The objective of the this project is to develop a Simulink-based semi-detailed simulation of a permanent-magnet AC motor drive that utilizes a sine-triangle modulator with third-harmonic injection. This simulation will be used to show that it is possible to rapidly achieve the desired (commanded) torque (within 10's of milliseconds), as long as the commanded torque is within limits. A secondary objective is to establish the torque limits given pertinent drive system parameters. An equivalent circuit/block diagram of the drive system is depicted in Fig. 1. Filter, motor, and control parameters are provided in Tables 1 through 3, respectively. A top-level simulation block diagram is shown in Fig. 2. The inverter switches and diodes are assumed to be ideal allowing the inverter to be represented using standard Simulink components as shown in Fig. 3 (do NOT use SimPowerSystems or Simscape toolboxes). The sine-triangle modulator is depicted in Fig. 4, and the current control subsystem is detailed in Fig. 5.

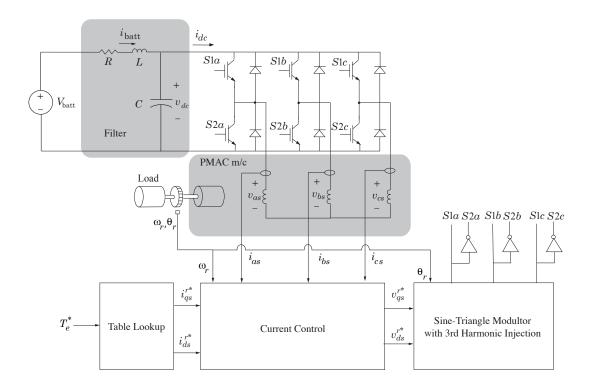


Figure 1: Circuit/block diagram.

Table 1: Source and Filter Parameters

$V_{ m batt}$	400 V
C	$2 \mathrm{mF}$
L	$20 \mu H$
R	$0.01~\Omega$

Table 2: Motor Parameters

$L_d$	2  mH
$L_q$	$3.3~\mathrm{mH}$
$r_s$	$0.02~\Omega$
$\lambda_m'$	0.2  V-s/rad
P	8
$I_{ m max}$	225 A

Table 3: Current Regulator Parameters

$K_q$	$2 \Omega$
$K_d$	$2~\Omega$

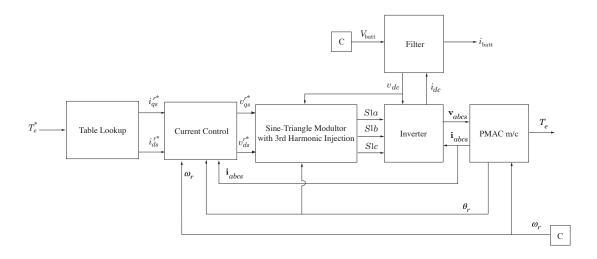


Figure 2: Top-level simulation block diagram.

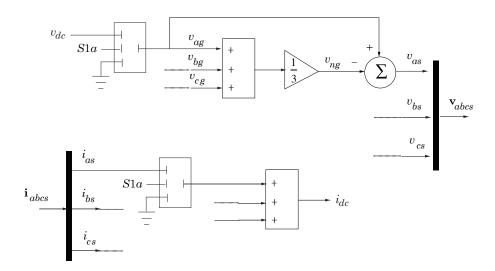


Figure 3: Inverter subsystem model.

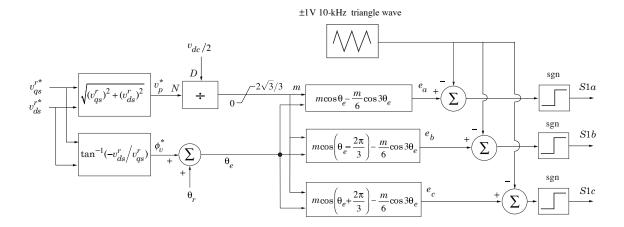


Figure 4: Sine-triangle modulator with third-harmonic injection.

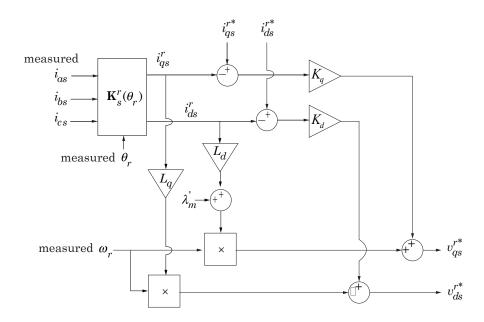


Figure 5: Current control.

1. Write a Matlab script to determine and plot optimal  $I_{qs}^r$  and  $I_{ds}^r$  as a function of desired torque. In this case, the objective is to minimize the peak stator current  $I_s = \sqrt{(I_{qs}^r)^2 + (I_{ds}^r)^2}$  subject to the constraint  $T_e = \frac{P}{2} \frac{3}{2} \left[ \lambda_m I_{qs}^r + (L_d - L_q) I_{qs}^r I_{ds}^r \right]$ . Consider the following Matlab code snippets to do this. The vectors I\_qs, I\_ds, and T\_e established in this step will be used to implement a table lookup in the Simulink model.

```
% use interior-point algorithm
 T_e = linspace(-400, 400, N);
  options = optimoptions('fmincon','Algorithm','interior-point');
      param.Te = T_e(i);
      iqd = fmincon(@(iqd)myfun(iqd), [0;0],[],[],[],[],[],[],...
                           @(iqd) mycon(iqd),options);
     I_qs(i) = iqd(1);
g
      I_ds(i) = iqd(2);
11
 end
12
13 save I_qs I_qs
14 save I_ds I_ds
  save T_e T_e
16
17
18
  function y = myfun(iqd)
19
   global param
20
   % define function to minimize
  y = sqrt(iqd(1)^2 + iqd(2)^2);
24
 function [c, ceq] = mycon(iqd)
   global param
27
   % define constraints
   +(param.L_d - param.L_q)*iqd(1)*iqd(2));
31
```

- 2. Assume the mechanical rotor speed is 500 rpm and the desired torque is 400 N·m. Given the values of  $I_{qs}^r$  and  $I_{ds}^r$  established in (1), calculate (using Park's equations) the steady-state values of  $V_{qs}^r$  and  $V_{ds}^r$ . Calculate the power supplied to the motor. If the inverter is composed of ideal switches and dc filter losses are small, the power supplied to the motor in the steady state will be close to the average power supplied by the battery. Knowing the battery voltage, estimate the average steady-state battery current. Repeat these calculations assuming the desired torque is  $-400 \text{ N} \cdot \text{m}$ .
- 3. Using the supplied subsystem models, implement a Simulink model of the drive system in accordance with Figure 2. Simulate a step change in  $T_e^*$  from 0 to 400 N·m and then to -400 N·m allowing the system to reach steady state before applying each step change. Assume that the mechanical speed is constant (500 rpm) throughout the study. Plot  $v_{as}$ ,  $i_{as}$ ,  $v_{dc}$ ,  $i_{dc}$ ,  $i_{batt}$ , and  $T_e$ , all versus time. Each plot should include a discussion of the associated results. From the simulated plots of  $i_{batt}(t)$  and  $T_e(t)$ , estimate their average steady-state values when  $T_e^*$  is equal to 400 and -400 N·m. Compare with steady-state values calculated in (2). Also, verify that the peak value of simulated  $i_{as}(t)$  is close to  $\sqrt{(I_{qs}^r)^2 + (I_{ds}^r)^2}$ .

Grading will be based upon the following criteria: documentation, results, discussion, and analysis (supporting calculations). Documentation should be sufficient to allow someone else to duplicate all results based upon information in your report. Each plot (figure) should be labeled and numbered. Each figure should include a discussion to describe the salient features of its content and any conclusions derived therefrom. Supporting calculations (analysis portion of grade) should verify that the average values of simulated  $v_{dc}$ ,  $i_{dc}$ ,  $i_{batt}$ , and  $T_e$ , and the peak value of  $i_{as}$  are close to what they should be based upon steady-state calculations. One bounus point will be awarded for submitting the project on the due date.

## Bonus (2 points)

Write a Matlab script that calculates and plots the first-quadrant maximum-torque-versus-speed characteristics of the given drive system. Assume that  $V_{s,\text{max}} = \sqrt{3}V_{\text{batt}}/3$  (modulation limit). Consider the following code snippet to do this. Plot maximum torque (in N-m) versus mechanical speed (in rpm), maximum mechanical power (in kW) versus mechanical speed (in rpm), and the  $I_s$  and  $V_s$  (peak fundamental current and voltage) needed to achieve maximum torque (plot these versus mechanical speed in rpm). At what rotor speed does the does the voltage constraint start to limit the maximum toque? At what rotor speed is the power maximum? What is the maximum power?

```
% use interior-point algorithm
  options = optimoptions('fmincon','Algorithm','interior-point');
5
  for i = 1 : N
6
      param.w_r = omega_r(i);
      iqd_forMaxT = fmincon(@(iqd_forMaxT)myfun(iqd_forMaxT),...
           [0;0],[],[],[],[],[],...
           @(iqd_forMaxT) mycon(iqd_forMaxT), options);
11
      Iqd_forMaxT(i,:) = iqd_forMaxT;
      Te_max(i) = -myfun(Iqd_forMaxT(i,:));
12
  end
14
  . . .
  function y = myfun(iqd)
16
    global param
17
    % define function to minimize
18
    % maximizing torque equivalent to minimizing negative torque
19
    y = -1.5 * param.P/2 * ...
20
          (iqd(1)*param.lambda_m + (param.L_d - param.L_q)*iqd(1)*iqd(2));
21
  \verb"end"
22
23
24
25
  function [c, ceq] = mycon(iqd)
    global param
26
   % define constraints
27
    v_q = param.r_s*iqd(1) + param.w_r*(param.lambda_m + param.L_d*iqd(2));
28
    v_d = param.r_s*iqd(2) - param.w_r*param.L_q*iqd(1);
29
30
    c(1) = sqrt(iqd(1)^2 + iqd(2)^2) - param.Is_max;
31
32
    c(2) = sqrt(v_q^2 + v_d^2) - param.Vs_max;
33
    ceq = []; % no equality constraints
34
35
  end
```