge. When the battery current reaches  $I_{TERM}$ , the CHG pin indicates charging done by going high-impedance.



**Figure 9:** Charge cycle [4]

#### 4.4.2 Set input current limit $I_{LIM}$

The BQ24075 IC offers a fully compliant USB charger, meaning:

1. Selectable 100 mA and 500 mA maximum input current
2. 100 mA Maximum current limit ensures compliance to USB-IF standard
3. Input-based dynamic power management (VINDPM) for protection against poor USB sources

As shown in table 1, EN1 and EN2 are used to configure the USB charge current.

**Table 1:** EN1/EN2 Settings [4]

EN2	EN1	MAXIMUM INPUT CURRENT INTO IN PIN
0	0	100 mA. USB100 mode
0	1	500 mA. USB500 mode
1	0	Set by an external resistor from ILIM to VSS (max. 1.5 A)
1	1	Standby (USB suspend mode)

USB1.0 specifications allow devices to draw up to 500 mA from one port. USB operates at 5V, so that means a maximum of 2.5 watts. USB 2.0 has the same power limit. But later there were add-ons to the spec for battery charging, allowing up to 1.5A (7.5W) while data transfer is going on, and up to 5A if not. Few USB 2.0 devices can deliver that much power. Also note that the Micro USB connector is only rated to carry 2.1A (10.5W). USB 3.0 increases the power limit to 900mA (4.5W). The battery charging spec from USB 2.0 can optionally be supported [5]. Since almost all USB chargers and ports are 2.0 and 3.0 nowadays, we can step up the current above 500 mA. The value of the input current limit  $I_{LIM}$  is set by the resistor connected from the ILIM pin (pin 12) to VSS, and is given by [4]

$$R_{ILIM} = \frac{K_{ILIM}}{I_{LIM}}, \quad (1)$$

with

$$K_{ILIM} = 1610A\Omega. \quad (2)$$

The valid resistor range is 1.1 k $\Omega$  to 8 k $\Omega$ . A value of 1.1 k $\Omega$  results in an input current limit

$$I_{LIM} = \frac{1610A\Omega}{1.1k\Omega} = 1.46A. \quad (3)$$

The maximum input current limit 1.5 A is reached. **Caution:** make sure this current doesn't exceed the value of the maximum charge current of the battery, which is in our case within the permitted limit of 1625 mA (section 4.1.1).

#### 4.4.3 Fast charge safety timer (TMR)

TMR controls the pre-charge and fast-charge safety timers. Leave TMR open to set to default safety timers. Connect to VSS to disable safety timers. Connect a 18 k $\Omega$  to 72 k $\Omega$  resistor between TMR and VSS to program the timers a desired length. Reset the timers by toggling the CE pin, or by toggling EN1, EN2 pin to put the device in and out of USB suspend mode (EN1 = 1, EN2 = 1). The charge time of the battery is 4 hours (section 4.1.1). We will calculate the TMR resistor  $R_{TMR}$  to meet the desired charge time of 4 hours, using equation [4]

$$R_{TMR} = \frac{t_{MAXCHG}}{10 \cdot K_{TMR}}, \quad (4)$$

with

$$K_{TMR} = 48 s/k\Omega, \quad (5)$$

$$t_{MAXCHG} = 4hr. \quad (6)$$



$$R_{TMR} = \frac{t_{MAXCHG}}{10 \cdot K_{TMR}} = \frac{4 \text{ hr} \cdot 3600 \text{ s/hr}}{10 \cdot 48 \text{ s/k}\Omega} = 30 \text{ k}\Omega \quad (7)$$

Select a resistor value of 33 k $\Omega$ , so it's E6-E12 compliant and to extend its charge time a little bit. Connect this resistor between TMR (pin 2) and VSS.

#### 4.4.4 Set fast charge current $I_{CHG}$

The value of fast-charge current  $I_{CHG}$  is set by the resistor connected from the ISET pin to VSS, and is given by [4]

$$R_{ISET} = \frac{K_{ISET}}{I_{CHG}}, \quad (8)$$

with

$$K_{ISET} = 890 \text{ A}\Omega. \quad (9)$$

The charge current limit is adjustable up to 1.5 A. The valid resistor range is 590  $\Omega$  to 8.9 k $\Omega$ . If  $I_{CHG}$  is programmed as greater than the input current limit  $I_{LIM}$ , the battery will charge at the rate of  $I_{LIM}$  instead of  $I_{CHG}$ . In this case, the charger timers will be proportionately slowed down. The maximum charge current for the Panasonic NCR18650B battery is 1625 mA (section 4.1.1). Set charge current to 1.3 A to have some margin for the battery lifetime and calculate the resistor value

$$R_{ISET} = \frac{890 \text{ A}\Omega}{1.3 \text{ A}} = 684.62 \Omega \approx 680 \Omega. \quad (10)$$

Select the closest standard value (E6,E12,...), which for this case is 680  $\Omega$ . Connect this resistor between ISET (pin 16) and VSS.

#### 4.4.5 TS function

The TS-pin is the external NTC thermistor input. Connect the TS input to the NTC thermistor in the battery pack. TS monitors a 10 k $\Omega$  NTC thermistor. For applications that do not use the TS function, connect a 10 k $\Omega$  fixed resistor from TS to VSS to maintain a valid voltage level on TS.

#### 4.4.6 Selecting IN-, OUT-, and BAT-pin capacitors

In most applications, all that is needed is a high-frequency decoupling capacitor (ceramic) on the power pin, input, output and battery pins. Using the values shown on figure 8 (these are taken from the typical application circuit in [4]) is recommended. After evaluation of these voltage signals with real system operational conditions, one can determine if capacitance values

can be adjusted toward the minimum recommended values (DC load application) or higher values for fast high amplitude pulsed load applications. Note if designed high input voltage sources (bad/wrong adaptors), the capacitor needs to be rated appropriately. Ceramic capacitors are tested to 2x their rated values so a 16-V capacitor may be adequate for a 30-V transient (verify tested rating with capacitor manufacturer).

#### 4.5 Battery protection circuit

Due the battery we selected doesn't has an integrated protection circuit, we also needed to consider a battery protection circuit in our design. As discussed in section 4.1 it could lead to battery defect when the voltage of the battery drops below 2.4 V threshold value. A Li-Ion is also likely to explode/combust when charging too high in voltage or current. Therefore a protection circuit is always needed. We went for the BQ29700 which is a battery cell protection IC that provides an accurate monitor and trigger threshold for overcurrent protection during high discharge/charge current operation or battery overcharge conditions. The BQ29700 provides the protection functions for Li-Ion/Li-Po cells, and monitors across the external power FETs for protection due to high charge or discharge currents. Figure 10 shows a typical application circuit of the BQ29700 IC. In normal mode FETs Charge FET (CHG) and Discharge FET (DSG) are closed, however in one of the following conditions the FETs will open to stop the current flow from/to the battery:

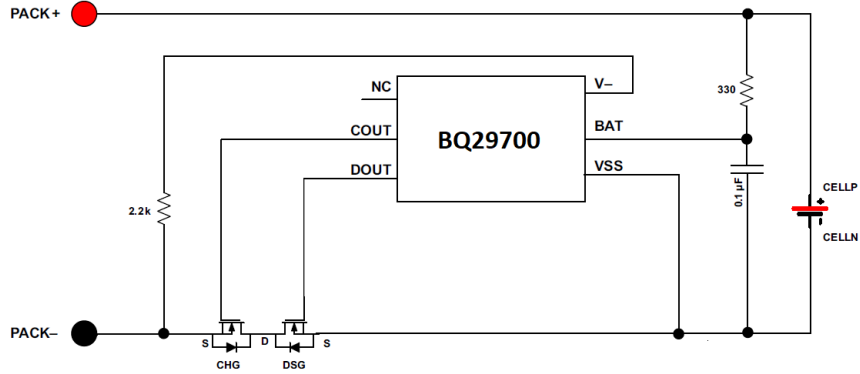
1. **Overcharge detection (OVP):** When the cell exceeds the overcharge detection threshold voltage  $V_{OVP}$  during charge, the safety circuit will interrupt the flow of current into the cell. When the overcharge voltage is exceeded, a delay of up to  $t_{OVP}$  will occur before the FETs open the circuit.
2. **Over-discharge detection (UVP):** When the cell exceeds the over-discharge detection threshold voltage  $V_{UVP}$  during discharge, the safety circuit will interrupt the flow of current out of the cell. When the over-discharge voltage is reached, a delay  $t_{UVP}$  will occur before the FETs open the circuit.
3. **Charge overcurrent detection (OCC):** When the pack output current the charge overcurrent detection threshold voltage  $V_{OCC}$  during charge, the safety circuit will interrupt the flow of current out of the pack. When the charge overcurrent threshold voltage is exceeded, a delay of up to  $t_{OCC}$  will occur before the FETs open the circuit.
4. **Discharge overcurrent detection (OCD):** When the pack output current the discharge overcurrent detection threshold voltage  $V_{OCD}$  during discharge, the safety circuit will interrupt the flow of current

out of the pack. When the discharge overcurrent threshold voltage is exceeded, a delay of up to  $t_{OCD}$  will occur before the FETs open the circuit.

5. **Load short-circuit detection (SCD):** Similar to overcurrent threshold values, except a short circuit will result in a much higher current, thus a higher sense voltage. The short-circuit detection threshold voltage is indicated as  $V_{SCD}$  with delay  $t_{SCD}$ .

Specifications of the BQ29700 IC are [6]:

- $V_{OVP} = 4.275$  V
- $t_{OVP} = 1.25$  s
- $V_{UVP} = 2.8$  V
- $t_{UVP} = 144$  ms
- $V_{OCC} = -0.1$  V
- $t_{OCC} = 8$  ms
- $V_{OCD} = 0.1$  V
- $t_{OCD} = 20$  ms
- $V_{SCD} = 0.5$  V
- $t_{SCD} = 250$   $\mu$ s



**Figure 10:** Typical application circuit BQ29700 [6]

#### 4.5.1 Dimensioning

Figure 11 shows the implemented BQ29700 IC in our design. An RC filter is required on the BAT-pin for noise, and enables the device to operate during sharp negative transients. The 330  $\Omega$  resistor also limits the current during a reverse connection on the system. TI recommends placing a high impedance 5 M $\Omega$  across the gate source of each external FET to deplete any charge on the gate-source capacitance. The voltage sense node  $V_-$  is a sense node used for measuring several fault detection conditions, such as overcurrent charging or overcurrent discharging configured as Vds sensing for protection. This input, in conjunction with VSS, forms the differential measurement for the stated fault detection conditions. A 2.2 k $\Omega$  resistor is connected between this input pin and Pack- terminal of the system in the application.

**FET Selection:** These should be MOSFETs who operate at relatively low voltages (2.8-4.2V battery cell) and that can handle a current of 1.3 A for charging (section 4.4.4). Due the current is measured by the voltage drop across the FETs, it's  $R_{DS(ON)}$  value is also an important value by choosing the right MOSFET. We chose FDS9926A, as it's a dual N-channel MOSFET IC. So both charge and discharge MOSFETs are integrated in one IC. Each FET's  $R_{DS(ON)} = 35 \text{ m}\Omega$  at  $T_j = 25^\circ\text{C}$  and  $V_{gs} = 3.7 \text{ V}$  (nominal battery voltage) [7]. Because both discharge and charge overcurrent detection levels are the same (100 mV), the discharge and charge current are limited to approximately  $\frac{100\text{mV}}{2 \cdot 35\text{m}\Omega} = 1.43 \text{ A}$  [6, 7].

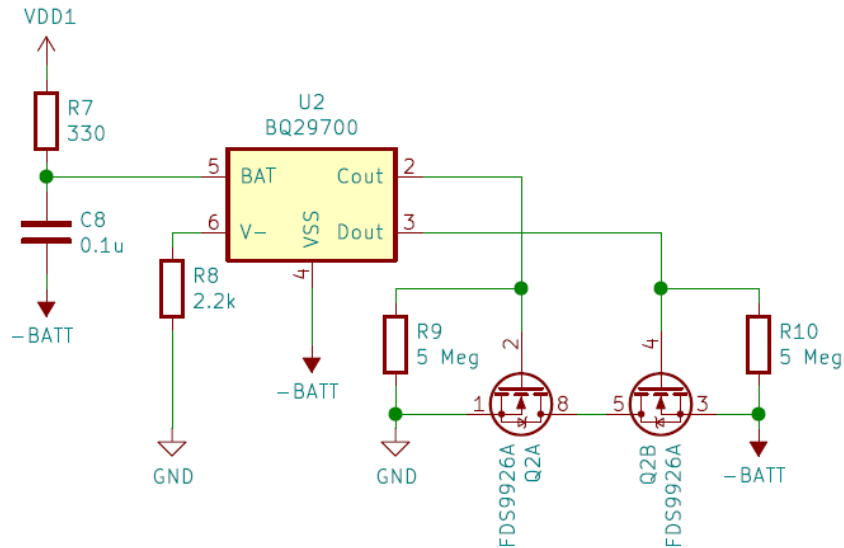


Figure 11: BQ29700 applied schematic

## 4.6 Voltage regulator

A few important points to consider when selecting the voltage regulator are:

1. Low quiescent current<sup>3</sup>  $I_Q$  to reduce power losses for extended battery lifetime.
2. Low dropout voltage<sup>4</sup>  $V_{DO}$  due to the small difference between the 3.7 V nominal voltage of the battery and 3.3 V supply voltage for the ESP32 microcontroller.
3. At least 500 mA maximum output current  $I_{OUT,MAX}$  needed for ESP32 spikes [8].

In low power applications a linear regulator is preferred over a switching regulator due the fact switching converters are inefficient at very low loads, and power dissipation in the linear regulator is also low when combined with a low dropout voltage ( $P^{\downarrow\downarrow} = U_{DO}^{\downarrow} \cdot I^{\downarrow}$ ). Linear regulators also have much lower quiescent currents in comparison to switching regulators [9, 10]

### 4.6.1 Selected regulator

As shown in figure 12 we chose TLV75533 from Texas Instruments, with following parameters:

- $I_Q = 25 \mu\text{A}$  (Typical)
- $V_{DO} = 150\text{-}238 \text{ mV}$  (@  $I_{OUT} = 500 \text{ mA}$  and  $V_{OUT} = 3.3 \text{ V}$ )
- $I_{OUT,MAX} = 500 \text{ mA}$

This device features an internal soft-start to lower inrush current, thus providing a controlled voltage to the load and minimizing the input voltage drop during start up. When shutdown, the device actively pulls down the output to quickly discharge the outputs and ensure a known start-up state. For protection reasons the TLV75533 has an integrated thermal shutdown, current limit, and undervoltage lockout (UVLO).

Additionally, the TLV75533 has an enable functionality to minimize standby power. Unfortunately we can't use this function because the LDO supplies the microcontroller (these control signals to drive the enable pin should originate from the microcontroller). Therefor the enable pin is connected to the input pin to enable when an input voltage is supplied.

---

<sup>3</sup>Current which is flowing though the converter when no load is applied.

<sup>4</sup>The Dropout Voltage of a regulator is the amount of voltage that a regulator needs to be fed above its rated output voltage to maintain the output voltage.

The TLV75533 requires an output capacitance of 0.47-200  $\mu\text{F}$  for stability. Use X5R- and X7R-type ceramic capacitors because these capacitors have minimal variation in capacitance value and equivalent series resistance (ESR) over temperature. Place a 1  $\mu\text{F}$  or greater capacitor on the input pin of the LDO. Some input supplies have a high impedance. Placing a capacitor on the input supply reduces the input impedance [11].

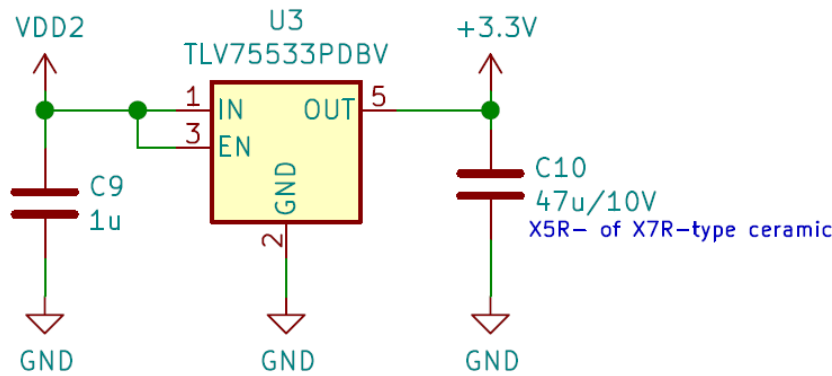


Figure 12: TLV75533 applied schematic

#### 4.7 Load switches

To reduce power even further you can disable the sensors by shutting off their supply voltage if they're not needed. This can be done by load switches or relays. A load switch is a small electronic switch used to configure and manage power distribution. You can make a load switch with discrete components, but there are significant advantages to using a fully integrated IC load switch [12]:

1. **Saves space:** A key advantage of the integrated device over discrete load switches is the small footprint.
2. **Simpler design:** No discrete design time is required. Just buy the integrated chip and design it in to get all benefits and features.

Load switches also have several advantages over relays [12]:

1. **Quick output discharge:** An internal resistance in the form of a conducting MOSFET is connected across the load. It serves to discharge to the output capacitor quickly when the enable input goes low.
2. **Reverse-current blocking:** Some IC load switches implement a feature that blocks any reverse current. When the enable input goes low to turn off the switch, the reverse current block circuit is enabled

thereby reducing any potential reverse current from output back to input to a very low level.

3. **Saves power:** Using load switches to manage the power output of the supply minimizes power consumption, saves energy, and provides for longer battery life in portable applications. In its off state, the IC draws minimal quiescent current.
4. **Manages inrush current:** This feature prevents input voltage droop that may transpire when the switch is first turned on. This is the result of a high inrush current that occurs when charging the output capacitor. Most load switches provide a controlled ramp up of the output voltage as it charges the output capacitor.
5. **Implements sequencing:** Load switches let you implement the sequencing of loads during a turn-on or turn-off operation. Some designs with processors, FPGAs, and other chips require that different supply voltages be applied or disconnected in a specific order. Multiple load switches for each supply that are operated by the related embedded controller for timing meet this need. Certain load switches also feature an output signal that indicates when the output is fully turned on. This signal can be used in sequencing operations with other load switches in the system.

#### 4.7.1 Selected load switches

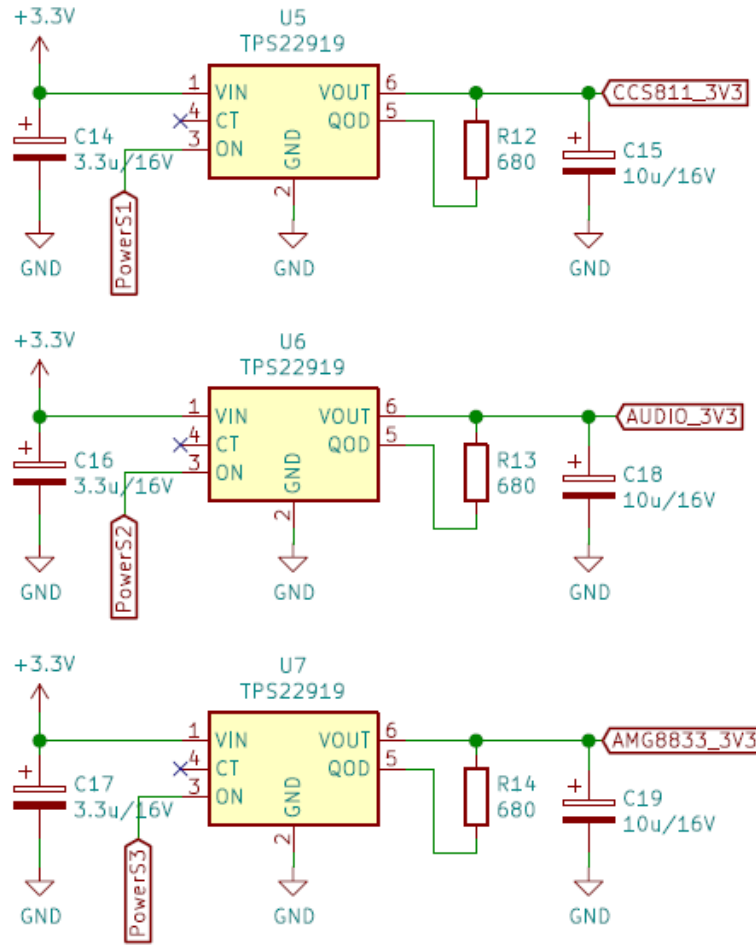
The TPS22919 device is a small, single channel load switch with controlled slew rate. The device contains an N-channel MOSFET that can operate over an input voltage range of 1.6 V to 5.5 V and can support a maximum continuous current of 1.5 A. A few important specifications are [13]:

- Input operating voltage range  $V_{IN}$ : 1.6 V to 5.5 V
- Maximum output current  $I_{OUT,MAX} = 1.5$  A
- Low power consumption:
  - ON-state  $I_Q = 8$   $\mu$ A (typical)
  - OFF-state  $I_{SD} = 2$  nA (typical)
- On-Resistance  $R_{ON}$ : 89 m $\Omega$  (typical) @  $V_{IN} = 5$  V

The switch ON state is controlled by a digital input that is capable of interfacing directly with low-voltage control signals. When power is first applied, a Smart Pull Down is used to keep the ON pin from floating until system sequencing is complete. Once the pin is deliberately driven High ( $> V_{IH}$ ), the Smart Pull Down will be disconnected to prevent unnecessary power

loss. The TPS22919 load switch is also self-protected, meaning that it will protect itself from short circuit events on the output of the device. It also has thermal shutdown to prevent any damage from overheating.

Figure 13 shows the application of TPS22919 for our 3 sensors. The resistor between VOUT and QOD pin is a quick discharge resistor to discharge the output capacitor when the enable pin goes low. For both in- and output capacitors, and the resistor, we used the recommended value as given in the datasheet [13].



**Figure 13:** TPS22919 applied schematic



## 5 Microcontroller

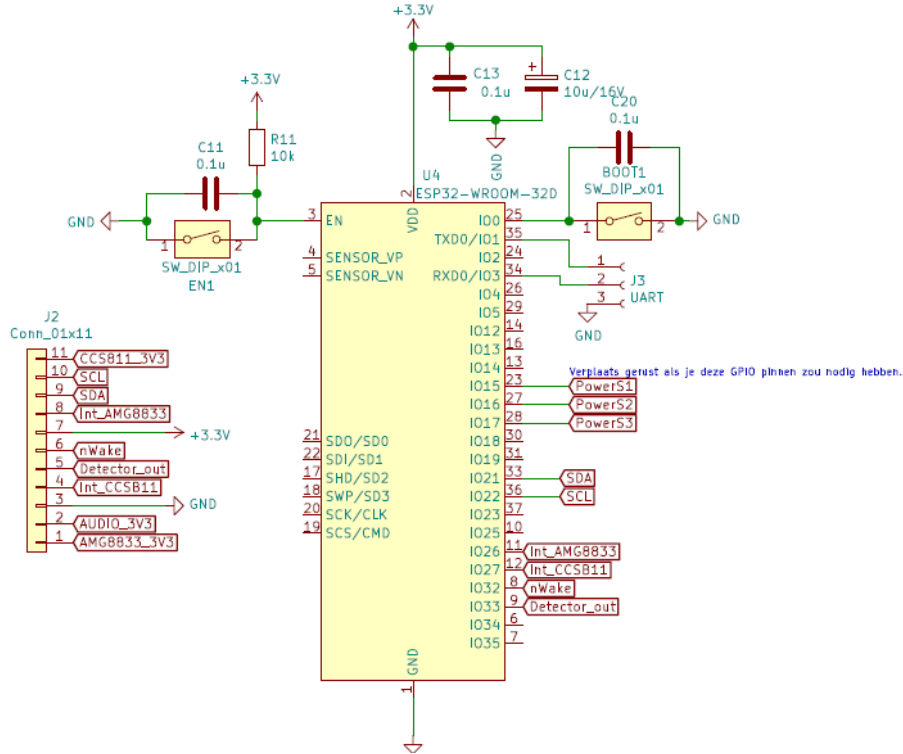


Figure 14: ESP32 applied schematic

## 6 Sensorboard

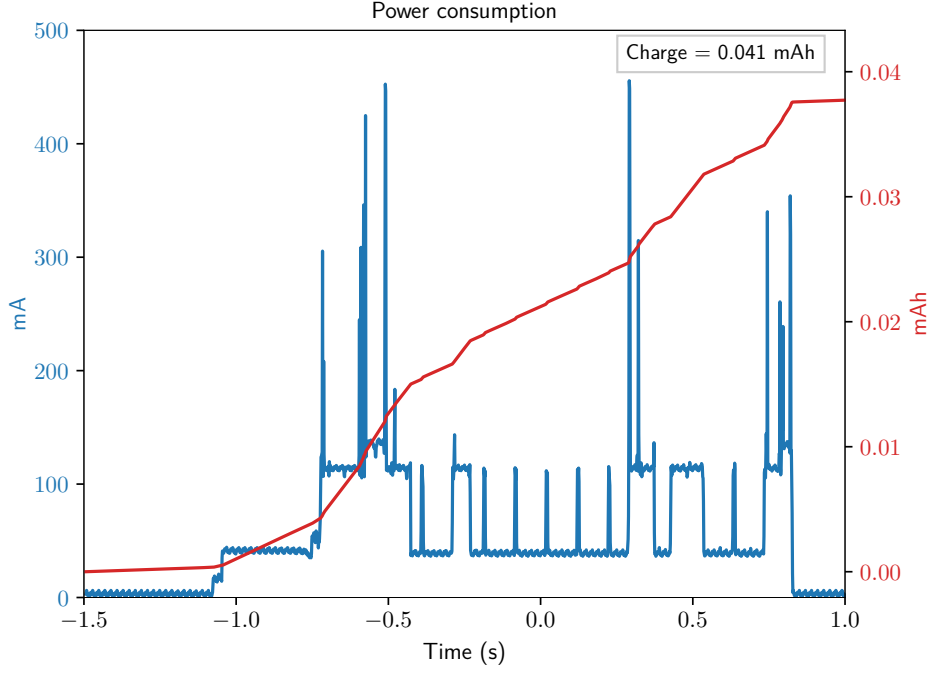
## 7 Wireless connectivity

### 7.1 Wi-Fi connection

In order to transmit the sensor data to the server, the Wi-Fi connectivity of the ESP32 is used. The transmission is provided by a TCP connection that is established between the ESP32 and the python server. At the initialisation of the python server, a socket is opened, this socket is used to receive the data. In this manner, the server is always listening on the socket, until a message is received. The ESP32 sends the data in the following order: pixeldata (64 floats), temperature (1 float), audio level (1 float),  $CO_2$ -level (1 uint16) and TVOC-level (1 uint64). The received data is processed by order to determine which data is represented by the received values. The data is parsed into different variable, these variables are then used to update the values in the database.

## 7.2 Power consumption

To determine the power that is consumed when the sensor data is transmitted once, a measurement is performed. The current consumption is measured, the result is displayed in figure 15.



**Figure 15:** Power consumption of one Wi-Fi transmission

In order to interpret the current consumption, the used capacity is displayed in [mAh]. This results in 0.041 mAh of capacity that is used in order to transmit the sensor data once. With this knowledge, we can calculate the amount of Wi-Fi transmissions that are possible with the 6400 mAh battery:

$$\frac{6400}{0.041} \approx 156097$$

156097 transmissions are possible, if there are 6 transmissions per hour and the system is active for 7 hours a day, this leads to a battery life off 3716 days. However, this calculation only accounts for the Wi-Fi transmission other power consumption such as stand-by power, CPU power and sensor power are not accounted for in the calculation.

## 8 Software design

### Functionality

- Pull sensors from sleep state every 10 minutes and read sensor values
- Send sensor data to server, over Wi-Fi
- Perform periodic synchronisations to get time information
- Use time information to disable power to sensors and put CPU in deepsleep during the night

### Overview

The software is based on a number of states these states are: NTPsync, checktime, nightsleep, wakefromnightsleep, wakesensors, readsensors, senddata and sleep. An overview of the complete software and the transitions between the states is illustrated in figure 16. The states are discussed further below.

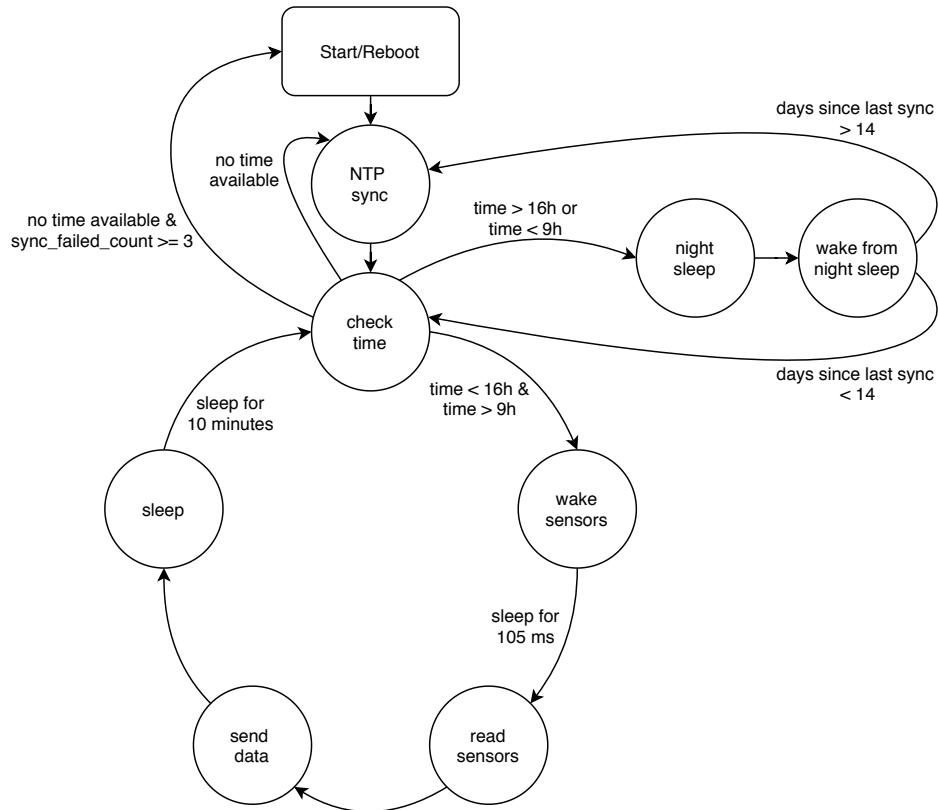


Figure 16: State diagram

### **NTP-sync**

In this state an NTP synchronisation is performed. This provides time information which is stored in the RTC memory and maintained by the RTC clock. The time information allows the system to know when it is night time. During the night the sensors can be disabled, using the load switches, and the microcontroller can go in to deepsleep until the morning. This way the sensors only receive power between 9 AM and 4 PM.

### **Check time**

This state has two functionalities. Firstly the current time of day is retrieved from the RTC clock. If this time info is not available, the NTP synchronisation was not successful. When this is the case the microcontroller goes in to deepsleep for five minutes and the next state will be the NTP sync to retry the synchronisation. If the synchronisation fails three times, the system is rebooted. Next to this, when the synchronisation was successful, the time information will be available. This time information is then used to check the current time. If the time is between 9 AM and 4 PM the system remains active, thus the next state is set to wakesensors. If the time is after 4 PM and before 9 AM, the system has to go to sleep, thus the next state is set to nightsleep.

### **Night sleep**

This state is entered when it is past 4 PM and before 9 AM. During this time the sensors are disabled and the microcontroller goes in deepsleep. The sensors are disabled by raising the GPIO pins which control the load switches. When the GPIO pins are high, the load switches cut off the power to the sensors. Before entering deepsleep, the next state is set to wakefromnightsleep. During the night, no sensor data has to be collected and transmitted because the campus is closed. So by cutting off the power to the sensors and putting the microcontroller in deepsleep during the night the power consumption is drastically reduced.

### **Wake from night sleep**

When the system wakes up at 9 AM, the power to the sensors has to be enabled. This is done by lowering the GPIO pins which control the load switches. Next to this, the system checks when the last synchronisation was performed. Because the RTC clock is derived from an internal RC oscillator with a frequency of 150 kHz and an accuracy of  $\pm 5\%$  the clock time will drift away from the actual time. In order to prevent this, an NTP synchronisation has to be performed periodically. In order to retain an accurate clock, the synchronisation is performed every 14 days. Thus if

the last synchronisation was performed 14 days ago, the next state is set to NTPsync. If the last synchronisation was more recent, the next state is set to checktime.

### **Wake sensors**

In the wake sensors state, the sensors are taken out of their sleep state and put in active mode. When the sensors wake from their sleep state the sensor values can not be read immediately. A waiting period of 105 milliseconds is necessary in order to have stable sensor values. During these 105 milliseconds the sensors remain active but the microcontroller is put into deepsleep mode. Before entering deepsleep, the next state is set to readsensors.

### **Read sensors**

In this state the sensor values are read out. Once the data is acquired, the sensors are put back in to their sleep state and the next state is set to senddata.

### **Send data**

In this state, the sensor data is transmitted to the python server which is running on a raspberry pi. Once the transmission is successful or the connection has timed-out the next state is set to sleep.

### **Sleep**

Once the sensor data has been transmitted to the server, the sleep state is entered. In this state, the microcontroller is put into deepsleep for 10 minutes. Before entering deepsleep, the next state is set to check time.

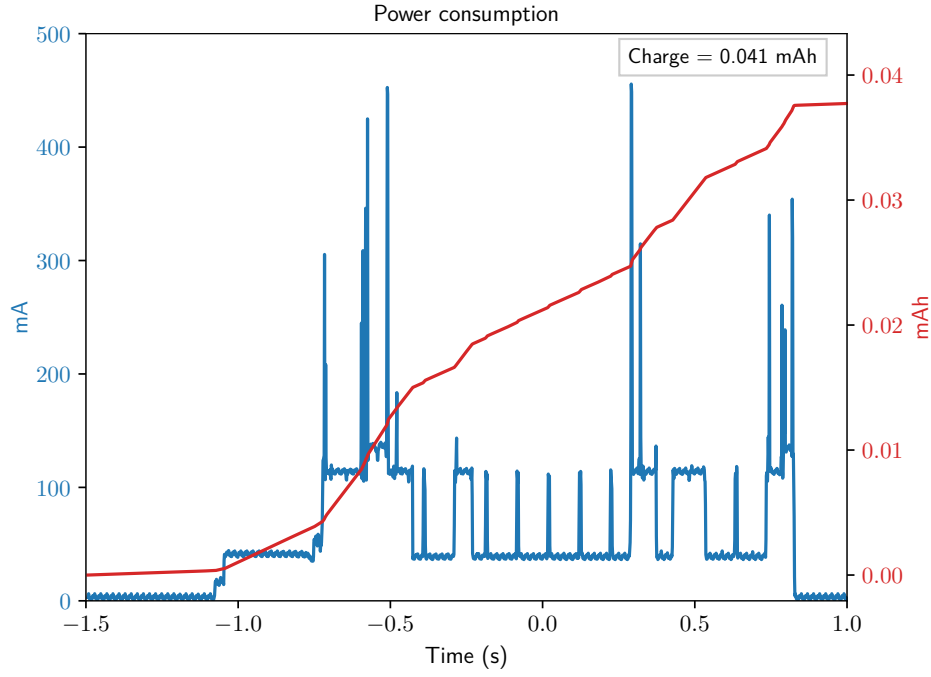
## **9 Autonomy**

### **9.1 Consumption sources**

In this section the different sources that consume power will be discussed.

#### **Wi-Fi communication**

The system transmits the sensor data to the server over a Wi-Fi connection. This data transfer happens every 10 minutes. Because the sensors are disabled between 4 PM and 9 AM, no Wi-Fi connection is needed during that time. With a wake time of seven hours and 6 transmissions per day, this leads to 42 transmissions per day. A measurement of the typical power consumption for one Wi-Fi transmission is illustrates in figure 17. The charge



**Figure 17:** Power consumption of one Wi-Fi transmission

that is used for one transmission is 0.041 mAh. This leads to the following consumption per day:

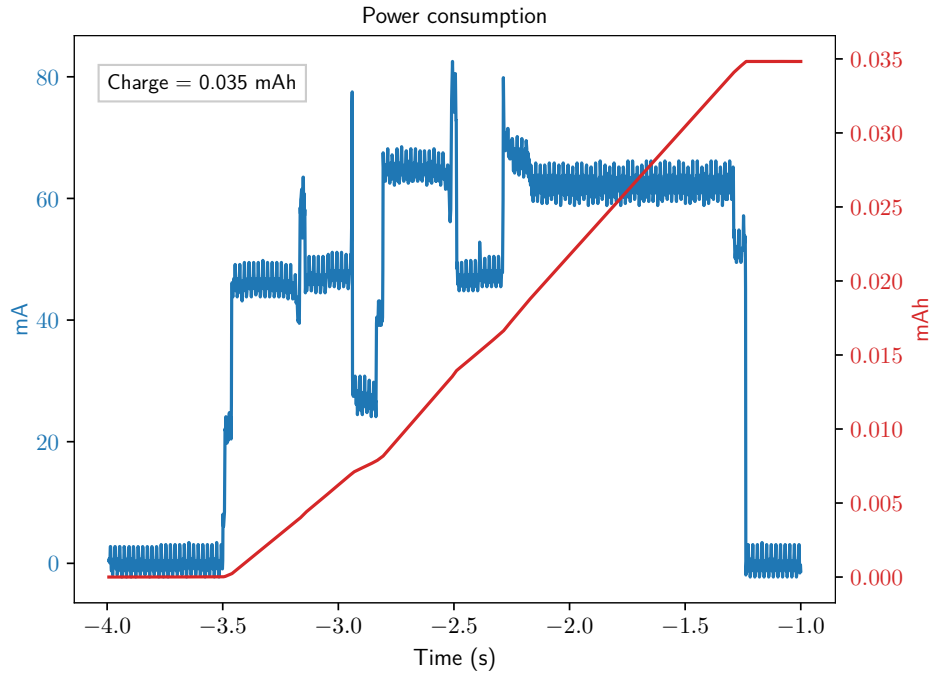
$$42 \cdot 0.041 = 1.722 \text{ mAh/day}$$

### Sensors

The sensors are read out every ten minutes. With a wake time of 7 hours<sup>5</sup>, this leads to 42 sensor measurements per day. The power consumption to read out the sensors once is illustrates in figure 18.

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<sup>5</sup>Only awake between 9 AM and 4 PM



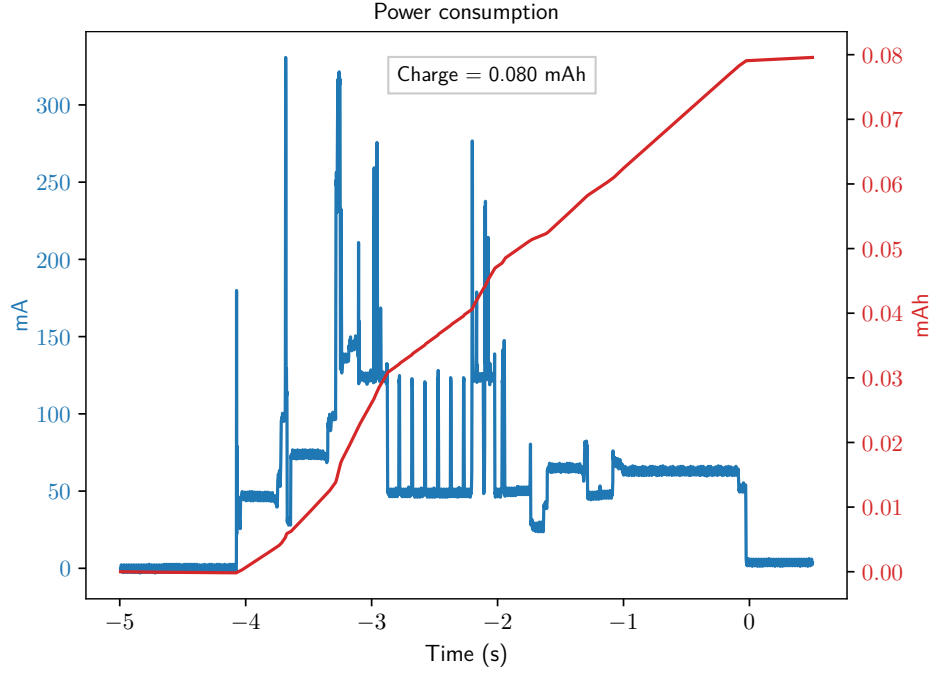
**Figure 18:** Power consumption of one sensor measurement

The charge that is used to read out the sensors once is 0.035 mAh. This leads to the following consumption per day:

$$42 \cdot 0.035 = 1.47 \text{ mAh/day}$$

### NTP synchronisation

In order to synchronise the RTC clock an NTP synchronisation has to be performed periodically. This synchronisation is performed once every 14 days. The power consumption for one synchronisation is illustrates in figure 19.



**Figure 19:** Power consumption of one NTP synchronisation

The charge that is used for one synchronisation is 0.08 mAh. However, this synchronisation only happens once every 14 days, this leads to the following consumption per day:

$$\frac{1}{14} \cdot 0.08 = 0.0057 \text{ mAh/day}$$

### Standby daytime

Between 9 AM and 4 PM the system is 'active', this means that the sensors receive power. However when the sensors are not being read out they will be put in their respective sleep modes. The theoretical consumption that are gathered from the datasheets is listed below:

- AMG8833 sleep mode: 0.2 mA
- CCS811 sleep mode: with  $V_{dd} = 1.8 \text{ V}$ :  $19 \mu\text{A}$   
 $\Rightarrow$  with  $V_{dd} = 3.3 \text{ V}$ :  $\frac{19}{1.8} \cdot 3.3 = 34.83 \mu\text{A}$
- microphone: the power to the microphone is only enabled just before the measurement because of this the microphone has no stand-by/sleep consumption.

Next to the consumption of the sensors, there is the sleep consumption of the microcontroller. If the microcontroller is not active, it is put in deepsleep. In



deepsleep there is a consumption of 10  $\mu\text{Ah}$ . Next to this consumption, two GPIO pins have to remain high during deepsleep: one to keep the CCS811 in sleep (nWake) and on to control the load switch to disable the power to the microphone. The GPIO pins use an internal pull-up resistor of 45 k $\Omega$  this leads to the following consumption for one GPIO pin:

$$\frac{3.3\text{V}}{45000\Omega} = 73.33 \mu\text{A}$$

For both GPIO pins this results in a consumption of 146.67  $\mu\text{A}$ . During the 7 hours a day the system is in active mode, this results in a charge consumption of:

$$7 \cdot (0.2 + 0.03483 + 0.01 + 0.1467) = 2.74 \text{ mAh/day}$$

### Standby nighttime

Between 4 PM and 9 AM the system goes in to sleep mode. In sleep mode no sensor measurements are performed and no data is transferred via Wi-Fi. To reduce the power, the power to the sensors is cut-off by using the load switches. The remaining stand-by/sleep consumption originates from the CPU consumption in deepsleep and the GPIO three pins that are kept high to drive the load switches. This leads to the following consumption:

$$10 \mu\text{A} + 3 \cdot 73.33 \mu\text{A} = 230 \mu\text{A}$$

The system remains in sleep mode for 17 hours a day this leads to the following consumption per day:

$$17 \cdot 230 \mu\text{A} = 3.91 \text{ mAh}$$

## 9.2 Total power consumption

In the previous section all the different sources that consume power were discussed an overview is given in table 2.

<i><b>Source</b></i>	<b>Charge per day [mAh/day]</b>
Wi-Fi	1.722 mAh/day
Sensors	1.47 mAh/day
NTP sync	0.0057 mAh/day
Standby daytime	2.74 mAh/day
Standby nighttime	3.91 mAh/day
Total	9.85 mAh/day

**Table 2:** Overview of the power consumption per day

There are two Li-Ion cells that are used to power the system, they both have a capacity of 3200 mAh which results in a total capacity of 6400 mAh. This leads to the following battery life:

$$\frac{6400}{9.85} = 649 \text{ days}$$

## **10 Website**

## **11 Financial estimate**

Kostprijs van het project opstellen.

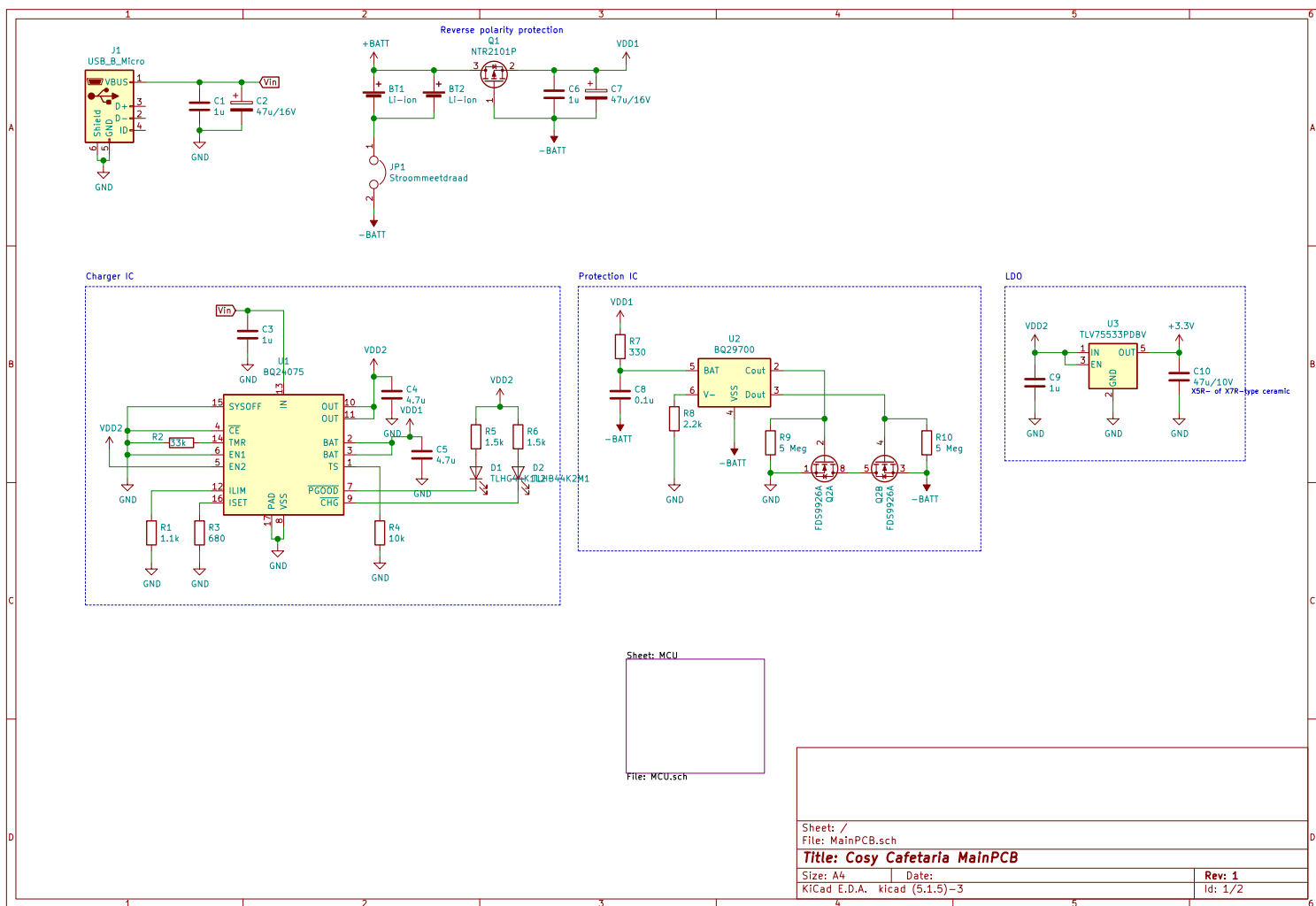
## **12 Validation and measurements**

Hier moeten we aantonen of dat alles werkt. Of eventuele fouten verklaren.

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## A MainPCB schematic



Sheet: MCU

File: MCU.sch

Sheet: /		
File: MainPCB.sch		
Title: <b>Cosy Cafeteria MainPCB</b>		
Size: A4	Date:	Rev: 1
KiCad E.D.A. kicad (5.1.5)-3		Id: 1/2

