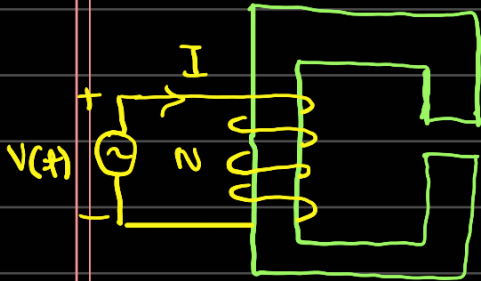


Day - 16

→ Inductor:



→ Air gap is introduced to magnetic circuit, to realise inductor, to make inductance not sensitive to variations in core permeability

$$L = \frac{N^2}{R} = \frac{N^2}{R_c + R_g} \approx \frac{N^2}{R_g} \quad (\because R_g \gg R_c)$$

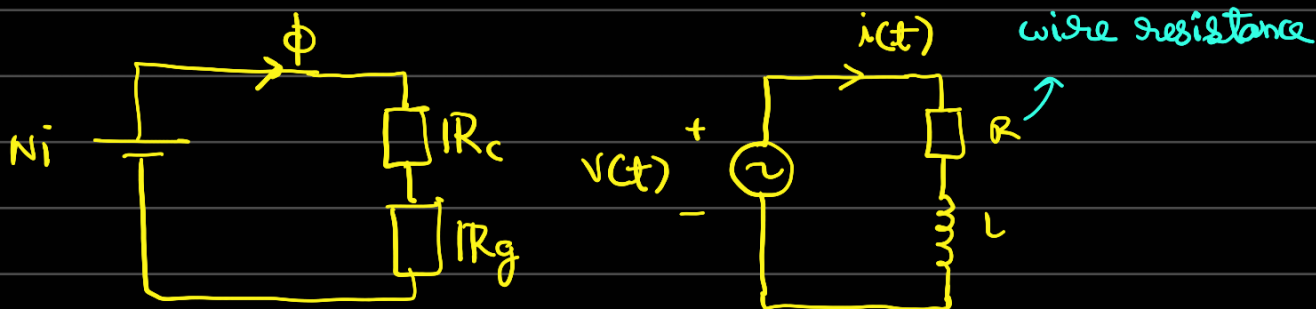
$$\Rightarrow L = \frac{N^2 \mu_0 A_c}{l_g}$$

$$V(t) = i(t)R + \frac{d\psi(t)}{dt}$$

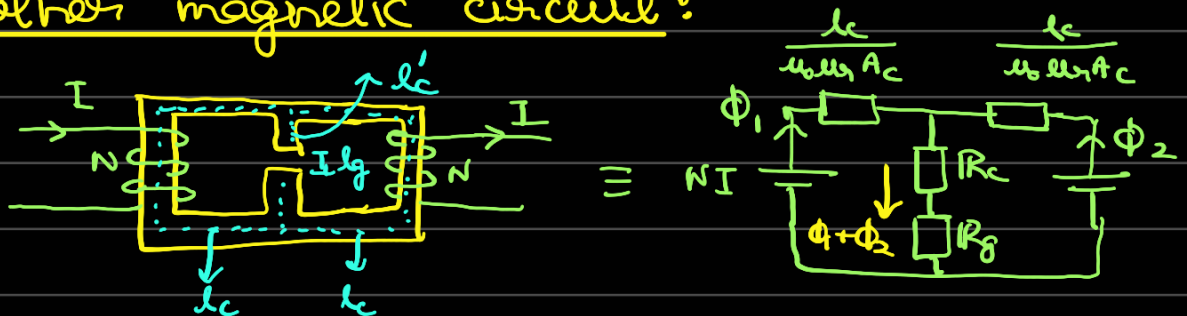
$$\Rightarrow V(t) = i(t)R + L \frac{di(t)}{dt}$$

⇒ Assume linear magnetic circuit (ψ vs i is linear)

☆ Equivalent circuit:



☆ Another magnetic circuit:



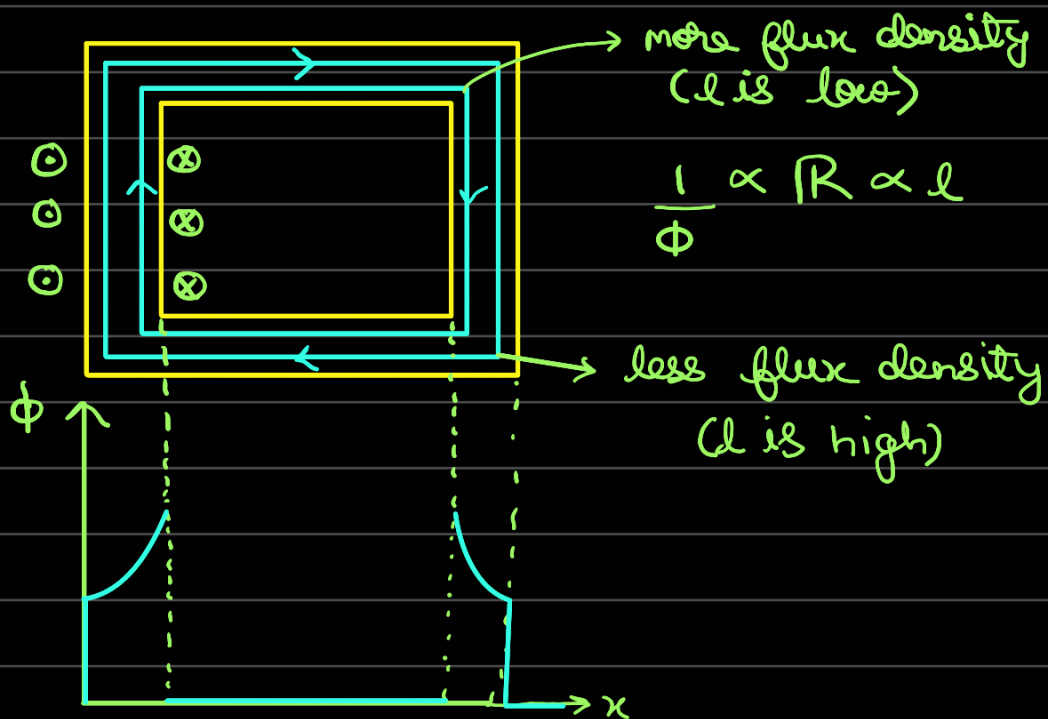
$$R_c = \frac{l_c}{\mu_0 \mu_r A_c}$$

$$R_g = \frac{l_g}{\mu_0 A_c}$$

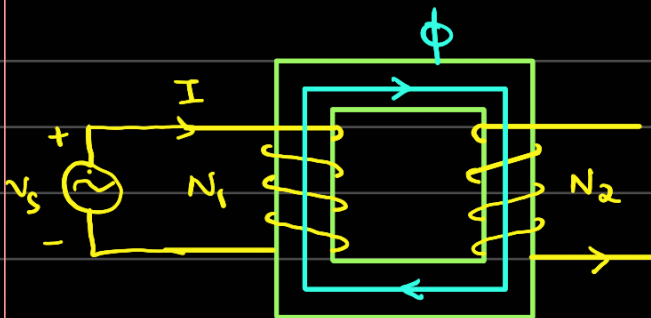
$$\oint \vec{B} \cdot d\vec{S} = 0 \equiv \text{KCL}$$

$$\oint \vec{H} \cdot d\vec{l} = \int \vec{J} \cdot d\vec{S} \equiv \text{KVL}$$

☆ The original circuit:



→ Transformer:



$$E = N \frac{d\phi}{dt}$$

But ϕ is same
(hence $d\phi/dt$)

$$\therefore E \propto N$$

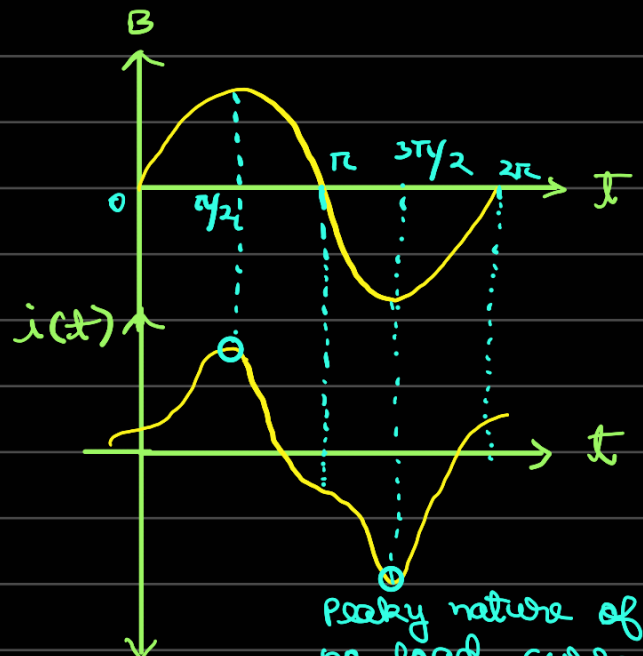
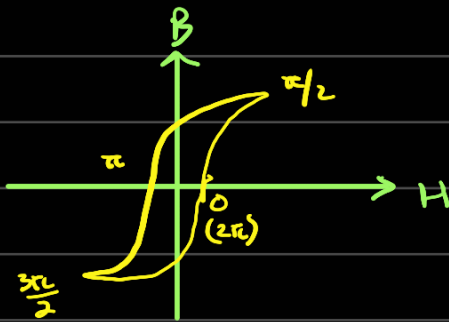
$$\therefore \frac{V_s}{N_1} = \frac{V_{out}}{N_2} \Rightarrow V_{out} = \frac{N_2}{N_1} V_s$$

☆ No load operation:

$$V_s(t) = \underbrace{i_s(t)R}_{\approx 0} + \frac{d\psi(t)}{dt} \approx \frac{d\psi(t)}{dt} = N_1 \frac{d\phi(t)}{dt}$$

If $V_s(t) = V_m \sin \omega t$
 so $\phi(t) = \frac{1}{N_1} \int V_m \sin \omega t dt$
 $= -\frac{V_m}{N_1 \omega} \cos \omega t$

i_s is not actually sinusoidal!



Peaky nature of no-load current in transformer is due to saturation effects of the core

→ Fourier Series:

$$i(t) = a_0 + \sum_{n=1}^{\infty} a_n \cos n\omega t + \sum_{n=1}^{\infty} b_n \sin n\omega t$$

$$f(\omega t) = -f(\omega t + \pi) \quad \forall \omega t \rightarrow \text{Half-wave symmetry (H.W.S.)}$$

(Assuming B-H curve is symmetric)

$$\Rightarrow \frac{1}{2\pi} \int_0^{2\pi} i(\omega t) d(\omega t) = 0$$

$$\text{so } a_0 = 0$$

If wave-form has H.W.S., then there are only odd harmonics ($\because a_{2k} = 0 \forall k \in \mathbb{N}$)