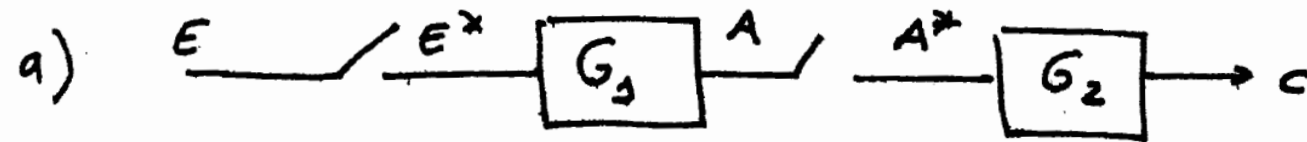


• Other configurations:



$$C(s) = G_2(s) A^*(s)$$

$$A(s) = G_1(s) E^*(s) \Rightarrow A^* = (G_1 E^*)^* = G_1^* E^*$$

$$C^*(s) = G_2^* A^* = G_2^*(s) G_1^*(s) E^*(s)$$

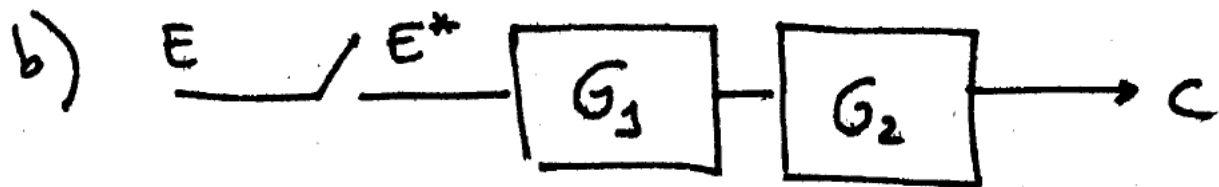


$$\boxed{C(z) = G_2(z) G_1(z) E(z)}$$

or

$$\boxed{G(z) = G_1(z) \cdot G_2(z)}$$

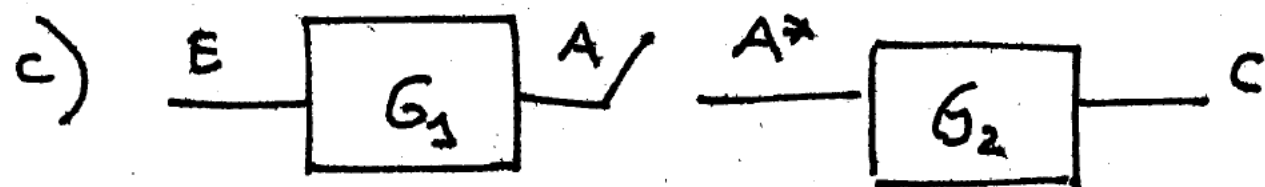
Key feature: we have an ideal sampler between  $G_1$  &  $G_2$

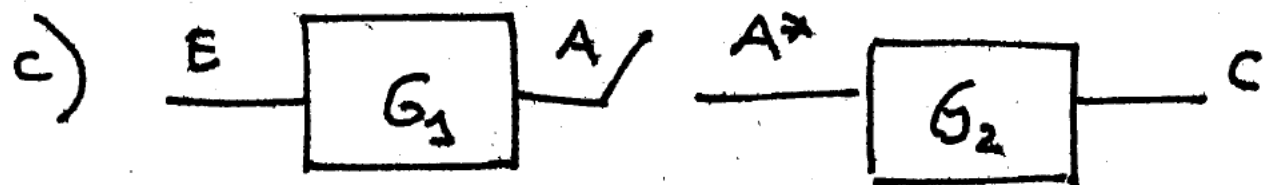


$$C(s) = G_2(s) G_1(s) E^*(s) \Rightarrow C^*(s) = [G_1 \cdot G_2]^* E^*(s) \quad \text{or}$$

$$C(z) = Z \{ G_1 \cdot G_2 \} \cdot E(z) \Rightarrow \boxed{G(z) = Z [G_1 \cdot G_2]}$$

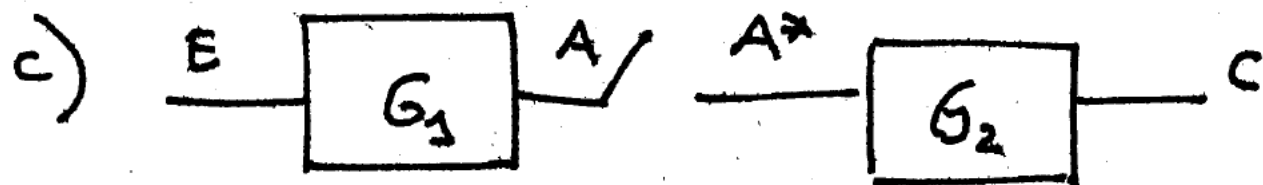
Note :  $Z [G_1 G_2] \neq G_1(z) G_2(z) !!$





$$C = G_2 A^* \Rightarrow C^* = G_2^* [G_1 E]^*$$

For this system a transfer function cannot be written!  
 The reason is that you can't factor  $E(z)$  out of  $[G_1 E](z)$



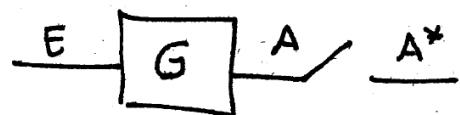
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Physical reason:

When you have  $E \xrightarrow{\text{sample}} E^* \xrightarrow{\text{block } G} C$ ,  $E^*$  contains information about  $E$  only at the sampling instants.  $\Rightarrow$  When you compute  $C^*$  you can factor  $E^*$  out.

On the other hand, if you have something like this:



$$A(s) = G(s) E(s)$$

$$a(t) = \int_0^t g(t-z) e(z) dz \Rightarrow$$

to compute  $A^*$  (and latter  $C^*$ ) you need information about  $e(t)$  at all times, not just the sampling instants.

# EECE 5610 Digital Control Systems

## *Lecture 10*

**Milad Siami**

Assistant Professor of ECE

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**Northeastern University**  
College of Engineering

Important consequence:

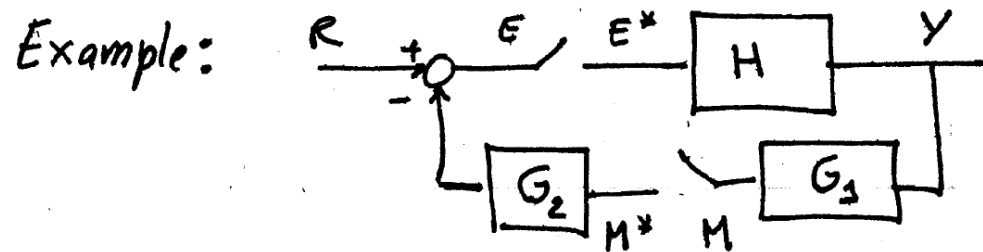
If you want to have a discrete T.F you have to select as your unknowns the inputs to the sampler

This variables will always "come free" after the equation sampling process and give a set of starred variables for which we can solve.

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If you want to have a discrete T.F you have to select as your unknowns the inputs to the sampler

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$$E(s) = R - G_2 M^*$$

$$E^* = R^* - [G_2 M]^* = R^* - G_2^* M^*$$

$$M = (G_1 H) E^* \Rightarrow M^* = (G_1 H)^* E^*$$

$$E^* = R^* - G_2^* [G_1 H]^* E^*$$

$$\Rightarrow \boxed{E^* = \frac{R^*}{1 + (G_1 H)^* G_2^*}}$$

or:

$$\boxed{\frac{E(z)}{R(z)} = \frac{1}{1 + [G_1 H](z) G_2(z)}}$$



Which one is correct?

**A**

$$\frac{Y(z)}{R(z)} = \frac{H(z)}{1 + (HG_1)(z) G_2(z)}$$

**B**

$$\frac{Y(z)}{R(z)} = \frac{G_1^* G_2^*}{1 + G_1^* G_2^* + (G_2 H)^*}$$

To obtain  $Y$  we can use the equation:  $Y(s) = H E^* \Rightarrow Y^* = H^* E^*$

$$\Rightarrow \frac{Y^*}{R^*} = \frac{H^*}{1 + (G_1 H)^* G_2^*} \quad \Longleftrightarrow$$

$$\boxed{\frac{Y(z)}{R(z)} = \frac{H(z)}{1 + (H G_1)(z) G_2(z)}}$$

Note that in this case we have a TF. This is because  $R$  goes right through a sampler before entering other blocks.

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- Open-loop Systems with Digital Filters

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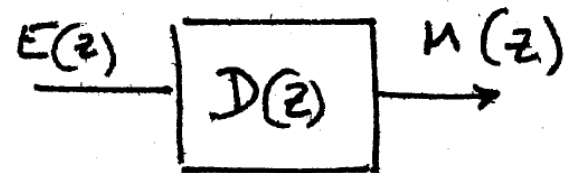
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## • Open-loop Systems with Digital Filters

We consider now the case where the sampled-data system contains a digital filter

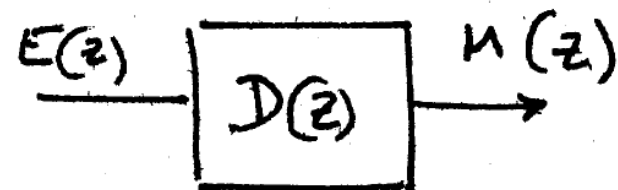


$$M(z) = D(z) E(z)$$

$$M^*(s) = D^*(s) E^*(s)$$

- Open-loop Systems with Digital Filters

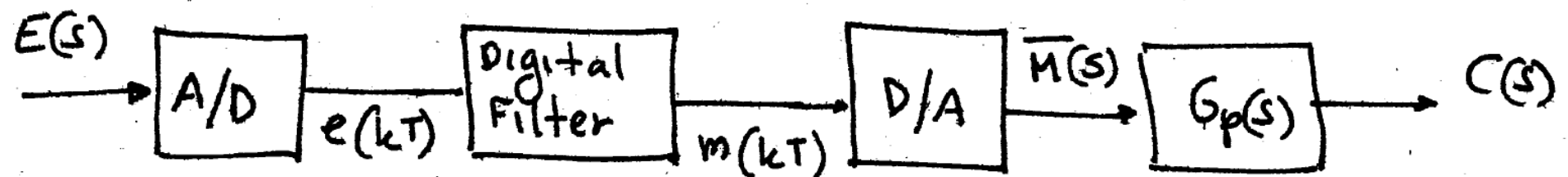
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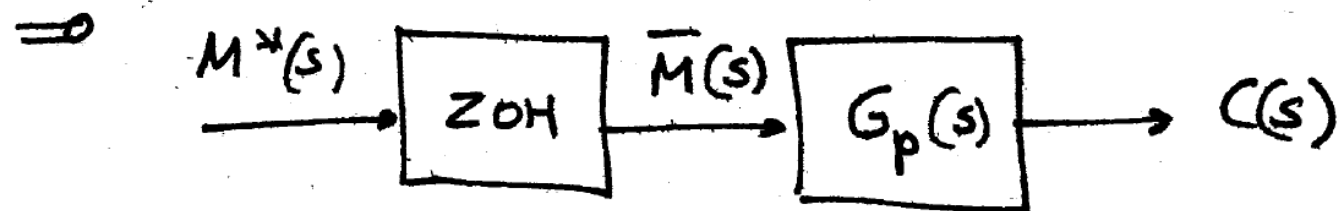
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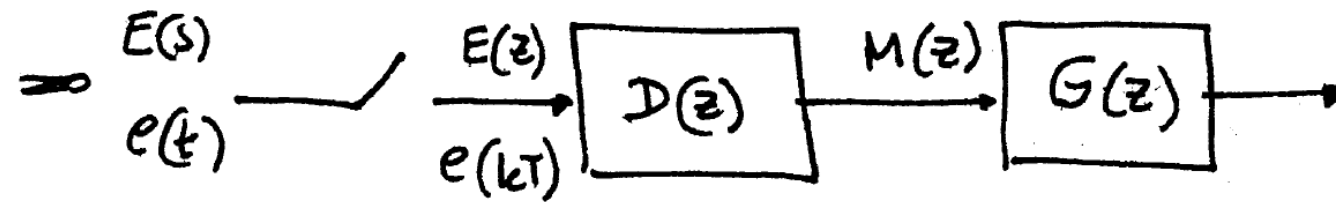
Physically:



We will assume that the D/A can be represented as a zero order hold

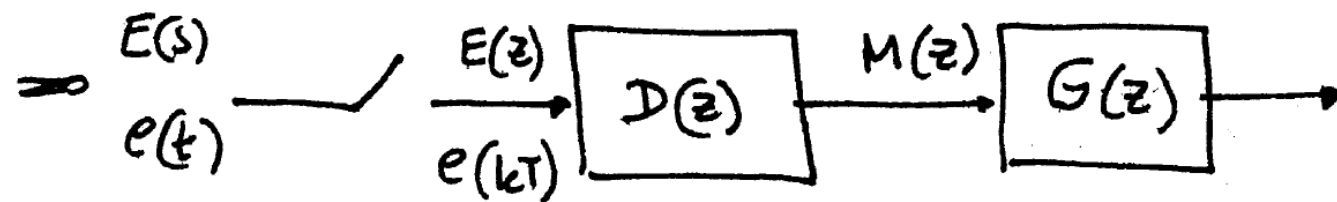


(Recall that  $G_{ho} = \frac{1 - e^{-sT}}{s}$ )



$$C(s) = \underbrace{G_{ho}(s) \cdot G_p(s)}_{G(s)} M^*(s) \quad \Rightarrow \quad C(z) = G(z) M(z) = G(z) D(z) \bar{E}(z)$$

(Recall that  $G_{ho} = \frac{1 - e^{-sT}}{s}$ )



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Example:

Suppose that the digital filter is given by the following diff. eq.

$$m(kT) = 2e(kT) - e[(k-1)T]$$

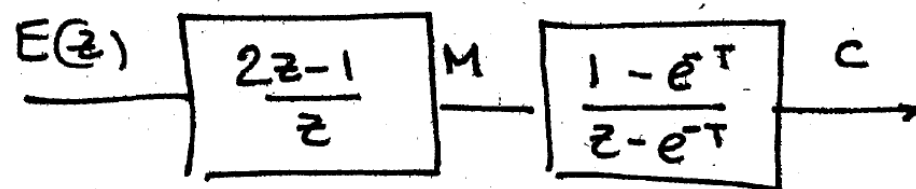
$$M(z) = 2E(z) - \frac{E(z)}{z} = \frac{2z-1}{z} E(z)$$

$$\Rightarrow D(z) = \frac{M}{E} = \boxed{\frac{2z-1}{z}}$$

$$G_p(s) = \frac{1}{(s+1)} \Rightarrow G(s) = G_{ho} G_p = \frac{1 - e^{-sT}}{s(s+1)}$$

$$G(z) = \left(1 - \frac{1}{z}\right) Z \left[ \frac{1}{s(s+1)} \right] = \left(1 - \frac{1}{z}\right) \left[ \frac{1}{s - 1/z} - \frac{1}{s - e^{-T}/z} \right]$$

$$= \frac{1 - e^{-T}}{z - e^{-T}}$$

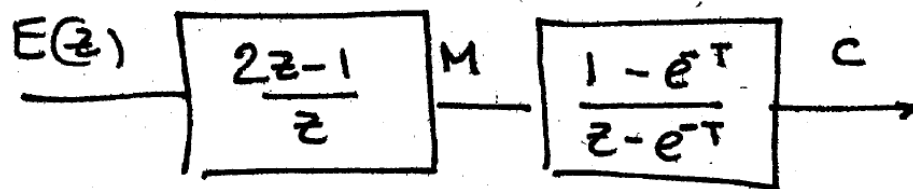




$$G_p(s) = \frac{1}{(s+1)} \Rightarrow G(s) = G_h G_p = \frac{1 - e^{-sT}}{s(s+1)}$$

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$$= \frac{1 - e^{-T}}{z - e^{-T}}$$



Assume that  $E(z)$  is a step:  $E(z) = \frac{z}{z-1} \Rightarrow$

$$C(z) = \left( \frac{1 - e^{-T}}{z - e^{-T}} \right) \left( \frac{2z-1}{z} \right) \left( \frac{z}{z-1} \right)$$

From here we can get  $c(kT)$  either by doing partial fraction expansion or using the residues formula.

## Effect of $T_s$

Recall that  $C^*(s)$  or  $C(z)$  gives you information only on what happens at the sampling instants, but not in-between.

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Q: Is this a problem?

A: Depends on how fast the dynamics of your plant are, compared to the sampling rate

Example :

$$G_p(s) = \frac{25}{s^2 + 2s + 25}$$

$$\Rightarrow \omega_n^2 = 25 \quad (\omega_n = 5)$$

$$\zeta = 0.2 \quad (\text{under damped})$$

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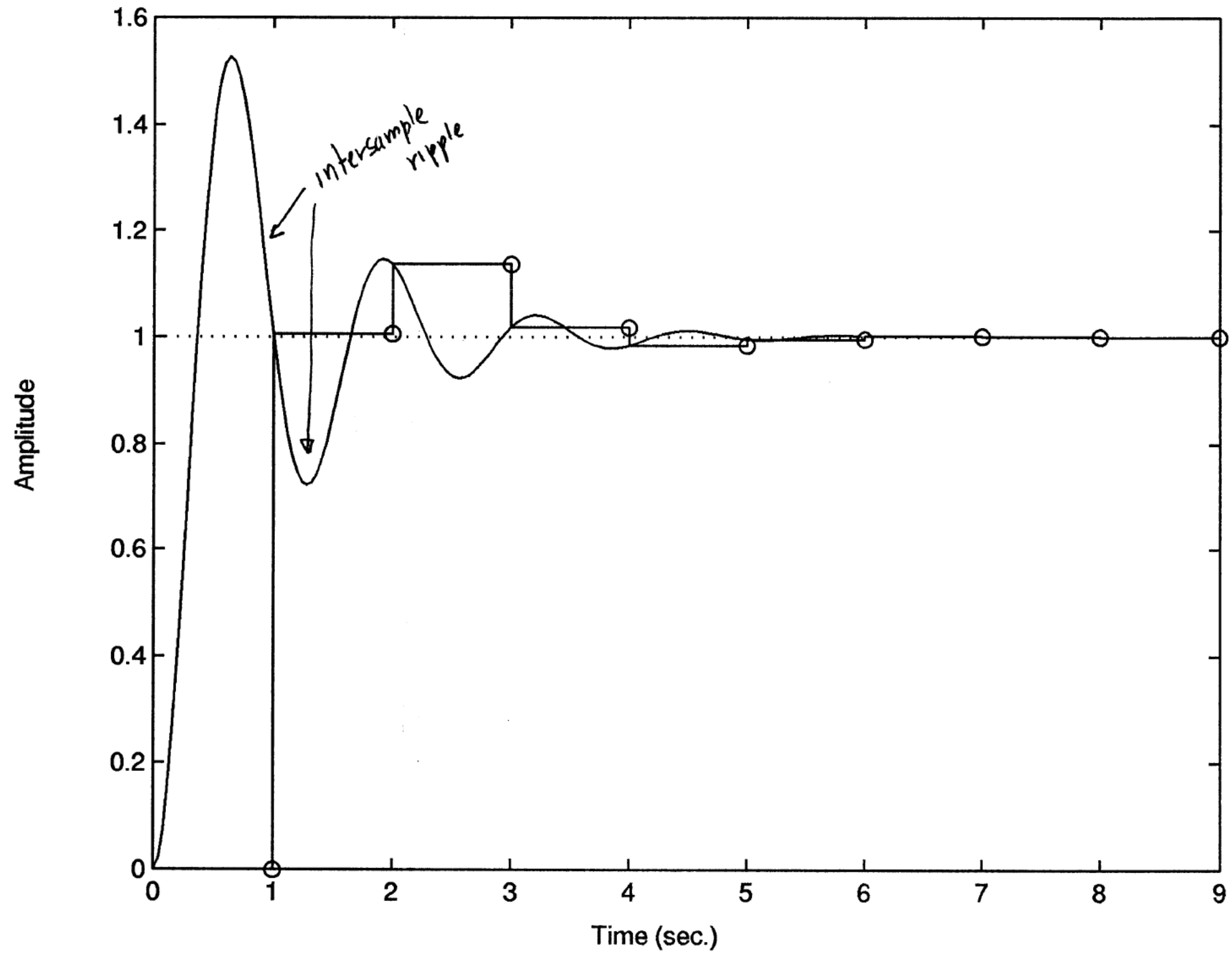
It can be shown that if we sample at  $T=0.1$  and  $T=1$  we get the following discrete time equivalents:

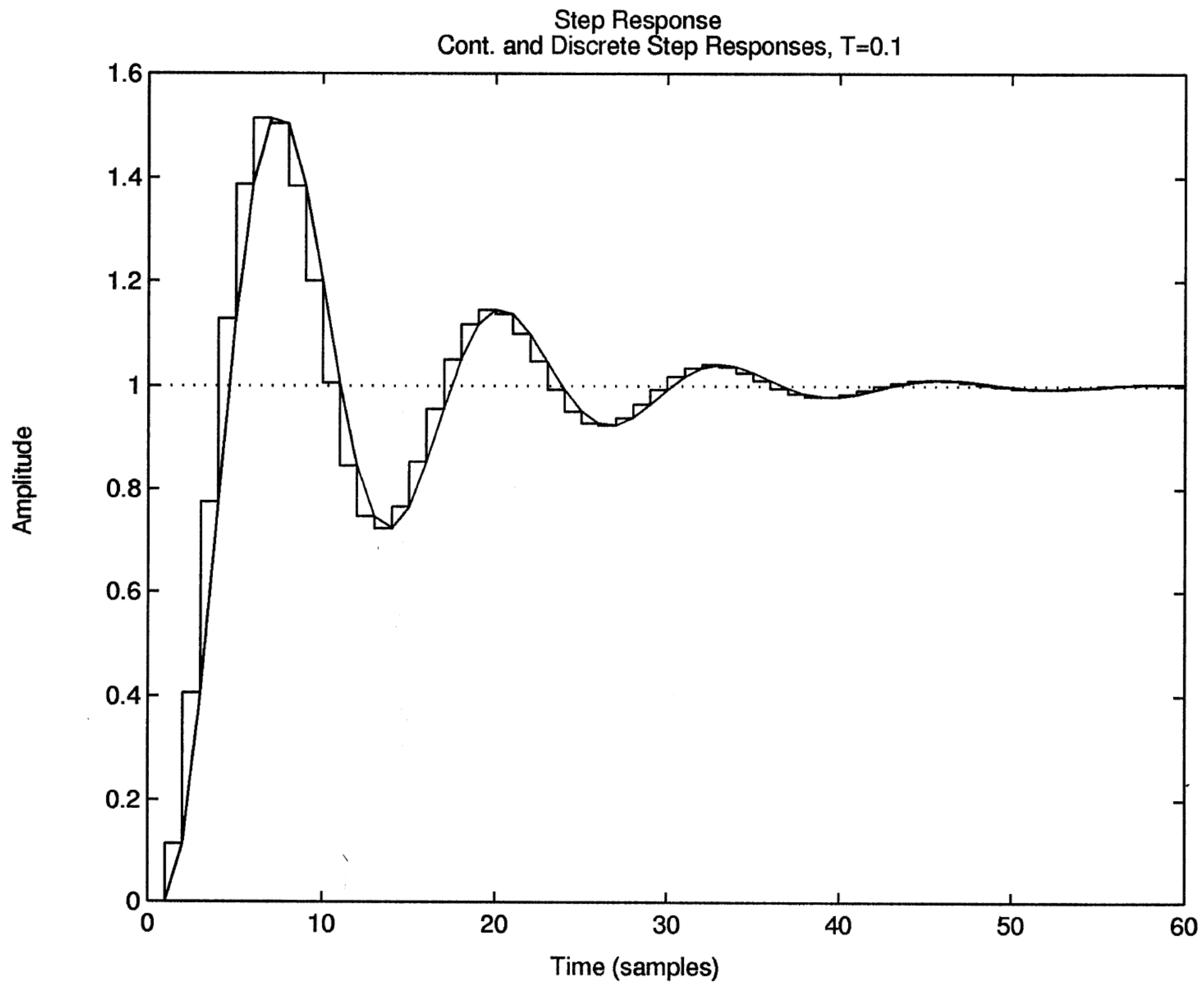
$$G(z) = \mathcal{Z} \left\{ \left( \frac{1 - e^{-sT}}{s} \right) \cdot G_p(s) \right\} = \left( 1 - \frac{1}{z} \right) \mathcal{Z} \left[ \frac{25}{s(s^2 + 2s + 25)} \right]$$

$$G_{T=1} = \frac{z - 0.007}{z^2 - 0.1365z + 0.1353}$$

$$G_{T=0.1} = \frac{0.115z - 0.107}{z^2 - 1.6z + 0.82}$$

Step Response ( $T=1$ )







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If we have more than one sampler then

- (a) They work at the same rate (single rate sampling)
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Q: How do we deal with these cases

A: We need a new tool: the "modified" z-transform.

- Modified z transform

So far we have been considering systems with integer number of sampling periods delays and synchronous sampling.

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Consider a function  $f(t)$  and delay it by an amount  $\Delta T$ ,  $0 < \Delta \leq 1$

$$f(t) \xrightarrow{\text{delay}} f(t - \Delta T) u(t - \Delta T) \xrightarrow{\mathcal{L}} F(s) e^{-s\Delta T}$$

$$f(kT) \longrightarrow f(kT - \Delta T)$$

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$$F(z, \Delta) \triangleq \mathcal{Z} [ f(t - \Delta T) u(t - \Delta T) ] = \mathcal{Z} [ F(s) e^{-s\Delta T} ]$$

Definition : Modified z-transform :

$$F(z, m) = F(z, \Delta) \Big|_{\Delta = \Delta - m}$$

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$$\Rightarrow F(z, m) = \mathcal{Z} \left[ F(s) e^{-s\Delta T} \Big|_{\Delta = \Delta - m} \right] = f(mT) \cdot \frac{1}{z} + f[(1+m)T] \frac{1}{z^2} + \dots +$$
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$$\Rightarrow F(z, m) = \mathcal{Z} \left[ F(s) e^{-s\Delta\tau} \Big|_{\Delta = \Delta - m} \right] = f(mT) \cdot \frac{1}{z} + f[(1+m)T] \frac{1}{z^2} + \dots +$$

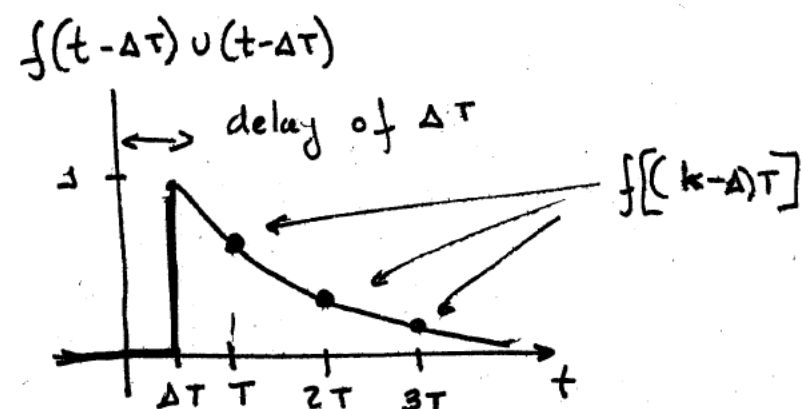
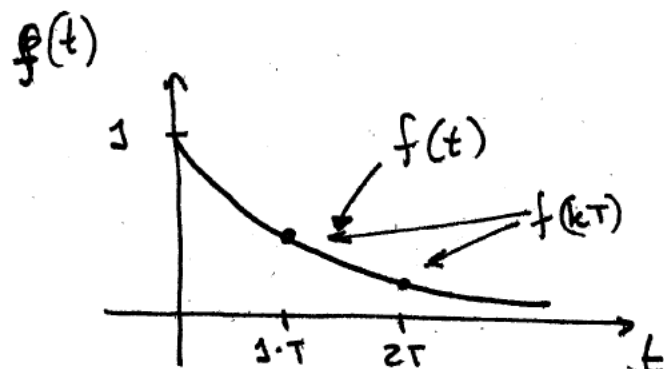
$$= \sum_{i=0}^{\infty} f[(m+i)T] z^{-(i+1)}$$

Example 1: Suppose that  $f(t) = e^{-t}$   $\Rightarrow f(kT) = e^{-kT}$   
and that we want to find out the z transform of the signal delayed by  $\Delta T$

$$F(z, m) = \sum_{i=0}^{\infty} f[(m+i)T] z^{-(i+1)} = \sum_{i=0}^{\infty} e^{-(m+i)T} z^{-(i+1)} = \frac{e^{-mT}}{z} \cdot \frac{1}{1 - \frac{1}{z \cdot e^T}}$$

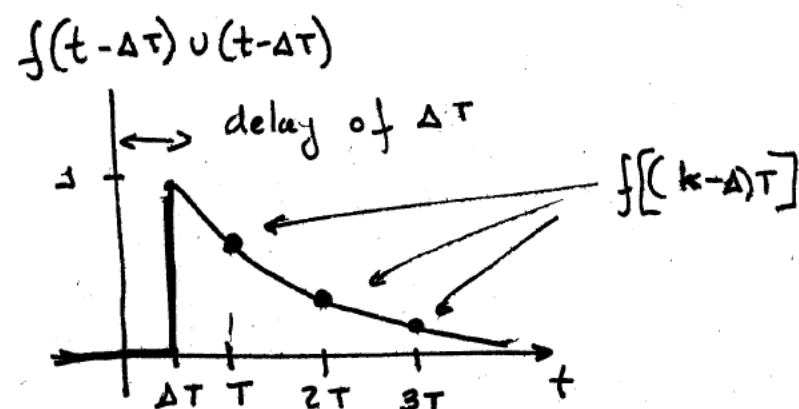
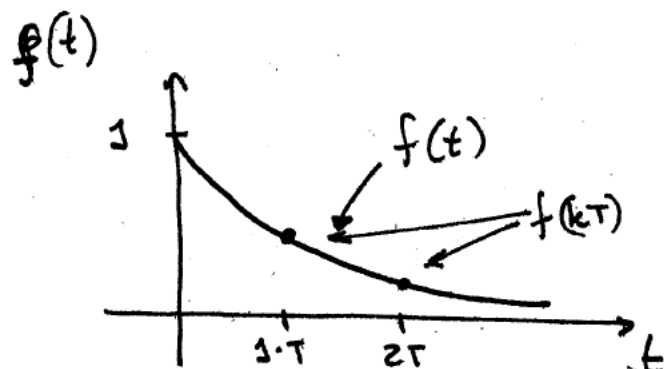
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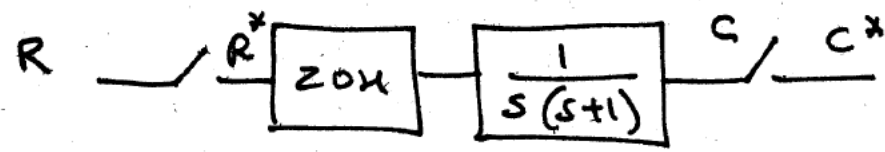
$$F(z, m) = \frac{e^{-mT}}{z - e^{-T}}$$



So we can use this technique to "peek" at the signal in between sampling instants (provided that we can handle that extra  $\Delta \cdot T$  delay at the beginning)

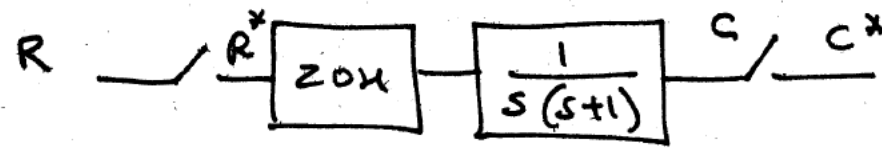


Example 2:

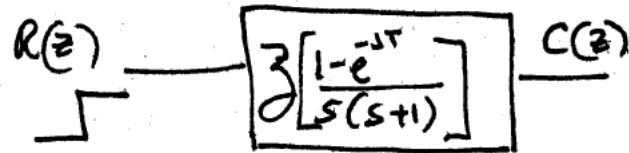




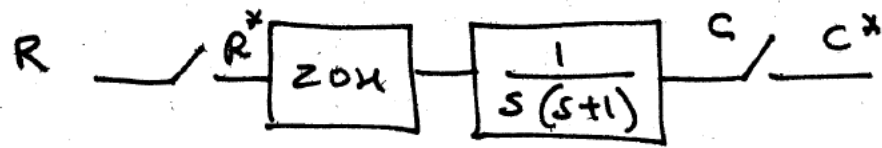
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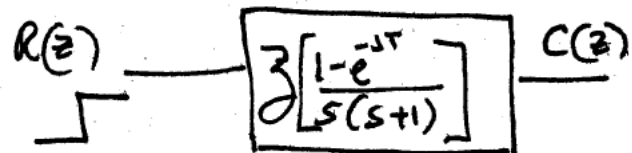
We may want to look at  $C(kT - \Delta T)$  to make sure that there is no intersample ripple. In this case we have



Example 2:



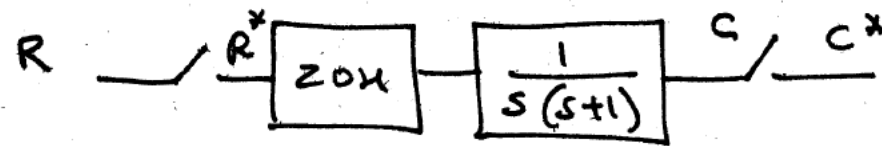
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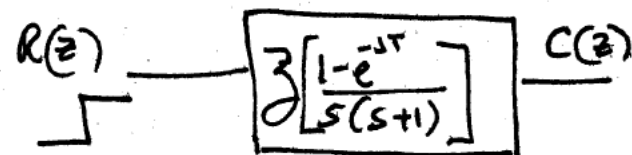
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and that  $C(z) = \left( \frac{1 - e^{-T}}{z - e^{-T}} \right) R(z) = \left( \frac{1 - e^{-T}}{z - e^{-T}} \right) \frac{z}{z - 1} = \frac{z}{z - 1} - \frac{z}{z - e^{-T}}$

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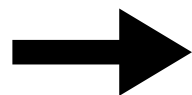
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Which one is correct?



$$C(kT) = 1 - e^{-kT}$$

**A**

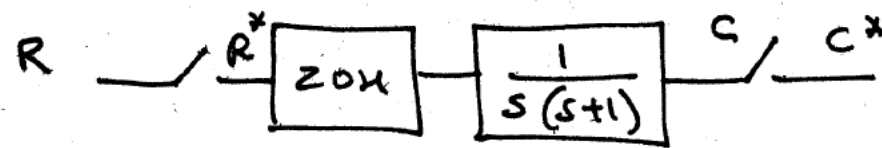
Or

$$C(kT) = 1$$

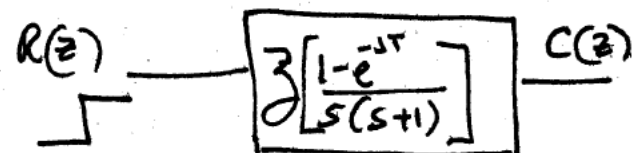
**B**

?

Example 2:



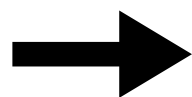
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Which one is correct?



$$C(kT) = 1 - e^{-kT}$$

**A**

Or

$$C(kT) = 1$$

?

**B**

What about the modified z transform?

$$G(s) = \frac{1 - e^{-sT}}{s(s+1)} = \underbrace{\frac{1}{s(s+1)}}_{C_1(s)} - \underbrace{\frac{e^{-sT}}{s(s+1)}}_{C_2(s)} =$$

$\Rightarrow$  We can find out  $C_1(z, m)$  proceeding as before.

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(2) However some of the properties are still valid. In particular, the time-shift theorem still valid, i.e.

$$\mathcal{Z}_m [e^{-kTs} E(s)] = z^{-k} \mathcal{Z}_m [E(s)]$$

Proof:

$$\mathcal{Z}_m [e^{-kTs} E(s)] = \mathcal{Z} [e^{-kTs} \cdot e^{-\Delta Ts} E(s)] = z^{-k} \mathcal{Z} [e^{-\Delta Ts} E(s)] = z^{-k} \mathcal{Z}_m [E(s)]$$



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(3) Additional properties:

$$\begin{aligned} E(z, 1) &= E(z, m) \big|_{m=1} = e(1)z^{-1} + \dots &= E(z) - e(0) \\ E(z, 0) &= E(z, m) \big|_{m=0} = e(0)z^{-1} + \dots &= \frac{1}{z} E(z) \end{aligned}$$

- How to compute the modified  $z$  transform

(Recall that usual tables do not apply)

$$E(z, m) = \mathcal{Z} [E(s) e^{-(1-m)Ts}] = \mathcal{Z} [E(s) e^{mTs} \cdot e^{-Ts}]$$

$$\text{Let } E_1(s) = E(s) e^{mTs} \Rightarrow E(z, m) = \mathcal{Z} [e^{-Ts} E_1(s)] = z^{-1} \mathcal{Z} [E_1(s)]$$

Now we can use the residue's formula for  $\mathcal{Z}[E_1(s)] \Rightarrow$

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$$E(z, m) = z^{-1} \left[ \sum_{\substack{\text{poles} \\ E_1(\lambda)}} \text{residues } E_1(\lambda) \frac{1}{1 - \frac{e^{\lambda T}}{z}} \right] = z^{-1} \left[ \sum_{\substack{\text{poles} \\ E(\lambda)}} \text{residues } E(\lambda) e^{mT\lambda} \frac{1}{1 - \frac{e^{\lambda T}}{z}} \right]$$

$$(\text{similarly: } E^*(s, m) = \frac{1}{T} \sum_{n=-\infty}^{n=+\infty} E(s + jn\omega_s) e^{-(1-m)(s + jn\omega_s)T})$$

Example 2: modified z transform of  $e(t) = e^{-t} \Leftrightarrow E(s) = \frac{1}{s+1}$

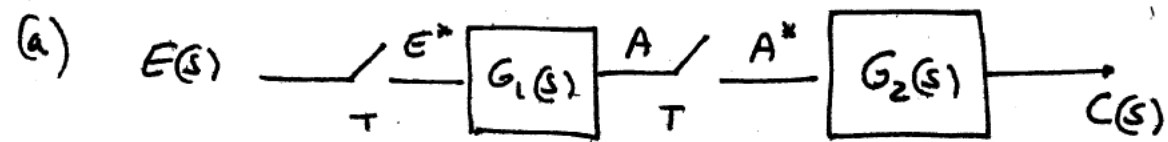
$$\begin{aligned} E(z, m) &= \frac{1}{z} \sum_{\text{poles } E(\lambda)} \left\{ \text{res } E(\lambda) e^{mT\lambda} \frac{1}{1 - e^{\lambda T} \frac{1}{z}} \right\} = \frac{1}{z} \frac{(1+\lambda)}{(1+\lambda)} e^{mT\lambda} \frac{1}{(1 - e^{\lambda T} \frac{1}{z})} \Big|_{\lambda=-1} \\ &= \frac{1}{z} e^{-mT} \frac{1}{1 - e^{-T} \frac{1}{z}} = \boxed{\frac{e^{-mT}}{z - e^{-T}}} \quad \# \quad (\text{same as before}) \end{aligned}$$

Now we will see how to use the modified z transform to deal with

- (a) systems with time delays
- (b) non-synchronous sampling
- (c) multirate sampling

## Summary of Chapter 4 :

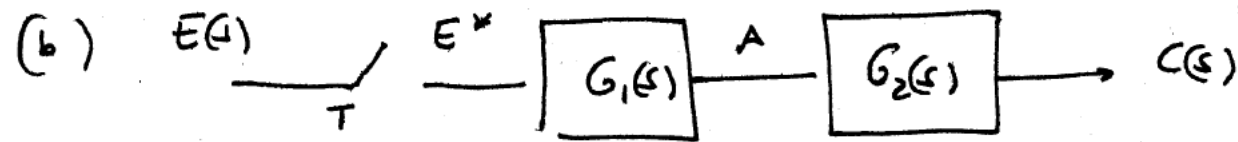
## Summary of Chapter 4 :



$$C(s) = G_2(s) A^* = G_2(s) G_1(s) E^*$$

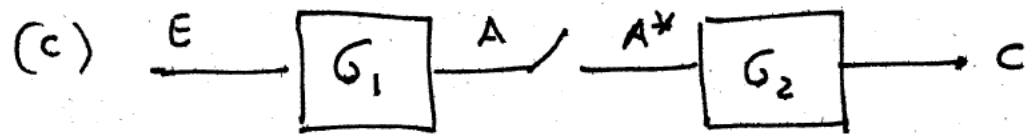
$$C^*(s) = G_2^* G_1^* E^*$$

$$C(z) = G_2(z) G_1(z) E(z)$$



$$C^*(s) = [G_2(s) G_1(s)]^* E^*(s)$$

$$C(z) = \mathcal{Z}[G_1 G_2] E(z)$$

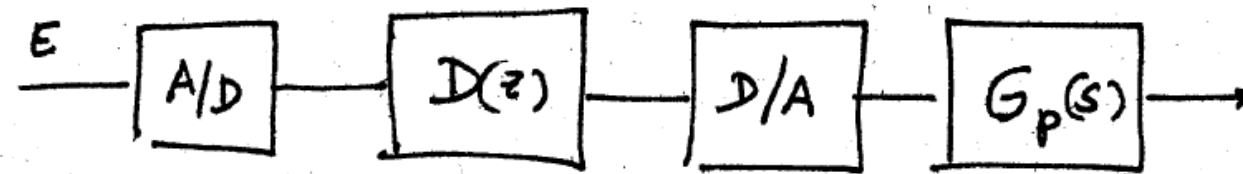


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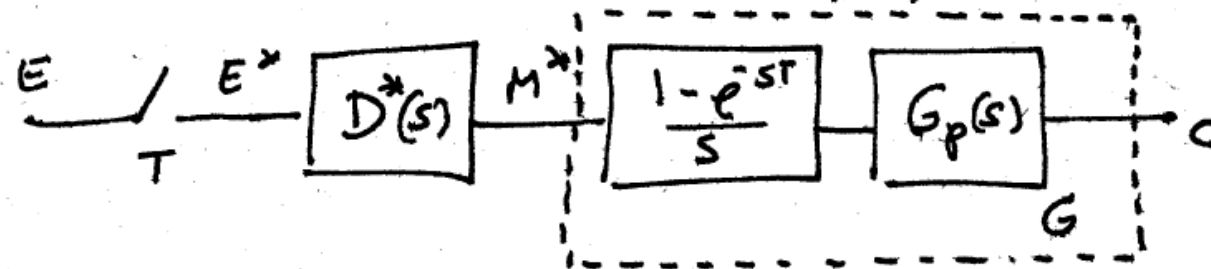
$$C^*(s) = G_2^* [G_1 E]^* \Rightarrow C(z) = G_2(z) \mathcal{Z}[G_1 \cdot E]$$

In this case a transfer function does not exist:  $E(z)$  can't be factored out

(a) Systems with digital filters:



model the A/D as an ideal sampler, D/A as a data hold:



$$G(z) = \mathcal{Z} \left[ \frac{1 - e^{-sT}}{s} \cdot G_p(s) \right] = \frac{z - 1}{z} \mathcal{Z} \left[ \frac{G_p(s)}{s} \right]$$

$$C(z) = G(z) \cdot D(z) \cdot E(z)$$

# CLOSED LOOP SYSTEMS

(chapter 5)



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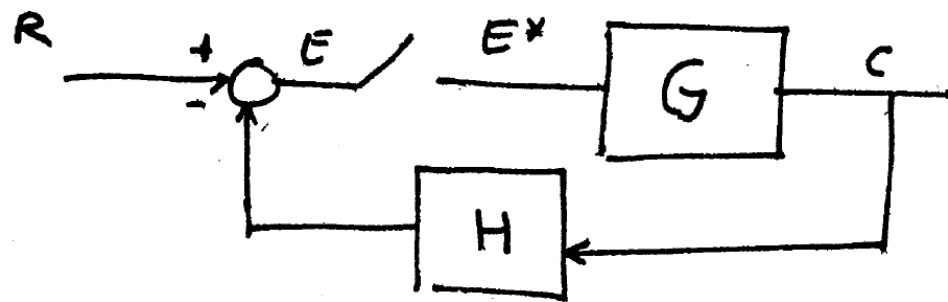
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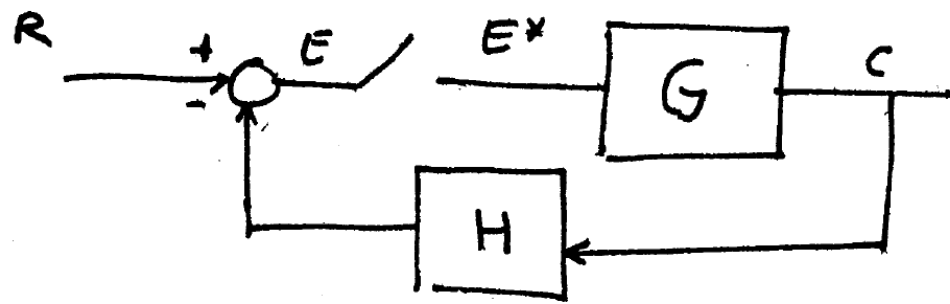


# CLOSED LOOP SYSTEMS

(chapter 5)

So far (chapter 4) we have considered only open-loop systems. The next step is to look into what happens when you close the loop.

Example:



Want to find closed loop transfer function:  $\Rightarrow$

$$E = R - HC = R - (HG)E^* \Rightarrow E^* = R^* - (HG)^*E^* \Rightarrow$$

$$E^* = \frac{R^*}{1 + [HG]^*} \quad \text{and} \quad C = \frac{GR^*}{1 + (HG)^*}$$



However, if we had selected  $C$  instead of  $E$  as variable we get

$$C = GE^*$$

$$E = R - HC \Rightarrow E^* = R^* - [HC]^* \Rightarrow C = GR^* - G[HC]^*$$

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Now we are stuck!! we can't proceed because we can't factor  $C^*$  out of  $[HC]^*$ .

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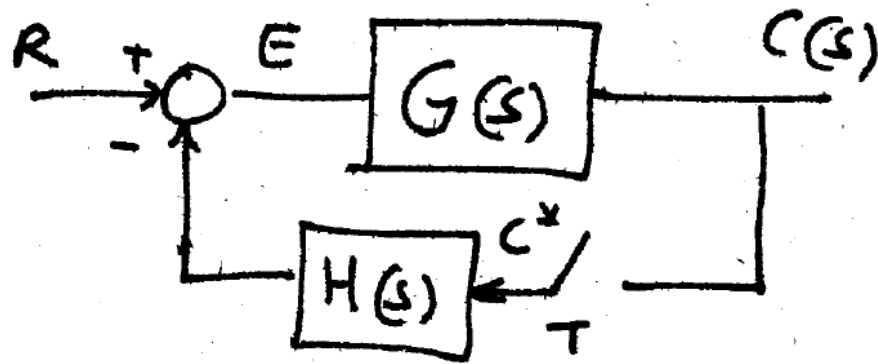
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Example 2 :



$$E = R - HC^* \\ C = GR - GH C^* \\ C^* = (GR)^* - (GH)^* C^*$$