

A Novel On-Board Electrochemical Impedance Spectroscopy System for Real-Time Battery Impedance Estimation

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Abstract—This paper proposes a real-time electrochemical impedance spectroscopy (EIS) technique, that can provide high accurate estimation of the impedance of each Li-ion cell of a battery (BT) stack, even for less than mOhm. Thus, the suggested EIS technique can be used in high demanding applications, such as nearly zero-energy buildings, microgrids and electric vehicles. This is attained, because a smooth cell excitation current is utilized that is provided by the proper control of the gate-source of each cell's parallel-connected MOSFET and thus, effective harmonic analysis can be accomplished. Since the circuit topology of the EIS is implemented without requiring expensive electronic equipment, it is affordable to be applied in the BT system of any application. The proposed EIS system can cooperate with a BT cell equalization (BCE) system that utilizes the same MOSFET control scheme to provide the excitation current. Thus, a combined EIS-BCE system is developed that can be used to improve the performance of a Li-ion BT management system (BMS). The accuracy of the EIS technique and its high performance by operating within a combined EIS-BCE system are experimentally validated.

Index Terms—Electrochemical impedance spectroscopy, battery management system, battery cell equalization, energy storage system, microgrid and electric vehicle.

I. INTRODUCTION

IT is well known that the electrochemical energy storage is increasingly emerged as the key technology which can play a crucial role in the improvement of the energy sustainability, in several sectors of the everyday life [1]. Especially, the wide-spread penetration of renewable energy and distributed generation (DG) in power networks, as well as, the increasing electric mobility have become significant fields of interest for the use of the energy storage systems [2].

The lithium-ion (Li-ion) BT is a key technology for the future energy storage systems [3], due to the competitive advantages against the other BT types, such as the high energy density, the high charge/discharge current capability and the low self-discharge rate [4]. Although, the Li-ion BTs could be considered as a promising solution, they have several drawbacks that should be considered during the design of an energy storage system, i.e. limited cycle and calendar life, higher cost, sensitivity in extreme temperature conditions and safety issues. Moreover, the Li-ion BTs performance is highly sensitive to overvoltage/undervoltage and overcurrent. Therefore,

in order to be protected the performance and the lifespan of a Li-ion BT cell, it should operate within the voltage, temperature and current rate limits, as that are defined by the manufacturer.

A common characteristic of the Li-ion BTs is the low operating voltage, and thus, several cells should be connected in series to meet the voltage requirements. This may cause imbalance problems in a BT stack that are mainly owed to the different internal characteristics of the cells, such as the coulombic efficiency, the capacity and the self-discharge rate [5]. Moreover, internal resistance growth and capacity fade, along with potential imbalance issues may result to significant reduction of the power and energy capability of a BT system [6].

The above can be avoided by properly controlling the cells of a Li-ion BT stack in order to reduce the imbalance effects and keep each cell operation within safety and acceptable limits of the voltage, current and temperature [7]. Thus, several BCE methods have been proposed in the technical literature that can be classified as energy dissipative and non-dissipative [8]. The dissipative cell balancing methods are simpler and low cost; however, the equalization electric energy is wasted in heat. In the non-dissipative methods, the equalization energy is transferred among the other cells and thus, they are more efficient [9]. However, they are more expensive and complicated in the implementation and thus, more susceptible to faults that may result to reduction of the BT system reliability [10].

For the proper operation of a BT system, it is highly important the accurate knowledge of the operating parameters of each BT cell, in real-time basis, such as the state of charge (SoC), state of health (SoH) and state of function (available charging and discharging power, SoF) [11]. Since the aforementioned parameters cannot be directly measured, they are usually estimated by utilizing the BT model, that is however highly influenced by the ageing level [12]. Therefore, several techniques have been proposed to accurately estimate the BT model parameters, so as, the model is updated with respect to the actual operating conditions [13]. However, due to the increase in the cost and complexity, these techniques are rarely embedded in a BT system [14].

It is well known that the impedance of a Li-ion BT can provide important information for the electrochemical condition within the cell that can be utilized for the accurate evaluation of the BT state. Therefore, an easily implemented and cost-effective estimation method of each cell impedance can

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be a useful tool for a high performance BT system [15]. One widespread non-invasive estimation method of the Li-ion BT impedance is the EIS [16], that has been adopted by several laboratory instruments for offline measurements of the cell impedance for a wide frequency range [17] and has also been utilized to estimate the BT model parameters [18].

The EIS technique can be categorized in *single-frequency*, where the individual frequencies are measured sequentially and *broadband*, that utilizes multiple simultaneous sinusoidal excitations [19]. Although the broadband methods are faster than the single-frequency, they need larger time to settle to a steady state response that may diminish the above advantage. On the other hand, the benefits of the single-frequency techniques are the higher accuracy and effectiveness in the EIS performance, since the fundamental frequency of each operation cycle is known a priori. Therefore, less interference by the noise in the impedance estimation is caused compared to the broadband methods, where advanced computation techniques are needed to reject the noise, that may result to the increase of the complexity [20], [21].

It is well known that, the frequency spectrum of interest for the BT cell's impedance estimation ranges from a few kHz to several mHz and thus, the EIS can be accomplished with the single-sine technique at an acceptable time duration [22]. Therefore, considering the capabilities of high accuracy and effectiveness, lower complexity and with an acceptable duration for the impedance estimation procedure, the single-frequency technique can be the suitable choice for an EIS system [23]. This is confirmed by the growing interest of the electronic equipment industry that works on the development of ICs to facilitate the real-time single-frequency EIS techniques for Li-ion BTs, such as [24].

Due to the advantages that the EIS technique can provide in the accurate estimation of the Li-ion BT impedance, it attracts a growing research interest by the research community. Thus, the research efforts are towards the development of an EIS system which can accurately and in real time estimate the cells' impedance, that then can be used for the evaluation of several BT operating states, such temperature and online modeling, as well as, various operating parameters, such as SoC, SoH and SoF have been pointed out in [25]-[28]. However, most of the published online EIS techniques are focused on the estimation of the impedance of the whole BT pack [29]-[41] and consequently, they do not provide information for the individual operating state of each cell that it could effectively contribute to the improvement of the BT system performance. Moreover, they use external power sources for the injection of the excitation current, such as the motor controller [31] and BT chargers based on several type dc-dc conversion topologies, such as dc-dc boost converter [29] and bidirectional dc-dc converter [30], as well as, ac-dc conversion topologies, such as dual active bridge converter [39] and single-phase two-level full-bridge converter [40]. Consequently, the implementation of the above EIS techniques is directly dependent on the external power sources and consequently, they cannot be embedded in an individually operated BT system.

Although an EIS technique that can real-time estimate the

impedance of each cell of a BT pack has been proposed in [42], it has been focused on BT cells with relatively high impedance (61.3mOhms). However, this does not correspond to BT systems for high demanding applications, such as nearly zero-energy buildings, microgrids and electric vehicles, since their impedance is in the range of mOhms so as, they are capable to provide the relatively high current which is required by those applications [43]. The limitation to relatively high impedance of the [42] is owed to the implementation of the EIS technique that has been designed for a low excitation current, since a high excitation current that could allow low values of cell's impedance estimation may increase the cost and the volume of the non-dissipative dc-dc converter layout and thus, it may become less practical for a real application. Some other attempts for online EIS impedance estimation on the cell level have been conducted in [44],[45]; however, the frequency range is confined with respect to the lower frequencies to 1Hz, which do not cover the required frequency range for Li-ion cells. The above publications do not give explicit information for the EIS software and they are referred to a relatively high energy capacity BT system utilizing a dc-dc converters' topology with ultracapacitors and switch matrix devices for the implementation of the cell equalization. Consequently, a larger frequency range for the EIS procedure may result to significantly increase of the hardware requirements and complexity.

From the above it is revealed that there is a need for an improved and effective EIS technique in an integrated scheme of hardware topology and software algorithm that is capable to accurately estimate Li-ion BT cells impedance even for less than mOhm. Moreover, it should be easily implemented and cost-effective, so as, it can be affordable to be embedded in a Li-ion BT system. Therefore, it can be utilized in a wide range of Li-ion BT systems and more important, for high demanding applications, such as nearly zero-energy buildings, microgrids and electric vehicles. Moreover, the hardware topology should ensure high accuracy in the measurements and the injection of the proper excitation current. Therefore, high performance of the EIS procedure and satisfactory accuracy of the cell impedance estimation can be attained.

The aim of this paper is to fulfil all the above requirements and to propose an effective and highly accurate EIS technique that can real-time estimate the impedance of Li-ion BT cell over a wide frequency range. The accuracy of the cell impedance estimation is attained through an advanced system of hardware topology and a Fourier analysis based calculation algorithm. Thus, contrarily to the up to now published EIS techniques that use sophisticated switching topologies based on ac-dc and dc-dc converters in order to inject the variable frequency excitation signal, the proposed EIS system employs a simpler and more reliable topology that is based on using a MOSFET in parallel connection with each BT cell that acts as controllable source to provide the required excitation current. The regulation of the excitation current is attained through the proper control of the gate-source of the MOSFET. Therefore, a smooth current profile is provided for accomplishing accurate and effective EIS procedure. Also, the requirements of

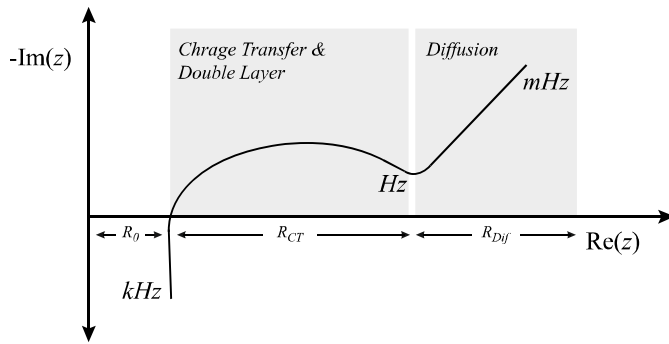


Fig. 1. EIS Nyquist plot representation.

low complexity, and thus, less vulnerability to faults as well as low cost are met, and thus, the proposed EIS scheme can be applied to any BT system. Moreover, the proposed EIS system can be housed on the BT control electronic board and thus, it can independently operate with respect to the power charger and the BT-powered application. The accuracy of the suggested EIS technique is validated by comparing it with a commercial laboratory instrument, while the high performance is experimentally verified by examining its operation within a combined EIS-BCE system for a Li-ion BT scheme of two series connected cells.

II. UNDERLYING THEORY OF EIS

The EIS is considered as a non-destructive characterization technique, that allows the physical interpretation and modeling of the underlying phenomena that takes place inside a Li-ion BT cell [46]. It can be used either in potentiostatic mode, where the voltage is used as excitation signal and the current as measurement signal, or in galvanostatic mode, where the opposite series in the signals is applied [47]. In most commonly used EIS applications, the excitation signal is a sinusoidal reference signal, and the real and the imaginary parts of the BT impedance can be estimated by the measurement signals [48]. The variation of the impedance of a BT cell with respect to the frequency, as resulted by the EIS technique, is more commonly represented by Nyquist and bode plots.

A typical Nyquist plot obtained by the EIS technique is illustrated in Fig. 1. The real part of the impedance is attributed to the ohmic character of the Li-ion BT cell, while the imaginary part is referred to the capacitive and inductive character. The plot can be divided into three regions with respect to the working frequency [49]-[51]. Specifically, the high frequency region on the left (in the range of kHz) is mainly attributed to the ionic resistance of the electrolyte, the ohmic resistance of the metal parts of the electrodes and the inductive behavior of the cell, whose role is more important as the frequency increases. The mid frequency region (kHz-Hz), where the semicircle occurs, represents the charge transfer and the double layer phenomenon which occurs at the area between the electrolyte and the electrodes. Depending on the chemistry and the degradation level of a BT, a second semicircle may occur between the high frequency and the mid frequency regions, that is attributed to the solid electrolyte interphase layer, which is

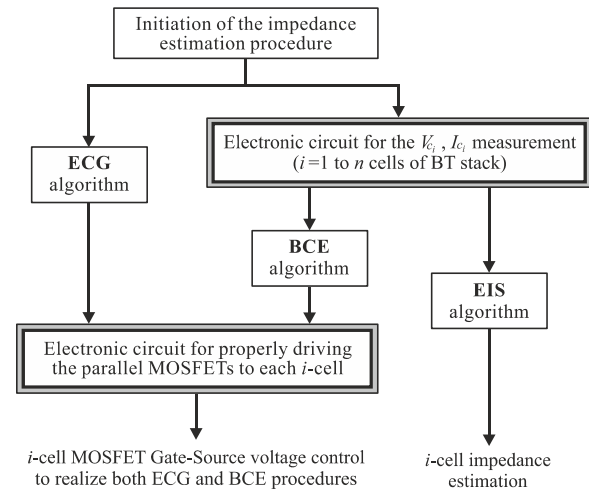


Fig. 2. Structure overview of the proposed BT cell impedance estimation scheme based on the EIS technique.

created on the negative graphite electrode. Finally, the low frequency region (Hz-mHz) represents the mass transport effects, which are mainly affected by the diffusion phenomena in the active materials inside the electrodes.

III. OVERVIEW OF THE PROPOSED EIS METHODOLOGY

The structure overview of the proposed BT cell impedance estimation scheme based on the EIS technique and combined with the BCE system is illustrated in Fig. 2. When the impedance estimation procedure is initiated, the excitation current generation (ECG) algorithm instructs an electronic circuit to provide the correct excitation current profile to each BT cell, as that is needed for the impedance calculations through the EIS algorithm. This electronic circuit comprises a MOSFET in parallel connection with the corresponding BT cell and a drive unit to regulate the operation of the MOSFET through the proper control of its gate-source voltage. The excitation current that is commanded by the ECG is a sinusoidal signal with controllable amplitude and frequency that can be injected, either in conjunction with the BCE system or only for the EIS operation.

The EIS algorithm measures the voltage and current of each cell, V_{c_i} and I_{c_i} , respectively and provides the impedance estimation that can be used for the calculation of several BT operation parameters. Note that, the BCE algorithm runs with a certain sampling ratio, while the combined system of ECG and EIS algorithms operate asynchronously and when the cell impedance estimation is required.

The proposed EIS system can accurately estimate the BT cell's impedance irrespective of the level of the load current, since the frequency of the excitation current is a priori known and also, smooth equalization current is provided by properly regulating the gate-source of the parallel connect MOSFET to each BT cell. Moreover, since the proposed EIS procedure is applied during the charging of the BT system of which the performance is properly controllable, high dynamic performance is not observed.

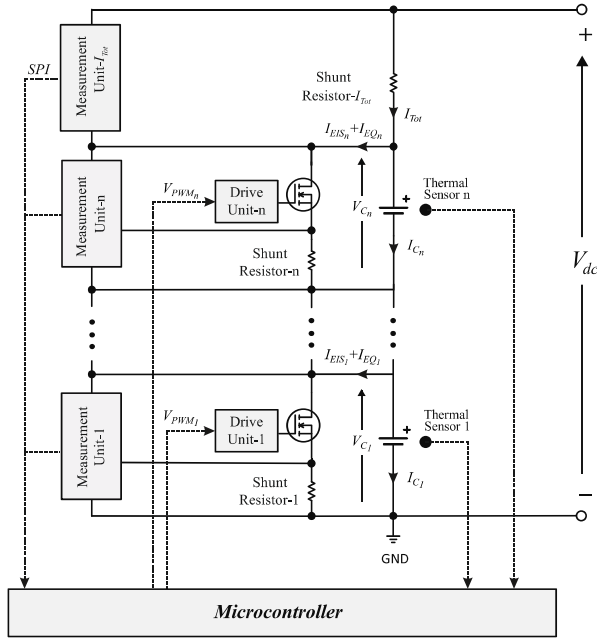


Fig. 3. Structure overview of the hardware topology for the implementation of the impedance estimation procedure, based on the EIS technique.

IV. STRUCTURE OF THE PROPOSED CONTROL SCHEME

The structure overview of the hardware topology of the proposed BT cell impedance estimation technique is shown in Fig. 3. It comprises the measurement and the drive units, the MOSFETs that are in parallel connection with the corresponding cells, and the appropriate temperature sensors for each i -cell. The voltage, current and temperature measurements are provided to the microcontroller through the serial peripheral interphase (SPI) protocol and are used by both the EIS and BCE systems. Each drive unit regulates the gate-source voltage of the corresponding MOSFET through the PWM signal that is provided by the microcontroller for realizing both the EIS and BCE procedures.

A. BT Cell Measurement Unit

The schematic layout of a measurement unit that is used to measure the voltage and the current of each cell and the whole BT stack is illustrated in Fig. 4. The four-terminal Kelvin measurement topology is used for both the voltage and the current measurements. A gain programmable instrumentation amplifier is used to measure the differential voltage across each BT cell, in order to eliminate any interferences with respect to the ground potential that could be introduced in the case of a single-ended measurement. The cell voltage and current measurements are buffered via an operational amplifier (Op-Amp), and they are provided to the ECG-EIS and BCE systems through the analog to digital converters (ADCs), utilizing the SPI protocol.

The gain for the cell voltage measurement has been set to 1V/V. The gain for the shunt voltage measurement has been set to 10V/V, while the exact gain for the current measurement depends on the proper selection of the shunt resistor. Finally, an external voltage reference is used for the ADCs in order to improve the accuracy of the measurements.

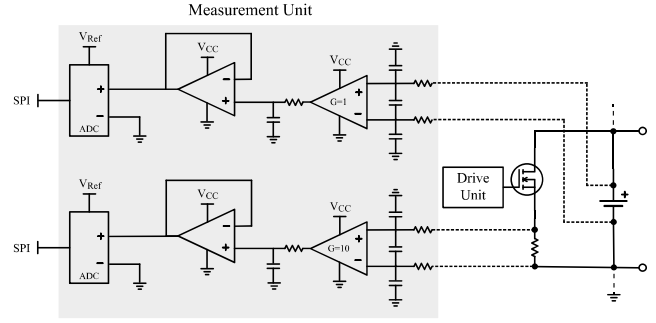


Fig. 4. Schematic layout of the measurement unit, that is utilized in the implementation scheme of the EIS-based impedance estimation procedure.

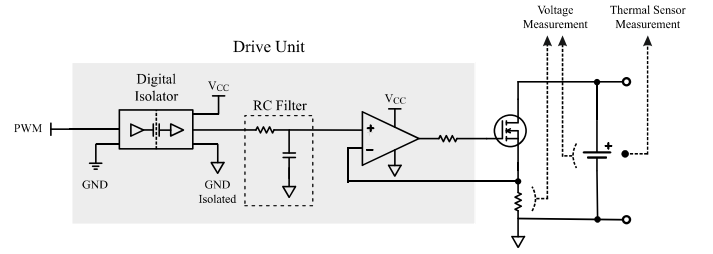


Fig. 5. Schematic layout of the MOSFET drive unit, that is utilized in the implementation scheme of the EIS-based impedance estimation procedure.

B. BT cell MOSFET Drive Unit

To produce the excitation and equalization currents for the EIS and BCE systems, respectively, the methodology of [52] has been adopted. Specifically, the excitation and equalization currents are provided by properly regulating the operation of each MOSFET that is parallel connected to the corresponding BT cell. Thus, each MOSFET operates at the saturation region and acts as a controllable source by properly regulating the gate-source voltage through the respective controllers. Therefore, unlike the highly pulsating current that would be applied if the MOSFET was in parallel connection with a fixed resistance which would be in series with the BT cell, a smooth current profile is provided with the above proposed configuration that can contribute to the effective harmonic analysis of the EIS and consequently, high accuracy of the cell's impedance estimation is accomplished.

Note that, when the BT system is online, the excitation current of the EIS is superimposed on the equalization current of the BCE, and consequently, a unique current with the proper profile is provided by the MOSFET. Whereas, when the BT system is off-line, only the excitation current is supplied to the corresponding cell. Thus, one current with the correct profile is provided by one power source (the parallel connected MOSFET at each BT cell) that is controlled by the combined EIS-BCE procedure. Since the excitation current of the EIS is superimposed on the equalization current of the BCE, they do not influence each other, and the two procedures can independently operate. Moreover, since a common power source is utilized, less hardware and lower complexity are attained. Contrarily, if a decoupled hardware topology of two power sources had been used (i.e. two dc-dc converters), the hardware requirements and the control complexity would be in-

creased without providing any advantageous features to the performance of the EIS and BCE.

The schematic layout of the MOSFET drive unit for both the EIS and BCE procedures is illustrated in Fig. 5. As can be seen, the topology is based on the current control of the MOSFET via the feedback measurement from the shunt resistor. The input PWM signal is isolated via the digital isolator and it is converted to an analog signal by the resistor-capacitor (RC) filter in order to drive the noninverting input of the Op-Amp. The MOSFET current is regulated by properly controlling the voltage drop across the feedback shunt resistor based on a closed-loop logic control technique and therefore, it is not affected by the delay that the RC filter may introduce, nor it is based on the ideal curve of the MOSFET. Since the voltage across the inputs of the op-amp increases as the number of series connected BTs increases, an isolation interface is needed in order to properly control the current at each MOSFET. Specifically, high speed isolators have been adopted, in order to isolate each drive unit and with adequately large bandwidth, in order to get the maximum response on the high frequency range of the EIS excitation current.

Since each MOSFET provides smooth current profile for both the EIS and BCE procedures by operating in the saturation region, through the proper regulation of the gate-source voltage, and thus, it does not operate with high switching frequency, it seems unlikely to fail during the normal operation. However, since the BT safety is extremely important, each MOSFET circuit is protected by a fuse. Note that, a specialized fault tolerance system or a backup system to replace any potential problematic MOSFETs will considerably increase the cost, the complexity and the size of the system and consequently, it is avoided.

V. REAL-TIME EIS-BASED ESTIMATION ALGORITHM

The flow chart that describes the proposed impedance estimation algorithm is illustrated in Fig. 6. It needs the measurements of the voltage and current of each i -cell, V_{C_i} and I_{C_i} , respectively, of the n cells of the BT stack. The ECG algorithm is activated by the enable command and it produces the proper reference excitation current I_{EIS_i} for each i -cell, which consists of sequential series of k -order frequency sinusoidal signals with controllable amplitude. The I_{EIS_i} current can be either superimposed on the cell equalization current I_{EQ_i} of the BCE (when the BT system is online) or it is solely supplied to the corresponding i -cell (when the BT system is offline). Thus, for each k -order frequency $I_{EIS_i}^k$, the resulting reference excitation current $I_{REF_i}^k = I_{EIS_i}^k + I_{EQ_i}$ is compared with the actual current I_{C_i} of the i -cell, that is obtained by the measurement unit. Then, the $error_i^k = I_{REF_i}^k - I_{C_i}^k$ is driven to a digital proportional-integral (PI) controller and the output is a PWM signal that controls the gate-source voltage of the corresponding MOSFET and consequently, the BT current I_{C_i} . Instead of the PI controller, a fuzzy-logic controller or simply a proportional control unit could be used to drive the gate-source of the MOSFET. However, the PI controller exhibits better performance due to its integral control term.

The ECG, apart from the I_{EIS_i} generation, is also responsi-

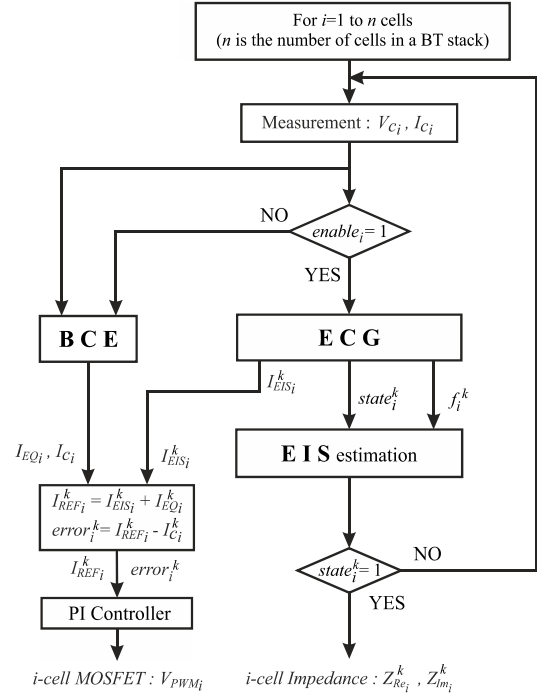


Fig. 6. Flow chart of the proposed real-time EIS estimation algorithm.

ble to regulate the operation of the EIS estimation procedure of any i -cell, through the $state_i^k$, and also to inform the EIS algorithm for the frequency f_i^k of the excitation current. The output of the EIS estimation procedure is the real and the imaginary part of the impedance Z_i^k of each i -cell of the Li-ion BT stack, per k -order frequency f_i^k .

A. ECG Algorithm

The ECG algorithm determines the proper excitation current for the effective performance of the EIS procedure and the satisfactory estimation of the Li-ion BT cells impedance. The frequency range, the number of the signal periods and the impedance estimation points per decade of the excitation current play a crucial role for the proper performance of the EIS [53], [54]. Specifically, the frequency range should be properly chosen, so as, both the diffusion phenomenon at low frequencies and the zero cross ohmic resistance at high frequencies are satisfactorily considered. The number of the signal periods per k -order frequency should ensure both short EIS procedure duration and satisfactory time margin for the proper estimation of the i -cell impedance. Also, an acceptable number of impedance estimation points per decade should be provided, so as, satisfactory information for the impedance variation throughout the whole frequency range are acquired. The above parameters should be properly determined before the EIS procedure is initiated, by considering the specific requirements of the Li-ion BT system application. For the examined case, the frequency range is selected from 2kHz to 20mHz, since frequencies outside of this range do not provide important information for the impedance of Li-ion BTs and also, it is selected that the cell impedance is estimated at 9 points per decade. Thus, the total points for the 5 logarithmic decades of the frequency range 1kHz to 20mHz is 45 and add-

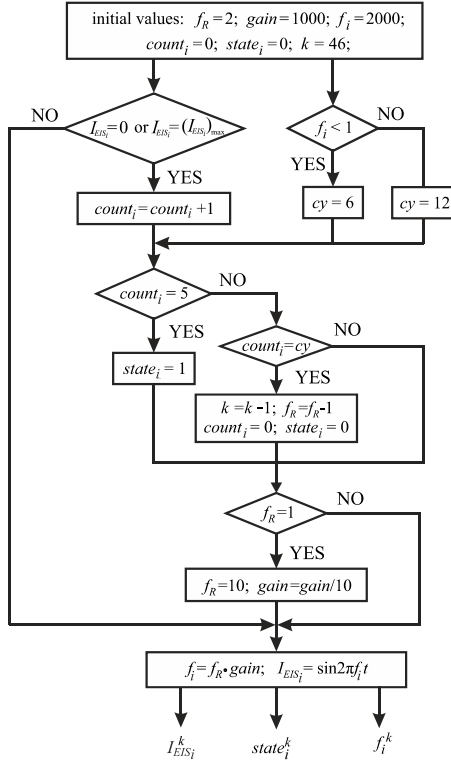


Fig. 7. Flow chart of the ECG algorithm.

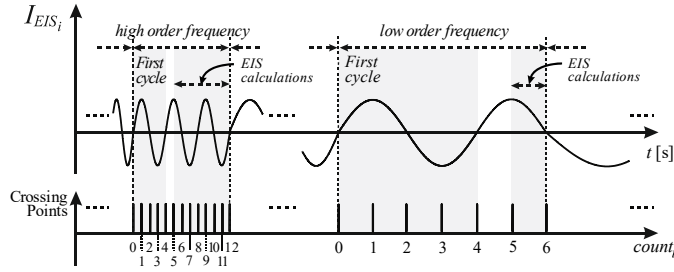


Fig. 8. Schematic representation of the cell excitation current for the EIS procedure.

ing one point that corresponds to the frequency of 2kHz, we have 46 impedance estimation points for the chosen frequency range 2kHz to 20mHz.

The flow chart of the ECG algorithm is shown in Fig. 7. It runs from the higher to lower frequencies with logarithmic variation of the step frequencies. The operation margins for each k -order frequency are delimited by the zero crossing and maximum value points of the excitation signal I_{EIS} . A schematic representation of the excitation current profile is illustrated in Figs. 8.

The initial values for the variables in the Fig. 7 are determined based on the previous analysis and the fact that the algorithm runs from the high to the minimum frequency limits. Specifically, the initial value of the f_R variable corresponds to the running point per decade (initially 2, for the starting frequency of 2 kHz), the gain variable determines the decade of the frequency points (initially 1000 for the 1-10 kHz decade), and the f_i variable corresponds to the running frequency (starting frequency 2 kHz). The counters $count_i$ and $state_i$ are initi-

ed by the zero value, while the cy variable is the limit for the counter $count_i$ and it takes values 6 and 12. Finally, the estimation point variable k , that is used in the tables which store the results of the EIS procedure, starts with the value 46 that corresponds to the maximum number of the estimation points.

As mentioned above, the frequency changes logarithmically with 9 frequency orders per decade, while adapted number of cycles are used per order. Specifically, 3 cycles are applied at higher frequencies (greater than 1Hz), while it is reduced to 1.5 cycles for the lower frequencies (less than 1Hz). This is allowed because a smooth cell current (sum of excitation and equalization current) is provided due to the the proposed MOSFET control topology and thus, there is no need for high settle time to reach the steady state. Therefore, a quarter of a cycle is sufficient for the low frequencies to get satisfactory measurements and to provide accurate impedance estimation. The impedance measurements acquisition is enabled at the end of the first $1^{1/4}$ cycle of the excitation current, since additional to the first cycle, a quarter of cycle is needed due to the delay of the voltage signal with respect to the current which is owed to the capacitive nature of the BT cell. For the higher frequencies, since the period per cycle has been reduced and considering the microcontroller frequency, a larger time interval is needed (at least 3 cycles) for accomplishing both, satisfactory settling to a steady-state condition and accurate impedance estimation.

The above setting in the number of cycles, with respect to the frequency order, shortens the duration of the EIS procedure and also ensures satisfactory accuracy in the impedance estimation. Thus, for the frequency range from 2kHz to 20mHz, the total impedance estimation points are 46, and the total duration of the EIS procedure is 5.4min.

The zero crossing and maximum value points of the excitation current are counted by the variable $state_i^k$ (for the i -cell and k -order excitation current). As can be seen in the flow-chart of Fig. 7, when the variable $count_i$ is equal to 5, it means that $1^{1/4}$ periods of the k -order frequency excitation current have been completed and thus, the variable $state_i$ becomes 1 and the EIS estimation procedure results are received. When the $count_i$ is equal to 6 (for the low frequencies $f_i < 1$ Hz), it means that 1.5 cycles of the k -order frequency have been completed, while, if it is equal to 12 (for the higher frequencies, $f_i \geq 1$ Hz) it means that 3 cycles have been completed. Thus, for both cases, the variable $state_i$ gets the value 0 and the frequency of the excitation current is reduced by one order ($k-1$). It is also examined if the 9 frequency orders, per decade, of the excitation current have been completed, and if this occurs, the frequency moves to the next decade by decreasing the parameter $gain$ to $gain/10$.

B. EIS Procedure for the Cell Impedance Estimation

For each k -order frequency, the results of the EIS procedure are acquired when the variable $state_i^k$ gets the value 1 (Fig. 6). Since the BT cell current is created by the sum of the excitation and the equalization currents, the Fourier analysis is utilized to obtain the fundamental voltage and current for each k -order frequency. Thus, the measured voltage and current V_{c_i} and I_{c_i} ,

respectively, are multiplied by cosine and sine signals and then, the Fourier components are calculated by the numerical integrations of the following

$$a_{V_{ci}}^k = \frac{2}{T^k} \int_{t_h}^{T^k+t_h} V_{ci}(t) \cos(2\pi f_i^k) dt \quad (1)$$

$$b_{V_{ci}}^k = \frac{2}{T^k} \int_{t_h}^{T^k+t_h} V_{ci}(t) \sin(2\pi f_i^k) dt \quad (2)$$

and

$$a_{I_{ci}}^k = \frac{2}{T^k} \int_{t_h}^{T^k+t_h} I_{ci}(t) \cos(2\pi f_i^k) dt \quad (3)$$

$$b_{I_{ci}}^k = \frac{2}{T^k} \int_{t_h}^{T^k+t_h} I_{ci}(t) \sin(2\pi f_i^k) dt \quad (4)$$

where T^k is the period of the k -order frequency excitation current and t_h is the time instant that the measurements are obtained. Therefore, the amplitude and the phase of the impedance are determined, respectively, by

$$|Z_i^k| = \frac{\sqrt{(a_{V_{ci}}^k)^2 + (b_{V_{ci}}^k)^2}}{\sqrt{(a_{I_{ci}}^k)^2 + (b_{I_{ci}}^k)^2}} \quad (5)$$

$$\phi_{Z_i^k} = \arctan(b_{V_{ci}}^k / a_{V_{ci}}^k) - \arctan(b_{I_{ci}}^k / a_{I_{ci}}^k) \quad (6)$$

and thus, the real and the imaginary parts of the impedance are

$$\text{Re}(Z_i^k) = |Z_i^k| \cos(\phi_{Z_i^k}) \quad (7)$$

$$\text{Im}(Z_i^k) = |Z_i^k| \sin(\phi_{Z_i^k}) \quad (8)$$

As aforementioned, during the quarter of a cycle, for the low frequencies and $1^{3/4}$ cycles for the high frequencies, the EIS algorithm obtains the i -cell voltage and current measurements and determines the real and the imaginary parts of the impedance for the k -order frequency.

VI. EXPERIMENTAL RESULTS

The theoretical considerations of this paper have been experimentally verified on a high-power Li-ion BT cell (Melasta LPB042126H) with nominal capacity, voltage and discharge current of 7.4Ah, 3.7V and 10C, respectively. The control software is realized on the microcontroller TMS320F28379D, which communicates with the measurement and drive units via the SPI protocol and PWM signals, respectively. The running frequency of both the EIS procedure and the PI controller is 40kHz, while the frequency of the excitation current ranges from 2kHz to 20mHz. Thus, both the EIS procedure and the PI controller are faster than the excitation current (e.g. the EIS procedure and PI controller are 20 times faster for the maximum excitation current of 2kHz and this ratio increases as the excitation current frequency reduces) and also, they are faster than the monitoring and equalization processes of the BCE system, for which the sampling ratio is 1kHz.

The measurement unit comprises the LTC2368 ADC, the LT6657 with reference voltage 5V and the LT6370 instrumentation amplifier. The gain for the cell voltage measurement has been set to 1V/V, while the gain for the 100mΩ shunt current resistor has been set to 1A/V. The signals are digitized through the 5V, 24-bit ADC, which results to a sense resolution of 0.3μV and 3μA for the voltage and current, respectively. The shunt resistor of 100mΩ handles the DC equalization current of 1A plus the AC current of the EIS of 1A (peak value). Thus, the maximum thermal power at the shunt resistor is 0.29W, which is considered acceptable compared to its thermal rating that is 5W. In case that lower heat generation on the shunt resistor is required, the ohmic value of the shunt resistor should be reduced.

The synchronization of the current and voltage measurements is critical to attain high accuracy at the BT cell's impedance estimation, especially at the imaginary part of the impedance, which is mainly determined by the phase difference between the voltage and the current measurements. This is accomplished by independently programming the conversion process of the ADC and the sampling process of the microcontroller. Specifically, the conversion process of the voltage and current measurements are simultaneously triggered via a common digital signal, and the measurements are provided to the microcontroller through a daisy chain configuration with sampling rate 200 Ksps (5 μs). Therefore, the microcontroller receives the synchronized measurements by the ADCs.

The frequency of the PWM signal provided by the microcontroller is 100kHz and the cut-off frequency of the RC low-pass filter is adjusted to 7.96 kHz (the R and C components are 200Ω and 0.1μF, respectively). Therefore, the lowpass filter can act as a digital to analog converter for providing a smooth signal to the Op-amp, while at the same time, the cut-off frequency is sufficiently larger than the excitation frequency. Furthermore, the Op-amps that are used both in the drive and the measurement units have a bandwidth at the range of MHz, which is much faster than the maximum frequency of the excitation signals.

The accuracy of the proposed EIS technique has been experimentally validated by comparing the estimated impedance of the tested BT cells with a commercial laboratory instrument (Metrohm Autolab ECI10M with a 10A booster and a 4-wire measurement setup). As explained in Section IV, the proposed algorithm is logarithmically performed with 9 impedance measurements per decade for a frequency range from 2kHz to 20mHz, that results to 46 measurement points, per each impedance estimation procedure. In order to have a common comparison basis, the same measurement setup is used for the laboratory instrument and also, the same BT cells at the same operating conditions (voltage, temperature, and current) are used.

In Fig. 9, the BT cell's impedance estimation obtained by the proposed EIS system is compared with the impedance estimation obtained by the laboratory instrument, which can be considered as the reference estimation. Three cases are examined for the same BT cell, for various SoC and temperature conditions. Specifically, Fig. 9(a) illustrates the impedance estimation for 50% SoC and 25°C operating temperature, Fig.

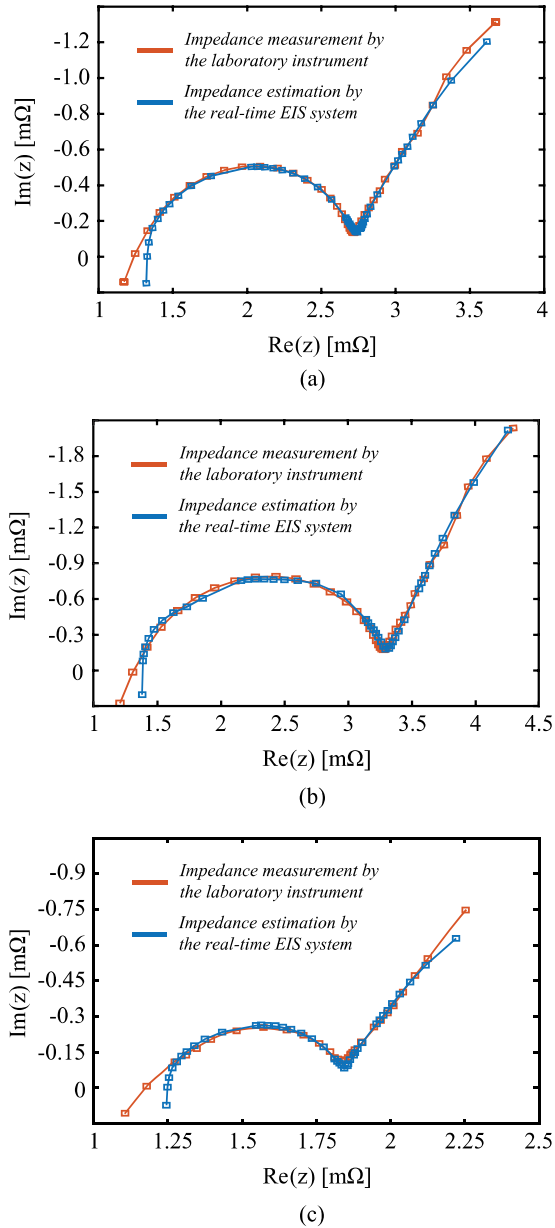


Fig. 9. Comparison of the proposed prototype with a commercial laboratory instrument: (a) 50% SoC and 25°C operating temperature, (b) 10% SoC and 25°C operating temperature, and (c) 50% SoC and 35°C operating temperature.

9(b) for 10% SoC and 25°C operating temperature and Fig. 9(c) for 50% SoC and 35°C operating temperature.

The measurements with the proposed EIS system and the laboratory instrument for each of the above three sets have been done within some minutes and with at least three days between each set of measurements. Thus, common comparison basis with respect to relaxation time is ensured, i.e. conduction of the experiments for the same operating conditions at almost the same time period and enough relaxation interval between the three sets of measurements [55], [56].

As can be seen in the inverted Nyquist plots of Fig. 9, the impedance estimated by the proposed EIS system is in good agreement with the reference measurements for all the examined cases and only some small discrepancies occur at the very high and very low frequencies. The small discrepancies that

occur at the very high frequencies are owed to the fact that the number of the sampling points per signal period is reduced, as the frequency of the excitation current is increased. Also, since these discrepancies occur at the frequency range 2kHz-800Hz that corresponds to a small operating time interval of 0.011s, they could not be attributed to the BT cell polarization or any change in the operating characteristics. Thus, if higher accuracy is required, the sampling frequency should be increased. Note that, in the experimental system, the sampling ratio at the higher frequency of 2kHz is 20 measurement points per signal period, since the running frequency of the EIS procedure is 40kHz, and the number of the sampling points increases as the examined frequency reduces. Thus, the cell's impedance estimation accuracy is improved at the lower frequencies. However, small discrepancies are observed at the very low frequencies, which are significantly smaller than that at the high frequencies. These discrepancies can be attributed to the different impact that may have the changes in the BT cell operating parameters, which are observed during the relatively large duration of the low frequency measurements, on the EIS estimation of the laboratory instrument methodology against the proposed technique.

The impedance measurement accuracy is also quantified by analyzing the RMS error for the real and imaginary parts. The RMS error for the real part is given by

$$\epsilon_{Re} = \sqrt{\frac{1}{N} \sum_{j=1}^N [\text{Re}_1(f_j) - \text{Re}_2(f_j)]^2} \quad (9)$$

where the subscript 1 indicates the data obtained by the proposed EIS system, the subscript 2 indicates the data obtained by the laboratory reference instrument and f_j is the frequency at each measurement point j , for the $N=46$ points. Similarly, the RMS error in the imaginary part is given by

$$\epsilon_{Im} = \sqrt{\frac{1}{N} \sum_{j=1}^N [\text{Im}_1(f_j) - \text{Im}_2(f_j)]^2} \quad (10)$$

From (9) and (10), the RMS errors for the real and imaginary parts of the impedance estimation by the proposed EIS procedure with respect to the reference estimation from the laboratory instrument are 0.012mΩ and 0.017mΩ, respectively, which can be considered negligible compared to the actual impedance value.

It should be noted that the four-terminal Kelvin measurement technique is applied for the voltage measurements, in order to eliminate the influence of the contact resistance effect. Specifically, two separate wires are used for the voltage sensing that are directly connected to the BT cell terminals and thus, the comparison of the cell impedance estimation between the proposed EIS system and the laboratory instrument can be considered accurate [57]. However, in some BT system applications, the mounting of the cells may introduce contact resistance even in the case of four-terminal Kelvin measurements. In that cases, the contact resistance should be considered, and an identification technique should be used,

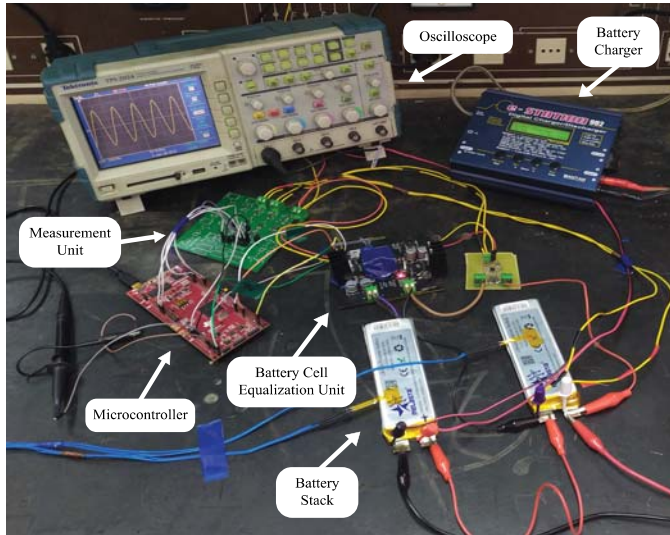


Fig. 10. Layout of the experimental system with the proposed combined EIS-BCE system.

such as that proposed in [58]

The effective cooperation of the proposed real-time EIS system with the BCE technique, has been experimentally validated by utilizing the prototype EIS system with two series connected BT cells. The layout of the experimental system is illustrated in Fig. 10. The two BT cells have different internal performance parameters, specifically, the Cell₁ is new, while the Cell₂ has been cycled many times and it is considered degraded. The above layout of two series connected BT cells is indicative and only for the purpose of the current experiments, since the proposed EIS-BCE technique can effectively estimate the BT impedance regardless of the number of series and parallel connected cells. The excitation current should be selected based on the typical rule of the AC perturbation of ~ 10 mV [56].

The proposed EIS technique is used both for the evaluation of the BT ageing, when the system is disconnected from the charger, and in cooperation with the cell equalization algorithm, during the charging procedure. Thus, it is examined the performance of the proposed EIS technique for both off-line and real-time operation during charging. Specifically, the BT ageing evaluation is performed when the BT system is disconnected and operates independently from the charging procedure. During the real-time operation, the algorithm of [52] is adopted for the balancing of the series-connected BT cells and the proposed EIS procedure is realized at specific time points, that are initiated by trigger signals provided by the BCE.

The performance of the combined EIS-BCE system for real-time operation is shown in Fig. 11. As can be seen, the EIS procedure is initiated when the BT system is in an idle mode with approximately 20% SoC and after 30 minutes of rest from the last discharge. It lasts 5.4min, for the whole frequency range of 2kHz-20mHz and it is realized by applying an AC current of amplitude 1A, which is considered a satisfactory trade-off between sufficient signal-to-noise ratio and minimal change in system linearity for the examined BT, based on the typical rule of the AC perturbation of ~ 10 mV [56]. Then, the system remains in an idle situation for an interval of approxi-

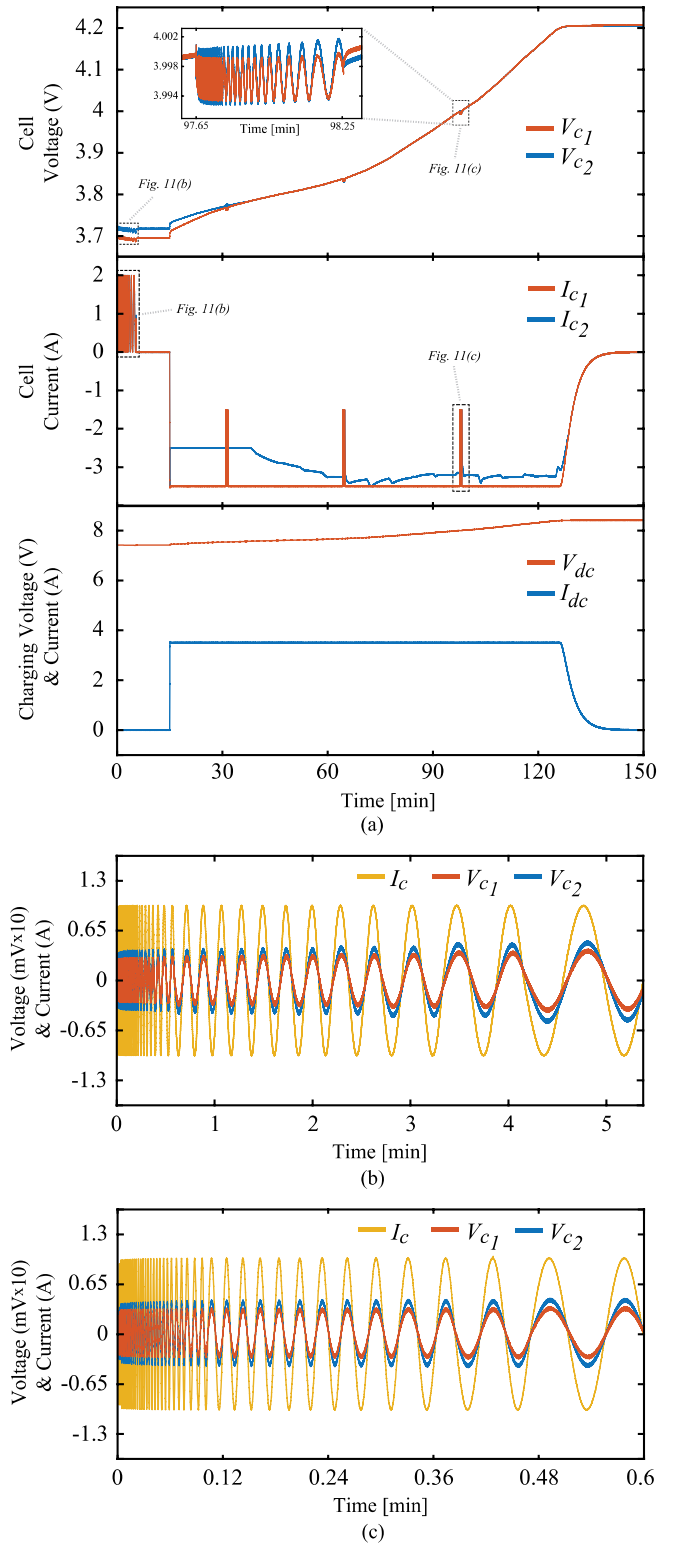


Fig. 11. Experimental results of the performance of the proposed combined EIS-BCE system for real-time operation: (a) the whole procedure (b) the first EIS procedure of duration 5.4min, and (c) the fourth EIS procedure of duration 0.6min.

mately 10 minutes. This time interval has been decided arbitrarily, just to separate the EIS for the BT ageing evaluation from the real-time EIS procedure during the BT charging. After the 10 minutes idle period, the charging procedure is started and the activation of the EIS is regulated by the BCE at specif-

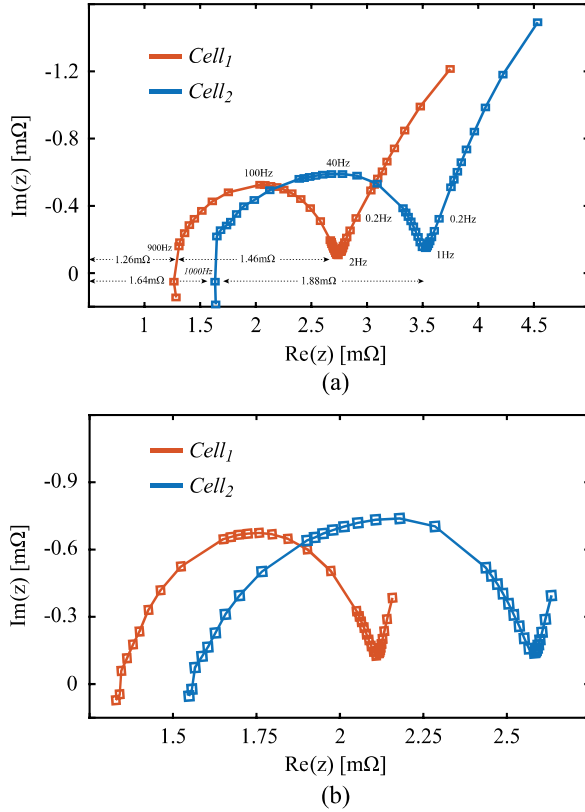


Fig. 12. Nyquist plots of the BT cells impedance obtained by: (a) the initial real-time EIS procedure of duration 5.4mins and (b) the 4th real-time EIS procedure of duration 0.6min.

ic time intervals. During the charging of the BT system, the duration of each EIS procedure has been reduced to 0.6min, which is much shorter than the EIS at the BT charging evaluation, since the frequency range has been decreased to 2kHz-0.2Hz. The confinement of the frequency range and consequently the shortening in the EIS duration is allowed, because during the real time operation, the information for the zero-crossing and the charge transfer resistances is enough for the proper BT cell balancing. Thus, the low frequency diffusion region can be omitted to significantly reduce the EIS implementation time. Note that, the required energy is 0.037 Wh for the 0.6min procedure and 0.333 Wh for the 5.4min procedure, which correspond to the 0.13% and 1.2% of the nominal BT capacity, respectively. In case that the proposed EIS technique operates during the charging mode, the above driving energy is provided by the BT charger. The EIS technique can also operate when the BT is in discharging mode; however, since in this case the driving energy is provided by the BT, it should be evaluated if and how often the EIS procedure should be conducted.

The current and the voltage of the BT cells during the EIS, for the initial EIS procedure of duration 5.4min and the fourth EIS procedure of duration 0.6min, are shown in Figs. 11(b) and (c), respectively. The BT cells impedance estimations of the above real-time EIS procedures are illustrated, in Nyquist plots, in Figs. 12(a) and (b), respectively. As can be observed, the EIS satisfactorily cooperates with the BCE (Fig. 11) and it can

effectively give the impedance estimations (Fig. 12). Note also that, the EIS can effectively estimate that the BT $Cell_2$ is significantly degraded, since both the high and the mid-frequency impedances are greater than the respective impedances of the new BT $Cell_1$. Furthermore, the local maximum point occurs at significantly decreased frequency (at 100Hz for the new $Cell_1$ compared to 40Hz for the aged $Cell_2$). This means that, apart from the impedance increase, the time constant of the cell has increased and thus, it is confirmed the degradation of the $Cell_2$.

Since the proposed EIS technique is a real-time procedure, the accuracy of the impedance estimation is not affected by the polarization effect that it is observed when the BT is rest for a short period. However, the impacts of the polarization and any other electrochemical effects such as the temperature and the SoC variations, that may occur during the use of the BT, affect the BT internal characteristics and thus, they are reflected on the cell's impedance. Therefore, the real-time BT impedance estimation through the proposed EIS method considers the aforementioned effects and thus, the current BT operating condition can be effectively evaluated.

It should be noted that, although the BCE method of [52] has been adopted in this paper, the proposed real-time EIS system can be utilized by any other BCE technique, such as the [59], where an hierarchical SoC balancing controller is used along with a multi-input single-output power converter for each series BT module and back-to-back MOSFETs for each parallel BT of the module. In the case of [59], the multi-input single-output power converter can be replaced by the proposed on-board EIS system and along with the back-to-back MOSFETs can be used for the impedance measurement of each BT cell in the series-parallel configuration of the system.

VII. CONCLUSIONS

In this paper, a real-time EIS technique combined with a BCE system has been proposed that can accurately estimate the BT cell impedance. The proper excitation current for the performance of the EIS technique is provided by a MOSFET that is in parallel connection with each BT cell and acts as a controllable current source, for both cell impedance estimation and cell equalization. Therefore, a smooth current profile is provided that ensures accurate and effective EIS procedure. The circuit topology of the EIS is implemented without requiring expensive electronic equipment, and therefore it is affordable to be applied in the BT system of any application. Additionally, due to the effective harmonic analysis that the smooth cell excitation current can provide, the proposed EIS technique can accurately estimate the BT cell impedance even at the range of $m\Omega$ and thus, it can be used in high demanding applications. The accuracy of the proposed EIS technique has been validated by comparing it with a commercial laboratory instrument. Also, the effectiveness and the practicality in the implementation of the proposed combined EIS-BCE system have been experimentally validated with two series connected BT cells, for demonstrating the use of the system in a real-time application.

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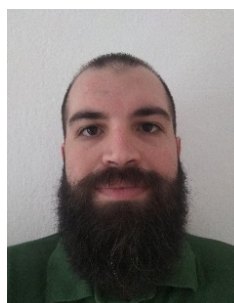
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