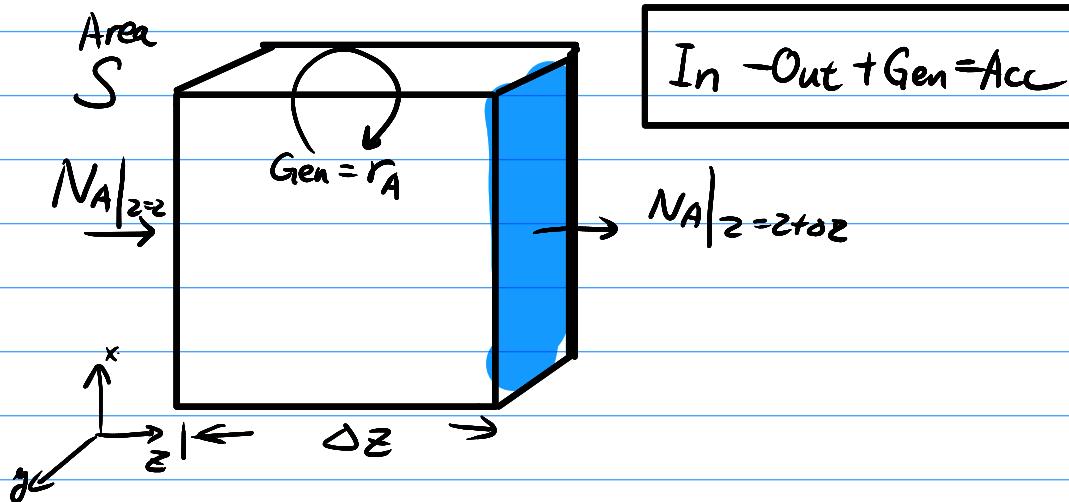


CHE 318 Lecture 09

Jan 21 - 2026

U.S.S mass transport



Derivation of govern eqn

$$N_A|_{z=z} - N_A|_{z=z+\Delta z} = - \left(\frac{N_A|_{z+\Delta z} - N_A|_z}{\Delta z} \right) \cdot \Delta z$$

↓ Def. of derivative

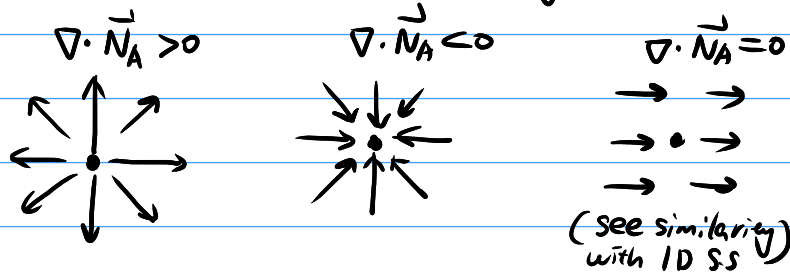
$$= - \frac{\partial N_A}{\partial z} \cdot \Delta z$$

$$\Rightarrow \frac{\partial C_A}{\partial t} = - \nabla \cdot N_A + r_A$$

$$1D \quad \frac{\partial C_A}{\partial t} = - \frac{\partial N_A}{\partial z} + r_A$$

Divergence operator $\nabla \cdot \text{vector} \Rightarrow \text{scalar}$

$$\nabla \cdot \vec{N}_A = \frac{\partial N_A}{\partial x} + \frac{\partial N_A}{\partial y} + \frac{\partial N_A}{\partial z}$$



Gradient $\nabla \text{ scalar} \rightarrow \text{gradient}$

$$\nabla C \rightarrow \left(\frac{\partial C}{\partial x}, \frac{\partial C}{\partial y}, \frac{\partial C}{\partial z} \right)$$

Laplace operator $\nabla^2 \text{ scalar} \rightarrow \text{scalar}$

$$\nabla^2 C \rightarrow \frac{\partial^2 C}{\partial x^2} + \frac{\partial^2 C}{\partial y^2} + \frac{\partial^2 C}{\partial z^2}$$

Special cases for U.S.S

① Fick's second law

$$\begin{cases} v_m = 0 \Rightarrow \text{EMCD flux} \\ D_{AB} \text{ constant} \\ r_A = 0 \end{cases}$$

$$\frac{\partial C}{\partial t} = 0 = \nabla \cdot (-D_{AB} \nabla C_A + 0)$$

no negative sign $\Rightarrow D_{AB} \nabla^2 C_A \Rightarrow \text{Fick's 2nd law}$

Fick's 1st law $J_{Az}^* = \ominus D_{AB} \frac{\partial C_A}{\partial z}$
 \uparrow negative sign

$$\frac{\partial C}{\partial t} = r_A - \nabla \cdot (-D_{AB} \nabla C_A + C_A v_m)$$

Only 1 governing eq, different simplification

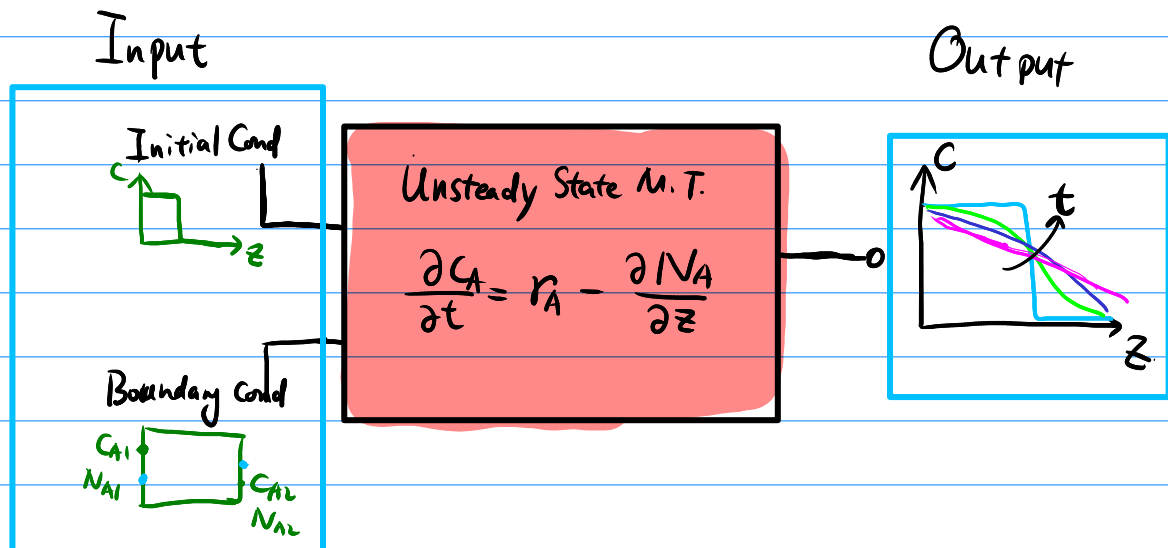
② Constant D_{AB} (no other simplification)

$$\begin{aligned}\frac{\partial C_A}{\partial t} &= D_{AB} \nabla^2 C_A - \nabla \cdot (C_A \vec{v}_m) + r_A \\ &= D_{AB} \nabla^2 C_A - C_A \nabla \cdot \vec{v}_m - \nabla C_A \cdot \vec{v}_m + r_A\end{aligned}$$

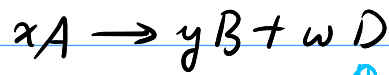
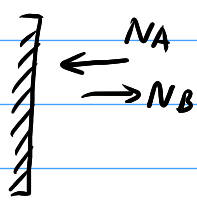
$\nabla \cdot (C_A \vec{v}_m) = \nabla C_A \cdot \vec{v}_m + C_A \nabla \cdot \vec{v}_m$
 $\nabla C_A \cdot \vec{v}_m$ → vector
 $C_A \nabla \cdot \vec{v}_m$ → scalar

③ case ② But incompressible ($\nabla \cdot \vec{v}_m = 0$)

$$\frac{\partial C_A}{\partial t} = D_{AB} \nabla^2 C_A - \nabla C_A \cdot \vec{v}_m + r_A$$

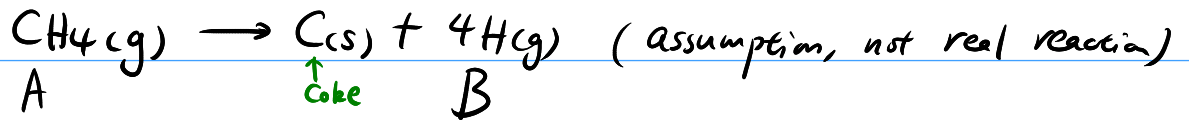


B.C for reaction



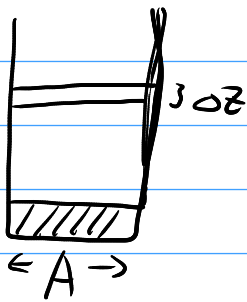
↑
solid

$$\frac{N_A}{x} = - \frac{N_B}{y}$$



$$\begin{aligned} N_A &= r_A \\ N_B &= -4 r_A \end{aligned} \Rightarrow \frac{N_A}{1} = - \frac{N_B}{4}$$

Solving U.S.S for stagnant B



Governing Eq (M.B)

$$\frac{\partial C_A}{\partial t} = - \frac{\partial N_A}{\partial z}$$

$$N_A = - C_T D_{AB} \frac{\partial x_A}{\partial z} + x_A (N_A + N_B)$$

↑ Cannot directly say $N_B = 0$!

Constraints between N_A & N_B

$$\frac{\partial C_T}{\partial t} = - \frac{\partial N_T}{\partial z} = - \frac{\partial N_A}{\partial z} - \frac{\partial N_B}{\partial z} = 0$$

$$\frac{\partial N_A}{\partial z} = - \frac{\partial N_B}{\partial z} \quad N_T \text{ is constant}$$

B.C.s

$$\begin{cases} x_A(z=0, t) = x_{A0} & x_A(L, t) = 0 \\ N_B(z=0, t) = 0 \end{cases} \quad \begin{matrix} \uparrow \\ \text{No flux BC} \end{matrix}$$

$$\rightarrow N_A(0, t) = - \frac{C_T D_{AB}}{1 - x_{A0}} \frac{\partial x_A}{\partial z} \bigg|_{z=0}$$

$$\begin{aligned} \frac{\partial C_A}{\partial t} = C_T \frac{\partial x_A}{\partial t} &= - \frac{\partial \left(- \frac{C_T D_{AB}}{1 - x_{A0}} \frac{\partial x_A}{\partial z} \right)}{\partial z} = \frac{\partial [x_A \cdot (N_A + N_B)]}{\partial z} \\ &= - C_T D_{AB} \frac{\partial^2 x_A}{\partial z^2} = \frac{\partial x_A}{\partial z} \cdot (N_A + N_B) \end{aligned}$$

↖ 2 parts...

What is $N_T = N_A + N_B$?

$$N_T(z \neq 0, t) = N_T(z=0, t) = N_A(0, t) + N_B(0, t)$$

$$= - \frac{C_T D_{AB}}{1 - x_{A0}} \frac{\partial x_A}{\partial z} \bigg|_{z=0}$$

NOT a constant over t !

Final expression for Govern. Equ.

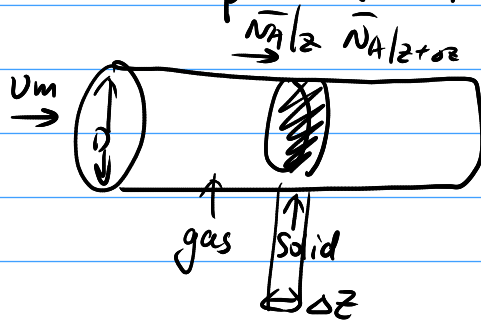
$$\frac{\partial x_A}{\partial t} = + D_{AB} \frac{\partial^2 x_A}{\partial z^2} + \left[\frac{D_{AB}}{1 - x_{A0}} \frac{\partial x_A}{\partial z} \right]_{z=0} \frac{\partial x_A}{\partial z}$$

And initial conditions

initial gradient!

$$x_A(z \neq 0, 0) = 0 \quad \text{Analytical solution exists}$$

Example 2 Reaction through catalyst wall



Reaction & M.T.

In the catalyst region Rate of reaction
 $r = k(C_{As} - C_A)$

$$\text{In} - \text{Out} + \boxed{\text{Gen}}^{\neq 0} = \text{Acc}$$

$$\frac{\pi D^2}{4} (N_A|_z - N_A|_{z+\Delta z}) + \pi D \cdot \Delta z \cdot k(C_{As} - C_A)$$

$$= \frac{\pi D^2}{4} \cdot \frac{\partial C_A}{\partial t}$$

$$\rightarrow - \frac{\partial N_A}{\partial z} + \left(\frac{4k}{D}\right)(C_{As} - C_A) = \frac{\partial C_A}{\partial t}$$

Use flux eq with v_m (easier!)

$$N_A = -D_{AB} \frac{\partial C_A}{\partial z} + C_A \cdot v_m$$

Constant v_m case

$$\frac{\partial N_A}{\partial z} = -D_{AB} \frac{\partial^2 C_A}{\partial z^2} + \frac{\partial C_A}{\partial z} v_m$$



$$\frac{\partial C_A}{\partial t} = - \left(-D_{AB} \frac{\partial^2 C_A}{\partial z^2} + \frac{\partial C_A}{\partial z} v_m \right) + \frac{4k}{D} (C_{As} - C_A)$$

- 1) Need initial & BC
- 2) Numerical integration