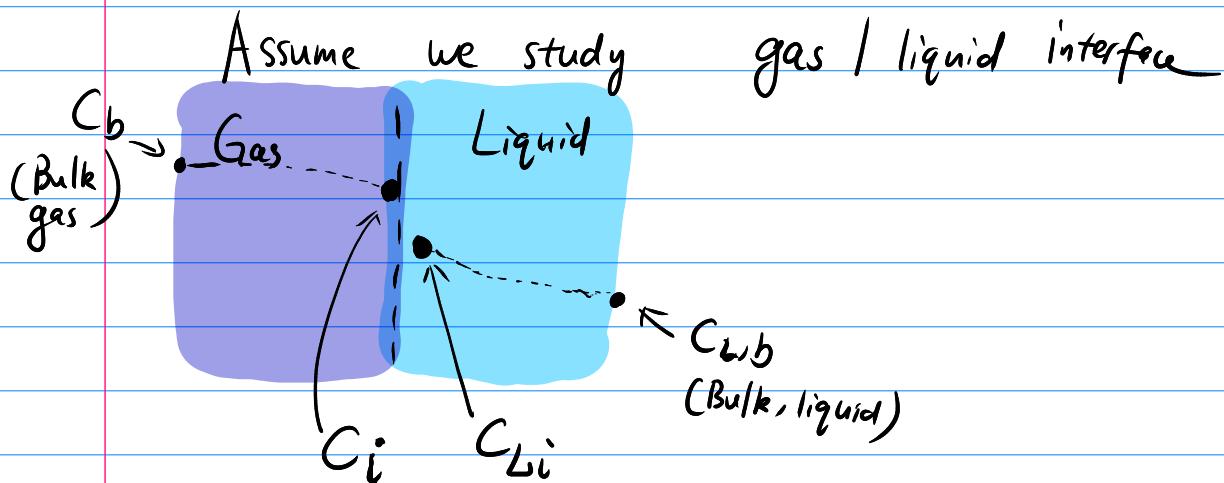


CHE 318 L14

Feb-04 2026

Mass Transfer coefficients

Recap: we need to know concentration across boundary between phases



Assume molecules acrossing interface has no resistance

$$\Rightarrow \text{Equilibrium constant } K = \frac{\text{Conc in gas}}{\text{Conc in liquid}} \rightarrow \begin{array}{l} \text{Interface} \\ \text{concentration} \end{array}$$

$$K : \text{dimensionless} \qquad \qquad = \frac{C_i}{C_{Li}}$$

Similarly, we have ① Henry's law $H = \frac{P_{\text{gas}}}{C_{Li}}$ $P_g = c g R T$

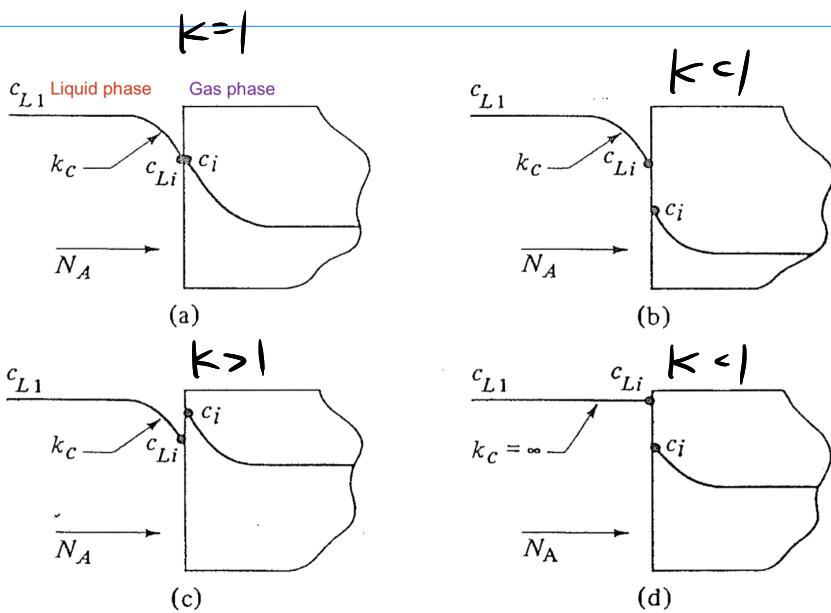
$$\textcircled{2} \text{ Solubility } C_A = \frac{S \cdot P_A}{22.414}$$

$K \rightarrow 0 \equiv \text{Gas phase vapor pressure} \approx 0$ ($A = \text{protein}$)

$K = 1 \equiv \text{same concentration}$ ($A: \text{liquid at boiling point}$)

$K = \infty \equiv \text{Liquid phase conc} = 0$ (insoluble gas)

Interfacial concentration profile may look very diff.



Gearkop 1/3

7.1.3 What else controls the profile?

M.B across interface

$$\frac{N_A}{\text{left}} : \frac{N_A}{\text{right}} \quad N_A/U = N_A/R$$

We can use $N_A = J_A^* zt C_A V_m$ in each phase,
but the actual form of J_A^* depends on local gradient
(harder to model)

Instead, without losing generality

$$[\text{Flux}] = \frac{[\text{Driving Force}]}{[\text{Resistance}]}$$

① We can have conc. diff. between $\begin{cases} C_b & \& C_i \\ C_{ub} & \& C_i \end{cases}$

② Driving force? Just use a coefficient $\frac{1}{k}$

$$\text{In general } N_A = k'_c \cdot (C_{L,b} - C_{U,i})$$

Meaning: $k'_c \rightarrow$ EMCQ-like

\Rightarrow concentration diff as driving force

Unit of k'_c ?

$$N_A \Rightarrow \frac{\text{mol}}{\text{m}^2 \cdot \text{s}} \quad \Delta C \Rightarrow \frac{\text{mol}}{\text{m}^3} \quad \text{So: } k'_c \text{ unit m/s}$$

(velocity !)

k'_c from multiple scenarios

$$\text{EMCD } N_A = \frac{D_{AB}}{Z_2 - Z_1} (C_{A1} - C_{A2})$$

$\Rightarrow k'_c$

$$\text{Stagnant B } N_A = \frac{D_{AB}}{Z_2 - Z_1} \cdot \frac{1}{x_{Bm}} (C_{A1} - C_{A2})$$

$\downarrow k'_c \quad k'_c \text{ (with } x_{Bm} \text{ contribution)}$

Solve concentration at boundaries

$$2 \text{ equations: } N_A|_L = N_A|R$$

$$k'_{c,L} (C_{L,b} - C_{L,i}) \stackrel{\text{var 1}}{=} k'_{c,g} (C_{g,i} - C_{g,b}) \stackrel{\text{var 2}}{=}$$

$$K = \frac{C_{g,i}}{C_{L,i}}$$

That explains the different shape

$k'_{c,L} \rightarrow \infty \Rightarrow$ concentration profile liquid = flat !

Idea of K & k'_c will be discussed in absorption process

k_c' makes calculating N_A convenient

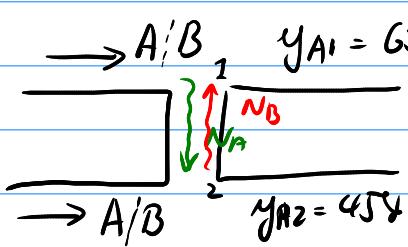
$$\begin{aligned} \text{We can write } N_A &= k_c'(C_{A1} - C_{A2}) \\ &= k_G'(P_{A1} - P_{A2}) \\ &= k_y'(y_{A1} - y_{A2}) \\ &= \dots \end{aligned} \quad \left(\begin{array}{l} \text{Convention} \\ \text{gas fraction } y_A \\ \text{liquid frac } x_A \\ k_c' = \text{EMCD-like} \\ k_c = \text{Stagnant B } \left(\frac{x_B}{p_{\text{atm}}} \right) \end{array} \right)$$

Unit? $k_c' k_c \Rightarrow \text{m/s}$

$k_y' k_y k_x' k_x \Rightarrow \text{kg mol/(m}^2 \cdot \text{s})$

$k_G' k_G \Rightarrow \text{kg mol/(m}^2 \cdot \text{s} \cdot P_A) \quad) \text{Choose your preference}$

Solution to Q1



1 → 2

$$\begin{aligned} N_A &= k_y' (y_{A1} - y_{A2}) \\ &= 1.5 \times 10^{-4} \times (0.65 - 0.45) \\ &= 3.0 \times 10^{-5} \text{ kg mol/(m}^2 \cdot \text{s}) \end{aligned}$$

$$N_B = -N_A \quad 2 \rightarrow 1$$

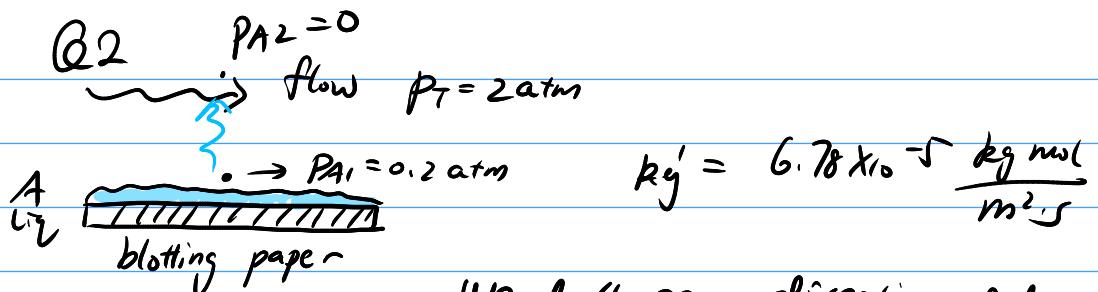
We realize k_y' is dependent on total pressure!

$$k_y' \rightarrow k_c' \quad k_y' = k_c' \cdot C_T = k_G' \cdot P_f$$

$$k_G' = \frac{k_y'}{P_f} = \frac{1.5 \times 10^{-4}}{2000 \text{ kPa}} = 2.14 \times 10^{-7} \text{ kg mol/(m}^2 \cdot \text{s} \cdot \text{kPa})$$

$$k_c' = \frac{k_y'}{C_T} = \frac{k_y'}{P_f} \cdot R_T = k_G' \cdot R_T = 6.65 \times 10^{-4} \text{ m/s}$$

superficial vel



$$k_y' = 6.78 \times 10^{-5} \frac{\text{kg mol}}{\text{m}^2 \cdot \text{s}}$$

We don't care direction of N_A in fluid

All mass transfer coefficient \Rightarrow lumped

$$N_A = k_y \cdot \frac{l}{y_{Bm}} \cdot (y_{A1} - y_{A2})$$

\leftarrow Stagnant B

$$y_{Bm} \approx \frac{y_{B1} + y_{B2}}{2} = 0.95 \quad y_{A1} = 0.1 \quad y_{A2} = 0$$

$$N_A = 6.78 \times 10^{-5} \cdot \frac{1}{0.95} \cdot 0.1 = 7.14 \times 10^{-6} \text{ kg mol/(m}^2 \cdot \text{s)}$$

$$k_y = k_y' / y_{Bm} = 7.14 \times 10^{-5} \text{ kg mol/(m}^2 \cdot \text{s})$$

$$k_G = k_y / p_T = 3.57 \times 10^{-5} \text{ kg mol/(m}^2 \cdot \text{s, atm})$$

Q3



$$\overline{\text{Flux}} = \frac{[\text{weight}]}{[\text{molar mass}][\text{time}]}$$

$$N_A \cdot 4\pi r_0^2 = \frac{m_1 - m_2}{M_A \cdot \delta t} = k_L (C_{AS} - 0)$$

$$k_L = \frac{1}{4\pi r_0^2} \cdot \frac{m_1 - m_2}{C_{AS} \cdot M_A \cdot \delta t}$$

≈ ← Get from solubility