

# 1 | Groundwave

When transmitting from one radio to another the signal travel as electromagnetic waves, these waves can reach the receiver taking multiple paths. It could be a direct path from transmitter to receiver, or a reflected wave of a surface such as the ground. This worksheet will focus on the paths close to the ground. The ground acts both as a reflector and also as an absorber [Bullington, 1947]. This means that a received wave can be contributed from three main factors. In 1947 Bullington wrote that *"The principal effect of plane earth on the propagation of radio waves is indicated by the following equation"*[Bullington, 1947]. The surface part comes from the ground's absorption of the electromagnetic wave, when the energy enters the ground it sets up ground currents. These currents are a representation of the imperfect reflection.

$$E = E_0 \left[ \underbrace{1}_{\text{direct}} + \underbrace{Re^{j\Delta}}_{\text{reflected}} + \underbrace{(1-R)Ae^{j\Delta}}_{\text{surface}} \right] \quad (1.1)$$

Where:

$E$	is the received field intensity	$\left[\frac{V}{m}\right]$
$E_0$	is the received field intensity in free space	$\left[\frac{V}{m}\right]$
$R$	is the reflection coefficient of the ground	$[1]$
$\Delta$	is the phase difference between direct and reflected wave	$[\text{rad}]$
$A$	is the surface-wave attenuation factor	$[1]$

The phase difference  $\Delta$ , is the difference in phase resulting only from the difference in length between the direct wave and the reflected wave,  $L$ , which can be found using geometry. The phase difference can be found as:

$$\Delta = 2\pi \frac{L}{\lambda} \quad (1.2)$$

Where:

$L$	is the difference in length between the direct wave and the reflected wave	$[\text{m}]$
$\lambda$	is wavelength	$[\text{m}]$

For a plane earth case this is  $L$  is found as:

$$L = \sqrt{(h_t + h_r)^2 + d^2} - d \quad (1.3)$$

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Where:

$d$	is the distance between the transmitter and receiver	[m]
$h_t$	is the height of the transmitter	[m]
$h_r$	is the height of the receiver	[m]

For cases where the  $d > 5(h_t + h_r)$  this can be approximated as [Bullington, 1947]:

$$L = \frac{2h_th_r}{d} \quad (1.4)$$

$$\Delta = 4\pi \frac{h_th_r}{d\lambda} \quad (1.5)$$

The reflection coefficient  $R$  is dependent on the incoming angle of the signal,  $\theta$ , as well as the electromagnetic properties of the ground,  $\epsilon$  and  $\sigma$ . The relation can be written as[Bullington, 1947]:

$$R = \frac{\sin(\theta) - z}{\sin(\theta) + z} \quad (1.6)$$

Where:

$z$	$\frac{\sqrt{\epsilon_0 - \cos^2(\theta)}}{\epsilon_0}$ for vertical polerization	[1]
$z$	$\sqrt{\epsilon_0 - \cos^2(\theta)}$ for horizontal polerization	[1]
$\epsilon_0$	$\epsilon - j60\sigma\lambda$	[1]
$\epsilon$	is the dielectric constant of the ground relative to unity in free space	[1]
$\sigma$	is the conductivity of the ground in mhos per meter	$\left[\frac{mhos}{m}\right]$
$\theta$	is reflection angle	[rad]

By looking at this equation it can be seen that as  $\theta$  goes towards 0,  $R$  goes towards -1. Which also implies that for sufficiently low receiver and transmitter, the direct and reflected wave is completely out of phase since  $Re^{j\Delta} = -1$ . This leaves only the surface wave part of the equation.

The surface wave attenuation factor can be approximated as[Bullington, 1947]

$$A \approx \frac{-1}{1 + j\frac{2\pi d}{\lambda} (\sin(\theta) + z)^2} \quad (1.7)$$

This approximation holds for  $A < 0.1$ , however for  $A$  approaching unity the phase approaches 180 degree [Bullington, 1947].

When  $\theta$  approaches zero only the surface wave component remain and it is thus sufficient to look at the magnitude of it [Chong and Kim, 2013]

$$|(1 - R)A| \approx \left| 2 \frac{-1}{1 + j \frac{2\pi d}{\lambda} (\sin(\theta) + z)^2} \right| \quad (1.8)$$

$$|(1 - R)A| \approx \frac{2}{\frac{2\pi d}{\lambda} z^2} \quad (1.9)$$

By introducing  $h_0$ , the minimum effective antenna height, as:

$$h_0 = \left| \frac{\lambda}{2\pi z} \right| \quad (1.10)$$

Where:

$h_0$  is the minimum effective antenna height [m]

By utilizing this Equation 1.9, can be written as:

$$|(1 - R)A| \approx \frac{4\pi h_0^2}{\lambda d} \quad (1.11)$$

The received power can then be found using [Chong and Kim, 2013]

$$P_r = P_0 \left( \frac{E}{E_0} \right)^2 \quad (1.12)$$

$$P_r = P_t G_r G_t \frac{\lambda^2}{(4\pi)^2 d^2} \left( \frac{E}{E_0} \right)^2 \quad (1.13)$$

Where:

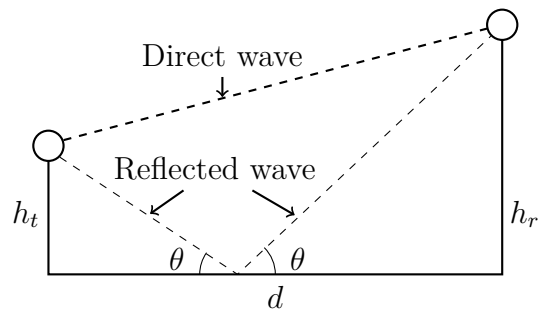
$P_r$  is the received power at the receiver antenna [W]

$P_0$  is the predicted power by the free space model [W]  
(see free space model worksheet)

$P_t$  is the transmitted power from the transmitter [W]

$G_r$  is the gain of the receiver antenna [1]

$G_t$  is the gain of the transmitter antenna [1]



**Figure 1.1:** Illustration

# Litteratur

- Bullington, K. (1947). Radio Propagation at Frequencies Above 30 Megacycles. *PROCEEDINGS OF THE I.R.E.* årg. 35, hft. 10, 10-1947, s. 1122–1136.
- Chong, P. K. and Kim, D. (2013). Surface-Level Path Loss Modelling for Sensor Networks in Flat and Irregular Terrain. *ACM Transactions on Sensor Networks*. Vol. 9, No. 2, Article 15.