

This problem and task contained within this report was formulated by Dr. Zhangming Wu of Cardiff University in 2025. The solution and the code are the author's own.

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Nomenclature

Term	Meaning
A_1	Cross-Sectional Area of Member 1 and 3
A_2	Cross-Sectional Area of Member 2
X	Tuple with A_1 and A_2
$f_1(X)$	Objective 1
$f_2(X)$	Objective 2
P	Load
H	Truss Dimension
E	Young's Modulus
$\sigma_i, i = 1,2,3$	Stress Constraints for Members 1,2,3.
SLSQP	Sequential Least Squares Quadratic Programming
SQP	Sequential Quadratic Programming
BFGS	Broyden–Fletcher– Goldfarb–Shanno (algorithm)
KKT	Karush-Kuhn-Tucker (conditions)

1. Introduction (385 Words)

Engineering design often requires making informed trade-offs between conflicting constraints. Typically, optimisation seek to minimise an objective function defined by design variables, subject to certain constraints. For example, in aerospace engineering, efficiency can be improved by reducing weight although this might compromise structural strength (Poll 2014). Thus, optimisations, like that performed by Wong et al. (2018), might aim to reduce weight via topology optimisation subject to constraints such as maximum allowable stress or mass retention. Similarly, optimisation algorithms can be used in non-structural applications such as in logistics processes. Pečený et al. (2020) discuss the use of optimisation in transport logistics to decrease costs or improve efficiencies.

This report concerns the optimisation of a three-member truss shown in Figure 1.1. The design variables are A_1 and A_2 which represent the cross-sectional areas of members 1 and 3, and member 2, respectively. (Wu 2025a)

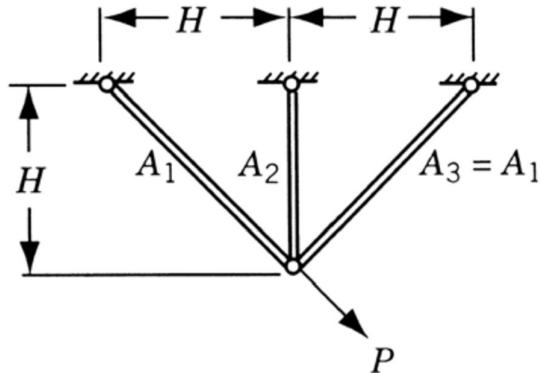


Figure 1.1 – The Truss Subject to Optimisation

The truss is subject to a load (P) and there were two objective functions $f_1(\mathbf{X})$ and $f_2(\mathbf{X})$, which concern weight and vertical deflection respectively. Three optimisations were carried out with the following objectives: minimise weight [$f_1(\mathbf{X})$], minimise vertical deflection [$f_2(\mathbf{X})$], and minimise both weight and vertical deflection with equal weighting [$0.5 \cdot f_1(\mathbf{X}) + 0.5 \cdot f_2(\mathbf{X})$]; herein referred to as optimisations 1, 2, and 3, respectively. The optimisation was subject to stress constraints for each member and bounds for the design variables A_1 and A_2 , giving the optimisation problem as follows (Wu 2025a):

Find:

$$\mathbf{X} = \begin{Bmatrix} A_1 \\ A_2 \end{Bmatrix}$$

which minimises:

$$f_1(\mathbf{X}) = 2\sqrt{2}A_1 + A_2 \quad 1.1$$

or/and

$$f_2(\mathbf{X}) = \frac{PH}{E} \left[\frac{1}{A_1 + \sqrt{2}A_2} \right] \quad 1.2$$

subject to:

$$\sigma_1 \leq \sigma^{(u)}$$

$$\sigma_2 \leq \sigma^{(u)}$$

$$\sigma_3 \leq \sigma^{(l)}$$

$$A_i^{(u)} \geq A_i \geq A_i^{(l)}, i = 1, 2$$

where:

$$\sigma_1(\mathbf{X}) = \text{stress in member 1} = P \left[\frac{A_2 + \sqrt{2}A_1}{\sqrt{2}A_1^2 + 2A_1A_2} \right] \quad 1.3$$

$$\sigma_2(\mathbf{X}) = \text{stress in member 2} = P \left[\frac{1}{A_1 + \sqrt{2}A_2} \right] \quad 1.4$$

$$\sigma_3(\mathbf{X}) = \text{stress in member 3} = P \left[\frac{A_2}{\sqrt{2}A_1^2 + 2A_1A_2} \right] \quad 1.5$$

and

$$P = 20, \quad H = 1, \quad E = 1, \quad \sigma^{(u)} = 20, \quad \sigma^{(l)} = -15, \quad A_i^{(u)} = 5.0, \quad A_i^{(l)} = 0.1$$

(Wu 2025a)

The optimisation was performed and results were presented using the various Python libraries, including SciPy's `scipy.optimize.minimize()` for the non-linear optimisation. The program also presented the solution and iteration data, calculated the active constraints, and presented figures to enable visualisation of convergence performance and the optimal solution in relation to the feasible region and objective function contours.

The aim of this report is to present the optimisation methodology used, present the optimal solutions for this problem, evaluate the performance of each objective function and the program more generally, and discuss the results and how the optimisation improved the design of the truss. The report will also consider how optimisation can be used in future designs and how this optimisation might have been improved.

2. Methodology and Implementation (514 Words)

2.1. Main Algorithms, Libraries, Data Structures, and Techniques

The core functionality of the programme was the numerical optimisation performed by the `scipy.optimize.minimize()` function. Within `minimize()`, the sequential least squares quadratic programming (SLSQP) method was used (SciPy Community 2023). SLSQP is a variation of the sequential quadratic programming (SQP) first introduced by Kraft (1988). Which remains one of the most modern and efficient techniques for solving medium-scale, smooth, and constrained optimisation problems (Nocedal and Wright 2006).

SQP solves nonlinear optimisation problems by applying Newton's method to a system of nonlinear equations derived from the Karush–Kuhn–Tucker (KKT) conditions and the Lagrangian of the constrained problem (Kraft 1988, Wu 2025b). In SLSQP, the quadratic subproblem is reformulated as a least-squares problem, which improves numerical efficiency, stability, and implementation (Kraft 1988). The search direction is obtained from this subproblem, and the Hessian of the Lagrangian is updated iteratively using a quasi-Newton BFGS approach (Kraft 1988, Wu 2025c).

The remainder of the programme was designed to prepare input data for the numerical optimisation and present the results. NumPy was used for efficient array handling and mathematical operations across the design region, matplotlib.pyplot was used for high-quality visualisation, and pandas.DataFrame was used to store iteration history and summarise results. This structure enabled clear and structured storage, simple plotting, and easy inspection of raw data.

2.2. The Programme Structure, Key Functions, and Implementation Techniques

The Python script was structured with clear separation between global variable definition, objective and constraint function declarations, optimisation execution, and plotting functions. This modular approach supported readability, maintainability, and reuse.

Three objective functions (two single-objective and one multi-objective) were defined to represent the optimisation goals, they returned the objective values for given design variables. The behaviour constraints were implemented as a single function returning a list of behaviour constraint values, all written in inequality form and rearranged to meet SciPy's expectation of the KKT condition where $g_j(X) \geq 0$. The geometric constraints were implemented directly through the bounds argument of the `minimize` function, improving numerical efficiency.

Two plotting functions were implemented: `contourplotfunc()` generated contour plots of the objective function with shaded feasible regions and marked optima, while `convergenceplotfunc()` displayed objective value versus iteration to evaluate convergence. Contour plots used a custom colour map

with manual label placement to clearly highlight contour levels, constraint boundaries, and the optimal solution. Both were tailored for clarity and informative visual output.

The minimise function was called from within a wrapper function, optifunc(), which managed the optimiser setup; It also passed relevant data to the plotting functions, contained a callback function to store iteration data, and returned the results to the main programme. The callback function logged the design variables and objective values at each iteration, enabling convergence analysis and graphical plotting via panda data frames. This enabled simple repeatability for multiple optimisations.

The main programme looped over the defined objective functions, calling optifunc() for each, determining active constraints, and calculating the values for $f_1(\mathbf{X})$ and $f_2(\mathbf{X})$ at each optimum. The final results were summarised and displayed via a data frame. A flowchart describing the code logic is shown in Figure 2.1.

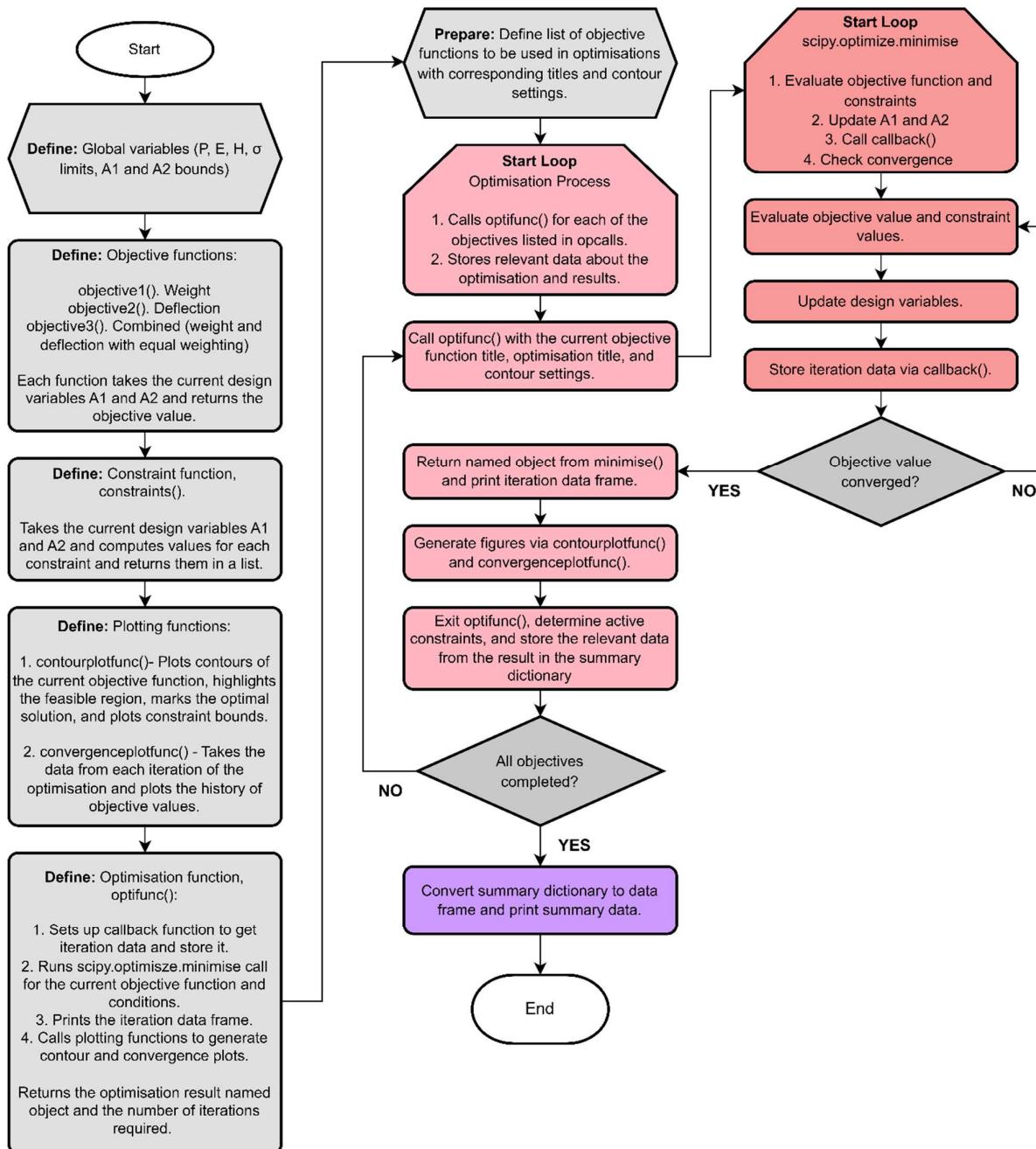


Figure 2.1 – Programme Logic Flowchart

3. Results (541 Words)

A summary of the results of the three optimisations is shown in Table 1. Figures 3.1, 3.2, and 3.3 show contour plots and convergence plots side by side for optimisations 1, 2, and 3, respectively.

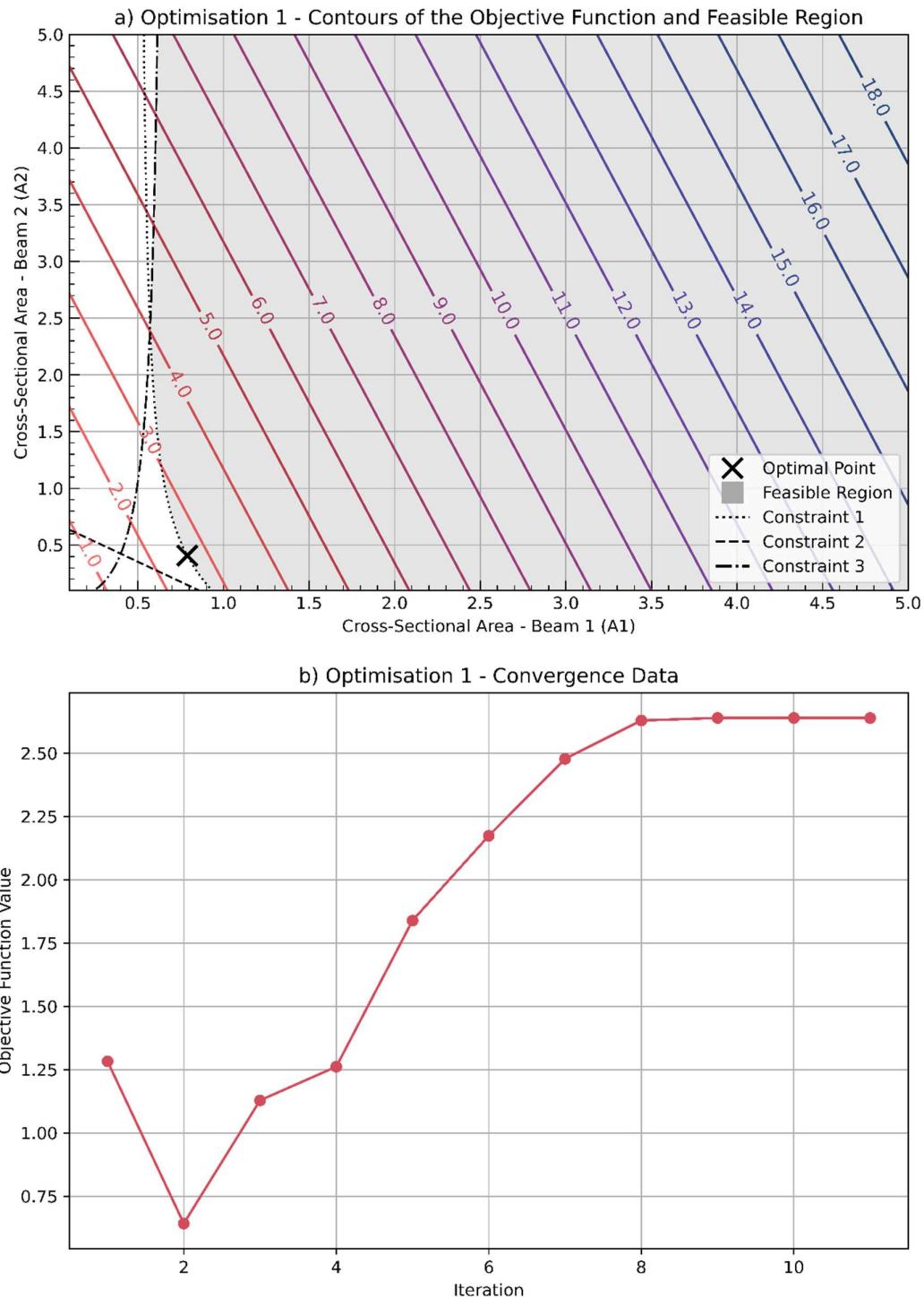


Figure 3.1 – Optimisation 1 Plots

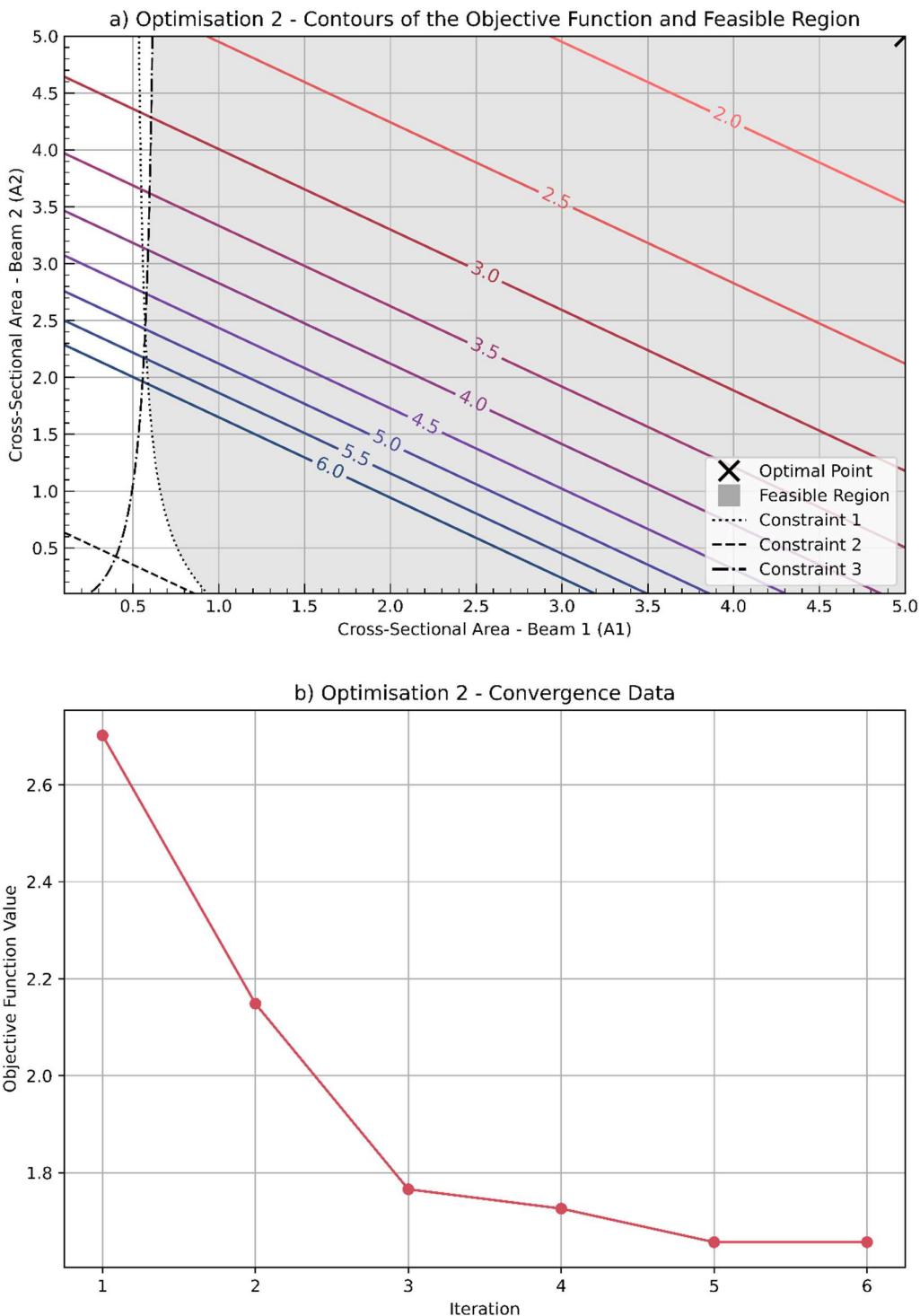


Figure 3.2 – Optimisation 2 Plots

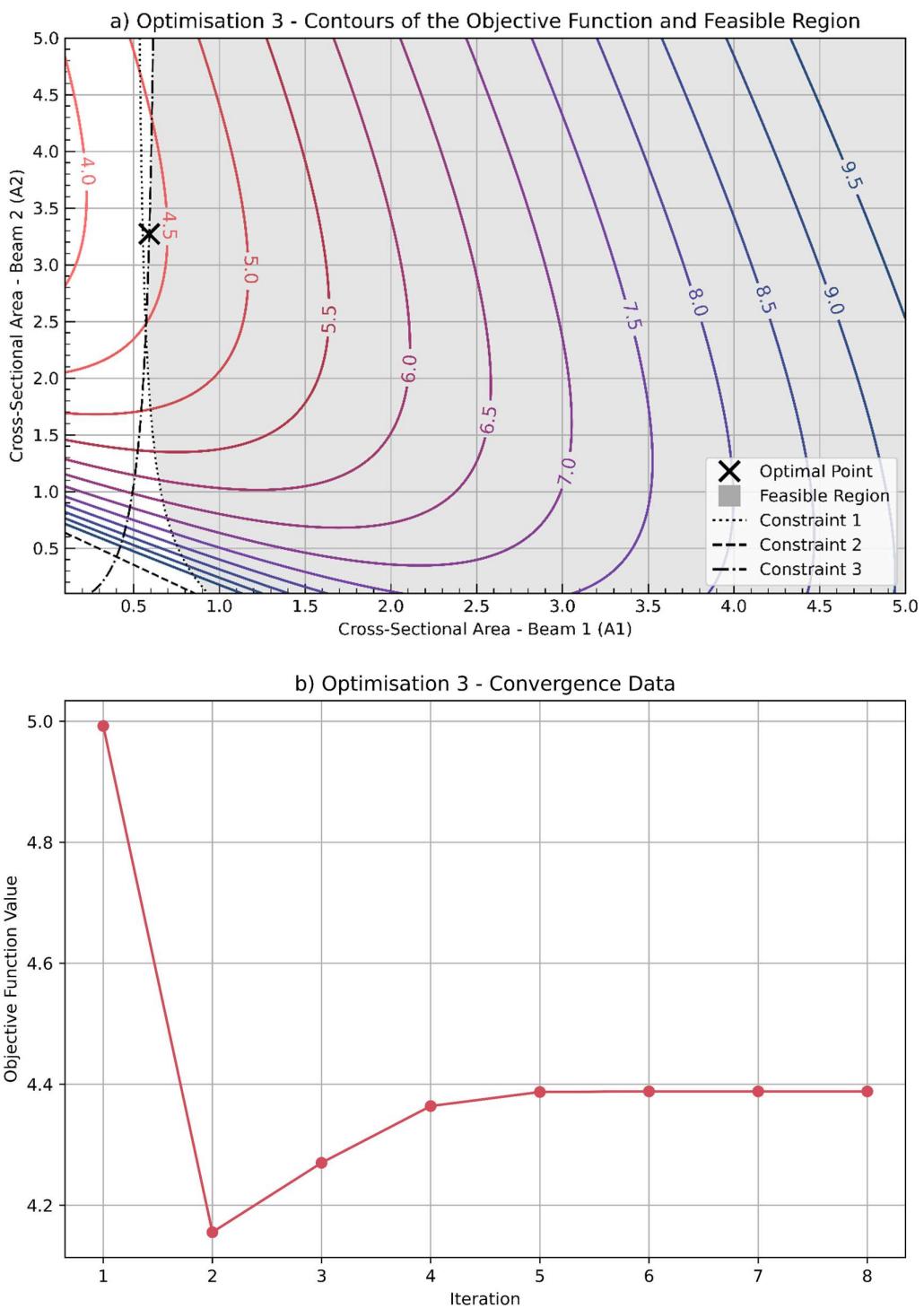


Figure 3.3 – Optimisation 3 Plots

Table 1 – Optimisation Results Summary

Optimisation Number	A ₁	A ₂	Objective Value	Iterations	Active Constraints	f ₁ (X)	f ₂ (X)
1	0.7887	0.4082	2.6390	10	Constraint 1	2.6390	14.6410
2	5.0000	5.0000	1.6569	6	None	19.4121	1.6569
3	0.5912	3.2722	4.3883	8	Constraint 3	4.9442	3.8324

Three optimisations were run on the truss structure using different objective functions: (1) minimise weight, (2) minimise deflection, and (3) minimise weight and deflection with equal weighting. Each optimisation used the same constraints and an initial guess of 2 for both the design variables A₁ and A₂; This initial guess was arbitrary, the only requirement was that the initial guess be feasible.

Table 1 shows that optimisation 1 resulted in cross-sectional area values of 0.7887 and 0.4082 for A₁ and A₂, respectively, with an objective value of 2.6390. The solution converged after 10 iterations and Figure 3.1b shows that, despite initially searching in the wrong direction, the optimisation iterations were stable. Figure 3.1a and Table 1 show that the active constraint in optimisation 1 was constraint 1 (the stress in member 1). The values of f₁(X) and f₂(X) were 2.6390 and 14.6410.

Similarly, from Table 1, optimisation 2 resulted in cross-sectional area values of 5.0000 for both A₁ and A₂. The objective value in this case was 1.6569. The solution converged after 6 iterations, and Figure 3.2b shows that the optimisation was entirely smooth. Table 1 shows that optimisation 2 was not limited by any of the three constraints, however, it is clear from logical interpretation and Figure 3.2a that the optimisation was limited by the upper bound of 5 for both design variables A₁ and A₂. The values of f₁(X) and f₂(X) were 1.6569 and 19.4121.

Table 1 also shows that optimisation 3 observed values of 0.5912 and 3.2722 for A₁ and A₂, respectively, with an objective value of 4.3883. The solution converged after 8 iterations and Figure 3.3b shows that, despite an initial overshoot of the optimum value, the optimisation iterations were stable. Figure 3.3a and Table 1 show that the active constraint in optimisation 3 was constraint 3 (the stress in member 3). The values of f₁(X) and f₂(X) were 4.9442 and 3.8324.

In all optimisations, convergence was relatively quick and stable, always achieving convergence within 10 iterations. In optimisations 1 and 2, large objective values for deflection and weight, respectively, were observed and they contrasted small values of the corresponding weight and deflections. Optimisation 3 struck a middle ground, with no extreme values for f₁(X) and f₂(X). Furthermore, a comparison of the design variables A₁ and A₂ in optimisations 1 and 3 show that A₁ decreased by 25.06% and A₂ increased by 701.63% in the multi-objective optimisation. Figures 3.1a, 3.2a, and 3.3a show that constraint 2 does form part of the boundary of the feasible region, indicating that it was never active and that stress in member 2 was not limiting. In terms of the design, optimisation 3 suggests that the balanced design, compromising between weight and deflection, had a small area A₁ and a relatively large cross-sectional area A₂.

4. Discussion (435 Words)

The optimum results showed that in optimisation 1, the minimisation of weight resulted in a large deflection, in optimisation 2, the minimisation of deflection resulted in a large weight, and in optimisation 3, the balancing of both weight and deflection resulted in an optimum that was a middle ground between weight and deflection. These results were as expected when considering fundamental solid mechanics.

Optimisation 2 was somewhat limited in its contribution to the understanding of the problem. From Figure 3.2a, it can be seen that the optimum point would only ever find the upper bounds of the design variables – an intuitive result because, to minimise deflection, the largest possible beams are required. This highlighted the effectiveness of optimisation 3; By considering weight alongside deflection, it was ensured that the design would not be unduly heavy nor have large deflection.

As constraint 2 was never active, this could have been removed from the optimisation with no effect on the optimum result and a reduction in computational time. Furthermore, this result indicates that the stress in member 2 is not limiting and that member 2 primarily serves to stiffen the truss.

In terms of the physical meanings of the results, optimisation 1 had small values of A_1 and A_2 which meant the truss, although lightweight, was weak. In optimisation 2, the values of A_1 and A_2 reached the maximum of 5, a design which was rigid but less practical than desired and not an efficient use of material. The balance struck in optimisation 3 resulted in a slightly lower value of A_1 but increased the value of A_2 by 706%. This indicated that the most balanced design should use a large cross-sectional area for member 2, to reduce deflection, and a low cross-sectional area for members 1 and 3, to reduce weight. This shows that the program ensured good material efficiency in the truss design because the smaller member, which could be widened with the lowest impact on weight, was used for stiffening the truss. Between optimisations 1 and 3, the active constraint switched from σ_1 to σ_3 , suggesting that the design in optimisation 1 supported the load mostly by tension of member 1, and in optimisation 3, member 2 supported most of load and the limiting factor became the compressive stress in member 3.

Overall computational performance was good, as indicated by the low iteration numbers in each optimisation. The plots aided the interpretation of the results by providing good visualisations. However, the programme could have been improved by incorporating additional objectives such as minimise cost or manufacturing considerations such as prefer beams of similar dimensions.

5. Conclusion (227 Words)

This study successfully optimised the three-member truss for the three objectives, with the cross-sectional areas of the beams as design variables and member stresses as constraints. It was shown that minimising weight alone causes a significant increase in deflection and that minimising deflection alone causes a significant increase in the weight. Optimisations 1 and 2, whilst feasible, exhibited real-world impracticalities that were balanced by the introduction of objective 3, used in optimisation 3, which assigned equal weighting to the weight and deflection objective functions. The resulting values of design variables A_1 and A_2 were 0.5912 and 3.2722, respectively, meaning the optimum truss had a large cross-sectional area in member 2, relative to that in members 1 and 3.

The findings confirmed fundamental structural mechanics principles and the presence of a trade-off between stiffness and weight. Furthermore, the study demonstrated how the design variables affected the load distribution, with a notable observation being the shift in the active constraint from σ_1 to σ_3 .

From this study, it was shown that optimisation offers a powerful, systematic method for exploring design trade-offs. Future work could enhance realism by introducing cost as a constraint, preferring consistent beam sizing, or modelling more complex load cases. Alternative solvers could also be explored to test the robustness of the solution or different initial guesses could be used to test the efficiency of the programme.

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