

23/02/24

## Operational Amplifier

→ Gets its name from Operational (performs addition, subtraction, integration, differentiation,..) + Amplifier.

→ Shortly called OpAmp.

### Applications:

(1) Mathematical operations

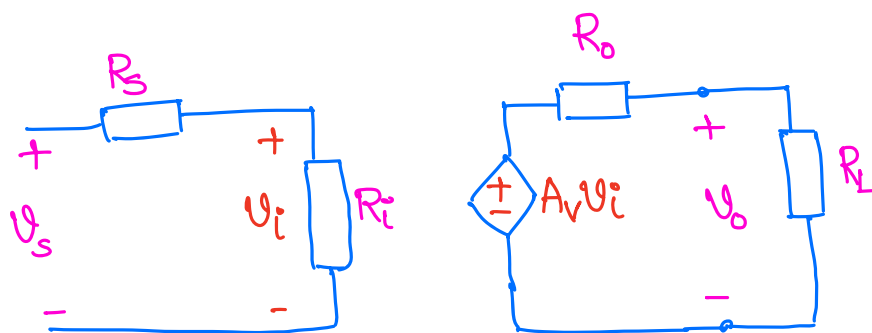
Addition, subtraction, integration, differentiation.

(2) Filtering applications

(3) Sensing voltage, current, pressure, temperature,...

### Ideal chara. of Amplifier:

Consider structure of amplifier given below.



$V_s$ : Source voltage

$V_o$ : Load voltage

$A_v$ : Voltage gain

$R_s$ : Source resistance

$R_i$ : Input resistance

$R_o$ : Output resistance

$R_L$ : Load resistance

$$V_o = \frac{R_o}{R_o + R_L} \cdot A_v V_i$$

$$\Rightarrow V_o = A_v \cdot \frac{R_o}{R_o + R_L} \cdot \frac{R_i}{R_i + R_s} \cdot V_s$$

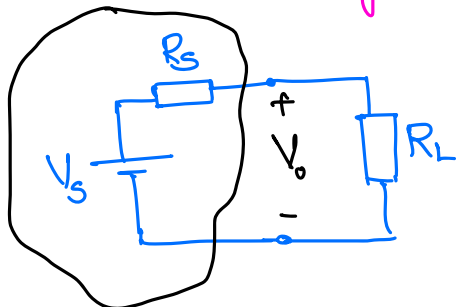
For  $\frac{V_o}{V_s}$  to be  $A_v \Rightarrow R_o \ll R_L$  (Low o/p impedance)  
 $R_i \gg R_s$  (High i/p impedance)

→ Ideal amplifier:  $R_i \rightarrow \infty$   $R_o \rightarrow 0$



Otherwise loading effects take place.

What is loading effect?



Source ( $V_s$ )

with internal  
resistance ( $R_s$ )



As you load this circuit ( $I \uparrow$ ) ⇒  
o/p voltage dips!!

$$V_o = \frac{R_L}{R_L + R_s} \cdot V_s$$

$$R_L = 1k\Omega$$

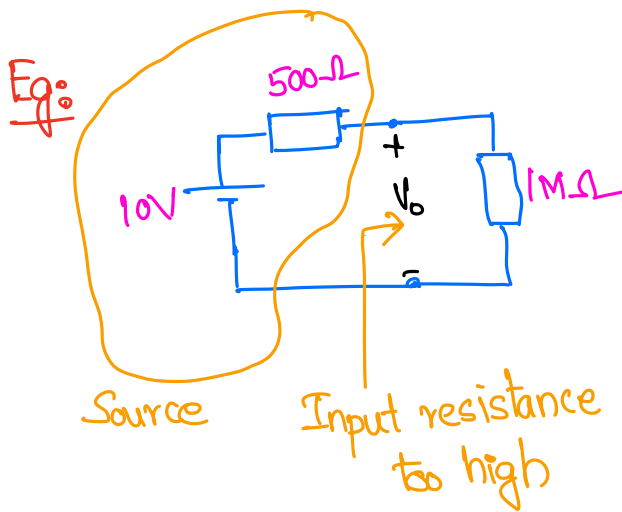
$$R_s = 500\Omega$$

$$V_s = 10V$$

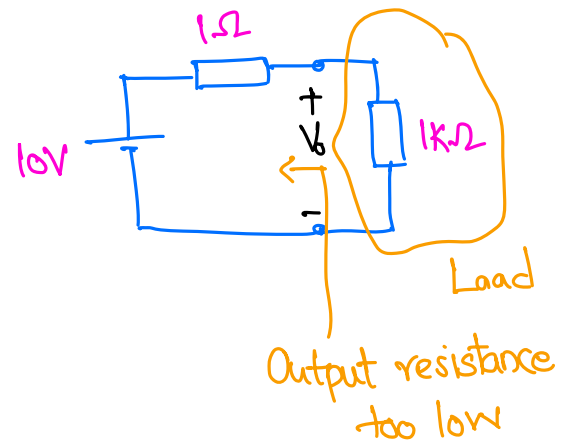


$V_o$  is only 6.67V (Not 10V).

→ For loading effect to be not much seen, Input resistance has to be very high and output resistance has to be too low.

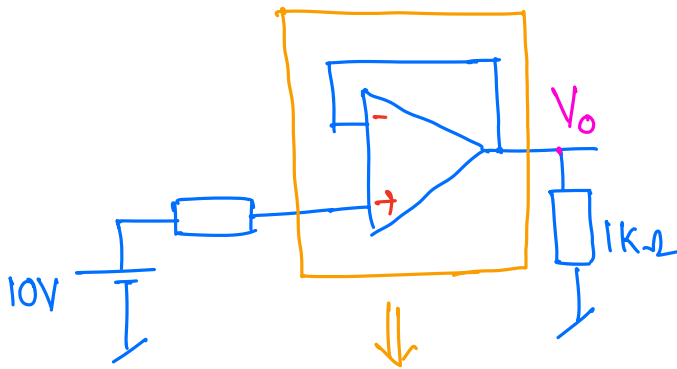


$$V_o \approx 10V$$



$$V_o \approx 10V.$$

→ Suppose that  $R_s = 500\Omega$  and  $R_L = 1k\Omega$ ? How to take care of loading effect?

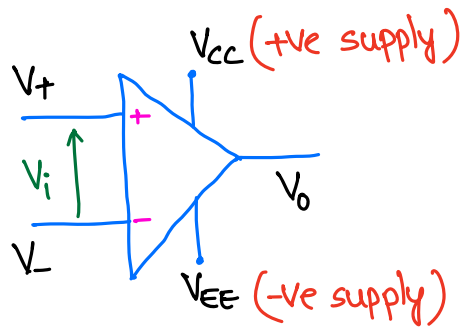


Put an OpAmp buffer here (since  $R_i$  is very high and  $R_o$  is very low for OpAmp).



We will understand how this works, in a few slides from here, after getting introduced to OpAmps.

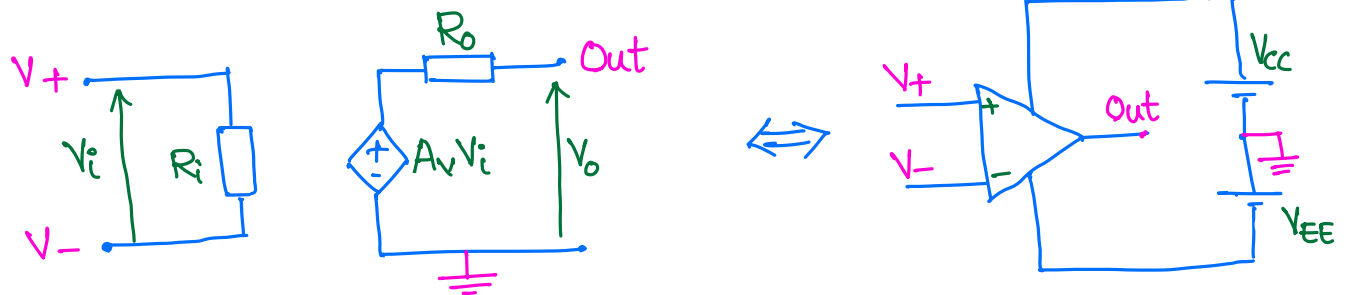
## Structure of OpAmp:



Open loop gain,  $A_v = \frac{V_0}{V_+ - V_-} = \frac{V_0}{V_i}$

→ Open loop gain of opamp is very high ( $= 2 \times 10^5$  for 741 IC)

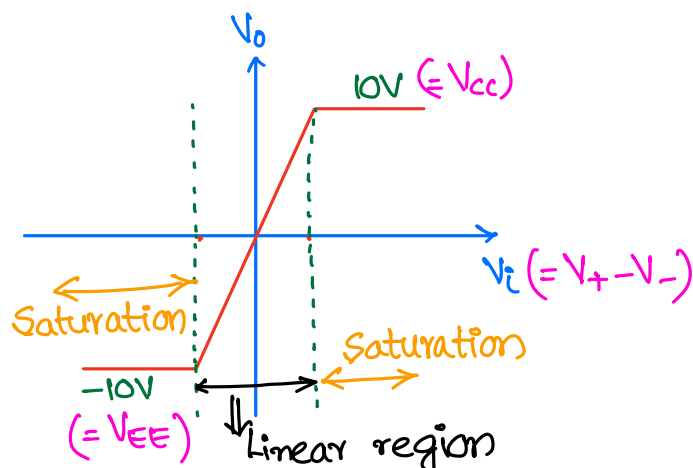
## Internal diagram of Opamp:



$R_i \rightarrow$  Input resistance of opamp  
( $= 2 \text{ M}\Omega$  for 741 IC)

$R_o \rightarrow$  Output resistance of opamp  
( $= 75 \Omega$  for 741 IC)

## Open-loop characteristics of Opamp:



Let  $V_{CC} = +10\text{V}$  and  $V_{EE} = -10\text{V}$ .

For 741;  $A_v = 2 \times 10^5 \Rightarrow$  In linear region  $\Rightarrow$

Virtual short  
phenomena

$$A_v = \frac{V_o}{V_i} \Rightarrow V_i \text{ is very small}$$

$$\Rightarrow V_+ \approx V_- \text{ (if opamp operates in linear region)}$$

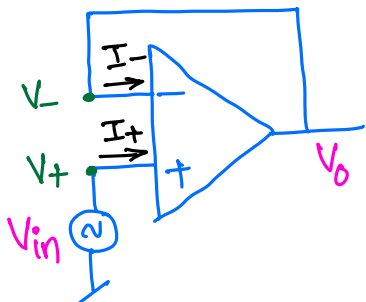
$\rightarrow$  Also, since  $R_i$  is very high  $\Rightarrow$  currents at both the inverting and non-inverting terminals of opamp can be neglected.

$$\therefore I_+ \approx I_- \approx 0 \text{ (if opamp operates in linear region)}$$

$\rightarrow$  Opamps with negative feedback operate in linear region, if voltages are within supply voltage range.

$\rightarrow$  Some of the opamp configurations operating in linear region are discussed below.

### (1) Opamp-buffer / Unity-gain Amplifier / Voltage Amplifier:



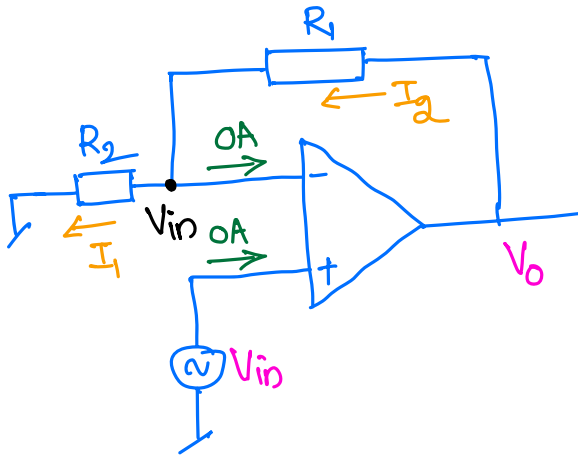
Linear region  $\Rightarrow V_+ \approx V_-$  and

$$I_+ \approx I_- \approx 0.$$

$$\therefore V_+ = V_{in} \Rightarrow V_- = V_{in}$$

$\therefore \boxed{V_o = V_{in}} \Rightarrow$  Hence the name voltage-follower / unity-gain amplifier.

## (2) Non-inverting Amplifier:



$$I_- \approx 0A \Rightarrow$$

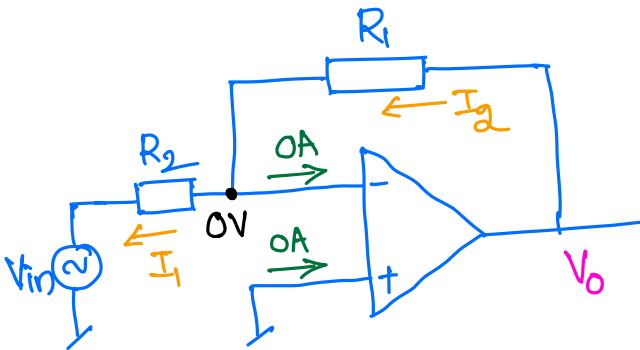
$$I_1 = I_2$$

$$\frac{V_{in}}{R_2} = \frac{V_o - V_{in}}{R_1}$$

$$\Rightarrow \frac{V_o - V_{in}}{V_{in}} = \frac{R_1}{R_2}$$

$$\Rightarrow \boxed{V_o = \left(1 + \frac{R_1}{R_2}\right) V_{in}}$$

## (3) Inverting Amplifier:



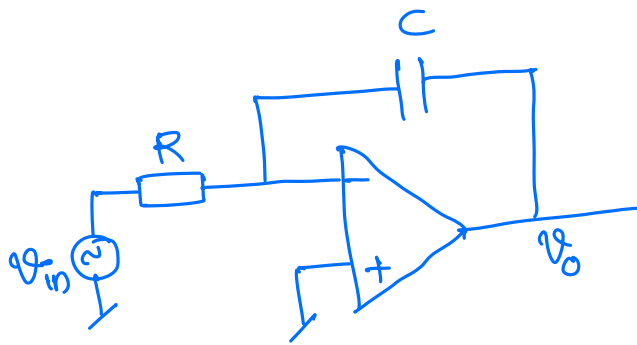
$$I_+ \approx I_- \approx 0A \Rightarrow$$

$$I_1 = I_2$$

$$\frac{-V_{in}}{R_2} = \frac{V_o}{R_1}$$

$$\Rightarrow \boxed{\frac{V_o}{V_{in}} = -\frac{R_1}{R_2}}$$

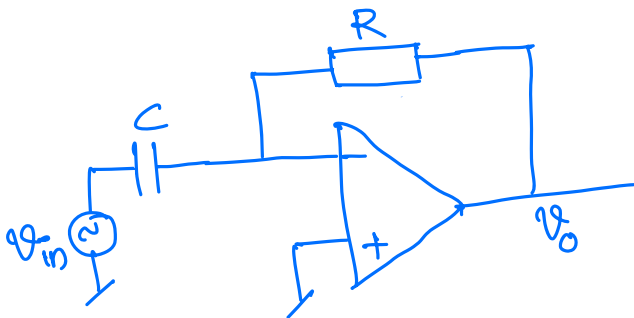
#### (4) Integrator:



$$C \frac{dv_o}{dt} = -\frac{v_{in}}{R}$$

$$\Rightarrow v_o = -\frac{1}{R_c} \int v_{in} dt$$

#### (5) Differentiator:

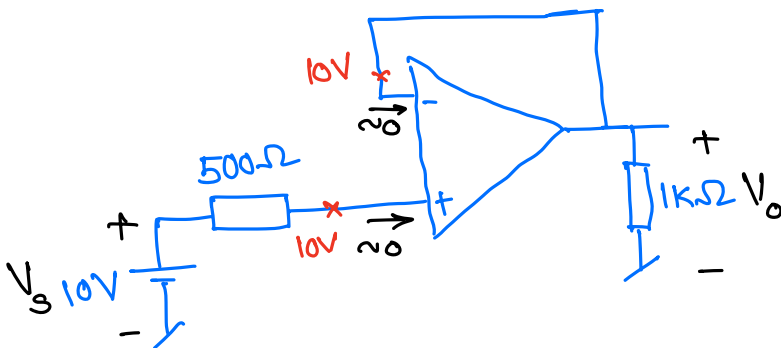


$$\frac{v_o}{R} = -C \frac{dv_{in}}{dt}$$

$$\Rightarrow v_o = -RC \frac{dv_{in}}{dt}$$

→ Let us now get back to the riddle of how unity gain buffer avoids loading effect.

#### (1) Applying Virtual short concept:



$$I_+ \approx I_- \approx 0$$

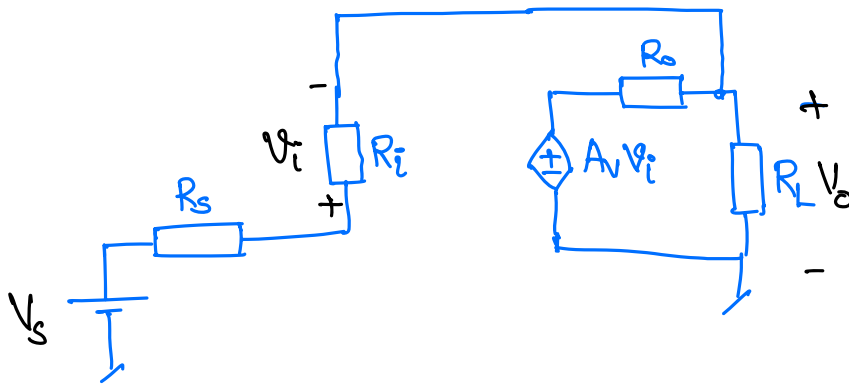
$$V_+ \approx V_- \approx 10V$$

$$\therefore V_o = 10V$$



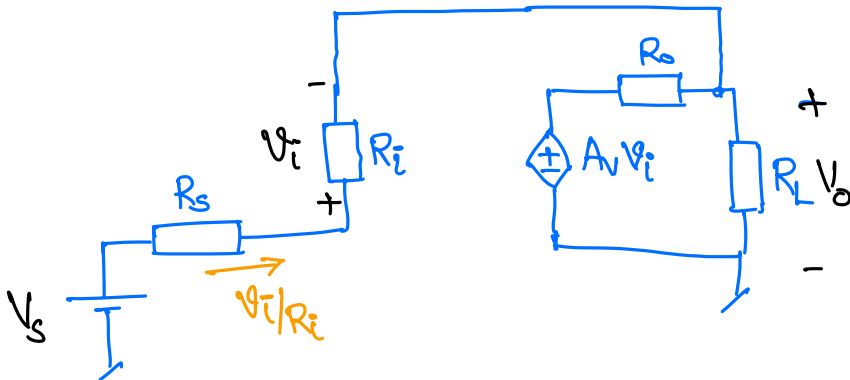
No loading effect seen!!

(2) Let's do the math rigour now (instead of applying virtual short).



$$\begin{aligned} V_s &= 10V \\ R_s &= 500\Omega \\ R_L &= 1K\Omega \\ R_i &\approx 2M\Omega \\ R_o &\approx 75\Omega \\ A_v &\approx 2 \times 10^5 \end{aligned} \left. \vphantom{\begin{aligned} V_s &= 10V \\ R_s &= 500\Omega \\ R_L &= 1K\Omega \\ R_i &\approx 2M\Omega \\ R_o &\approx 75\Omega \\ A_v &\approx 2 \times 10^5 \end{aligned}} \right\} \text{for T41 IC.}$$

Apply KVL and KCL  $\Rightarrow$



Take  $R_o = 0$  (only to ease analysis)

$$V_o = A_v V_i \quad \text{---(1)}$$

$$V_s - V_o = (R_s + R_i) \frac{V_i}{R_i} \quad \text{---(2)}$$

(1), (2)  $\Rightarrow$

$$V_s - V_o = \frac{R_s + R_i}{R_i} \times \frac{V_o}{A_v}$$

$$\Rightarrow V_o = \frac{V_s}{1 + \frac{1}{A_v} \left[ 1 + \frac{R_s}{R_i} \right]} \approx V_s$$

$$\because A_v = 2 \times 10^5 \quad R_s \ll R_i \quad (R_s = 500\Omega, R_i = 2M\Omega)$$



$$\therefore V_o \approx V_s = 10V.$$

(No loading effects seen)