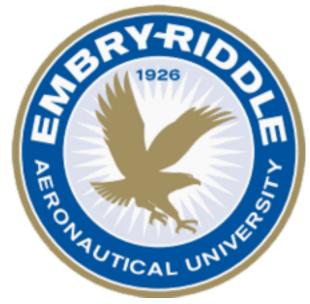
Homework 9



Date of Submission: April 5, 2019

Thorne Wolfenbarger wolfent1@my.erau.edu

Submitted to: Professor Kaela Martin College of Engineering

In Partial Fulfillment of the Requirements of

AE 313 Space Mechanics Spring, 2019

AE 313 Homework 9

- 2. Draw the heliocentric trajectory of Insight. On separate page.

```
3. Determine Earth's and InSight's heliocentric properties (r, v, \gamma) at departure.
1 r_earth = r('Earth');
2 r_{mars} = r('Mars');
3
4 v_earth = sqrt(MU('Sun')/r_earth);
5 \text{ FPA\_earth} = 0;
6
   . . .
                          149600000 \ km
     r_{Earth} = r_{InSight} =
                v_{Earth} =
                           29.7845 \ km/s
                          32.7285 \ km/s
              v_{Insight} =
    \gamma_{Earth} = \gamma_{InSight} =
   4. Draw the vector diagram in the heliocentric orbit and determine v_{\infty/Earth}^+.
1 v_inf_earth = v_sc1 - v_earth;
```

Diagram on separate page.

```
v_{\infty/Earth}^{+} = 2.944 \ km/s
```

5. What is the Δv_1 to depart Earth? Don't forget the vector diagram!

```
energy_inf_earth = v_inf_earth^2/2;
2 r_sc_earth = 300 + R('Earth');
3 ...
```

Diagram on separate page.

```
\Delta v_1 = 3.5898 \ km/s
```

6. Now move to the capture portion of the orbit. Determine Mars' and InSight's heliocentric properties at arrival (r, v, γ) .

```
r_mars = r('Mars');
v_mars = sqrt(MU('Sun')/r_mars);
3 \text{ FPA\_mars} = 0;
4 ...
```

```
r_{Mars} = r_{InSight} = 227920000 \ km
                         24.1304 \ km/s
           v_{Insight} =
                         21.4920 \ km/s
\gamma_{Mars} = \gamma_{InSight} =
```

7. Draw the vector diagram in the heliocentric orbit and determine $v_{\infty/Mars}^-$.

1 v_inf_mars = abs(v_sc2 - v_mars);

Diagram on separate page. $v_{\infty/Mars}^-=$ 2.6484 km/s

8. What is the required Δv_2 to capture at Mars? Don't forget the vector diagram!

1 dv_capture = v_mars_circ - v_mars_peri;

Diagram on separate page.

 $\Delta v_2 = 2.1075 \ km/s \ (slowing down)$

9. Are the required Δv values reasonable? Why or why not?

The Δv values are quite small compared to many transfer maneuvers. Given the small size of a lander these Δv values are not unreasonable for the reasource costs associated with them. Therefore they are reasonable.

HW9.m

```
1 clc; clear;
 2 % Constants
3 planets = {'Sun', 'Moon', 'Mercury', 'Venus', 'Earth', 'Mars', 'Jupiter',
       'Saturn', 'Uranus', 'Neptine', 'Pluto'};
 4 rad_list = [695990.0, 1739.2, 2439.7, 6051.9, 6378.0, 3397.0, 71492.0,
       60268.0, 25559.0, 25269.0, 1162.0];
 5 \text{ mu\_list} = [132712440000.0, 4902.8, 22032.0, 324860.0, 398600.0, 42828.0,
       126713000.0, 37941000.0, 5794500.0, 6836500.0, 981.6];
 6 sma_list = [0.0, 384400.0, 57910000.0, 108210000.0, 149600000.0,
       227920000.0, 778570000.0, 1433530000.0, 2872460000.0, 4495060000.0,
       5906380000.0];
7 R = containers.Map(planets, rad_list);
8 MU = containers.Map(planets,mu_list);
9 r = containers.Map(planets,sma_list);
11 % 3. Determine Earth and InSight heliocentric properties (r,v GPA) at
12 % departure
13 r_earth = r('Earth');
14 \text{ r\_mars} = r('Mars');
15
16 v_earth = sqrt(MU('Sun')/r_earth);
17 FPA_earth = 0;
18
19 r_sc1 = r_earth;
20 \text{ FPA\_sc1} = 0;
21
22 r_sc2 = r_mars;
23 a_t = (r_sc1 + r_sc2)/2;
24
25 syms v_sc1
26 eq = -MU('Sun')/(2*a_t) == v_sc1^2/2 - MU('Sun')/r_sc1;
27 \text{ v\_sc1} = \max(\text{double}(\text{solve}(\text{eq}, \text{v\_sc1})));
28 \% v_sc1 = sqrt(2*MU('Sun')/r_sc1 - MU('Sun')/a_t)
29
30 % 4. Determine v_inf_earth
31
32 \text{ v\_inf\_earth} = \text{v\_sc1} - \text{v\_earth};
33
34 % 5. Required dv to depart earth
35 energy_inf_earth = v_inf_earth^2/2;
36 r_sc_earth = 300 + R('Earth');
37 % dv = sgrt(v_inf_earth^2 + 2*MU('Earth')/r_sc_earth) - sgrt(MU('Earth')/
       r_sc_earth);
```

```
38 syms v_earth_peri
39 eq = energy_inf_earth == v_earth_peri^2/2 - MU('Earth')/r_sc_earth;
40 v_earth_peri = max(double(solve(eq, v_earth_peri)));
41 v_earth_circ = sqrt(MU('Earth')/r_sc_earth);
42 dv_escape = v_earth_peri - v_earth_circ;
43
44 % 6. Mars and insight properties at arrival (r, v, FPA)
45 \text{ r\_mars} = r('Mars');
46 \text{ v_mars} = \text{sqrt}(\text{MU}('\text{Sun'})/\text{r_mars});
47 \text{ FPA\_mars} = 0;
48
49 	ext{ r_sc2} = 	ext{r_mars};
50 \text{ syms } v_{sc2}
51 eq = -MU('Sun')/(2*a_t) == v_sc2^2/2 - MU('Sun')/r_sc2;
52 \text{ v\_sc2} = \max(\text{double}(\text{solve}(\text{eq, v\_sc2})));
53 \text{ FPA\_sc2} = 0;
54
55 % determine v_inf_mars
56 v_inf_mars = abs(v_sc2 - v_mars); % Positive by convention
57 energy_inf_mars = v_inf_mars^2/2;
58 r_sc_mars = 150 + R('Mars');
59
60 syms v_mars_peri
61 eq = energy_inf_mars == v_mars_peri^2/2 - MU('Mars')/r_sc_mars;
62 v_mars_peri = max(double(solve(eq, v_mars_peri)));
63 v_mars_circ = sqrt(MU('Mars')/r_sc_mars);
64 dv_capture = v_mars_circ - v_mars_peri;
```