

Electrochemical Modeling of PEM Fuel Cells

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Understanding fuel cell behavior

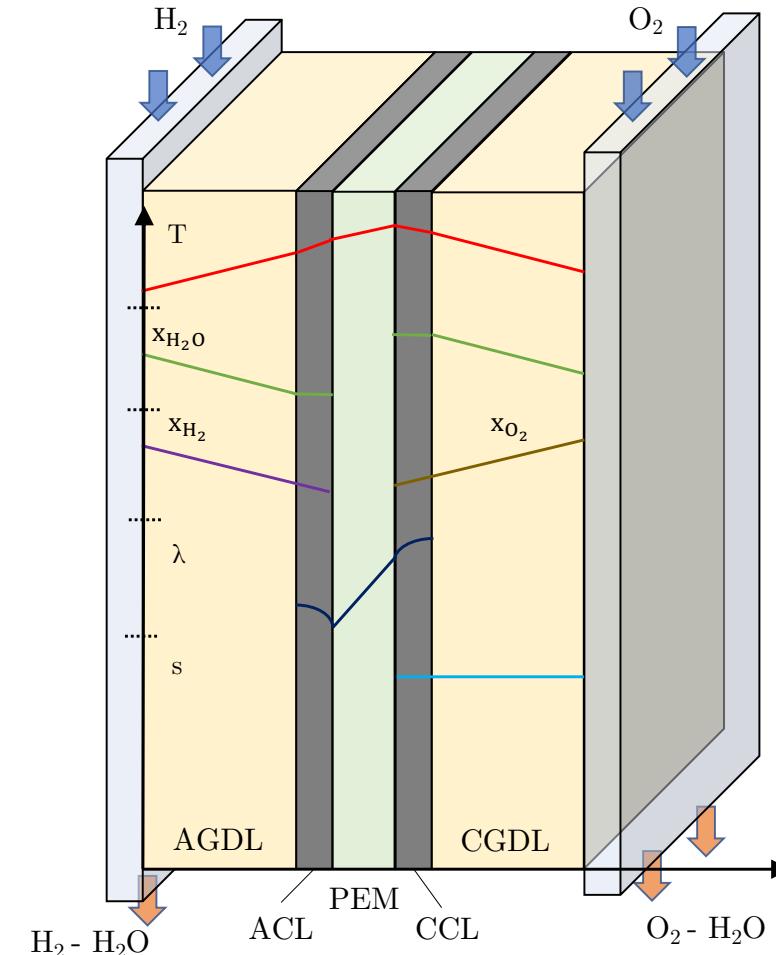
- How do we understand the complex electrochemical phenomena occurring in fuel cells?
- Physical models can help but are often computationally expensive
- Reduced-order modeling gives efficient and accurate solutions of physical models
- Asymptotic analysis provides additional physical insights into dominant effects



Modeling approaches

Different approaches possible:

- Full 3D (serpentine channels)
- Full 2D (straight channels)
- 1D through-cell (lumped channels)
- 1D channel (lumped through-cell)
- 1+1D (decomposed through-cell and channel)





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REDUCED-ORDER MODELING



Two-step approach

1. Non-dimensionalization

- Identify scales
- Prepare for asymptotically reduced-order models
- Reduce stiffness (faster, more stable numerical solution)

2. Asymptotic analysis

- Systematically derive reduced-order model based on dimensionless parameter scales
- Retain same physical parameter values (unlike most other ROM methods)
- Shown to work well for battery models (similar)



Nondimensionalization: basic principles

1. Example: membrane water

$$\frac{\epsilon_i}{V_m} \frac{\partial \lambda}{\partial \hat{t}} = - \frac{\partial \hat{N}}{\partial \hat{x}} + \hat{S}_{ad} + \frac{\hat{a} \hat{j}}{2F}$$

$$\hat{N} = -\hat{D}_\lambda \frac{\partial \lambda}{\partial \hat{x}} + \frac{n_d \hat{i}_p}{F}$$

$$\hat{S}_{ad} = \frac{\hat{k}_{ad}}{\hat{h} V_m} (\lambda_{eq} - \lambda)$$

2. Set

$$\hat{t} = \hat{\tau} t$$

$$\hat{x} = \hat{h} x$$

$$\hat{i}_p = \hat{I} i_p$$

$$\hat{j} = \frac{\hat{I}}{\hat{a} \hat{h}} j$$

\hat{h} : known
 \hat{I} : known
 $\hat{\tau}$: t.b.d.

3. Substitute

$$\epsilon_i \frac{\partial \lambda}{\partial \hat{t}} = \frac{\partial}{\partial x} \left(\frac{\hat{D}_\lambda \hat{\tau} V_m}{\hat{h}^2} \frac{\partial \lambda}{\partial x} - \frac{\hat{I} \hat{\tau} V_m}{F \hat{h}} n_d i_p \right) + \frac{\hat{k}_{ad} \hat{\tau}}{\hat{h}} (\lambda_{eq} - \lambda) + \frac{\hat{I} \hat{\tau} V_m}{F \hat{h}} \frac{j}{2}$$

4. Choose timescale to balance one of the terms; here

$$\hat{\tau} = \frac{F \hat{h}}{\hat{I} V_m} \approx 1s$$

5. Finally

$$\epsilon_i \frac{\partial \lambda}{\partial t} = \frac{\partial}{\partial x} \left(D_\lambda \frac{\partial \lambda}{\partial x} - n_d i_p \right) + k_{ad} (\lambda_{eq} - \lambda) + \frac{j}{2}$$

$$D_\lambda = \frac{\hat{D}_\lambda \hat{\tau} V_m}{\hat{h}^2}; k_{ad} = \frac{\hat{k}_{ad} \hat{\tau}}{\hat{h}}$$

Parameter groupings



Dimensionless through-cell model

$$0 = \frac{\partial}{\partial x} \left(\sigma_e \frac{\partial \phi_e}{\partial x} \right) - j,$$

$$0 = \frac{\partial}{\partial x} \left(\sigma_p \frac{\partial \phi_p}{\partial x} \right) + j,$$

$$\rho c_p \frac{\partial T}{\partial t} = \frac{\partial}{\partial x} \left(k_T \frac{\partial T}{\partial x} \right) + \theta_{ad} k_{ad} (\lambda_{eq} - \lambda) + \theta_{ec} \gamma_{ec} (c_{H_2O} - c_{sat}) \\ + \sigma_e (\nabla \phi_e)^2 + \sigma_p (\nabla \phi_p)^2 + j\eta - \theta_r (1 + \Theta T) \frac{j}{2},$$

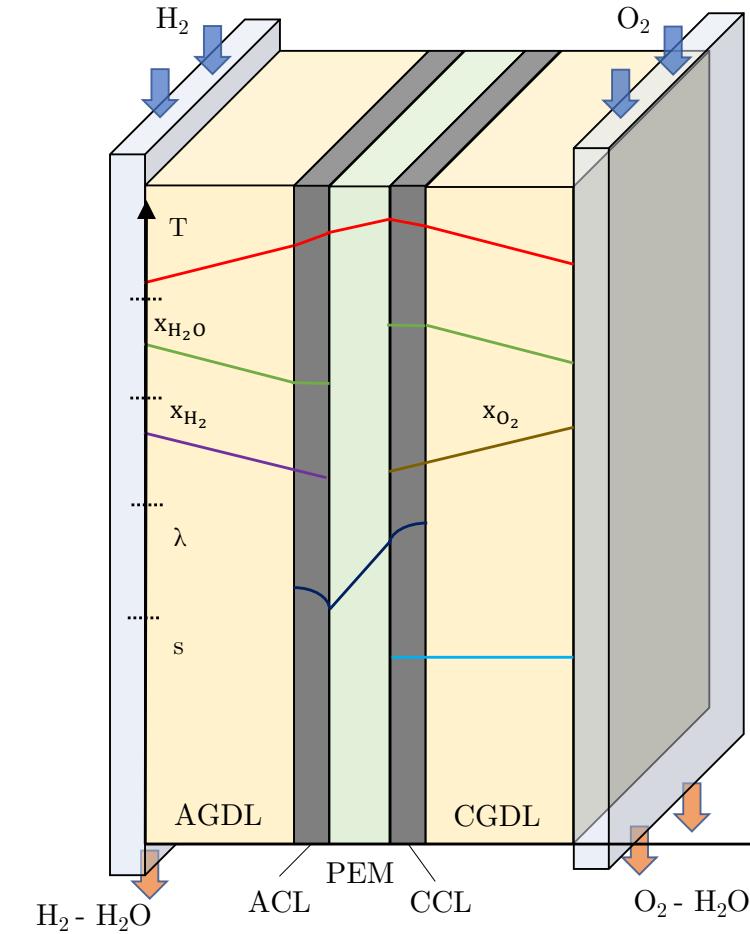
$$\varepsilon_i \frac{\partial \lambda}{\partial t} = \frac{\partial}{\partial x} \left(D_\lambda \frac{\partial \lambda}{\partial x} - n_d i_p \right) + k_{ad} (\lambda_{eq} - \lambda) + r_{H_2O},$$

$$v_m \varepsilon_g \frac{\partial c_{H_2O}}{\partial t} = \frac{\partial}{\partial x} \left(D_{H_2O}^{\text{eff}} \frac{\partial c_{H_2O}}{\partial x} \right) - k_{ad} (\lambda_{eq} - \lambda) - \gamma_{ec} (c_{H_2O} - c_{sat}),$$

$$v_m \varepsilon_g \frac{\partial c_{H_2}}{\partial t} = \frac{\partial}{\partial x} \left(D_{H_2}^{\text{eff}} \frac{\partial c_{H_2}}{\partial x} \right) - \frac{j}{2},$$

$$v_m \varepsilon_g \frac{\partial c_{O_2}}{\partial t} = \frac{\partial}{\partial x} \left(D_{O_2}^{\text{eff}} \frac{\partial c_{O_2}}{\partial x} \right) + \frac{j}{4},$$

$$v_V \varepsilon_l \frac{\partial s}{\partial t} = \frac{\partial}{\partial x} \left(D_s \frac{\partial s}{\partial x} \right) + \gamma_{ec} (c_{H_2O} - c_{sat}),$$





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$$v_m \varepsilon_g \frac{\partial c_{H_2}}{\partial t} = \frac{\partial}{\partial x} \left(D_{H_2}^{\text{eff}} \frac{\partial c_{H_2}}{\partial x} \right) - \frac{j}{2},$$

$$v_m \varepsilon_g \frac{\partial c_{O_2}}{\partial t} = \frac{\partial}{\partial x} \left(D_{O_2}^{\text{eff}} \frac{\partial c_{O_2}}{\partial x} \right) + \frac{j}{4},$$

$$v_V \varepsilon_l \frac{\partial s}{\partial t} = \frac{\partial}{\partial x} \left(D_s \frac{\partial s}{\partial x} \right) + \gamma_{ec} (c_{H_2O} - c_{sat}),$$

large

small

- Electron conductivity large (~uniform electron potential)
- Thermal conductivity large (~uniform temperature)
- Gas diffusivities large (~uniform gas concentrations)
- Evaporation/condensation large
- Fast gas time constants (quasi-steady)
- Liquid water transport slow



Asymptotic analysis: basic principles

1. Dimensionless equation

$$\epsilon \frac{\partial c}{\partial t} = \frac{\partial}{\partial x} \left(\frac{D(c) \partial c}{\epsilon} \right) - j$$

2. Asymptotic expansion ($\epsilon \ll 1$)

$$c = c^0 + \epsilon c^1 + \dots$$

$$j = j^0 + \epsilon j^1 + \dots$$

$$D = D^0 + \epsilon D^1 + \dots$$

3. Substitute

$$\begin{aligned} \epsilon \frac{\partial}{\partial t} (c^0 + \epsilon c^1 + \dots) \\ = \frac{\partial}{\partial x} \left(\frac{(D^0 + \epsilon D^1 + \dots)}{\epsilon} \frac{\partial}{\partial x} (c^0 + \epsilon c^1 + \dots) \right) \\ - (j^0 + \epsilon j^1 + \dots) \end{aligned}$$

4. Match orders of ϵ .

a) $O(1/\epsilon)$:

$$0 = \frac{\partial}{\partial x} \left(D^0 \frac{\partial c^0}{\partial x} \right)$$

So $c^0 = c_{ch}$ (value at the boundary)

b) $O(1)$:

$$0 = \frac{\partial}{\partial x} \left(D^0 \frac{\partial c^1}{\partial x} \right) - j^0$$

Linear equation: easy to solve for c^1



Reduced-order fuel cell model

	Full Model	Linearized model
Membrane water content	Nonlinear diffusion-drag-reaction	Nonlinear diffusion-drag-reaction
Water vapor	Nonlinear diffusion	Single ODE
Oxygen and hydrogen	Nonlinear diffusion	Closed-form solution (steady-state)
Electric potentials (voltage)	Ohm's law + Butler-Volmer	Closed-form solution
Thermal	Full energy balance	Single ODE
Liquid water saturation	Unsaturated flow	Closed-form solution
Channel concentrations	Nonlinear diffusion-convection	Convection only

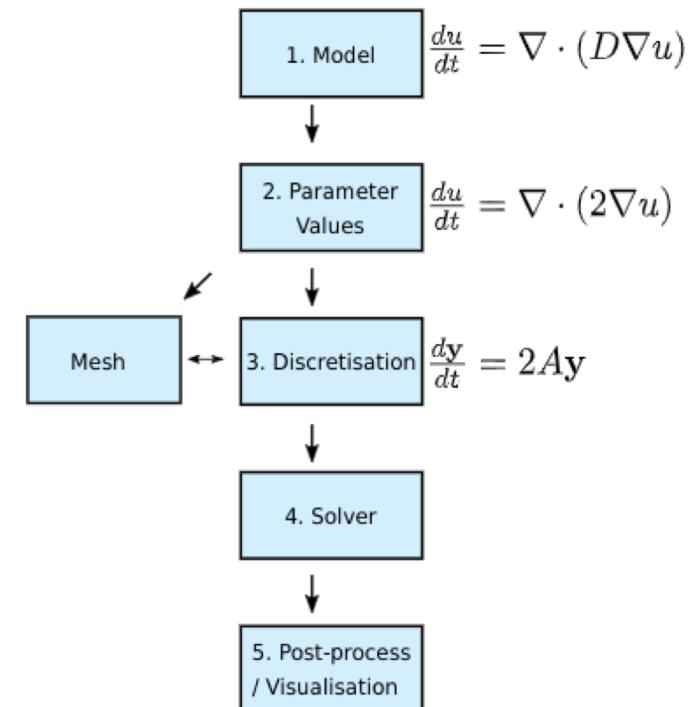


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SIMULATION RESULTS



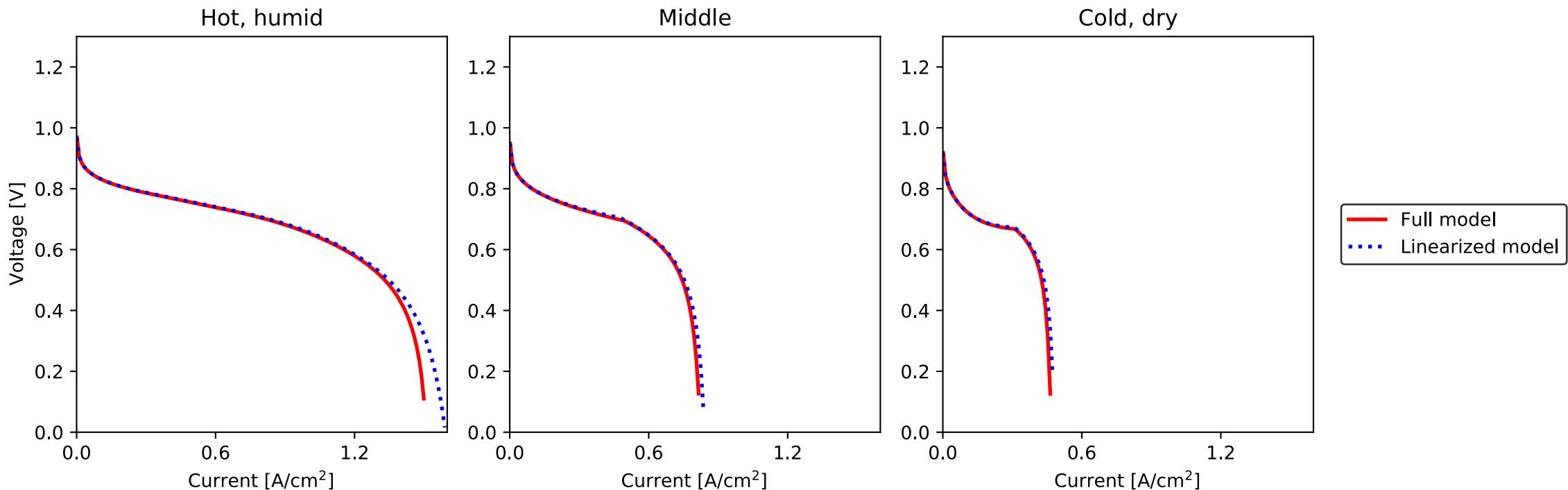
- Models implemented using PyBaMM framework
- Method of Lines:
 - Finite Volume spatial discretization
 - Use IDA (SUNDIALS) to solve resulting DAE system





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Polarization curves

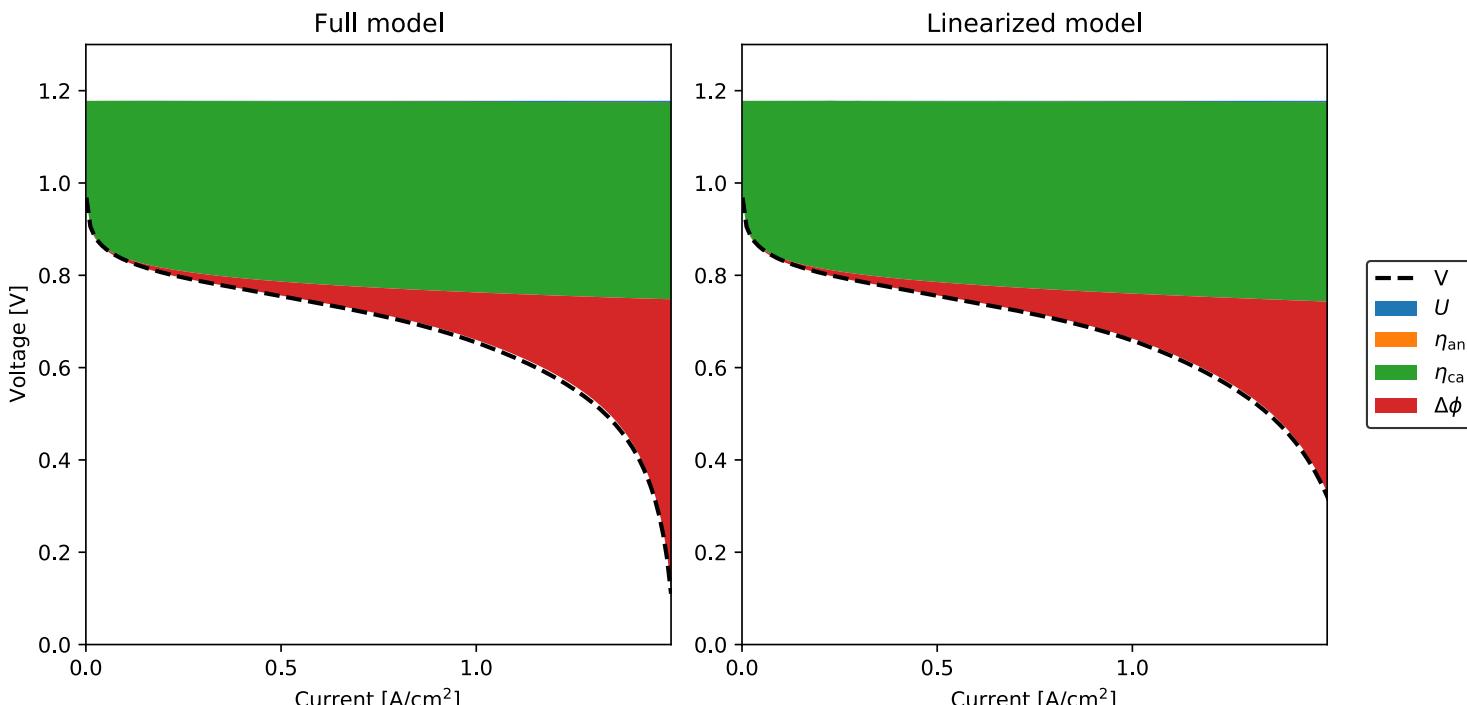




Voltage decompositions

$$V = U - \underbrace{\frac{IF}{RTi_0^{\text{an}}h_{\text{ACL}}}}_{\eta^{\text{an}}} - \underbrace{\frac{F}{2RT(1-\beta^{\text{ca}})} \log \left(\frac{I}{i_0^{\text{ca}}h_{\text{CCL}}} \right)}_{\eta^{\text{ca}}} - \underbrace{\frac{IF}{RT} f(\sigma_p, i_0^{\text{an}})}_{\Delta\phi}$$

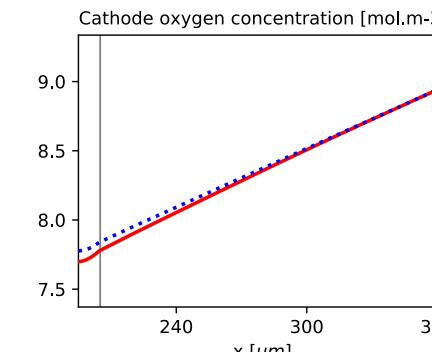
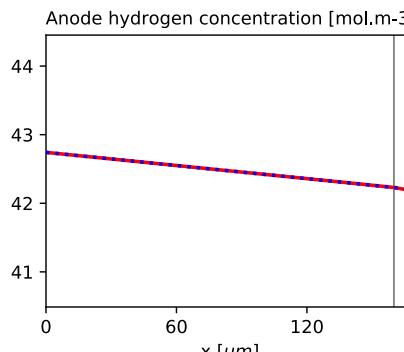
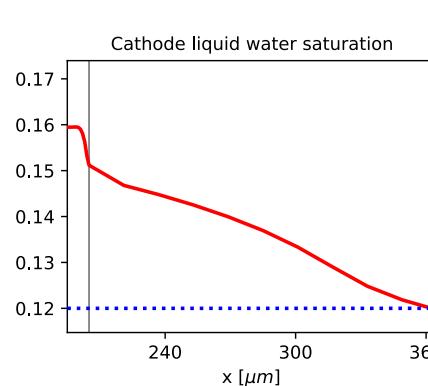
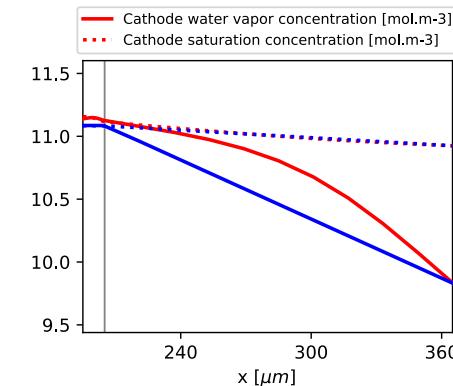
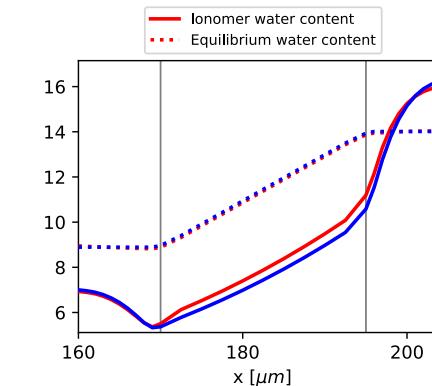
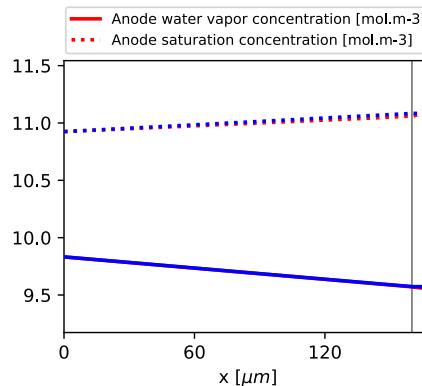
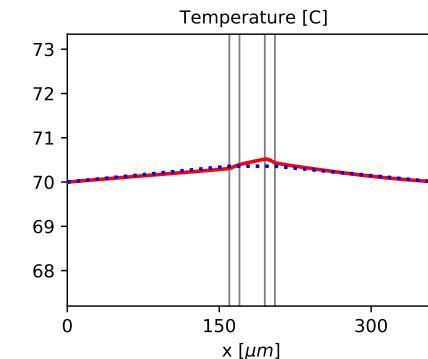
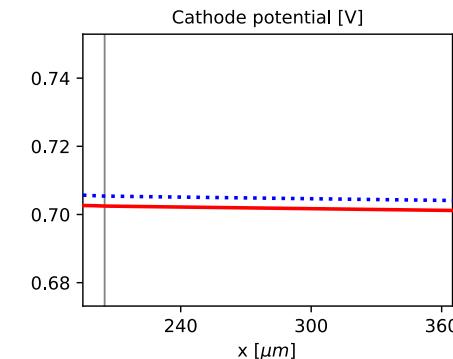
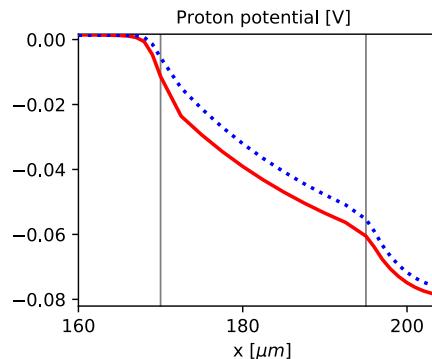
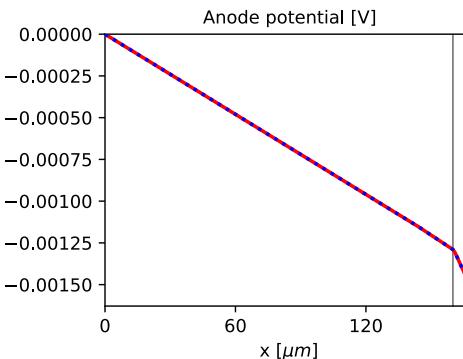
$$f(\sigma_p, i_0^{\text{an}}) = \frac{1}{a\bar{\sigma}_{p,\text{cl}}^{\text{an}} \tanh(ah_{\text{ACL}})} + \int_{x=x_{\text{ACL}}}^{x=x_{\text{PEM}}} \frac{1}{\sigma_p} dx + \int_{x=x_{\text{PEM}}}^{x=x_{\text{CCL}}} \frac{1 - (x - x_{\text{PEM}})}{\sigma_p h_{\text{CCL}}} dx$$



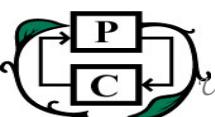


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One-dimensional results



Full model
Linearized model



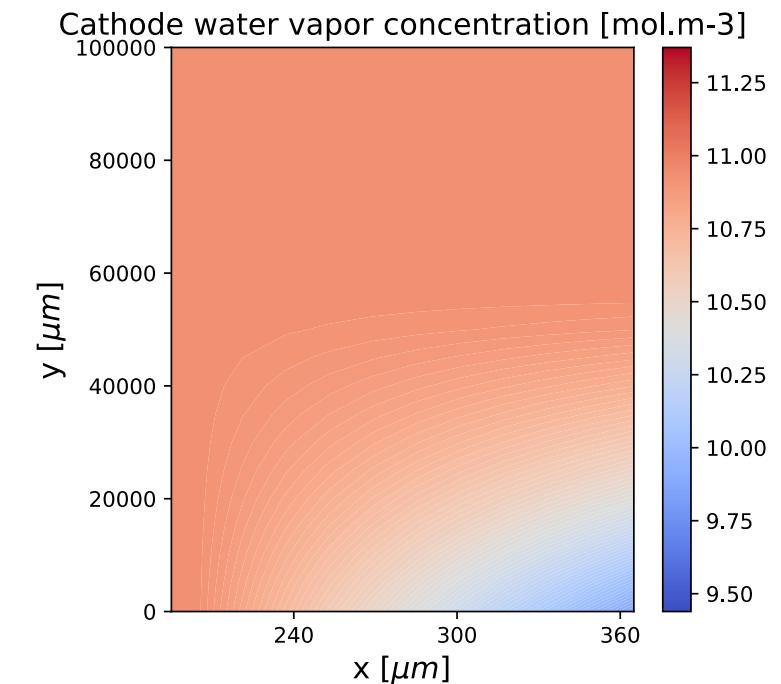
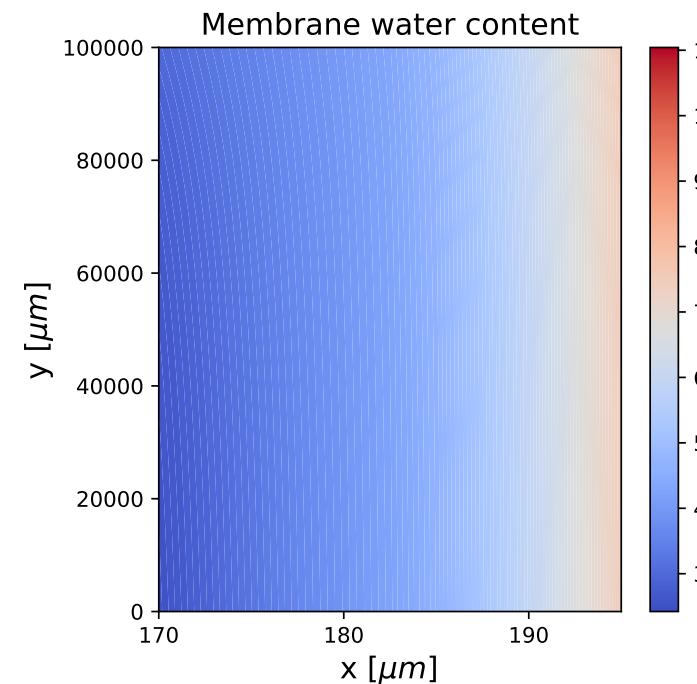
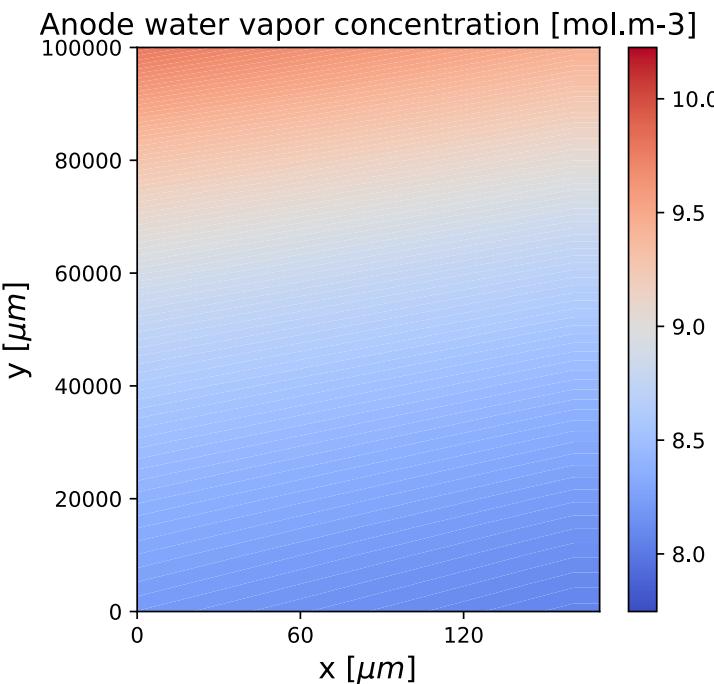
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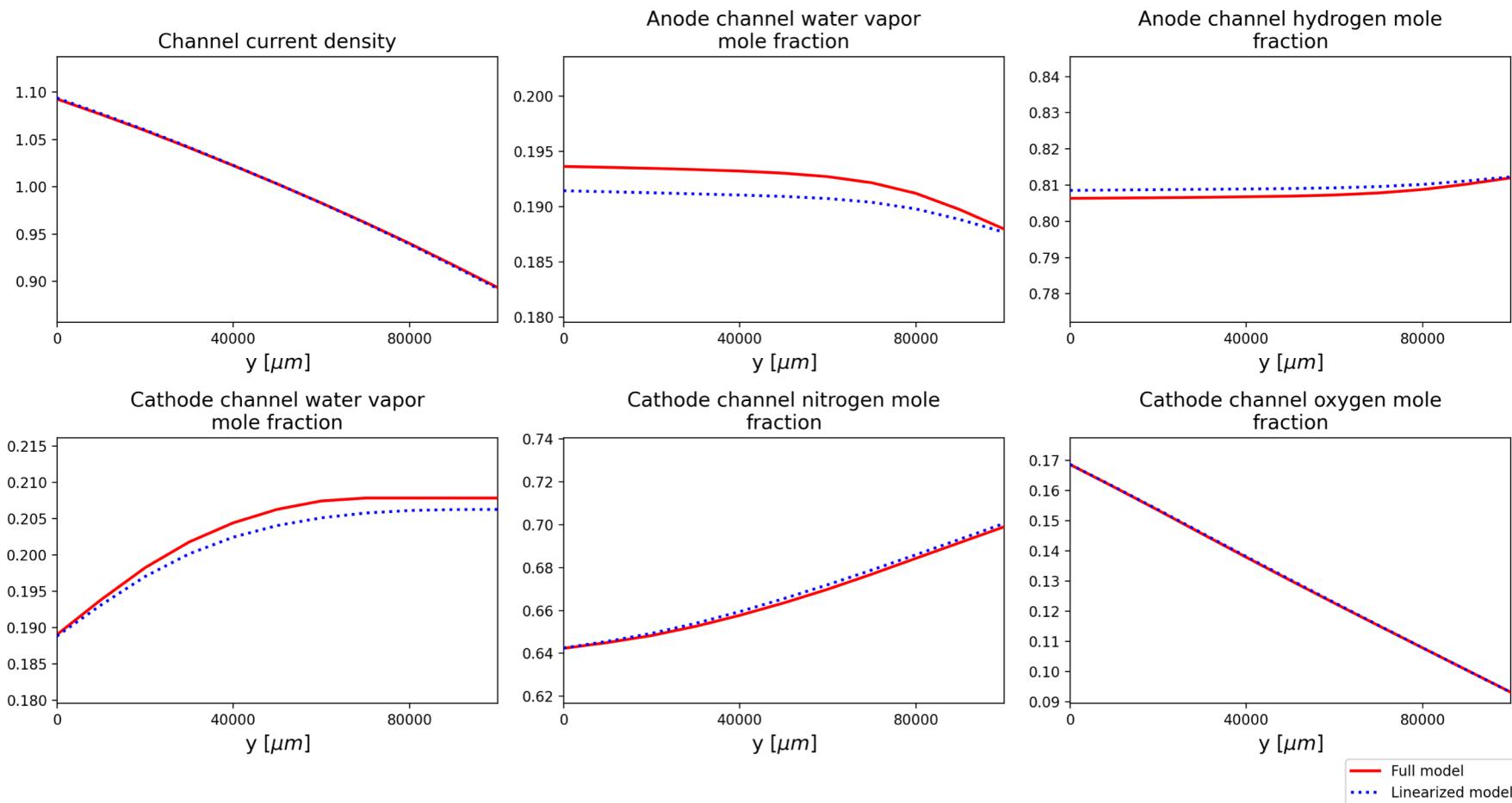
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Two-dimensional results





Two-dimensional results





Model performance

	1D model		1+1D model	
	States	Solve time (s)	States	Solve time (s)
Full model	230	1.40	4740	232
Linearized model	33	0.13	780	3.37

Simulating constant-current operation for 100 seconds.

Simulation with 10 grid points in each through-cell domain (50 total) and 20 grid points in each channel.

Solved using CasADi, with absolute and relative tolerances of 1e-6, on a laptop with a 2.3 GHz 8-Core Intel Core i9 processor



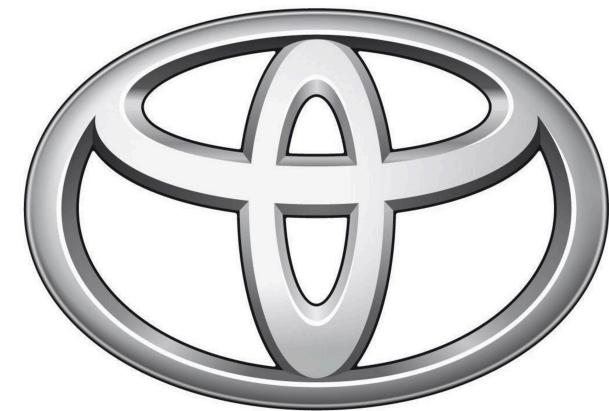
Conclusions

- Reduced-order modeling (from asymptotic analysis) provide efficient and accurate solutions for PEMFC models
- Simplified model give additional insight
 - Closed-form expressions for most variables, but:
 - Membrane water transport is very important and must be fully resolved
- Next step: use these models to learn missing physics



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