

# Given a helical compression spring in a spring-mass-damper system, what are optimal springs?

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## Abstract

## 1 Introduction

The use of mechanical switches in industry is a cornerstone of the modern world. Many mechanical switches are designed to use a spring. Depending on the use of the switch, the spring can be optimized for the function of the spring.

For example, consider an acceleration switch in figure 1.

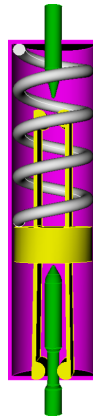


Figure 1: An example of an acceleration switch

**Describe problem, approach, and summarize contribution and results.** This switch is used in high acceleration testing. The use is to only record information at crucial times of the test. For this reason when a certain force is exerted on the switch the pins at both ends will connect. When this happens we have a circuit that will enable data collection. It is important that the switch does not open too soon or too late otherwise the data collection will be too large or too little. This is just one example of a switch that we must know the best spring to make the performance maximal. For a more in depth look at this example look at [1]

Given that a switch may be used in a myriad of ways, it is important that one can find an optimal spring, after the use of the spring is known. This leads to an optimization problem. Even more this leads to an optimization problem that requires the flexibility to allow how a spring is determined to be optimal by an objective function and constraints. In addition there are fabrication constraints that exist during manufacturing.

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Given any constraint or objective function it will depend on a set of variables. In optimization we only wish to concern ourselves with the state variables that are allowed to change during optimization. For this reason, we construct a spring object that will hold all attributes of a spring and we can pull the relevant variables when it is determined what they are.

In addition to this spring object, to reduce the uncertainty of the problem we conduct a sensitivity analysis of the objective function subject to the constraints and variables given. Allowing the user to reduce the state variables if it is determined that for a set of variables given there exist insensitive state variables.

A main contribution of this work is the framework to add constraints and objectives that may be unknown at the point of this paper. In parallel to this we have built a framework that is flexible enough to address the issue of unknown constraints and objectives. **ADD!**

**review history and existing literature** Designing an optimal spring is not a new problem. In 2010 at the SAMSI IMSM workshop a team considered the design of an acceleration switch with enabled uncertainty. In fact, the switch they considered was in figure 1. This approach lead to a paper [1]. This is not the only approach to uncertainty, in [2] probabilistic response surface methodology was implemented to investigate the complications of uncertainty in designing a spring. In addition to these types of approaches it is possible to narrow focus to a single parameter, in [3] they focus on the spring stiffness. In [4] they attempt to design an optimal spring, with the introduction of a sizing tool. All references listed are informed to some extent by [5].

Our approach is not limited to an acceleration switch, instead it is but a special case of our approach. We do not focus on a set of parameters or attempt to fix the uncertainty of the spring design problem initially. We attempt to allow any possible construction of a spring optimization possible.

This does not rule out if a construction is not physically or mathematically invalid. We will dispose of that case when we are unable to find a feasible point for optimization within our feasibility check. In summary, we need to allow any possible construction of a spring design problem, and adjust accordingly.

**outline** In this paper we will give a description of the springs of interest, helical compression springs. Next, the formulation of the problem, and the approach taken to the problem. Following will be a section on workflow with descriptions of each step in the workflow. Lastly, we will discuss a few case studies given the framework constructed and a summary with future work that can be worked on.

## 2 Helical Compression Springs

Helical springs are the typical spring that comes to most peoples mind, for illustrative purposes, see figure 2.

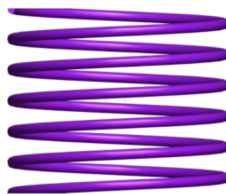
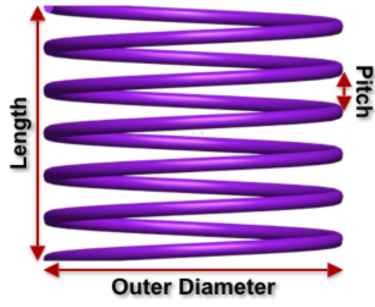


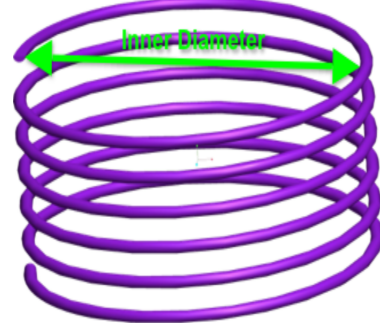
Figure 2: An example of a helical compression spring.

Below is a list of a spring's key design parameters. We have added a few illustrations to illustrate some of the parameters.

1. Spring's inner diameter  $d_i$ , illustrated in figure 3b.
2. Spring's outer diameter  $d_o$  illustrated in figure 3a.
3. Spring's wire diameter  $d_w$ .
4. Total number of spring coils  $N_t$ .
5. Active number of spring coils  $N_a$ , active coils are not touching any other coils, and is subject to the spring being closed or open.



(a) Pitch, outer diameter, and length of a spring.



(b) Inner diameter

Figure 3: A few illustrations of parameters for a helical compression spring.

6. Pitch  $p$  illustrated in figure 3a.
7. Spring's free length  $L_{free}$ , the spring's length without any force applied.
8. Spring's solid length  $L_{solid}$ , the spring's length when all coils are compressed together.
9. Spring's open length  $L_{open}$ , the spring's length at open position, open is beginning state.
10. Spring's open length  $L_{close}$ , spring length at close position, close is the ending state.
11. Spring's open length  $L_{hard}$ , the maximum a spring can compress for the application.
12. Spring's open force  $F_{open}$ , this is the force on the spring in open position.
13. Spring's shear modulus  $G$ , this is determined by the material of the spring.
14. Spring's youngs modulus  $E$ , this is determined by the material of the spring.
15. Spring's poisson ratio  $\nu$ , this is determined by the material of the spring.
16. Ultimate torsional stress, UTS.

In addition to these parameters there are the following attributes that are empirical. We care about these attributes within some regime. This is because outside of certain conditions these attributes exhibit special behavior.

Spring Rate:

$$k = \frac{G}{8N_a} \frac{d_w^4}{(d_i + d_w)^3} \quad (1)$$

Spring Index:

$$C = \frac{d_i}{d_w} + 1. \quad (2)$$

Coil Binding Gap

$$g = \frac{L_{hard} - L_{solid}(d_w, N_a; ec)}{N_t - 1} \quad (3)$$

Max Shear Stress

$$\frac{G(L_{free} - L_{hard})}{4\pi N_a(ec)} \left[ \frac{d_w(4d_i^2 + 9.46d_id_w + 3d_w^2)}{d_i(d_i + d_w)^3} \right] < UTS \quad (4)$$

Diametral Expansion

$$d_{expand} = d_w + \sqrt{(d_i + d_w)^2 + \frac{p^2 - d_w^2}{\pi^2}} \quad (5)$$

### 3 The Problem

Design an algorithm that optimizes springs with interchangeable objectives and constraints. In addition, attempt to incorporate properties stress relaxation and creep into the available objectives and constraints.

A list of possible constraints/objectives given in minimization form is below

1.  $d_i < d_i^{max}$
2.  $d_i < d_o$
3.  $d_i + 2d_w < d_o^{max}$
4.  $d_{expand} - d_0^{max} < 0$
5.  $\frac{G}{8N_a} \frac{d_w^4}{(d_i + d_w)^3} - k_{max} \leq 0$
6.  $\frac{d_i}{d_w} + 1 - C_{max} < 0$
7.  $(L_{free} - L_{open}) \frac{G}{8N_a} \frac{d_w^4}{(d_i + d_w)^3} - F_{open} = 0$
8.  $\frac{L_{hard} - L_{solid}}{N_t - 1} + g_{min} \leq 0$
9.  $\frac{L_{free}}{d_i + d_w} - \pi \sqrt{\frac{2(2\nu + 1)}{\nu + 2}}$
10.  $-UTS + \frac{G(L_{free} - L_{hard})}{4\pi N_a(ec)} \left[ \frac{d_w(4d_i^2 + 9.46d_id_w + 3d_w^2)}{d_i(d_i + d_w)^3} \right] < 0$

This list is not exhaustive as we want a user to be able to define new constraints and objectives. In addition to these we should be able to minimize any parameter of the spring.

#### **ADD RELAXATION HERE!**

In order to simplify the problem we have made some assumptions. First, we have assumed that constraints and objectives are all in terms of the number of total coils. This is to reduce the complexity of knowing if a constraint is dependent on the active number or total number of coils. These two numbers are dependent on the end conditions of the spring, whether it is open or closed at the end.

For simplicity we also will consider all springs to be have a closed end condition. With these assumptions we simplify our constraints for pitch,  $p$ , solid length,  $L_{solid}$ , and the diametral expansion,  $d_{expand}$ .

#### **JUSTIFY ASSUMPTIONS**

**Describe your data, how you collected them, their properties, and whether you did anything to them (removed noise, filled in missing data, applied normalizations).**

### 4 The Problem

- Give a precise technical description of your problem.
- State and justify all your assumptions.
- Define notation.
- Describe your data, how you collected them, their properties, and whether you did anything to them (removed noise, filled in missing data, applied normalizations).

## 5 The Approach

To be as flexible as possible we must be able to handle constraints and objectives that have an unknown number of variables a priori. To handle this uncertainty we instead of evaluating an objective or constraint with a set of values we evaluate with a "spring object" in the programming sense [6]. This spring has all the attributes of interest and the function merely picks what values it needs for evaluation.

This approach is also implemented in the design of a constraint and objective. An objective is an expression that we must be able to evaluate. A constraint is an expression that we must evaluate and check if this evaluation violates the constraint condition. We use the idea of inheritance and let a constraint inherit the properties of being an objective with additional framework to compare to a condition. This allows the user to interchange constraints and objectives seamlessly.

Along with the flexible software design, we have implemented the ability to run feasibility and sensitivity checks before trying to optimize. This will allow the user to know additional information about the problem. First, from feasibility, the user will know quickly if the run is unable to find a feasible point to run optimization. Second, from sensitivity, the user can know which parameters will dramatically change the optimization versus which parameters are unnecessarily adding to the dimension of the optimization space.

## 6 The Approach

- Present and justify your approach for solving the problem.
- Explain the advantages of your approach over existing ones.
- Tell a story. Don't just say: "I did this, then I did this, and at last I did this".

## 7 Workflow

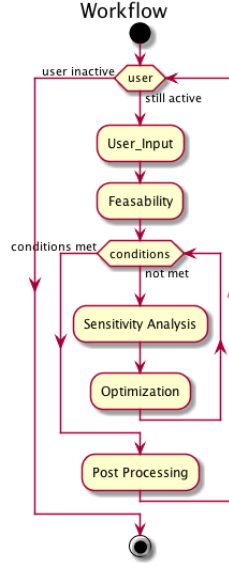


Figure 4: Illustration of the flow of our approach.

Above is an illustration of the workflow that is our approach. This section will go in depth into the feasibility, sensitivity analysis and optimization of our approach.

### 7.1 Feasibility

### 7.2 Sensitivity Analysis

As the dimension of design variable space increases, the computational expense of the optimization procedure increases. To reduce the computational expense, it is often desirable to reduce the design variable space by removing the variables that have very little influence on the objective function. Thus, a dimension reduction strategy is required to reduce the design variable space. Dimension reduction approaches, in the literature have been divided into two categories - (1)filter approach, and (2)wrapper approach. In the filter approach, the input variables are ranked according to a ranking criterion and the most dominant variables can be selected by assuming a threshold influence value. In the wrapper approach, a subset of variables is selected from the list of all possible subsets of the input variables that best estimate the output variable. An optimization technique is used to obtain the best subset of input variables. In this work, the variance-based Global Sensitivity Analysis (GSA), a filter approach, is used for dimension reduction. Note that the input variables represent the design variables for the objective function.

Consider a objective function,  $G$ , with  $n$  design variables given by  $x_1, x_2, \dots, x_n$ , given by

$$Y = G(x_1, x_2, \dots, x_n)$$

In GSA, two types of indices can be calculated for each variable - first order index and total effects index. The first-order index ( $S_i^I$ ) quantifies the uncertainty contribution of an input variable, without considering its interactions with other variables, to the output variable uncertainty. Similarly, the total effects index ( $S_i^T$ ) quantifies the uncertainty contribution of an input variable by considering its interactions with all variables, to the output uncertainty. The expressions for the two sensitivity indices are given below as

$$S_i^I = \frac{V_{X_i}(E_{X_{-i}}(Y|X_i))}{V(Y)}$$

$$S_i^T = \frac{E_{X_{-i}}(V_{X_i}(Y|X_{-i}))}{V(Y)}$$

Given a design range (lower and upper bounds), a variable can be assumed to be uniformly distributed in the design range. For each variable, the total-effects index is calculated and if it is less than an assumed

threshold value, then that variable is assumed insensitive and removed from the optimization procedure. Thus, dimension reduction is implemented for a faster design optimization.[7] [8] [9] [10]

### 7.3 Optimization

[11] [12] [13] [14]

## 8 Computational Experiments

### 8.1 Basics about uni-axial creep and stress relaxation

The spring is heated to  $0.3 - 0.5T_m$  ( $T_m$  is the melting temperature of the material) and loaded by a tensile force. The induced normal stress  $\sigma$  is much less than the yield limit of the material  $\sigma_y$ . The load and temperature are constant throughout the test. The strain  $\epsilon^{cr}$  will slowly increase.

Conventionally, creep can be divided into 3 stages. In the first stage(primary/reduced/transient), the creep strain rate decreases to a certain value(minimum creep rate). The second stage(secondary/steady/stationary creep) is characterized by a nearly constant creep rate(minimum creep rate). In the third stage(tertiary creep), the creep strain rates increases rapidly and leads to rupture. The first stage is usually reversible with time after unloading, while the second/third ones are not. Since the primary creep occurs in a short duration and the tertiary one leads quickly to rupture, the secondary creep is under most serious consideration in many design in many engineering applications.

Stress relaxation is the phenomenon that the stress decreases when the strain is held constant in time. During the test the load is continuously decreased in such a way that the initial strain remains constant.

### 8.2 Creep rate law of material

The starting point is the assumption that the creep rate may be described as a product of two separate functions of stress, temperature and time

$$\epsilon^{cr} = f_\sigma(\sigma)f_T(T)f_t(t)$$

The widely used functions of stress  $f_\sigma(\sigma)$  are:

$a\sigma^n$	Norton, 1929, Bailey, 1929
$b\left(\exp \frac{\sigma}{\sigma_0} - 1\right)$	Soderberg, 1936
$a \sinh \frac{\sigma}{\sigma_0}$	Prandtl, 1928, Nadai, 1938, McVetty, 1943
$a_1\sigma^{n_1} + a_2\sigma^{n_2}$	Johnson et al., 1963
$a \sinh \left(\frac{\sigma}{\sigma_0}\right)^n$	Garofalo, 1965

where  $a, b, a_1, a_2, \sigma_0, n_1, n_2$  are material constants that could depend on time  $t$ . The dependence on the temperature  $f_T(T)$  is usually expressed by the Arrhenius law

$$f_T(T) = \exp\left(\frac{-Q}{RT}\right)$$

where  $Q$  and  $R$  denote the activation energy and the Boltzmann's constant.

The time dependence part  $f_t(t)$  is

$t$	secondary creep
$bt^m$	Bailey
$(1 + bt^{1/3}) \exp kt$	Andrade
$\sum_j a_j t^{m_j}$	Graham and Walles

For simplicity, we are going to only use the Norton-Bailey law.

### 8.3 Stress relaxation of helical spring

Due to conservation of the total shear strain, the sum of the creep strain  $\epsilon^{cr}$ 's rate of change and that of elastic shear strain  $\epsilon_{el}$  is zero:

$$\dot{\epsilon}_{cr} + \dot{\epsilon}_{el} = 0$$

The elastic shear strain is related to the shear stress by shear modulus  $G$ :

$$\epsilon_{el} = \sigma/G$$

and therefore

$$\dot{\epsilon}_{el} = \dot{\sigma}/G$$

According to Norton-Bailey law(also known as time hardening law),

$$\dot{\epsilon}_{cr}(t) = c\sigma^{n+1}t^{k-1} \quad (6)$$

where  $c$  is the shear strain rate,  $n, k$  are temperature dependent material constants.

Substituting the above two equations to the conservation law,

$$\dot{\sigma}(t)/G + c\sigma(t)^{n+1}t^{k-1} = 0 \quad (7)$$

The initial condition is

$$\sigma(0) = G\theta r$$

where  $\theta$  is the initial twist angle per unit length,  $r$  the radius of wire.

$$\sigma = \left( (G\theta r)^{-n} + \frac{c}{k} G n t^k \right)^{-\frac{1}{n}}$$

The torque can be written as

$$M(t) = 2\pi \int_0^{d_w} r^2 \sigma(r, t) dr = {}_2F_1 \left( \frac{4}{n}, \frac{1}{n}; \frac{4+n}{n}; \frac{c\theta^n G^{n+1} n t^k}{k} \frac{d_w^n}{2^n} \right) M(0)$$

where  $d_w$  is the wire diameter.

Since the spring load is linearly related the torque  $P_z(t) \propto M(t)$ , given the constant deflection  $s$ ,

$$\frac{P_z(t)}{P_z(0)} = {}_2F_1 \left( \frac{4}{n}, \frac{1}{n}; \frac{4+n}{n}; \frac{c\theta^n G^{n+1} n t^k}{k} \frac{d_w^n}{2^n} \right)$$

where

$$\theta = \frac{2s}{\pi N_a ((d_i + d_o)/2)^2}$$

The closer this quantity is to 1, the better the spring quality is.

### 8.4 Creep of helical spring

The starting point is still the Norton-Bailey law (). There is naturally another way to write the shear strain rate:

$$\dot{\epsilon}^{cr} = \dot{\theta} r = \frac{8\dot{s}r}{\pi N_a (d_i + d_o)^2}$$

We obtain  $\sigma$  from substiting the above equation into Norton-Bailey law. Given the constant spring force  $P_z^0$ ,

$$P_z^0 \frac{d_i + d_o}{4} = M(0) = 2\pi \int_0^{d_w} r^2 \sigma(r, t) dr = \frac{\pi}{4} \frac{n+1}{4+3n} \left( \frac{8d_w^{4+3n}\dot{s}}{t^{k-1}(d_i + d_o)^2 \pi N_a c (d_i + d_o)^2} \right)^{\frac{1}{n+1}}$$

It can be deduced that the spring length  $s$  follows

$$s(t) = s(0) + \left( \frac{(d_i + d_o)P_z^0}{\pi} \frac{4+3n}{n+1} \right)^{n+1} \frac{\pi (d_i + d_o)^2 N_a c}{8k d_w^{4+3n}} t^k$$



where  $s(0)$  is the initial spring length. The less the difference of the spring length  $s(t) - s(0)$ , the better the spring quality is.

Give enough details so that readers can duplicate your experiments.

- Describe the precise purpose of the experiments, and what they are supposed to show.
- Describe and justify your test data, and any assumptions you made to simplify the problem.
- Describe the software you used, and the parameter values you selected.
- For every figure, describe the meaning and units of the coordinate axes, and what is being plotted.
- Describe the conclusions you can draw from your experiments

## 9 Summary and Future Work

The ability to interchange constraints and objective functions with any number of design variables allows the user the utmost flexibility. With the addition of feasibility and sensitivity analysis it is possible for any configuration of objective function, constraints, and design variables to be analyzed for refinement. The quantification of stress relaxation and creep allow the user a chance to incorporate these properties into any configuration, especially those that have never been tested.

Some limitations of the approach outlined are as follows. The choice of optimization and sensitivity analysis are fixed, however, they are modularized to allow a different optimization routine and sensitivity analysis to be ported in. Given the amount of flexibility that is enabled, a user will have to be able to decide if a infeasible solution is due to user error.

Future work is bountiful for this approach. More analysis of the stress relaxation and creep could result in better performance. An in depth analysis of different models of stress relaxation and their performance in our model would be beneficial.

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