

# One dimensional defects

---

## Dislocations

“Introduction to dislocations”

By D. Hull and D.J. Bacon

Section 1.4, 3.1 to 3.6



# One dimensional defects

---

## Dislocations

“Solid State Chemistry and its Applications”

By A. R. West

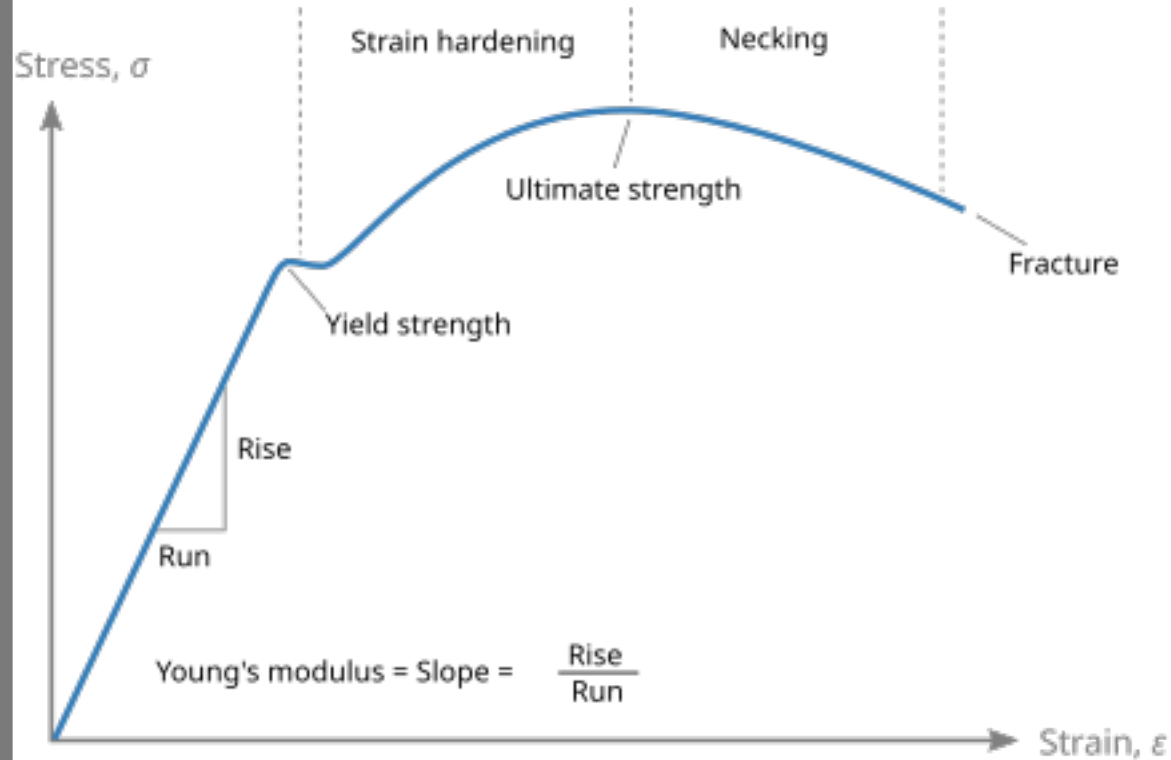
Section 2.5

“Introduction to dislocations”

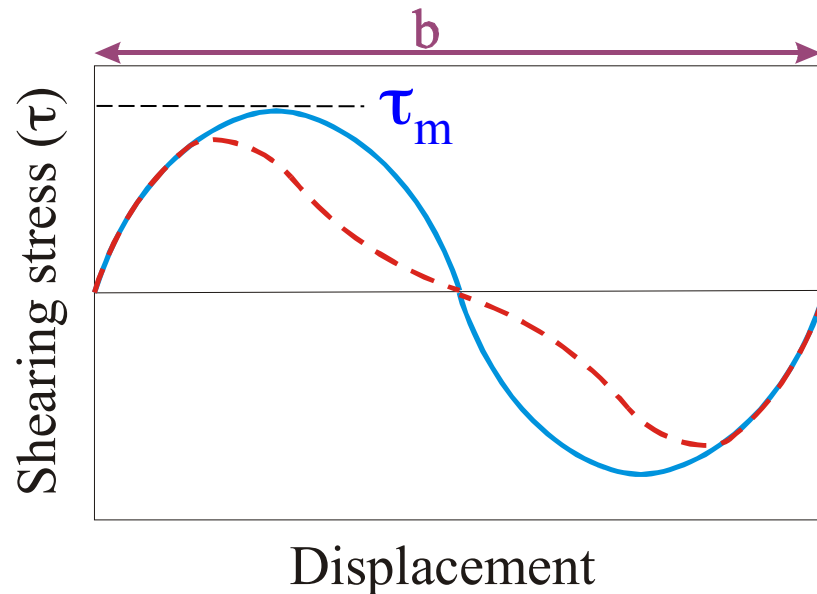
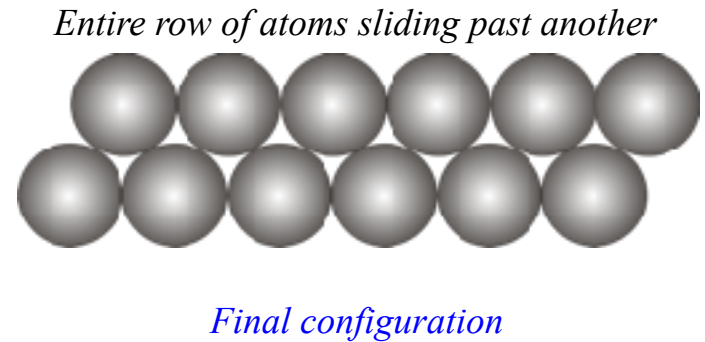
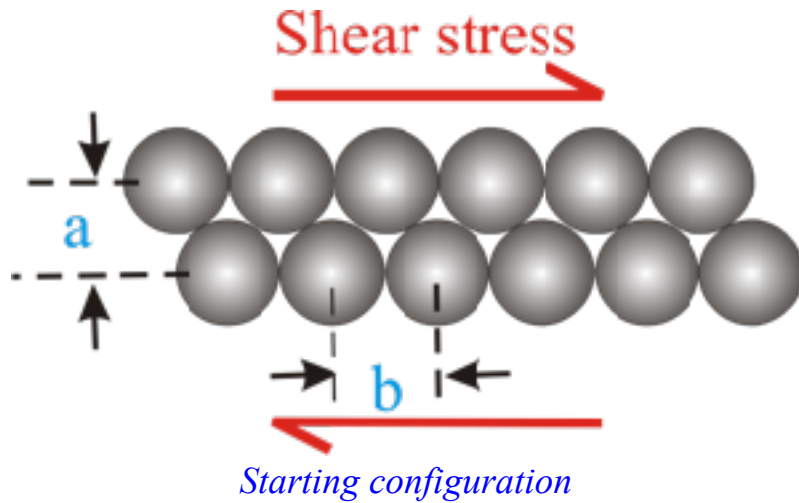
By D. Hull and D.J. Bacon

Section 1.4, 3.1 to 3.6

# Mechanical response of materials



# Extending elastic deformation concept



$$\tau = \tau_m \sin \left( \frac{2\pi x}{b} \right)$$

# Maximum Shear stress

$$\tau = \tau_m \sin \left( \frac{2\pi x}{b} \right)$$

# Maximum Shear stress

$$\tau = \tau_m \sin \left( \frac{2\pi x}{b} \right)$$

Small displacements



# Maximum Shear stress

$$\tau = \tau_m \sin \left( \frac{2\pi x}{b} \right)$$

Small displacements



$$\tau = \tau_m \times \left( \frac{2\pi x}{b} \right)$$

# Maximum Shear stress

$$\tau = \tau_m \sin \left( \frac{2\pi x}{b} \right)$$

Small displacements

$$\tau = \tau_m \times \left( \frac{2\pi x}{b} \right)$$

Hooke's Law:





# Maximum Shear stress

$$\tau = \tau_m \sin \left( \frac{2\pi x}{b} \right)$$

Small displacements

$$\tau = \tau_m \times \left( \frac{2\pi x}{b} \right)$$

Hooke's Law:

$$\tau = G \times \left( \frac{x}{a} \right)$$

# Maximum Shear stress

---

$$\tau = \tau_m \sin \left( \frac{2\pi x}{b} \right)$$

Small displacements

$$\tau = \tau_m \times \left( \frac{2\pi x}{b} \right)$$

Hooke's Law:

$$\tau = G \times \left( \frac{x}{a} \right)$$

Equating R.H.S  $\therefore \frac{G}{a} = \frac{2\pi\tau_m}{b}$

# Maximum Shear stress

$$\tau = \tau_m \sin \left( \frac{2\pi x}{b} \right)$$

Small displacements

$$\tau = \tau_m \times \left( \frac{2\pi x}{b} \right)$$

Hooke's Law:

$$\tau = G \times \left( \frac{x}{a} \right)$$

Equating R.H.S  $\therefore \frac{G}{a} = \frac{2\pi\tau_m}{b}$

$$\text{With } b \sim a, \tau_m = \frac{G}{2\pi}$$



The need  
for a  
different  
mechanism

The need  
for a  
different  
mechanism

- Shear Modulus of metals,  $G = 20 - 150 \text{ GPa}$



# The need for a different mechanism

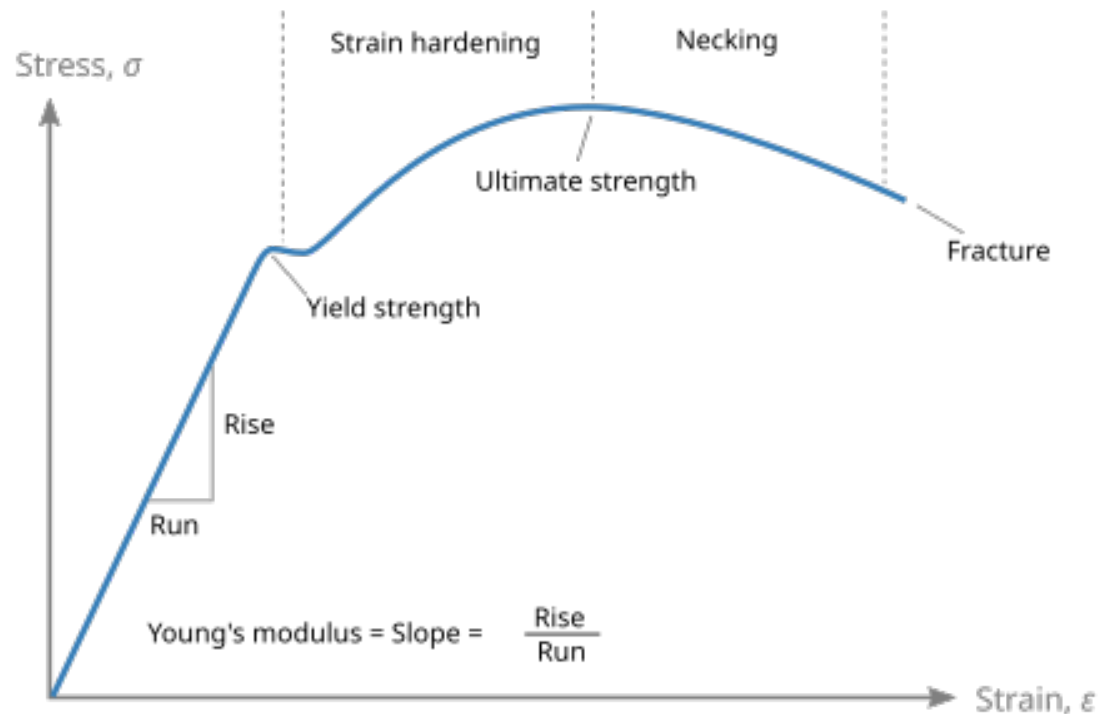
- Shear Modulus of metals,  $G = 20 - 150 \text{ GPa}$
- $\tau_m = \frac{G}{2\pi}$  , even if we take  $\tau_{m,theory} = 0.1 \times \tau_m$

# The need for a different mechanism

- Shear Modulus of metals,  $G = 20 - 150 \text{ GPa}$
- $\tau_m = \frac{G}{2\pi}$  , even if we take  $\tau_{m,theory} = 0.1 \times \tau_m$
- Theoretical shear stress is  $0.32 - 2.39 \text{ GPa}$

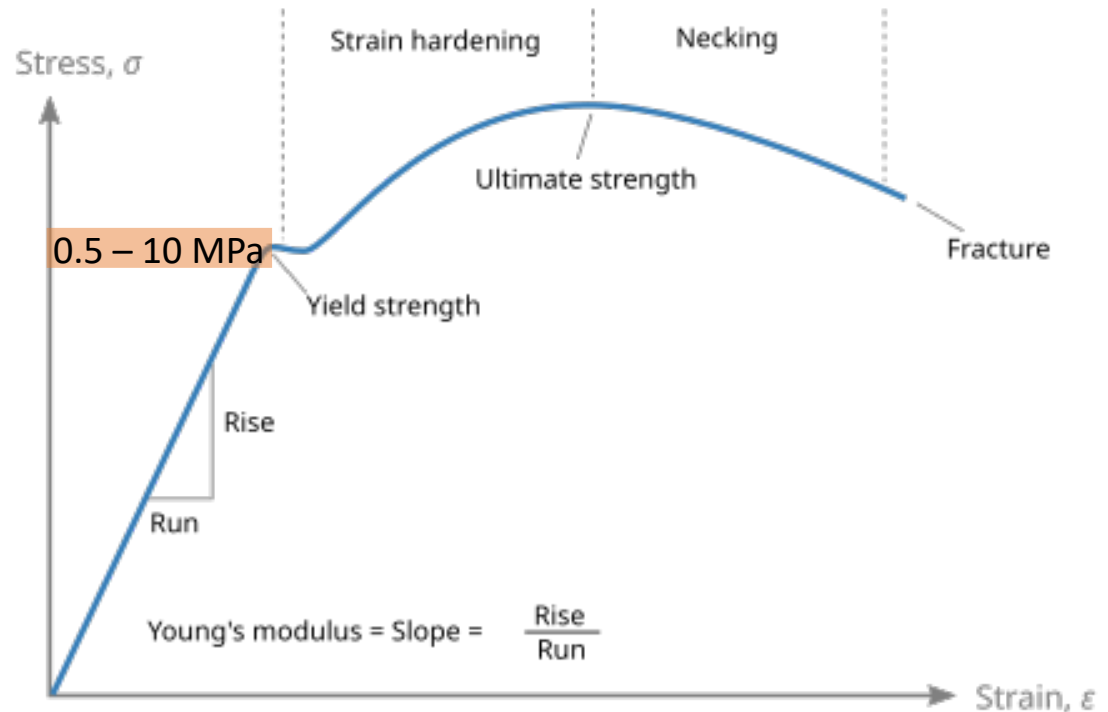
# The need for a different mechanism

- Shear Modulus of metals,  $G = 20 - 150 \text{ GPa}$
- $\tau_m = \frac{G}{2\pi}$ , even if we take  $\tau_{m,theory} = 0.1 \times \tau_m$
- Theoretical shear stress is  $0.32 - 2.39 \text{ GPa}$



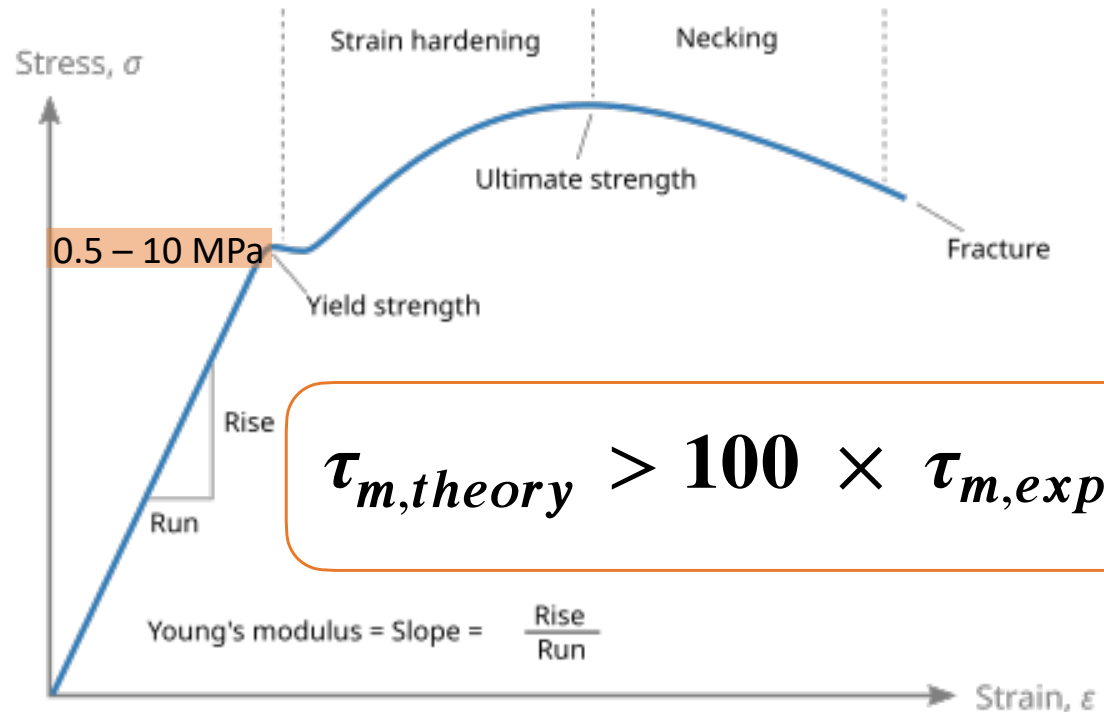
# The need for a different mechanism

- Shear Modulus of metals,  $G = 20 - 150 \text{ GPa}$
- $\tau_m = \frac{G}{2\pi}$ , even if we take  $\tau_{m,theory} = 0.1 \times \tau_m$
- Theoretical shear stress is  $0.32 - 2.39 \text{ GPa}$



# The need for a different mechanism

- Shear Modulus of metals,  $G = 20 - 150 \text{ GPa}$
- $\tau_m = \frac{G}{2\pi}$ , even if we take  $\tau_{m,theory} = 0.1 \times \tau_m$
- Theoretical shear stress is  $0.32 - 2.39 \text{ GPa}$



$$\tau_{m,theory} > 100 \times \tau_{m,expt}$$

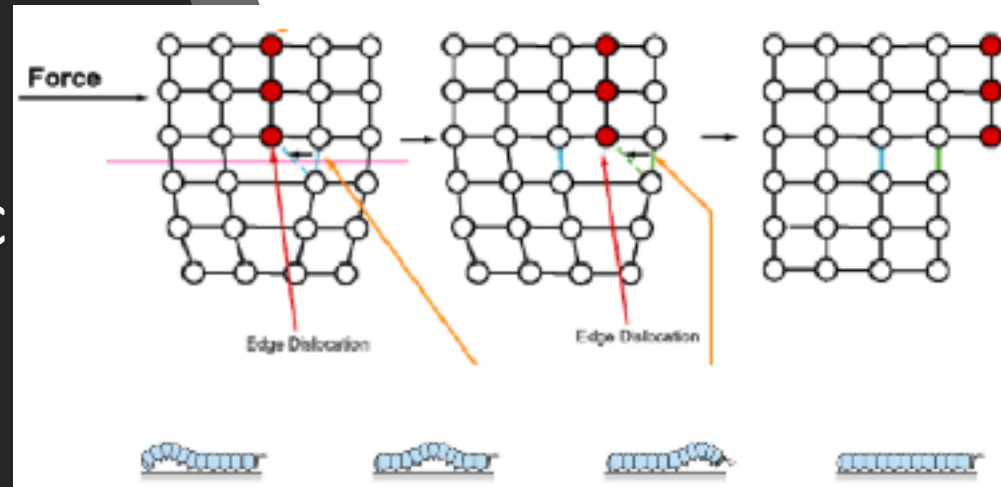
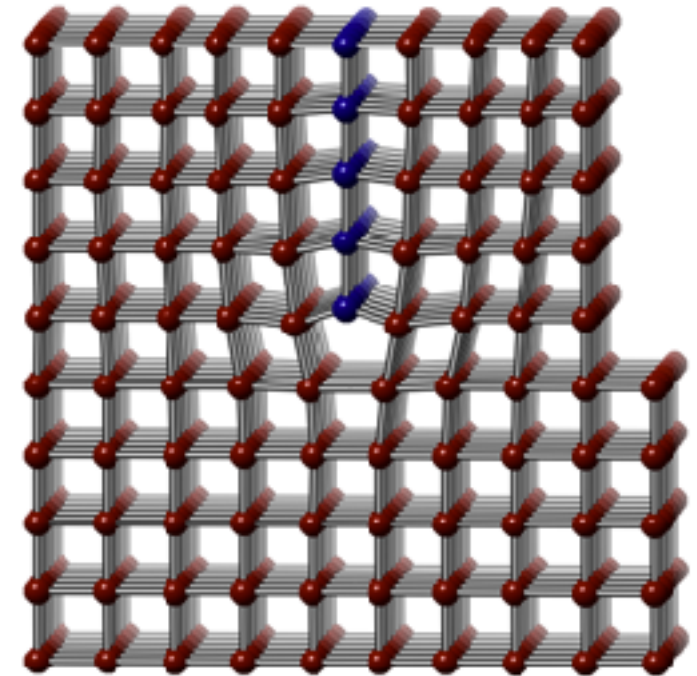


# Dislocations

## – 1-D defects

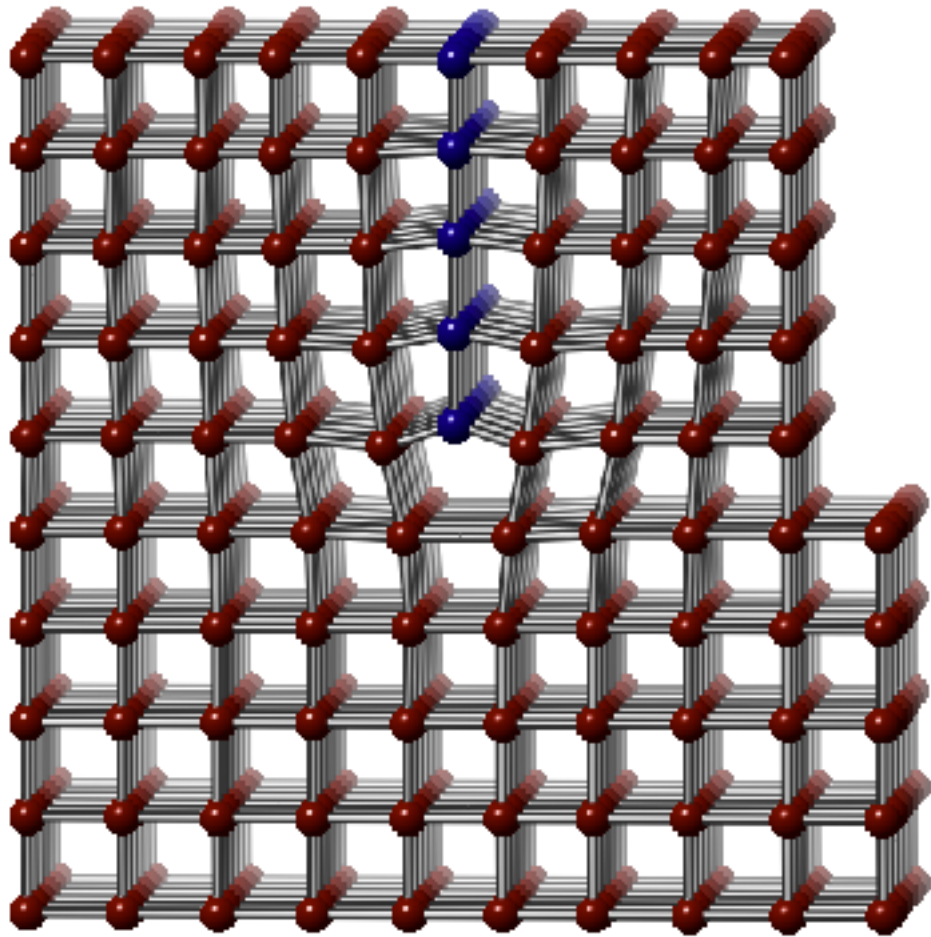
Line defects are called dislocations

- Lower stress to plastic deformation



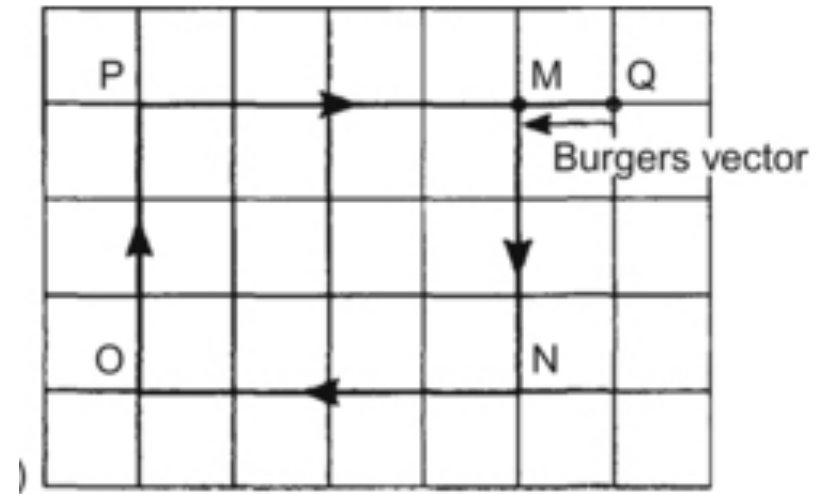
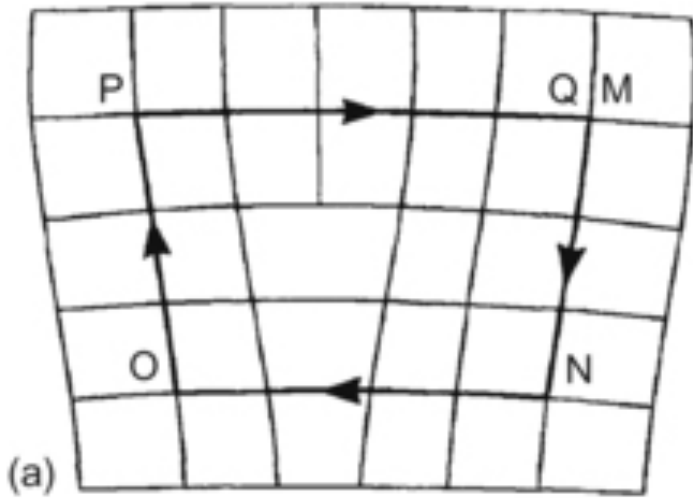
# Geometry of dislocations

- Two vectors define a dislocation
  - Line Vector
  - Burgers vector
- Angle between these vectors characterizes it
  - Always  $90^\circ$  - Edge dislocation
  - Always  $0^\circ$  - Screw dislocation
  - Any other - Mixed dislocation



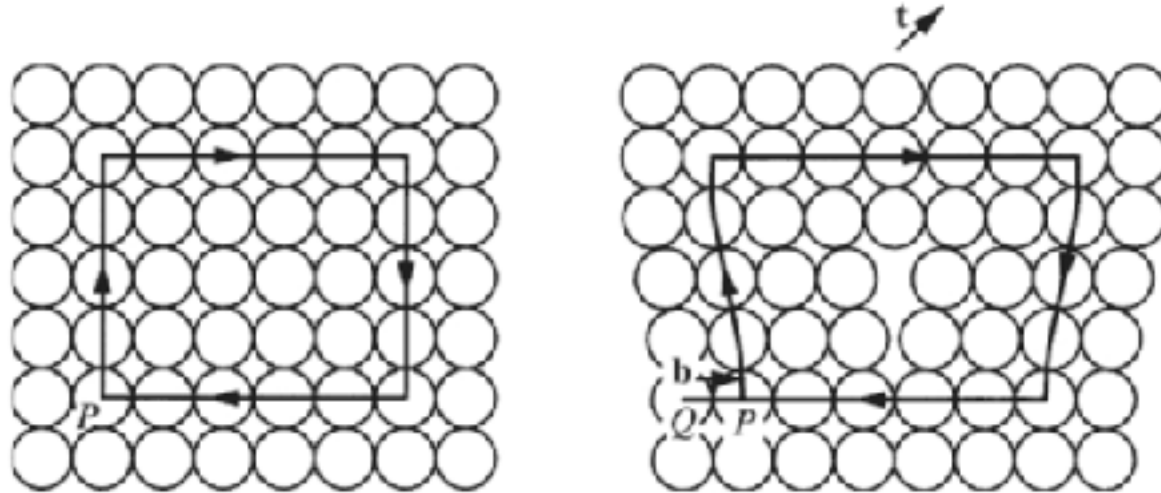
- extra half-plane of atoms
- distortion concentrated around the bounding line
- deflection and distortion of the interatomic bonds decrease with increasing distance from the line
- line sense taken as positive going in to the plane of the paper

## Edge Dislocations – Line vector



- Circuit MNOPQ with Ds. inside :  $3 \downarrow, 4 \leftarrow, 3 \uparrow, 5 \rightarrow$  (*Right Handed, RH*)
- Follow the same steps in the perfect crystal
- The 'missing link' (*Finish to Start, FS*) in the *perfect crystal* is the **Burgers vector**
- In this case,  $\overrightarrow{QM}$  is the Burgers vector,  $\vec{b}$

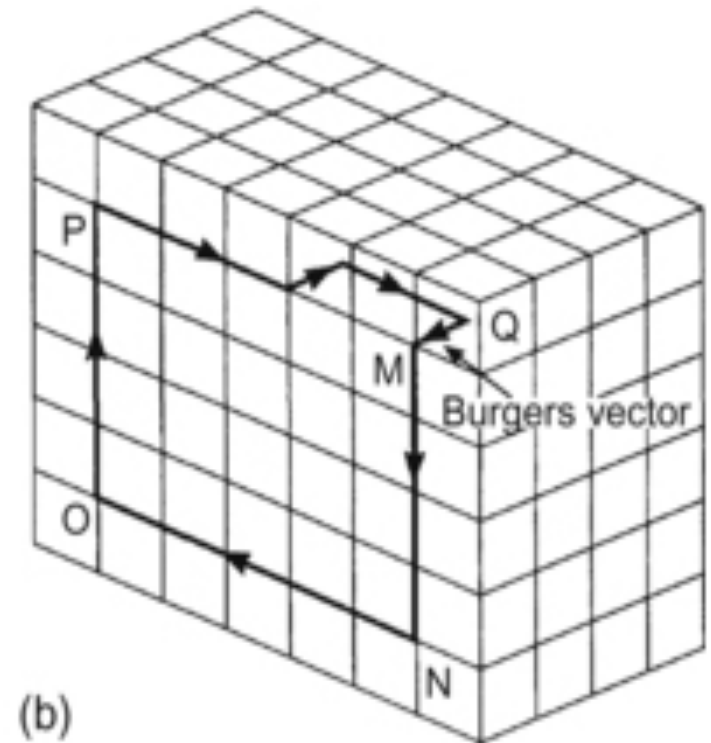
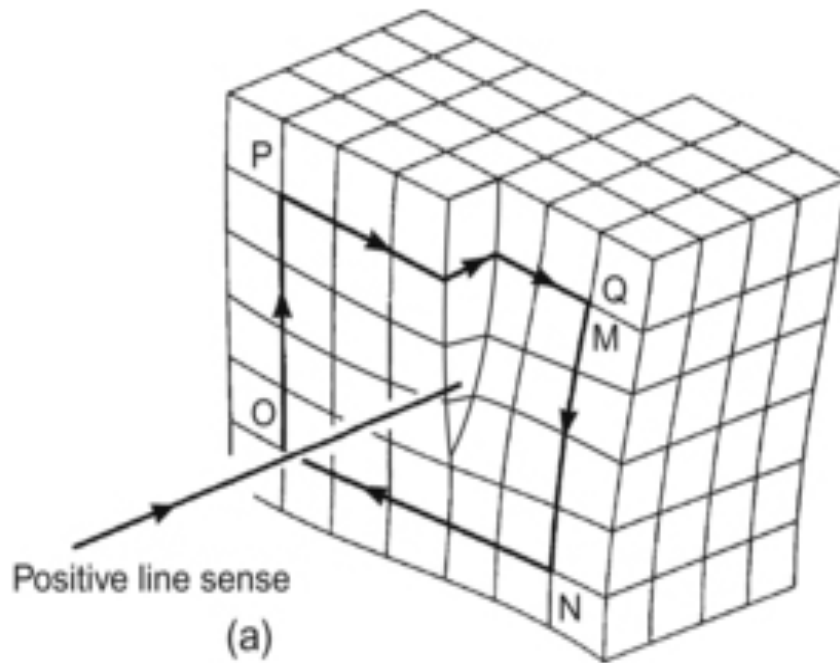
# Edge Dislocations – Burgers vector



- Circuit  $P \rightarrow P$  in perfect crystal:  $4 \uparrow, 5 \rightarrow, 4 \downarrow, 5 \leftarrow$  (*Right Handed, RH*)
- Follow the same steps in the defected crystal, the circuit will end at Q
- The ‘missing link’ (*Finish to Start, FS*) in the *defected crystal* is the **Burgers vector**
- In this case,  $\overrightarrow{QP}$  is the Burgers vector,  $\vec{b}$

# Alternate conventions



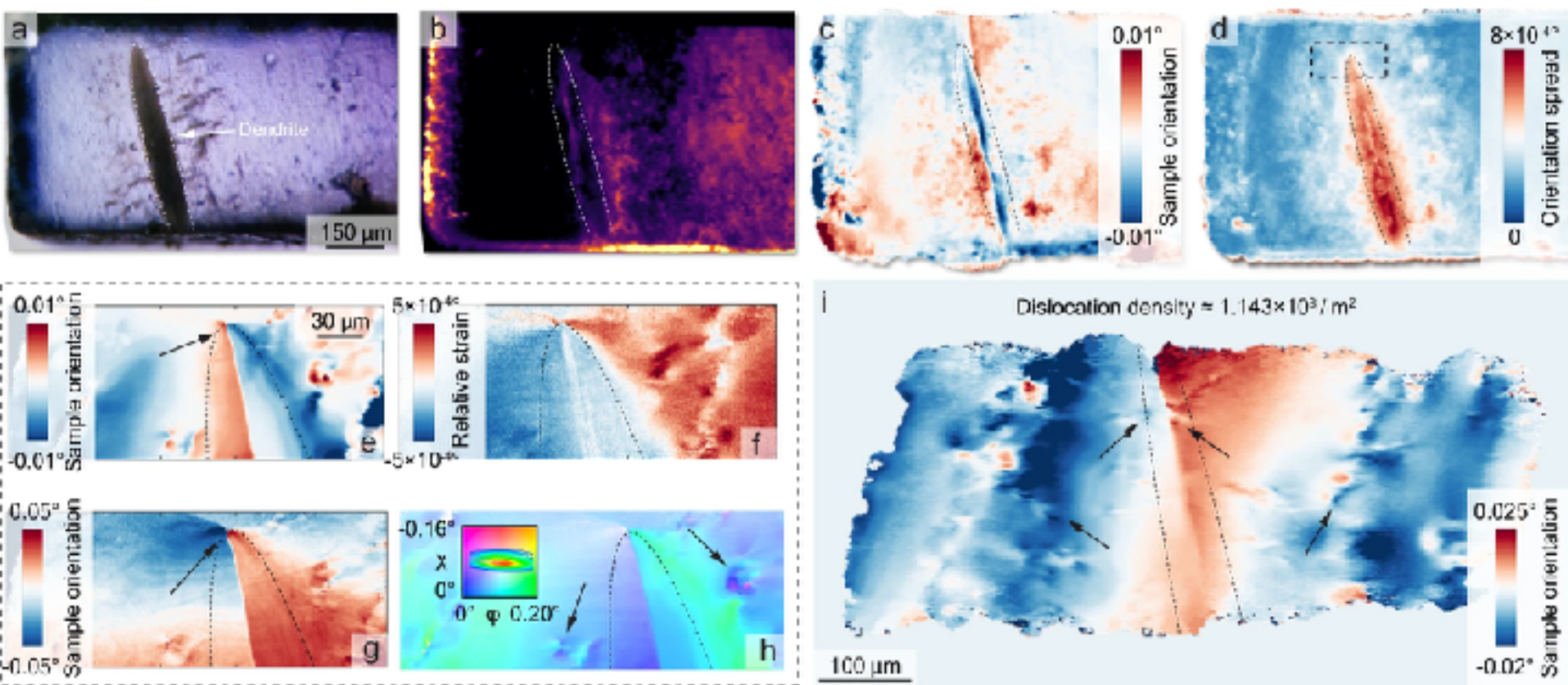


# Screw dislocations

---

## Line and Burgers vector

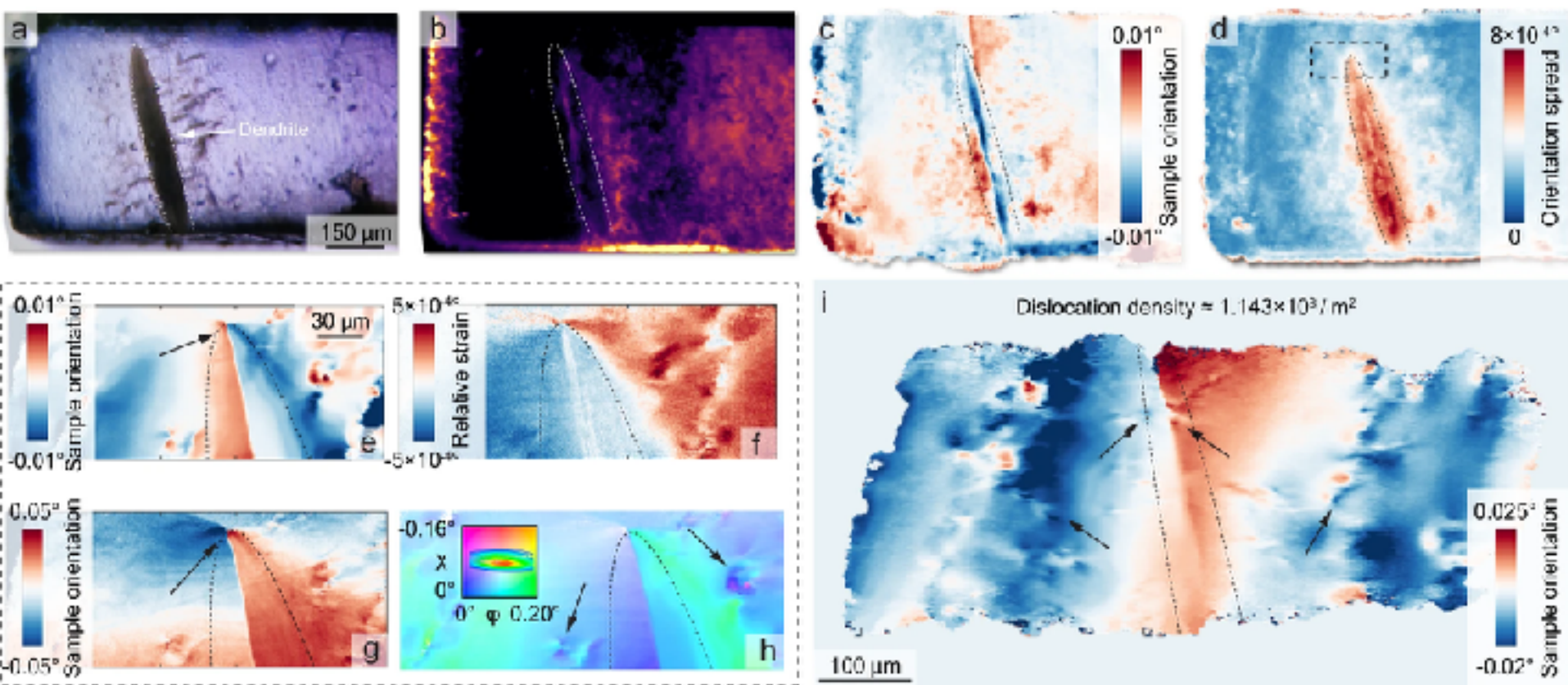
# Dislocation density



Dislocation density,  $\rho :=$  
{

 → Length of dislocations per unit volume  
 → Number of dislocations intersecting unit area

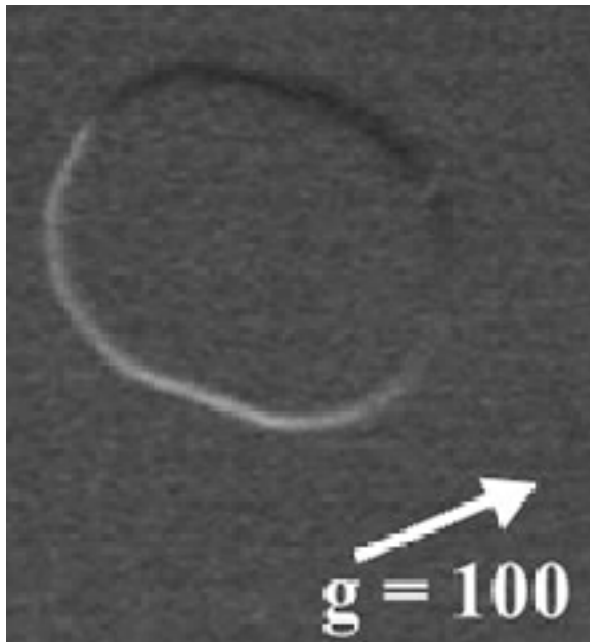
# Dislocation density



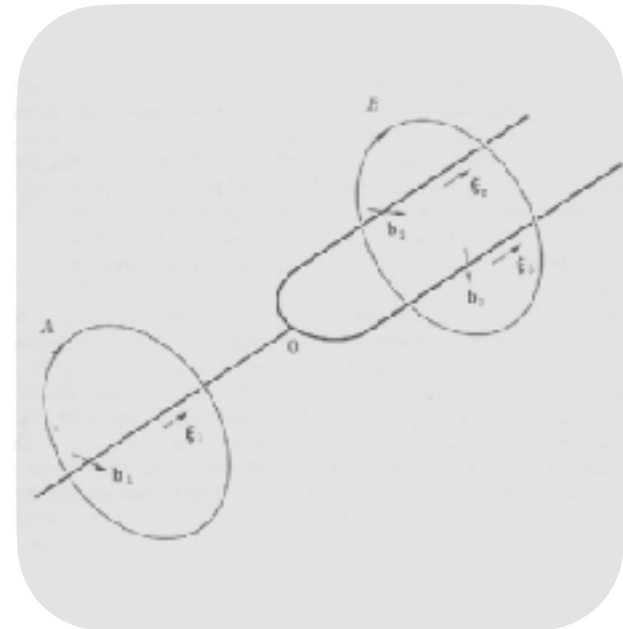
- Units of  $/ m^2$
- High in metallic materials ( $10^{12} - 10^{14}$ )
- Increases with plastic deformation to  $10^{15}$
- Low in non-metallic crystals, as low as  $10^5$

# Dislocation loops and branches

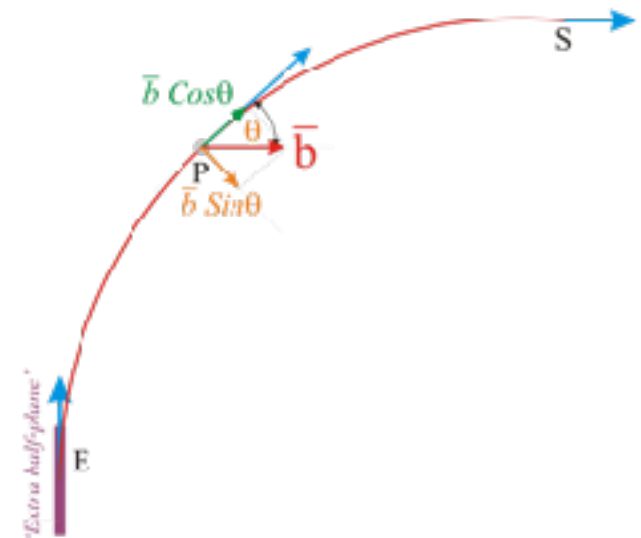
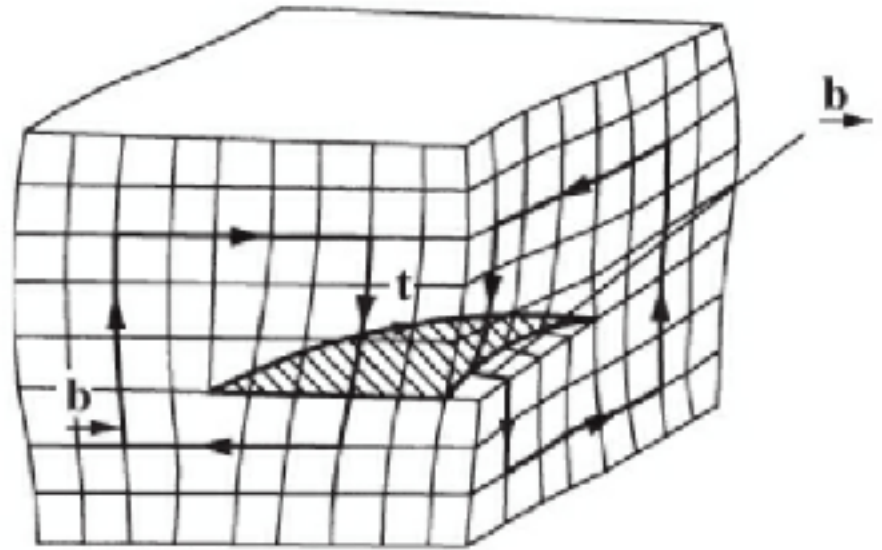
- Dislocation lines can end at the surface of a crystal and at grain boundaries
  - never inside a crystal
  - form closed loops
  - branch into other dislocations
- When three or more dislocations meet at a point, or node
  - Burgers vector is conserved
  - vector total in equals vector total out



Kamaladasa, Ranga & Jiang,  
Wenkan & Picard, Yoosuf.  
(2011). Imaging Dislocations in  
Single-Crystal SrTiO<sub>3</sub>  
Substrates by Electron  
Channeling. Journal of  
Electronic Materials - J  
ELECTRON MATER. 40.  
2222-2227. 10.1007/  
s11664-011-1723-9.



# Mixed Dislocation Loop





# Problem

- Cubic crystal
- Mixed dislocation straight line
  - Along  $[112]$  direction
  - Burgers vector is  $\frac{1}{2}[110]$

What are the edge and screw vector components of the Burgers vector

# Dislocation motion

# Dislocation motion

- Two types of movement of dislocations

# Dislocation motion

- Two types of movement of dislocations
  - Glide or conservative motion

# Dislocation motion

- Two types of movement of dislocations
  - Glide or conservative motion
    - dislocation moves in the surface which contains both its line and Burgers vector

# Dislocation motion

- Two types of movement of dislocations
  - Glide or conservative motion
    - dislocation moves in the surface which contains both its line and Burgers vector
    - a dislocation able to move in this way is glissile

# Dislocation motion

- Two types of movement of dislocations
  - Glide or conservative motion
    - dislocation moves in the surface which contains both its line and Burgers vector
    - a dislocation able to move in this way is glissile
    - one which cannot is sessile

# Dislocation motion

- Two types of movement of dislocations
  - Glide or conservative motion
    - dislocation moves in the surface which contains both its line and Burgers vector
    - a dislocation able to move in this way is glissile
    - one which cannot is sessile



# Dislocation motion

- Two types of movement of dislocations
  - Glide or conservative motion
    - dislocation moves in the surface which contains both its line and Burgers vector
    - a dislocation able to move in this way is glissile
    - one which cannot is sessile
  - Climb or non-conservative motion

# Dislocation motion

- Two types of movement of dislocations
  - Glide or conservative motion
    - dislocation moves in the surface which contains both its line and Burgers vector
    - a dislocation able to move in this way is glissile
    - one which cannot is sessile
  - Climb or non-conservative motion
    - occurs when the dislocation moves out of the glide surface

# Dislocation motion

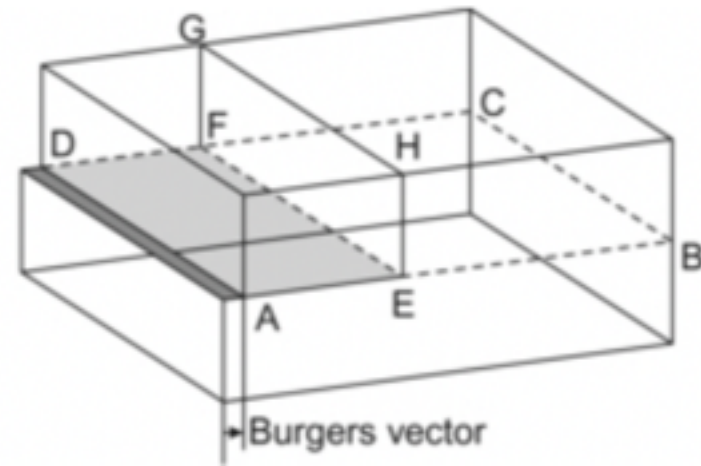
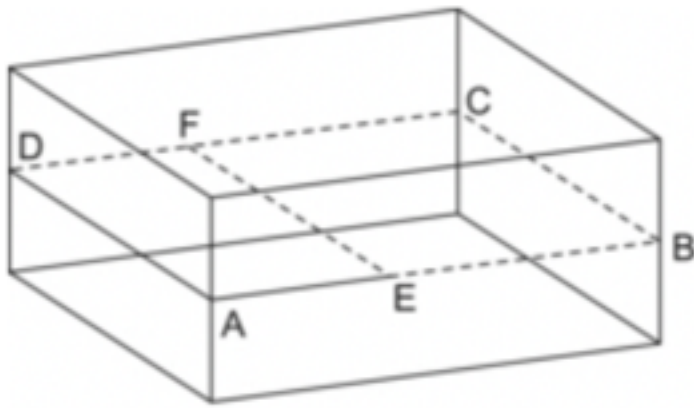
- Two types of movement of dislocations
  - Glide or conservative motion
    - dislocation moves in the surface which contains both its line and Burgers vector
    - a dislocation able to move in this way is glissile
    - one which cannot is sessile
  - Climb or non-conservative motion
    - occurs when the dislocation moves out of the glide surface
    - normal to the Burgers vector

# Dislocation motion

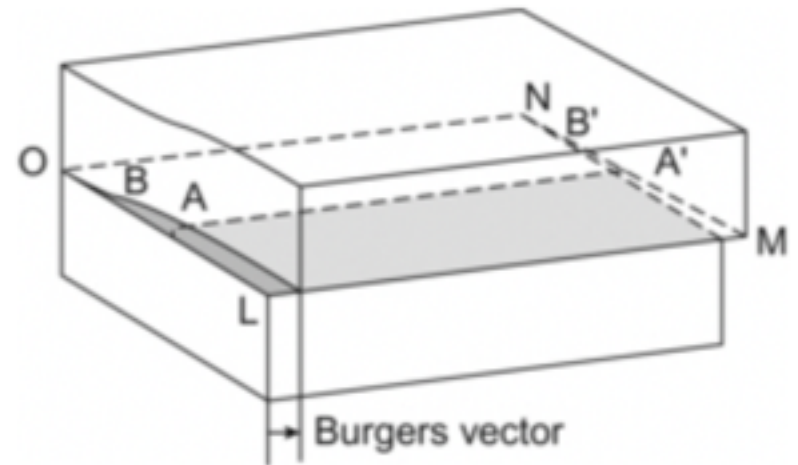
- Two types of movement of dislocations
  - Glide or conservative motion
    - dislocation moves in the surface which contains both its line and Burgers vector
    - a dislocation able to move in this way is glissile
    - one which cannot is sessile
  - Climb or non-conservative motion
    - occurs when the dislocation moves out of the glide surface
    - normal to the Burgers vector

# Dislocation motion

- Two types of movement of dislocations
  - Glide or conservative motion
    - dislocation moves in the surface which contains both its line and Burgers vector
    - a dislocation able to move in this way is glissile
    - one which cannot is sessile
  - Climb or non-conservative motion
    - occurs when the dislocation moves out of the glide surface
    - normal to the Burgers vector
- Glide of many dislocations results in slip: most common manifestation of plastic deformation in crystalline solids

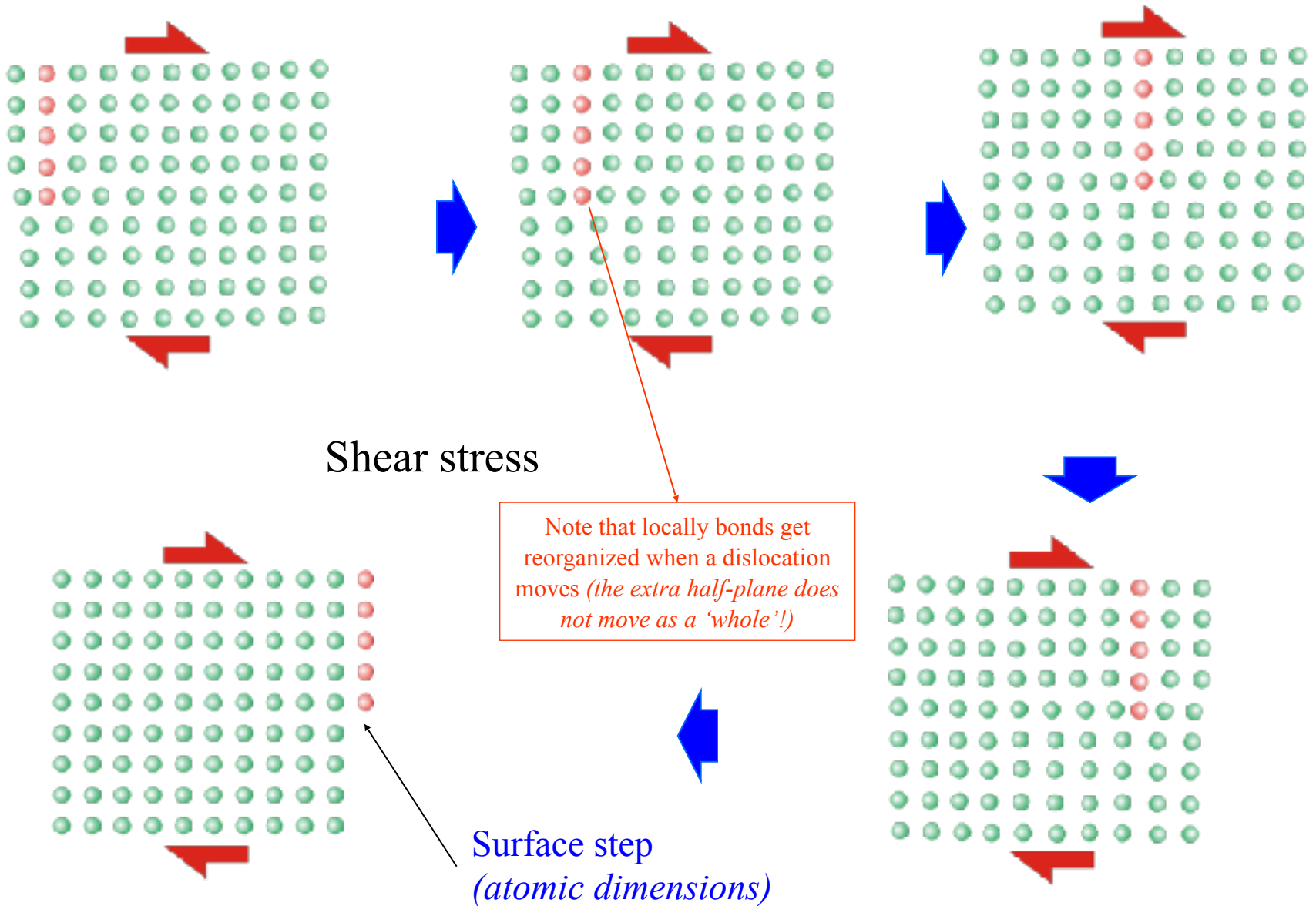


- Boundary between *slipped* and the *un-slipped* parts of the crystal
- Plane containing the line and Burgers vector defines a *slip plane*

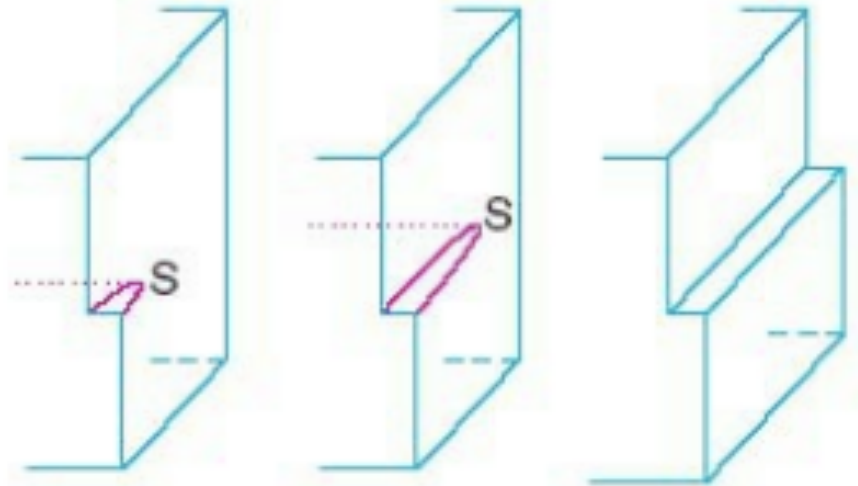
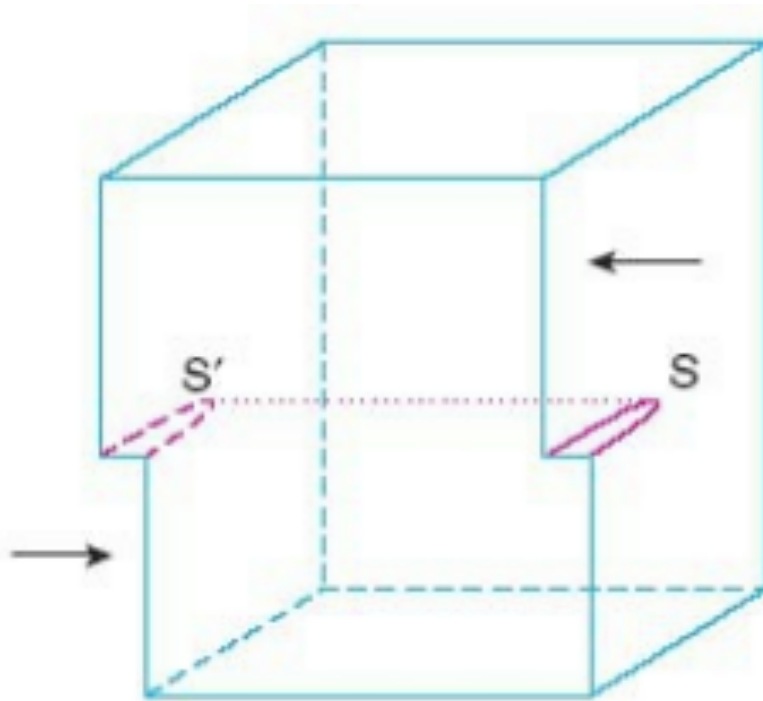


# Dislocation - alternative definition

# Dislocation Glide or Slip - Edge Ds



# Dislocation Glide or Slip - Screw Ds.





# Slip in Crystals

A diagram showing a 3D representation of a crystal slip system. It features a dark gray rectangular prism with a blue line representing the slip direction and a blue plane representing the slip plane. The blue line and plane intersect at a point. Two blue arrows point from text labels to this intersection point: one from the left labeled 'High planar density' and one from the bottom right labeled 'High linear density in that plane'.

---

Slip occurs in that crystallographic plane that contains both line vector and Burgers vector

---

Burgers vector is the slip direction

---

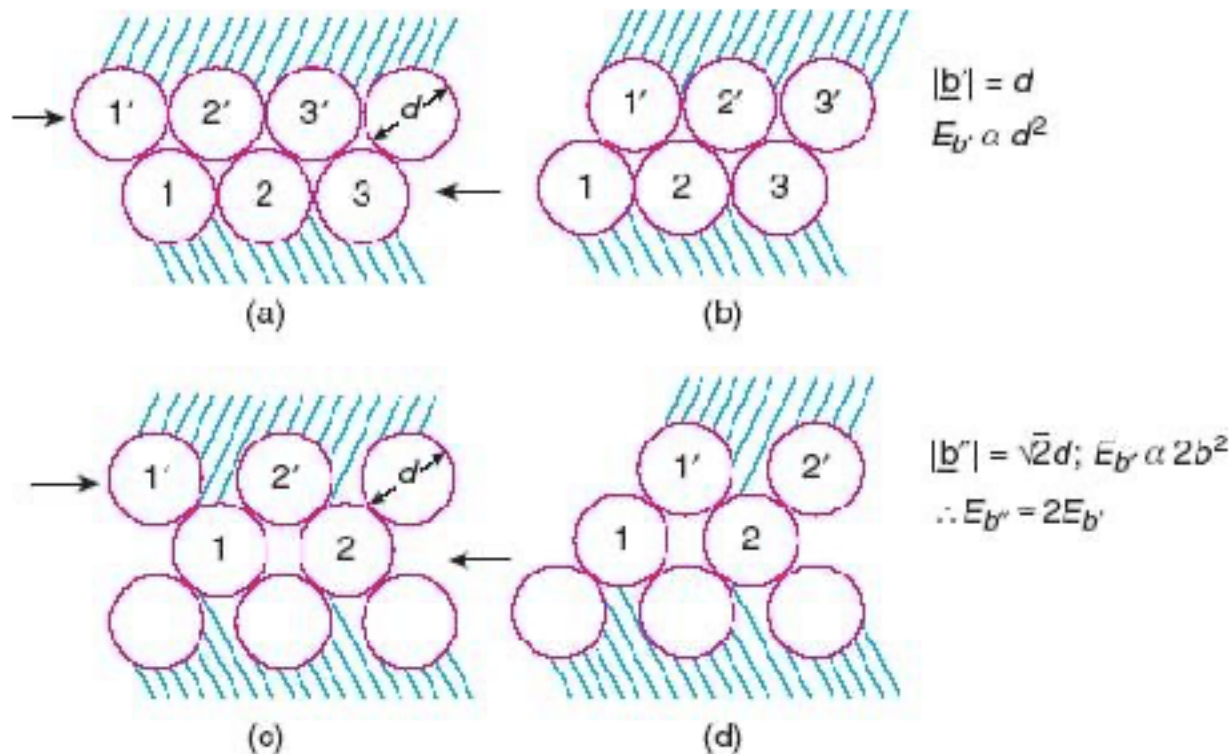
The plane and direction constitute a slip system

High planar density

High linear density in that plane

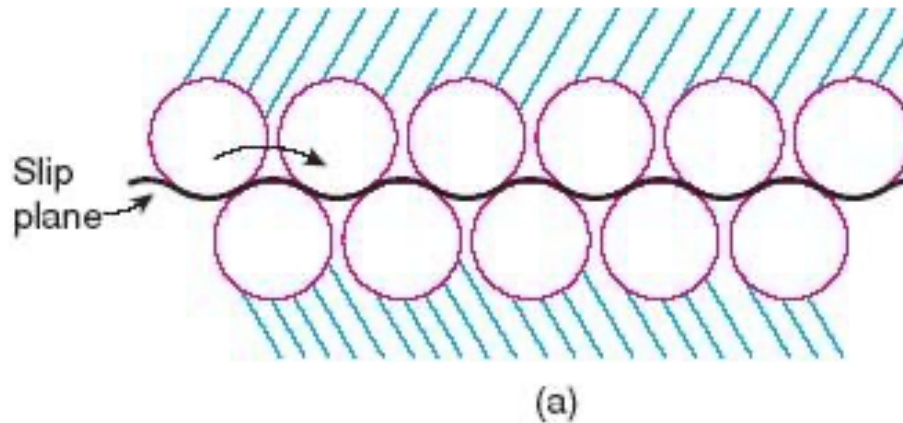
# Why does a slip system exist?

$$E \propto b^2$$

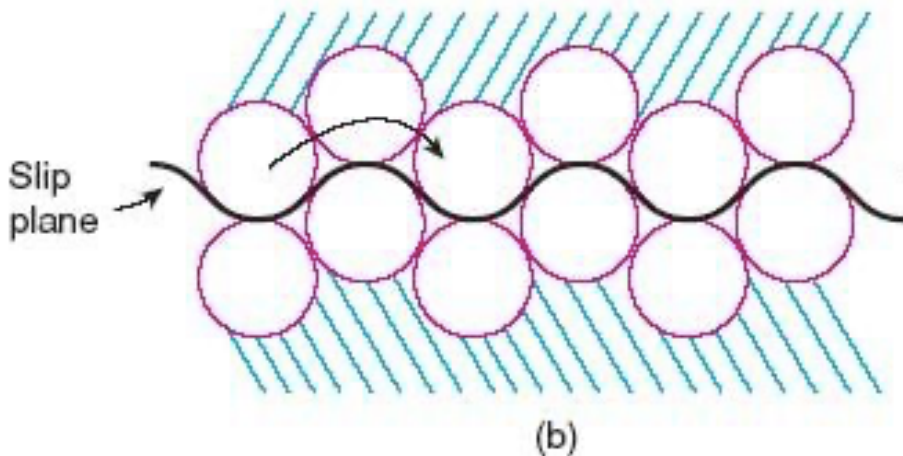


Burgers vector is along a close packed direction

# Why does a slip system exist?



Lower energy barrier for atom movement



Slip occurs on a close packed plane

# Slip systems

Crystal system	Slip Plane	Slip direction	Degeneracy
FCC	{111}	$\langle 1\bar{1}0 \rangle$	12
	{110}		12
BCC	{211}	$\langle \bar{1}11 \rangle$	12
	{321}		24
HCP	{001}		3
	{100}	$\langle 01\bar{1} \rangle$	3
	{101}		6

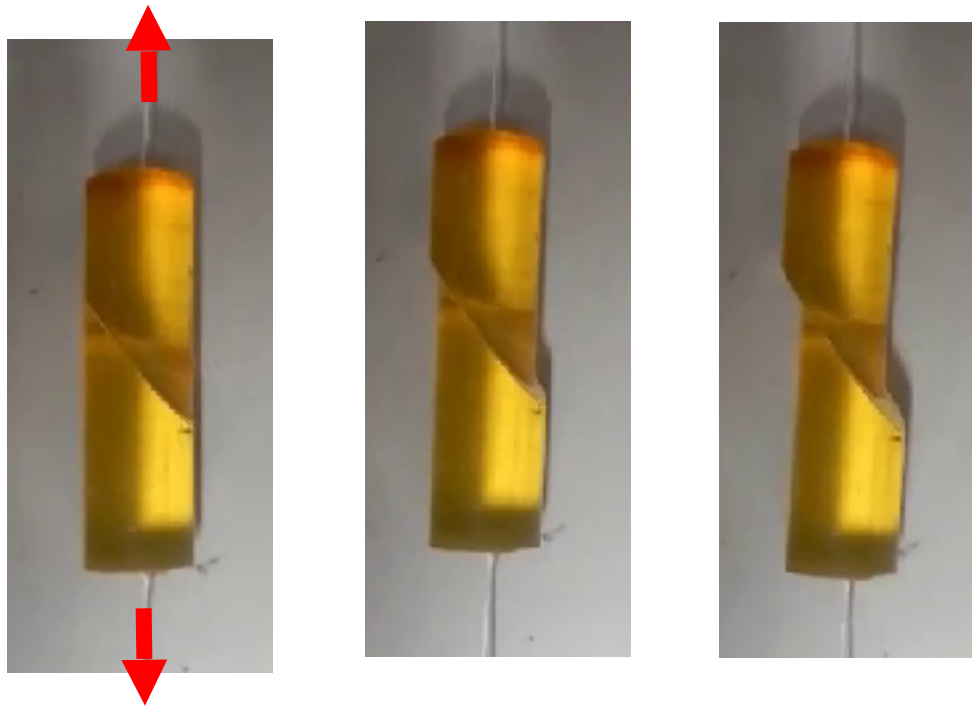
# Glide and Deformation

- Uniaxial tensile test – shear stress on all planes
- shear stress  $>$  stress needed to move dislocation

Resolved shear stress



Critical Resolved shear stress



# Resolved shear stress

$$\text{Stress} = \left( \frac{\text{Force}}{\text{Area}} \right)_{1D}$$

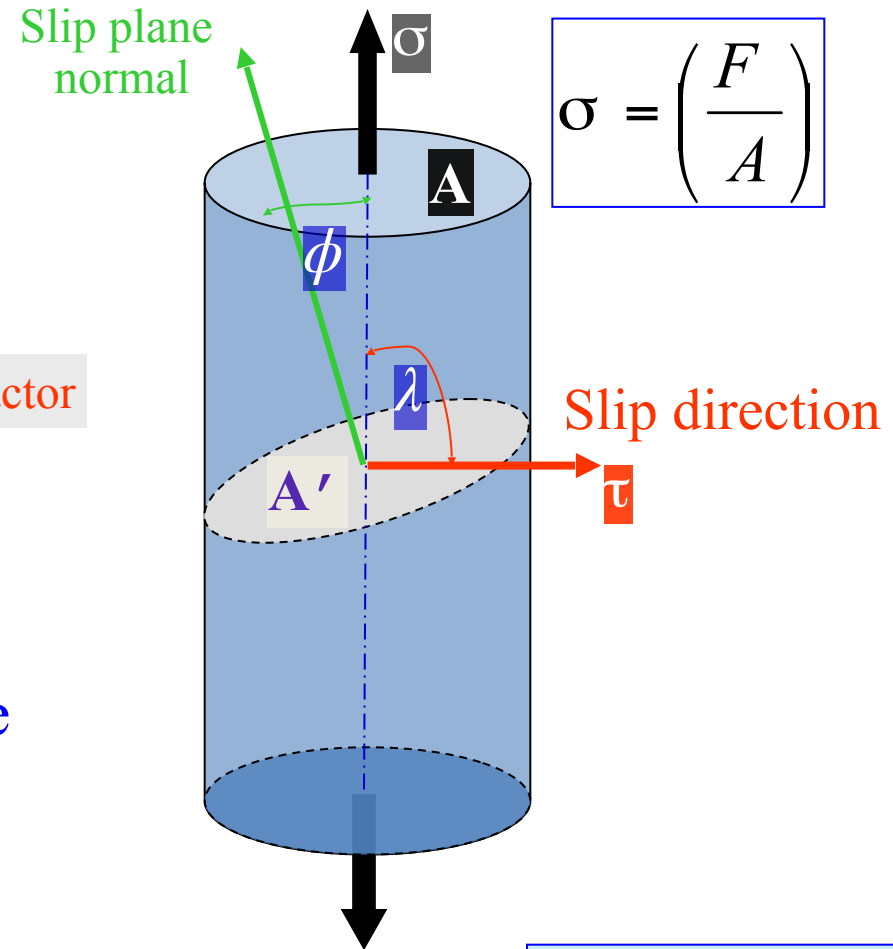
$$\tau_{RSS} = \frac{F \cos \lambda}{\frac{A}{\cos \phi}}$$

$$\sigma = \left( \frac{F}{A} \right)$$

$$\tau_{RSS} = \sigma \cos \phi \cos \lambda$$

Schmid factor

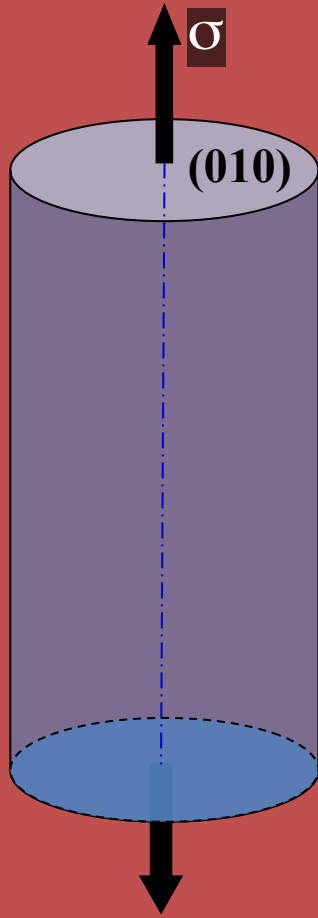
- Maximum shear stress is in a plane inclined at  $(\theta =) 45^\circ$ .
- The vertical ( $90^\circ$ ) and horizontal plane ( $0^\circ$ ) feel no shear stresses.



Slip is initiated when

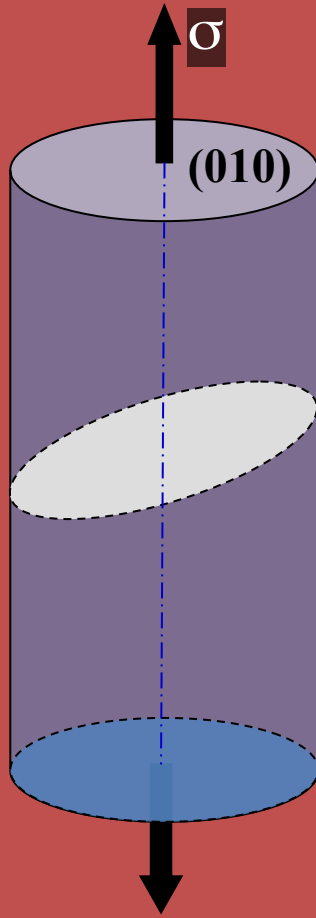
$$\tau_{RSS} \geq \tau_{CRSS}$$

# Problem



- Single crystal bcc Fe
  - Tensile stress on (010)
  - Slip initiated in a slip system
  - $\tau_{CRSS} = 30 \text{ MPa}$
1. Compute resolved shear stress when a tensile stress of 52 MPa is applied
  2. Compute the yield strength

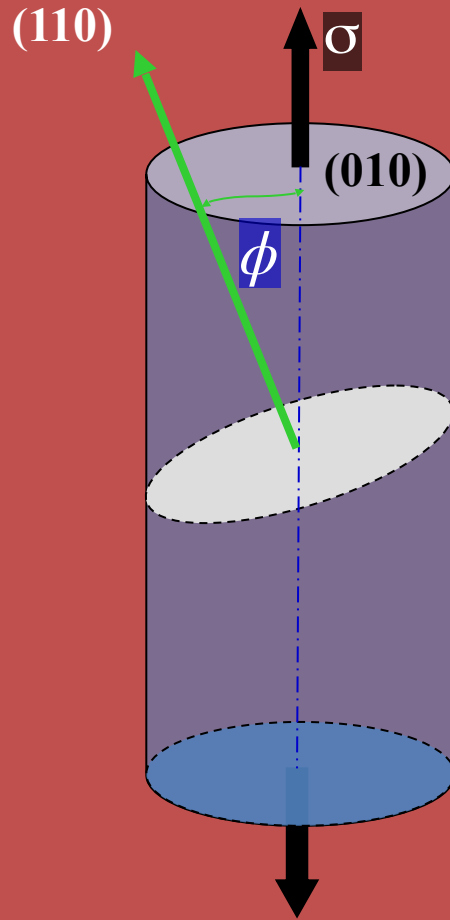
# Problem



- Single crystal bcc Fe
  - Tensile stress on (010)
  - Slip initiated in a slip system
  - $\tau_{CRSS} = 30 \text{ MPa}$
1. Compute resolved shear stress when a tensile stress of 52 MPa is applied
  2. Compute the yield strength

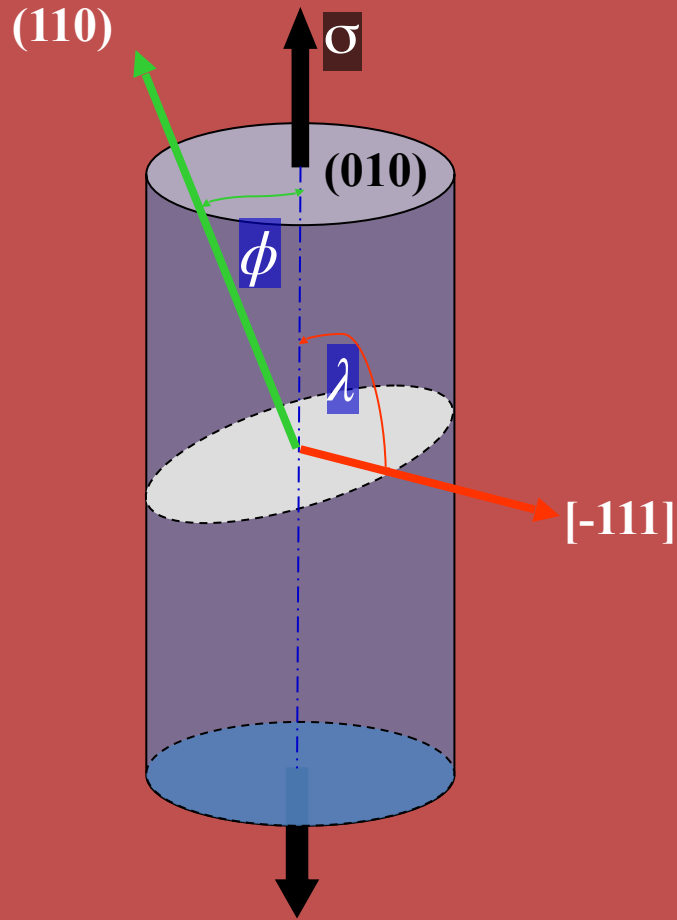


# Problem



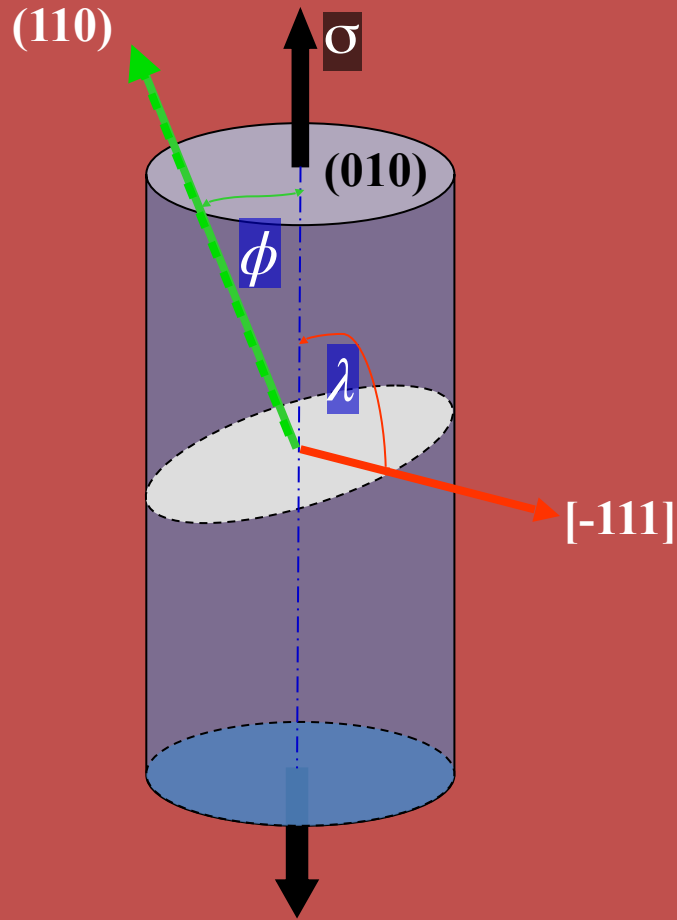
- Single crystal bcc Fe
  - Tensile stress on (010)
  - Slip initiated in a slip system
  - $\tau_{CRSS} = 30 \text{ MPa}$
1. Compute resolved shear stress when a tensile stress of 52 MPa is applied
  2. Compute the yield strength

# Problem



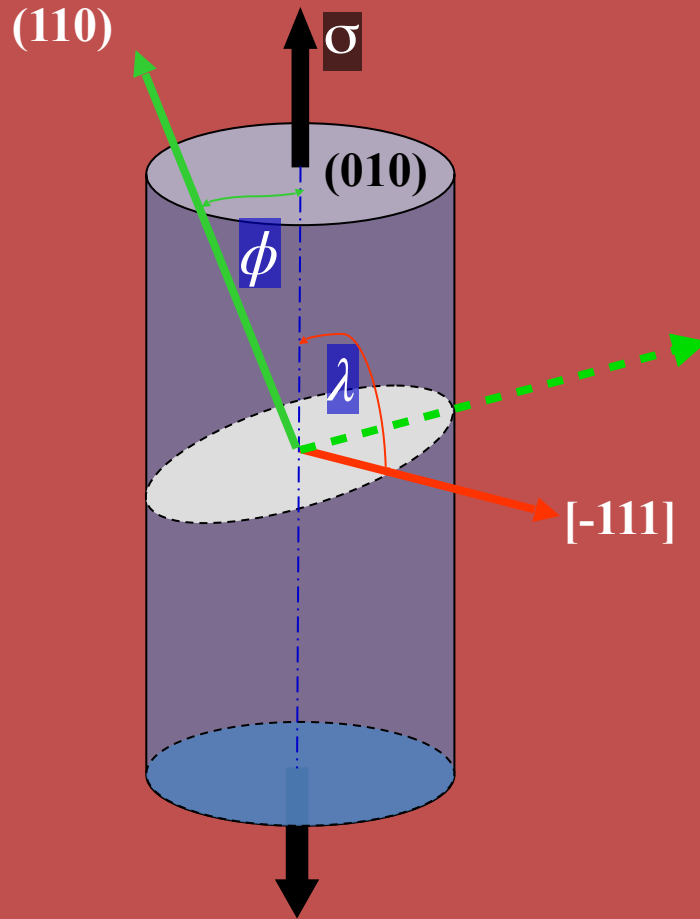
- Single crystal bcc Fe
  - Tensile stress on (010)
  - Slip initiated in a slip system
  - $\tau_{CRSS} = 30 \text{ MPa}$
1. Compute resolved shear stress when a tensile stress of 52 MPa is applied
  2. Compute the yield strength

# Problem



- Single crystal bcc Fe
  - Tensile stress on (010)
  - Slip initiated in a slip system
  - $\tau_{CRSS} = 30 \text{ MPa}$
1. Compute resolved shear stress when a tensile stress of 52 MPa is applied
  2. Compute the yield strength

# Problem



- Single crystal bcc Fe
  - Tensile stress on  $(010)$
  - Slip initiated in a slip system
  - $\tau_{CRSS} = 30 \text{ MPa}$
1. Compute resolved shear stress when a tensile stress of 52 MPa is applied
  2. Compute the yield strength