1 Stochastic

1.1 PDFs

Valid PDF: $\int_{-\infty}^{\infty} f(x) dx = 1$ and $f(x) > 0 \forall x$

Independency: $f(x,y) = f(x) \cdot f(y)$ and f(x|y) = f(x)

Marginalization: $f(x) = \int f(x, y) dy$

Cumulative Distribution Function: $F_x(x) = \int_{-\infty}^x f_x(\bar{x}) d\bar{x}$

1.1.1 Normal Distribution

$$w \sim \mathcal{N}(\mu, \sigma^2); \quad f_w = \Sigma^{-1} \frac{1}{\sqrt{2\pi}} exp\left(-\frac{1}{2}(x-\mu)^T \Sigma^{-1}(x-\mu)\right)$$

1.2 Expected Value

$$E[x] = \int x \cdot f(x);$$
 $E[x] = \sum x \cdot f(x)$

$$E[ax] = a \cdot E[x]; \qquad \qquad E[x+y] = E[x] + E[y]$$

$$E[x|y] = \int x \cdot f(x|y); \qquad E[y] = E[g(x)]; \quad y = g(x)$$

If (x,y) independent: $E[x y] = E[x] \cdot E[y]$

1.3 Variance

$$Var[x] = E[(x - \mu)(x - \mu)^T] \stackrel{2D}{=} E[x^2] - E[x]^2$$
 (cont.)

$$Var[x] = \sum_{i=1}^{n} p_i \cdot (x_i - \mu)^2 = \sum_{i=1}^{n} (p_i \cdot x_i^2) - \mu^2$$
 (discrete)

1.4 Conditioning

$$f(x,y) = f(x|y) \cdot f(y)$$

1.5 Total Probability Theorem

$$f(x) = \sum_{y} f(x|y) f(y) \qquad f(x) = \int f(x|y) f(y) dy$$

1.6 Baye's Theorem

$$P(A|B) = \frac{P(B|A) \cdot P(A)}{P(B)}$$

1.7 Multivariable Change of Variables

$$\text{discr.:} \quad f_x(x_j) = \sum_{y_{j,i} \in \mathcal{Y}_i} f_y(y_{j,i}) \quad \text{ cont.:} \quad f_{z|x} = \frac{f_{w|x}(h(z,x))}{\left|\frac{\partial g}{\partial w}(h(z,x)\right|}$$

2 Bayesian Tracking

Process Model:

$$x(k) = q_{k-1}(x(k-1), v(k-1))$$

$$z(k) = h_k(x(k), w(k))$$

Step 1 (Prior Update):

$$f(x(k)|z(1:k-1)) = \sum_{x(k-1)\in\chi} f(x(k)|x(k-1)) f(x(k-1)|z(1:k-1))$$

Step 2 (Measurement Update):

$$f(x(k)|z(1:k)) = \frac{f(z(k)|x(k)) f(x(k)|z(1:k-1))}{\sum_{x} f(z(k)|x(k)) f(x(k)|z(1:k-1))}$$

3 Extracting Estimates from PDFs

3.1 Maximum Likelihood Estimation (MLE)

$$\hat{x}_{ML} = arg \, max \, f(z|x)$$

3.2 Maximum a Posteriori (MAP)

$$\hat{x}_{MAP} = \arg\max f(z|x)f(x)$$

3.3 Minimum Mean Squared Error (MMSE)

$$\hat{x}_{MMSE} = \arg\min E[(\hat{x} - x)^T \cdot (\hat{x} - x)|z]$$

$$\frac{d}{d\hat{x}}E[(\hat{x}-x)^T\cdot(\hat{x}-x)|z]=0 \text{ (nur CRV) gibt } \hat{x}_{MMSE}=E[x|z]$$

3.4 Recursive Least Squares (RLS) Algorithm

Observation Model:

$$\begin{split} z(k) &= H(k)x + w(k) \\ \bar{x} &= E[x], \quad E[w(k)] = 0, \quad R(k) = Var[(w(k)] \end{split}$$

Initialization: $\hat{x}(0) = \bar{x}, \quad P(0) = P_x = Var[x]$

Recursion: observe z(k) and then update as follows

$$K(k) = P(k-1)H^{T}(k) \cdot [H(k)P(k-1)H^{T}(k) + R(k)]^{-1}$$

$$\hat{x}(k) = \hat{x}(k-1) + K(k) \cdot [z(k) - H(k)\hat{x}(k-1)]$$

$$P(k) = [I - K(k)H(k)]P(k-1)[I - K(k)H(k)]^{T} + K(k)R(k)K(k)^{T}$$

$$e(k) = [I - K(k)H(k)]e(k-1) - K(k)w(k)$$

4 Kalman Filter

Process Model

$$x(k) = A(k-1)x(k-1) + B(k-1)u(k-1) + v(k-1)$$

$$z(k) = H(k) \cdot x(k) + w(k)$$

x(k): State $x(0) \sim \mathcal{N}(x_0, P_0)$ v(k): Process Noise $v(k) \sim \mathcal{N}(0, Q(k))$ w(k): Sensor Noise $w(k) \sim \mathcal{N}(0, R(k))$

4.1 Time varying KF

Initialization: $\hat{x}_m(0) = x_0$, $P_m(0) = P_0$ Step 1 (Prior Update):

$$\hat{x}_p(k) = A(k-1)\,\hat{x}_m(k-1) + B(k-1)\,u(k-1)$$

$$P_p(k) = A(k-1)\,P_m(k-1)\,A^T(k-1) + Q(k-1)$$

Step 2 (Measurement Update):

$$\begin{split} K(k) &= P_p(k)H^T(k) \cdot [H(k)P_p(k)H^T(k) + R(k)]^{-1} \\ \hat{x}_m(k) &= \hat{x}_p(k) + K(k) \cdot (z(k) - H(k)\hat{x}_p(k)) \\ P_m(k) &= [I - K(k)H(k)]P_p(k) \\ &= [I - K(k)H(k)]P_p(k)[I - K(k)H(k)]^T + K(k)R(k)K^T(k) \\ e(k) &= [I - K(k)H(k)]A(k-1)e(k-1) + \dots \\ &\dots [I - K(k)H(k)]v(k-1) - K(k)w(k) \end{split}$$

The time-varying KF is the exact solution to the Bayesian tracking problem for linear systems with Gaussian distributions.

4.2 Kalman Filter as State Observer

A, B, H, Q, R constant, but the KF is still varying:

$$P_p(k) = A P_m(k-1) A^T + Q$$

$$K(k) = P_p(k) H^T (H P_p(k) H^T + R)^{-1}$$

$$P_m(k) = [I - K(k) H] P_p(k)$$

The variance $P_p(k)$ converges if (A, H) is detectable or observable.

4.2.1 Observability

$$\mathcal{O} = \begin{bmatrix} H \\ HA \\ \vdots \\ HA^{n-1} \end{bmatrix} \qquad \begin{array}{ll} \text{If } rank(\mathcal{O}) & = & n, \text{ the pair } (A,H) \text{ is observable.} \\ \\ \text{Observability} \Rightarrow \text{Detectability.} \\ \end{array}$$

4.2.2 Detectability (Check observability first)

(A,H) is detectable if $\begin{bmatrix} A-\lambda I \\ H \end{bmatrix}$ has full column rank. It is sufficient to only check the unstable Eigenvalues $(|\lambda_i|>1)$ of A. Detectability implies convergence of the variance $P_p(k)$: $\lim_{k\to\infty}P_p(k)=P_\infty$.

4.3 Steady state KF

A, B, H, Q, R constant; $\lim K(k) = K_{\infty}$; $\lim P_{p}(k) = P_{\infty}$

Discrete Algebraic Riccati Equation:

$$P_{\infty} = AP_{\infty}A^T + Q - AP_{\infty}H^T(HP_{\infty}H^T + R)^{-1} \cdot HP_{\infty}A^T$$

$$K_{\infty} = P_{\infty}H^T(HP_{\infty}H^T + R)^{-1}$$

Steady State Estimator:

$$\hat{x}(k) = (I - K_{\infty}H)A\hat{x}(k-1) + (I - K_{\infty}H)Bu(k-1) + K_{\infty}z(k)$$
$$= \hat{A}\hat{x}(k-1) + \hat{B}u(k) + K_{\infty}z(k)$$

DARE only has a unique solution for P_{∞} if (A,H) detectable and (A,G) stabilizable (guaranteed if $Q\geq 0$) with $Q=GG^T$. Existence of unique positive semidefinite solution guarantees stable error dynamics.

4.4 Extended KF (EKF)

Process Model:

$$x(k) = q_{k-1}(x(k-1), u(k-1), v(k-1))$$

$$z(k) = h_k(x(k), w(k))$$

$$\begin{array}{ll} E[x(0)] = x_0 & Var[x(0)] = P_0 \\ E[v(k-1)] = 0 & Var[v(k-1)] = Q(k-1) \\ E[w(k)] = 0 & Var[w(k)] = R(k) \end{array}$$

Initialization: $\hat{x}_m(0) = x_0$, $P_m(0) = P_0$

Step 1 (Prior Update):

$$\begin{split} A(k-1) &= \frac{\partial q_{k-1}}{\partial x(k-1)} (\hat{x}_m(k-1), u(k-1), \mathbf{v(k-1)=0}) \\ L(k-1) &= \frac{\partial q_{k-1}}{\partial v(k-1)} (\hat{x}_m(k-1), u(k-1), \mathbf{v(k-1)=0}) \\ \hat{x}_p(k) &= q_{k-1} (\hat{x}_m(k-1), u(k-1), \mathbf{v(k-1)=0}) \\ P_p(k) &= A(k-1) P_m(k-1) A^T(k-1) + L(k-1) Q(k-1) L^T(k-1) \end{split}$$

Step 2 (Measurement Update):

$$\begin{split} H(k) &= \frac{\partial h_k}{\partial x(k)}(\hat{x}_p(k), \mathbf{w(k)} = \mathbf{0}) \\ M(k) &= \frac{\partial h_k}{\partial w(k)}(\hat{x}_p(k), \ \mathbf{w(k)} = \mathbf{0}) \\ K(k) &= P_p(k)H^T(k)[H(k)P_p(k)H^T(k) + M(k)R(k)M^T(k)]^{-1} \\ \hat{x}_m(k) &= \hat{x}_p(k) + K(k)\left(z(k) - h_k(\hat{x}_p(k), 0)\right) \\ P_m(k) &= (I - K(k)H(k))P_p(k) \end{split}$$

4.5 Hybrid KF (HKF)

System with continuous process model and discrete measurements:

$$\dot{x}(t) = q(x(t), u(t), v(t), t)$$
 $E[v(t)] = 0;$ $E[v(t)v(t+T)^T = Q_c \delta$
 $z[k] = h_k(x(k), w(k))$ $E[w(k)] = 0;$ $Var[w(k)] = R$

Initialization: $\hat{x}_m(0) = E[x_0] = x_0; \quad P_m(0) = Var[x_0] => P_0$

Step 1 (Prior Update):

Solve
$$\dot{\hat{x}}(t) = q(\hat{x}(t), u(t), \mathbf{v=0}, t)$$
 for $(k-1)T \le t \le kT$ and $\hat{x}((k-1)T) = \hat{x}_m(k-1)$ Then $\hat{x}_n(k) = \hat{x}(kT)$

Solve
$$\dot{P}(t)=A(t)\,P(t)+P(t)\,A^T(t)+L(t)\,Q_c\,L^T(t)$$
 for $(k-1)T\leq t\leq kT$ and $P((k-1)T)=P_m(k-1)$ where $A(t)=\frac{\partial q}{\partial x}(\hat{x}(t),u(t),0,t)$ and $L(t)=\frac{\partial q}{\partial v}(\hat{x}(t),u(t),0,t).$ Then $P_p(k)=\dot{P}(kT)$

Step 2 (Measurement Update): Same as EKF $z(k) \rightarrow z[k]$

5 Particle Filter

Process model: Same as EKF

Initialization: Draw N samples $x_m^n(0)$ from f(x(0))

Step 1 (Prior Update): draw N samples for $v^n(k-1)$

$$x_p^n(k) = q_{k-1}(x_m^n(k-1), v^n(k-1))$$

Step 2 (A Posterior):

$$\beta_n = \alpha f_{z|x(k)};$$
 $\alpha = \left(\sum_{n=1}^N f_{z_n|x_p}\right)^{-1}$

Resampling:

Select random number r on uniform [0,1], find \bar{n} s.t. $\sum_{n=1}^{\bar{n}} \beta_n \geq r$ and $\sum_{n=1}^{\bar{n}-1} \beta_n \leq r$. Then draw new particles from old particles as if they were a PDF. New particle subset:

$$x_m^n(k) = x_n^{\bar{n}}$$

5.1 Roughening

Perturb particles after resampling: $x_m^n(k) \leftarrow x_m^n(k) + \Delta x^n(k)$

Where $x^n(k)$ is from a zero-mean finite-variance distribution, e.g $Var[\Delta x_i^n(k)] = \sigma_i^2$ and $\sigma_i = KE_i N^{-1/d}$ where

K: Tuning Parameter
b: Dimension of the state space

 $N^{-1/d}$: Space betw. nodes of the corresponding uniform square grid E_i : $= \max_{n_1,n_2} |x_{m,i}^{n_1}(k) - x_{m,i}^{n_2}(k)|$

6 Observer Based Control

6.1 LTI Observer

LTI System:

$$x(k) = Ax(k-1) + Bu(k-1) + v(k-1)$$

$$z(k) = Hx(k) + w(k)$$

Linear Static Gain Observer (Luenberger Observer):

$$\begin{split} \hat{x}(k) &= A\hat{x}(k-1) + Bu(k-1) + K(z(k) - \hat{z}(k)) \\ \hat{z}(k) &= H(A\hat{x}(k-1) + Bu(k-1)) \\ e(k) &= (I - KH) \, A \, e(k-1) \end{split}$$

 $e(k) \to 0$ for $k \to \infty$ only if (I - KH)A is stable.

Steady State:

$$\hat{x}(k) = (I - K_{\infty}H) A \hat{x}(k-1) + (I - K_{\infty})B u(k-1) + K_{\infty}z(k)$$

The steady-state KF is one way to design the observer gain K (optimal in minimizing the Steady State mean squared error).

(A, H) detectable $\Rightarrow K$ exists such that (I - KH)A is stable.

6.2 Static State Feedback Control

Design of a controller without paying attention to the state estimation:

$$x(k) = Ax(k-1) + Bu(k-1)$$
 (Process without noise)
 $z(k) = x(k)$ (Perfect State information)
 $u(k) = F \cdot z(k) = F \cdot x(k)$ (Control Law)

Closes loop dynamics: x(k)=(A+BF). Hence system is stable if (A+BF) is stable. Such an F exists only if (A,B) is stabilizable. If (A,B) is stabilizable and (A,G) detectable, then F is given by

$$F = -(B^T P B + \bar{R})^{-1} \cdot B^T P A; \qquad P \ge 0$$

 $P \text{ from DARE: } P = A^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - A^T P B (B^T P B + \bar{R})^{-1} \cdot B^T P A + \bar{Q} - \bar{Q$

6.3 Separation Principle (Linear Systems only)

Combining Luenberger Observer and Static State Feedback control yields:

$$\begin{bmatrix} x(k) \\ e(k) \end{bmatrix} = \begin{bmatrix} A+BF & -BF \\ 0 & (I-KH)A \end{bmatrix} \cdot \begin{bmatrix} x(k-1) \\ e(k-1) \end{bmatrix}$$

Eigenvalues of closed loop are given bei Eigenvalues of (I-KH)A and (A+BF). System is stable as long as there exists no $|\lambda|>1$.

6.4 Separation Theorem

- 1. Design steady-state KF which does not depend on $\bar{Q}, \bar{R}. \Rightarrow \hat{x}(k)$
- 2. Design state-feedback u(k) = Fx(k) and put both together.