What is the relationship between the mass of a damped spring-block oscillator {52.48g, 60.94g, 69.72g, 86.51g, 93.47g, 113.27g} and the damping ratio?

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1 Introduction

This essay extends the investigation of simple harmonic motion by studying the damping force of a damped oscillator submerged in water, aiming to scrutinize the relationship between the mass of the block and the damping ratio. By scrutinizing this relationship, the study aims to offer valuable insights that can inform the design of systems seeking to optimize damping levels for safety-related objectives.

1.1 The Research Question

What is the relationship between the mass of a damped spring-block oscillator {52.48g, 60.94g, 69.72g, 86.51g, 93.47g, 113.27g} and the damping ratio?

1.2 Background Information

An ideal and rather theoretical spring-mass system oscillates indefinitely, producing an ongoing sine or cosine curve. In reality, there will be a damping force that can be as minimally consequential as air resistance or as observable as viscous drag in a liquid. Anyway, energy is dissipated to the surroundings and hence the amplitude will gradually decrease until the oscillation stops. This investigation delves into the relationship between the mass m of an oscillator and the damping ratio ζ for each oscillator, which is a measure of how rapid the amplitude of oscillation drops.

Let us now study the foundational model used in this investigation. The motion of the oscillator is modeled by the following differential equation (Miller, 2004):

$$m\ddot{x}(t) + b\dot{x}(t) + kx(t) = 0 \tag{1}$$

where

- m denotes the mass of the oscillator
- b denotes the damping coefficient that is constant in a system of constant fluid viscosity
- k represents the spring constant
- x(t), $\dot{x}(t)$, and $\ddot{x}(t)$ denote the displacement, velocity, and acceleration of the oscillator respectively, at any time t.

It must be noted that, in the above differential equation, the **damping force**, which will tell us about the damping ratio ζ , is represented by $b\dot{x}(t)$, which is proportional to the speed of the oscillator.

Now, let us quantify the variable ζ , the damping ratio, which is defined as the ratio of the damping coefficient to the critical damping coefficient — the damping coefficient when the system returns to equilibrium in the shortest time possible without completing an oscillation. That is

$$\zeta = \frac{b}{c_c} = \frac{b}{2mw_0}$$

where w_0 is the natural frequency of the system

$$w_0 = \sqrt{\frac{k}{m}} \implies \zeta = \frac{b}{2\sqrt{mk}} \tag{2}$$

This gives us some knowledge about our dependent variable ζ , but we need further information about b to make more meaningful deductions. This is where Stoke's Law comes in.

As previously mentioned, the damping force is proportional to the velocity of the oscillator —

this is a desirable property that allows us to estimate this damping force using Stoke's Law, which also uses the fact that force is proportional to the object's velocity. By doing so, we proceed with the assumption that the damping force is just the viscous drag force.

As per the Data Booklet, Stoke's Law determines the drag force acting upon an object traveling through a fluid – proportional to the object's velocity and is the following per the Data Booklet, in newtons

$$F_d = 6\pi r \eta v$$

where

- r (m) is the radius of the sphere
- η (N s m⁻²) is the viscosity of the fluid at some temperature
- $v \text{ (m s}^{-1})$ is the velocity of the object in the fluid

In the upcoming hypothesis, we work under the reasonable assumption that the damping force is the drag force, which allows us to express b using more meaningful quantities.

Hypothesis **INTRODUCTION** 1.3

1.3 Hypothesis

By previous argument, the constant of proportionality of the damping force with speed is given by $b = 6\pi r\eta$, per Stoke's law. We now use eq. (2) to obtain the following

 $6\pi r\eta = 2\zeta\sqrt{mk}$

$$9\pi^{2}r^{2}\eta^{2} = \zeta^{2}mk$$

$$\frac{\zeta^{2}}{m^{-1}} = \frac{9\pi^{2}r^{2}\eta^{2}}{k}$$
(3)

Proposition 1. For a fixed sphere radius r and viscosity η ,

$$\zeta^2 \propto m^{-1} \tag{4}$$

Equivalently, the graph ζ^2/m^{-1} is ideally a straight line, although not necessarily passing through the origin, as some form of systematic errors are expected.

There exist other physics conditions that we must examine to determine the sensibility of estimating the damping force as the viscous drag of the liquid.

Firstly, one must recognize that Stoke's Law requires that the flow is laminar. This is a reasonable assumption to make given that the spheres are relatively small, and the speed is low; the potential for turbulence is negligible, and even if it is present, the impact would be minimal. Furthermore, the buoyancy force on the object

$$F_b = \rho g V$$

given in newtons, where

- ρ is the density of the fluid, in kg m⁻³
- V is the volume of the object, in m^3
- \bullet g is the gravitational field strength, in ${\rm m}\,{\rm s}^{-2}$

(3)

1.3 Hypothesis 1 INTRODUCTION

is always present but is not modeled in the differential equation at eq. (1). Notwithstanding, the absence of considerations of buoyancy has negligible impact on the results. The setup involves spheres of radius 2.5cm and water of density 997kg m⁻³, then

$$F_b \approx 10 \times 1000 \times \frac{4}{3}\pi (2.5 \times 10^{-2})^3 < 1$$
N

which confirms that the buoyancy force is sufficiently infinitesimal to be neglected in the model.

Null hypothesis (H_0) : There is no relationship between the mass and the damping ratio. Alternative hypothesis (H_1) : There is a relationship between the mass and the damping ratio.

2 Research Design

2.1 Variables

Variables		Explanation	Measurement
Independent Mass m		The masses of the spherical	Measured using an electric
		metal bobs	balance, to two d.p. with
			uncertainty ± 0.01 g
Dependent	Peak Am-	3 peaks will be measured.	Ruler, with uncertainty
plitude		These data points are used	$\pm 0.1 \mathrm{cm}$
		to compute the damping ratio.	

Table 1: Variables of investigation

	Control Variables					
Variable	Rationale	Means of Control				
Liquid viscosity 0.85	To keep the drag coefficient	Using water from the				
$(\mathrm{N}\mathrm{s}\mathrm{m}^{-2})$	per Stoke's Law constant	same source throughout				
		the experiment, and keep				
		the room temperature				
		constant by turning off the				
		air conditioning. In fact,				
		during the experiment, the				
		room temperature was 27°C				
Radius of the sphere, $r =$	This is so that the drag	Using spherical masses of				
2.5cm	force, per Stoke's law, is	the same diameter				
	constant					
Spring constant, $k =$	This is so that the natural	Using the same spring				
$100 \rm N m^{-1}$	frequency of the system is	throughout the experiment.				
	constant	Read from the label on the				
		box.				
Initial amplitude, $A_0 = 5$ cm	So that the damping ratio	Pulling the spring down by				
	is not affected by the initial	equal distances for every				
	conditions	mass. Measured by a ruler				
		with ± 0.1 cm				
Damping coefficient	Linearizes relationship be-	Previous means of control				
	tween damping ratio and	keep fluid viscosity and ob-				
	mass	ject dimensions constant, so				
		the damping coefficient will				
		be constant.				

Table 2: Control variables

2.2 Apparatus and Materials

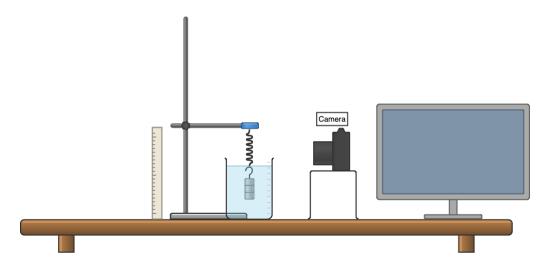


Figure 1: The experimental setup

- 1. Ruler $(\pm 0.1 \text{cm})$
- 2. Electric balance $(\pm 0.01g)$
- 3. Spring with spring constant $k = 100 \text{N m}^{-1}$
- 4. Mass set with six spherical masses of diameter 2.5cm
- 5. Beaker
- 6. Tap water
- 7. Camera keeps a record for future reference
- 8. Thermometer to ensure that the liquid stays at a constant temperature
- 9. Retort stand
- 10. Clamp

2.3 Methodology

- 1. Take a scotch tape, and cut into segments of 8 cm in length.
- 2. Arrange the six masses in increasing order, i.e. $m_1 < m_2 < ... < m_6$
- 3. Fill in the beaker with A mL of tap water
- 4. Measure the temperature of the water, and record as T_0
- 5. Attach the clamp to the retort stand.
- 6. Fix the ruler vertically against the retort stand.
- 7. Place the beaker directly under the clamp such that the clamp lies at the center of the beaker in bird's eye view.
- 8. For i from 1 to 6 inclusive, repeat the following
 - (a) Measure the water temperature and wait until it stays constant at 27°C.
 - (b) Take the *i*th mass, m_i , and attach its hook to the spring.
 - (c) Take a piece of tape, wrap it as many times as possible across the point of connection.
 - (d) Attach the spring-mass pair to the clamp and let the mass hang freely.
 - (e) Adjust the height of the clamp so that the mass is submerged in the water.
 - (f) Measure the height of the mass from the surface of the desk, and record as h_0
 - (g) Adjust the vertical camera position such that it levels with the reading $(h_0 \frac{A_0}{2})$ cm to minimize parallax error of the camera.
 - (h) For j from 1 to 5 inclusive, repeat the following (this represents the 5 repeats)
 - i. Pull the mass down by A_0 cm by reading $h_0 A_0$ from the ruler at eye level. The center of the mass should be the height a which readings are taken.
 - ii. Start the camera recording.
 - iii. Release the mass.

- iv. Record the clip until the 3rd negative peak is reached.
- v. Save the clip as Mass_i_Trial_j.mp4
- vi. Open the clip in a video viewer.
- vii. Identify the first 3 negative peaks, one in each cycle.
- viii. Record the respective heights above the desk as $\{h_k\}_{k=1}^5$.
- ix. Then the corresponding peak amplitudes are $A_k = h_0 h_k$
- (i) Take the average values across the three trials for each peak amplitude.

2.4 Preliminary Trials

Preliminary trials were conducted to identify and resolve potential challenges, as well as to refine the experimental conditions. As planned, lighter masses were used but during the experiment, more material was used to assemble heavier masses; this is because the trial proved that spheres with insufficient masses do not oscillate. Initially, no mechanism was utilized to attach the masses to the spring, which led to slipping. To improve the attachment's security and uniformity, Scotch tape was tested and found to be more effective, significantly reducing variability and enhancing setup repeatability. Precise measurement of the initial height (h_0) and consistent displacement of the mass by A_0 , cm were also challenging. Aligning the ruler vertically proved crucial for accuracy. Adjustments to the clamp and careful ruler leveling minimized parallax error, further reduced by positioning the camera at eye level.

2.5 Risk Assessment

Consideration	Relevance and Mitigation
Safety	All valuable assets are kept away from the experimental setup to
	prevent accidental detachments of the spring-mass system lead-
	ing to the mass being thrown out and causing damage. Moreover,
	the amplitude was kept low to prevent fierce movements of the
	spheres that could break the beaker or computer camera. Also,
	water spillage is minimized to keep electrical devices safe.
Ethical	No use of animals or human bodies involved. However, the record-
	ing selects the location and angle that avoids the storage and ex-
	posure of any personal information or objects of the lab owner,
	ensuring maximum privacy protection.
Environmental	The entire experiment aims to reuse the same water throughout
	to minimize water wastage. Furthermore, the spring was carefully
	pulled to prevent it from passing its elastic limit and becoming
	unusable for future experiments.

Table 3: Risk Assessment

3 Results

3.1 Raw Data

3.1.1 Qualitative Data

During the entire experiment, there is no spillage of water, which means that the volume is kept constant. Moreover, the spring is always able to return to its original length without any permanent deformation, indicating that the spring is not stretched beyond its elastic limit and that Hooke's Law applies throughout.

3.1.2 Quantitative Data

Let m denote the mass of a bob, and A_n denote the n-th peak height.

$A_1 \pm 0.1 \text{ (cm)}$ $A_2 \pm 0.1 \text{ (cm)}$					$A_1 \pm 0.1 \text{ (cm)}$						$A_3 \pm$	0.1 (c	m)		
52.48	2.9	2.9	2.8	2.8	2.9	1.7	1.8	1.7	1.7	1.7	1.0	1.0	1.0	1.1	1.0
60.94	2.9	3.0	3.0	2.9	3.0	1.8	1.9	1.8	1.8	1.8	1.1	1.1	1.1	1.2	1.1
69.72	3.1	3.1	3.1	3.1	3.1	1.9	2.0	1.8	1.9	1.9	1.2	1.2	1.2	1.3	1.2
86.51	3.3	3.3	3.3	3.3	3.3	2.1	2.1	2.2	2.1	2.1	1.4	1.4	1.4	1.4	1.3
93.47	3.5	3.3	3.4	3.3	3.5	2.4	2.2	2.4	2.2	2.2	1.5	1.5	1.5	1.5	1.5
113.27	3.5	3.5	3.7	3.6	3.5	2.3	2.4	2.4	2.5	2.3	1.6	1.4	1.5	1.7	1.4

Table 4: Raw data of peak amplitudes

3.2 Data Processing

3.2.1 Transformation

For the sake of consistency, let us start with the following definition.

Definition 1. Let the tuple (i, j) denote the pair of peaks at i and j respectively, with i < j.

Using the *logarithmic decrement* method per Inman (2008)

$$\delta_{(i,j)} = (j-i) \ln \left(\frac{A_i}{A_j}\right) \text{ and } \delta = \frac{2\pi\zeta}{\sqrt{1-\zeta^2}}$$

where A_i and A_j denote the peak height measurements at the *i*-th and *j*-th peaks respectively. It then follows that

$$\delta^2 = \frac{4\pi^2 \zeta^2}{1 - \zeta^2}$$

$$\delta^2 - \delta^2 \zeta^2 = 4\pi^2 \zeta^2$$

$$\delta^2 = \zeta^2 \left(4\pi^2 + \delta^2 \right)$$

$$\zeta = \frac{\delta}{\sqrt{4\pi^2 + \delta^2}}$$

 ζ , by definition, may be considered as a function of a pair of peaks. This function is applied to **every pair**, producing a set of values of ζ , across which we will take the average to most accurately identify the damping ratio — computing ζ from a mere peak-pair poses vulnerability to random error and lacks reliability. This step is encapsulated in the Python snippet attached in the appendix section at section 5.1, which belongs to an overall script for processing the data and generating the graph.

Note that $\overline{A_i}$ denotes the average value of the *i*-th peak across the five repetitions.

$m \pm 0.01 \; (10^{-3} \text{kg})$	$\overline{A_1} \ (10^{-2} \text{m})$	$\overline{A_2} \ (10^{-2} \text{m})$	$\overline{A_3} \ (10^{-2} \text{m})$	$\zeta^2/10^{-3}$ (unitless)
52.48	2.9	1.7	1.0	7.13
60.94	3.0	1.8	1.1	6.33
69.72	3.1	1.9	1.2	5.67
86.51	3.3	2.1	1.4	4.63
93.47	3.4	2.3	1.5	4.22
113.27	3.6	2.4	1.5	4.83

Table 5: Processed data

3.2.2 Uncertainty Analysis

In this section, one will learn about how uncertainties propagate through the calculation of the damping ratio.

We will adopt the following method for the computation of uncertainties: Let Δx denote the absolute uncertainty of x. For $\Delta x \ll x$, the uncertainty of f(x) is given by the following (Vacher, 2001)

$$\Delta f(x) \approx \frac{\mathrm{d}f(x)}{\mathrm{d}x} \times \Delta x$$
 (5)

From the raw data of the peak heights to ζ , as seen in the data transformation section at section 3.2.1, the initial measurements have gone through a series of functions to finally arrive at a value for ζ . Thus, to visualize the propagation of uncertainty, we will consider how the uncertainty is propagated in each individual step of the transformation linearly. The highlighted rows represent the final stages of the uncertainty propagation for the independent and dependent variables respectively.

Let i, j be the indices of any pair of peaks such that i < j, and also let $\gamma_{i,j} = \frac{A_i}{A_j}$, the following table summarizes the uncertainties involved in the calculation of the damping ratio from a pair of peaks indexed with (i, j). The right-most column is obtained by applying the procedure outlined by eq. (5).

Variable	Represented Transformation	Propagated Absolute Uncertainty
m		$0.01{\rm g} \equiv 10^{-5}{\rm kg}$
m^{-1}		$(m^{-2} \times 10^{-5}) \text{ kg}^{-1}$
$A_k, \forall k$		0.1cm
$\gamma_{i,j}$	$rac{A_i}{A_j}$	$\Delta \gamma_{i,j} = \frac{A_i}{A_j} \left(\frac{\Delta A_i}{A_i} + \frac{\Delta A_j}{A_j} \right)$
$\delta_{i,j}$	$\frac{1}{j-i} \ln \gamma_{i,j}$	$\Delta \delta_{i,j} = \frac{1}{j-i} imes rac{\Delta \gamma_{i,j}}{\gamma_{i,j}}$
$\zeta_{i,j}$	$\frac{\delta_{i,j}}{\sqrt{4\pi^2+\delta_{i,j}^2}}$	$\Delta \zeta_{i,j} = \frac{\mathrm{d}\zeta}{\mathrm{d}\delta} \times \Delta\delta$
$\zeta_{i,j}^2$		$2(\zeta_{i,j}) \times (\Delta \zeta_{i,j})$

Table 6: Uncertainty Propagation

Let us manually carry out this procedural analysis for one of the data points in section 3.2.1 to visualize the propagation of uncertainty:

- 1. Consider the first row, with $m=52.48\times 10^{-3}\,\mathrm{kg}$
- 2. We start by calculating the x-axis uncertainty
 - (a) The uncertainty of the mass reciprocal is calculated as

$$(52.48 \times 10^{-3})^{-2} \times 10^{-5} \approx 0.003631$$

- 3. We now calculate the uncertainty along the y-axis
 - (a) Take a pair of peaks' average heights, say $(\overline{A_1}, \overline{A_2}) = (2.9, 1.7)$
 - (b) We compute $\gamma_{1,2} = \frac{2.9}{1.7} \approx 1.706$ and $\Delta \gamma_{1,2}$

- (c) We move along the uncertainty formulae table in section 3.2.2 to calculate the $\zeta_{1,2}^2$ and its uncertainty.
- (d) We repeat a similar procedure to arrive at a value of 2.71×10^{-3} for $\Delta(\zeta_{1,2}^2)$.
- (e) The process is repetitive by nature, for the sake of clarity, the numeric working is omitted.
- (f) We iterate over previous steps to compute $\Delta(\zeta_{1,2}^2)$, $\Delta(\zeta_{2,3}^2)$, $\Delta(\zeta_{3,1}^2)$, among which we will take the average as the final y-axis uncertainty for the sake of reliability.

To implement the above logic in Python, the previous code snippet in fig. 4 under section 5.1 is extended to include the uncertainty calculations. See section 5.2 for the full code snippet. Running the script again yields the following table of uncertainties:

$\Delta m/10^{-3} \; ({\rm kg})$	$m^{-1}(kg^{-1})$	$\Delta m^{-1} (\mathrm{kg}^{-1})$	$\frac{\Delta \zeta^2 / 10^{-3}}{\text{(unitless)}}$
52.48	19.23	$0.003631 \approx 0.00$	2.71
60.94	16.39	$0.002693 \approx 0.00$	2.24
69.72	14.29	$0.002057 \approx 0.00$	2.17
86.51	11.49	$0.001336 \approx 0.00$	1.91
93.47	10.75	$0.001145 \approx 0.00$	1.63
113.27	8.850	$0.000779 \approx 0.00$	1.62

Table 7: Absolute uncertainties

3.3 Graphical Interpretation

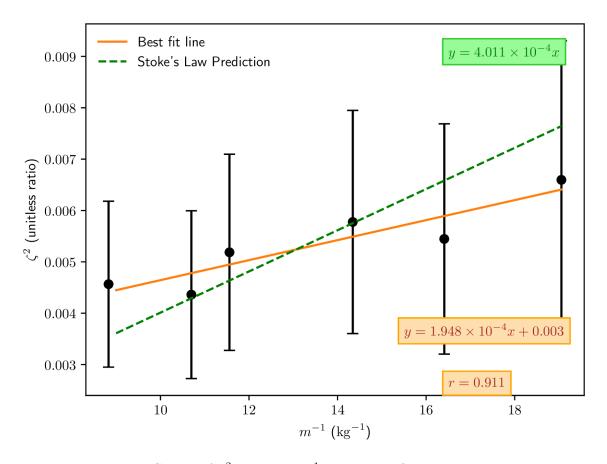


Figure 2: Graph of ζ^2 against m^{-1} , with best-fit line and predicted line

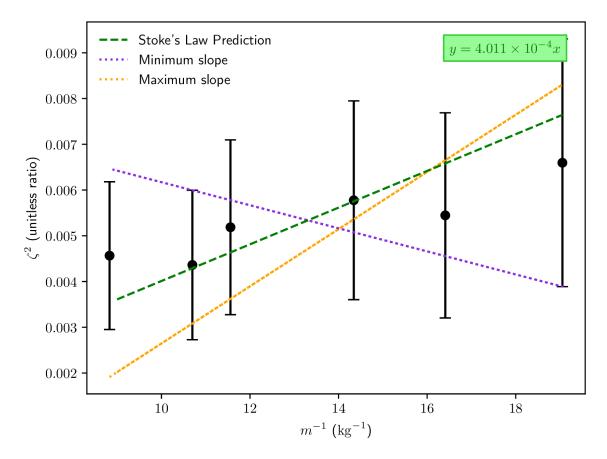


Figure 3: Graph of ζ^2 against m^{-1} — literature review

The two graphs above show the relationship between the damping ratio squared and the inverse of the mass from the resultant dataset, with error bars plotted. The first graph, fig. 2, shows a scatter plot of the data points from section 3.2.1, with the best-fit line and the line predicted using Stoke's Law stated in the hypothesis proposition section. The data points suggest a linear relationship between ζ^2 and m^{-1} , with the Pearson correlation coefficient r = 0.684. The second graph, fig. 3, shows the prediction line in comparison to the maximum and minimum-slope lines resulting from the propagation of uncertainty — indeed, the theoretical prediction does lie within the error bars of the data points.

4 Conclusion

This essay delved into the effect of mass m on the damping ratio ζ of a damped spring-block oscillator submerged in water, with the hypothesis that

$$\zeta^2 \propto m^{-1}$$

The results from the experiment suggest a linear relationship between the damping ratio squared and the inverse of the mass, with a Pearson correlation coefficient of $0.684 \approx 0.7$, indicating a relatively strong linear trend. This evident linearity confirms our implied conjecture that the damping force can be estimated using the viscous drag force per Stoke's Law.

Let us now evaluate our result against the expected gradient K predicted by eq. (3). By substituting the control variables, we obtain

$$K = \frac{9\pi^2 (0.025)^2 (0.85)^2}{100} \approx 4.011 \times 10^{-4}$$

This theoretically predicted gradient falls within the interval of the maximum- and minimumslope lines, namely the range $[-2.264 \times 10^{-4}, 5.086 \times 10^{-4}]$, validating the hypothesis that the damping ratio squared is inversely proportional to the mass and that the constant of proportionality is correctly estimated by our hypothesis, within the experimented range of 52.48 to 113.27 grams.

The observation that the data points are not perfectly collinear is a consequence of the uncertainties that arise from the limitations of measuring devices and human errors. One primary source of random error is the unintentional but inevitable extra force applied when releasing the spring in the liquid. Nonetheless, the mass set did not produce anomalies and massive systematic errors, suggesting that the environment and the experimental setup were controlled effectively.

Finally, it should be noted that the error propagation procedure does create rather significant

error bars due to the already small values of ζ^2 , particularly for smaller masses. However, this should be expected since ζ^2 is very sensitive to a change in mass, and this high sensitivity would naturally lead to larger ranges of uncertainty.

4.1 Evaluation

4.1.1 Strengths

Strength	Observations
Attempt to minimize ran-	Across the three peaks, all possible pairs were used to
dom error in peak ampli-	calculate a value of ζ , across all of them an average is
tudes	taken. This produces the $\overline{\zeta}$ that is closer to the true
	value for each possible oscillation, as the average mea-
	surement is less susceptible to arbitrary changes in the
	system.
Error minimization proce-	The experiment was designed to minimize random and
dures	systematic errors. Taking fix trials and computing the
	average builds upon the attempt to minimize error by
	averaging pairs across three peaks, further diminishing
	the impact of potential anomalies and outliers in the
	dataset.
Consistency	The entire experiment followed a sequence of algorith-
	mic and rigid instructions to ensure that each trial was
	conducted in the same conditions.
Preliminary tests	Preliminary tests were conducted to identify potential
	challenges and refine the experimental conditions, en-
	suring that the final experiment was conducted under
	optimal conditions.

${\bf 4.1.2 \quad Weaknesses -- Random \ Errors}$

Weakness	Observations	Improvements
Inaccuracy	The manual identification of the	Integrating computer vision
of manual	peaks from the video clip may	can automatically identify the
identification	have introduced human error,	peaks would reduce human error
from video	leading to further inaccuracies	and improve the accuracy of the
clip	in the peak amplitude measure-	measurements.
	ments. These uncertainties may	
	not have been captured by the	
	data analysis.	
Release of the	The release of the oscillator may	Using tongs, for instance, would
oscillator	have introduced an additional	ensure a consistent force and
	force, leading to inconsistencies	minimize the introduction of
	in the peak amplitude measure-	additional forces.
	ments.	
Scotch tape	At times the attachment demon-	Using a more secure attachment
attachment	strated signs of slipping or	method, such swivel connectors,
	looseness, which may have af-	would ensure the mass' hook is
	fected the oscillation and effect	firmly attached to the spring.
	of damping.	

${\bf 4.1.3 \quad Weaknesses -- Systematic\ Errors}$

Weakness	Observations	Improvements
Limited sam-	The experiment only used six	Increasing the range of masses
ple strength.	masses, which may not be suffi-	tested would provide a more
	cient to draw generalized conclu-	comprehensive dataset and en-
	sions. This was due to limited	hance the reliability of the re-
	equipment provided by the lab-	sults.
	oratory. Moreover, it does not	
	cover a great range of masses ei-	
	ther, hence the model failed to	
	inspect the behavior of the oscil-	
	latory motion for larger masses	
	and validate the hypothesis for	
	them.	
Varying	The spring constant was as-	Preparing a set of identical
spring con-	sumed to be constant, but in re-	springs and consistently switch-
stant	ality, it may have varied slightly	ing between them would mini-
	with use, leading to inaccuracies	mize fatigue.
	in theoretical prediction of the	
	gradient.	
Camera posi-	The camera positioning may	Through calculations, find the
tioning	have introduced parallax errors,	optimal position to minimize the
	leading to systematic errors in	average uncertainty across the
	all of the peak amplitude mea-	peak measurements.
	surements.	

Large uncer-	The error spans in ζ^2 were large,	Using more accurate measuring
tainty ranges	particularly for smaller masses.	devices, such rulers and electric
$\int in \zeta^2$		balances with even finer resolu-
		tions.

4.1.4 Extensions

A possible extension of this experiment involves investigating the effect of different fluid densities on the damping ratio of the oscillating system. By repeating the experiment with fluids of known densities (e.g., water, glycerol, oil) whose values can be found on the Internet, and keeping control variables constant, i.e. mass, initial amplitude, spring constant, and temperature, one can analyze how changing densities influence the damping behavior. As a hypothesis, the higher the density is, the larger the viscous drag force, and thus the greater the damping ratio.

Alternatively, one may also explore the impact of varying the spring constant on the damping ratio. By using springs varying in stiffness, one can investigate how the damping ratio changes with the spring constant. The hypothesis, based on Proposition 1, would be that the higher the spring constant, the lower the damping ratio, as the spring would exert a greater force to counteract the damping force.

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5 Appendix

5.1 Python Script for Data Processing

```
1 # Calculate the average damping ratio for each row in the dataframe
2 def avgDampingRatio(row: pd.Series):
       ratios = np.array([]) # Create an empty array to store the damping ratios
4
5
      # Iterate over the range of peak indices
      for i in range(PEAK_IND[0], PEAK_IND[1] - 1):
6
7
           # Iterate over the range of peak indices starting from i+1
          # the purpose of this double loop is to calculate the damping
8
           # ratio between every possible pair of peaks
9
          for j in range(i + 1, PEAK_IND[1]):
10
              n = j - i # Calculate the number of cycles between i and j
11
              delta = (1 / n) * math.log(
12
13
                   (row.iloc[i]) / row.iloc[j]
               ) # Calculate the logarithmic decrement between the peaks
14
               zeta = delta / math.sqrt(
15
                  4 * (math.pi) ** 2 + delta**2
16
               ) # Calculate the damping ratio using the logarithmic difference
17
18
               ratios = np.append(
19
                   ratios, zeta
20
               ) # Append the damping ratio to the ratios array
21
22
      return np.average(ratios) # Return the average damping ratio
23
24 def processData():
25
      # reads the data tables and find the average across 5 trials
26
      df = averageData()
27
      # ...
28
29
      # populate the column of damping ratio in the table for each mass
30
      df["Damping Ratio"] = df.apply(
31
          avgDampingRatio,
32
          axis=1,
33
```

Figure 4: Calculating the damping ratio with pandas in Python

5.2 Extended Script with Uncertainty Propagation

```
1\ \mbox{\# Calculate} the average damping ratio for each row in the dataframe
 2 def avgDampingRatio(row: pd.Series, mode: Union["uncertainties", "vals"]):
       if type(row.iloc[-1]) == str:
           return 0
       ratios = np.array([]) # Create an empty array to store the damping ratios
       zetaSqUncertainties = np.array(
       ) # Create an empty array to store the uncertainties of the damping ratios
       # Iterate over the range of peak indices
      for i in range(PEAK_IND[0], PEAK_IND[1] - 1):
            # Iterate over the range of peak indices starting from i+1
           # the purpose of this double loop is to calculate the damping
           # ratio between every possible pair of peaks
           for j in range(i + 1, PEAK_IND[1]):
               n = j - i # Calculate the number of cycles between i and j
               A_i, A_j = row.iloc[i], row.iloc[j] # Get the amplitudes of the peaks
               if type(A_i) != float:
               gamma = A_i / A_j # Calculate the ratio of the amplitudes of the peaks
               delta = (1 / n) * math.log(
               ) # Calculate the logarithmic decrement between the peaks
               errAbsGamma = (A_i / A_j) * (
                   (peakError / A_i) + (peakError / A_j)
               ) # Calculate the absolute error of gamma
 31
               # Calculate the absolute error of delta
 33
               errAbsDelta = errAbsGamma / gamma
               zeta = delta / math.sqrt(
 35
                   4 * (math.pi) ** 2 + delta**2
 36
 37
               ) # Calculate the damping ratio using the logarithmic decrement
 38
 39
                   4 * math.pi**2 / math.pow(delta**2 + 4 * math.pi**2, 1.5)
 40
 41
               ) # Calculate the derivative of zeta wrt delta
 42
 43
               errAbsZeta = (
                   dzeta ddelta * errAbsDelta
 44
 45
               ) # Calculate the absolute error of zeta
 46
               errAbsZetaSq = (
 47
                   2 * zeta * errAbsZeta
 48
               ) # Calculate the absolute error of the squared damping ratio
 49
 50
 51
               ratios = np.append(
 52
                   ratios, zeta
               ) # Append the damping ratio to the ratios array
 5.3
 54
 55
               zetaSqUncertainties = np.append(
                   zetaSqUncertainties, errAbsZetaSq
 57
                ) \# Append the uncertainty of the damping ratio
 58
       return (
 59
           np.average(ratios) if mode == "vals" else np.average(zetaSqUncertainties)
 60
 61
          # Return the average damping ratio or the average
           uncertainties of the damping ratios based on the mode
```

Figure 5: Calculating the damping ratio with uncertainties in Python