

The CLAS12 RICH Detector

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Abstract

A Ring Imaging Cherenkov detector has been installed in the CLAS12 spectrometer at Jefferson Laboratory (JLab) to provide kaon identification in the momentum range between 3 and 8 GeV. The detector adopts a hybrid optics solution with aerogel radiator, light planar and spherical mirrors, and highly segmented photon detectors. We report here on the design, construction, and initial performance of the RICH during the commissioning of the detector and the first physics data taking period.

Keywords: Ring-imaging Cherenkov detectors, PID detectors, Single-photon detection



Figure 1: The first module of the CLAS12 RICH installed in sector 4 of the Hall B Forward Carriage.

1. Overview

Particle identification (PID) of hadrons in the original baseline design of the Forward Detector of CLAS12 is obtained by

combining the information from the High Threshold Cherenkov Counter (HTCC) [1], Low Threshold Cherenkov Counter (LTCC) [2], and Forward Time-of-Flight (FTOF) [3] systems. However, no sufficient separation of kaons from pions and protons can be achieved by using only these detectors in the momentum range relevant for the approved Semi-Inclusive Deep Inelastic Scattering (SIDIS) physics program, i.e. between 3 and 8 GeV. Therefore, improved particle identification in this momentum range is achieved by replacing two sectors of the existing LTCC with Ring Imaging Cherenkov (RICH) detectors. The first module of the RICH detector was completed before the start of the physics run, see Fig. 1, while the installation of the second module in the opposite sector is foreseen for the beginning of the CLAS12 operation with polarized targets. This article reports on the design, construction, and initial performance of the first RICH module. The second module will be identical to the first one.

The idea of a RICH detector is based on the fact that when a fast particle crosses a radiator with a velocity β larger than the velocity of the light in that medium, it emits Cherenkov photons. The light is emitted in a cone with opening angle θ_C given by $\cos(\theta_C) = [\beta n(\lambda)]^{-1}$, where $n(\lambda)$ is the refractive index of the radiator, which may depend on the wavelength λ . After a gap region where the cone opens up, the photons are detected and the ring can be reconstructed. A precision measurement of the Cherenkov angle provides the velocity of the particle and, together with information from the tracking system, it allows

its identification. Thus, the capability of identify particles with a known momentum and different velocity is governed by the Cherenkov angle resolution, and it can be effectively parameterized by the separation in units of resolution n_σ between the angle distributions for the various particles.

2. Detector Requirements

The CLAS12 spectrometer in Hall B [4] is designed to operate with highly polarized beams and nucleon targets at a luminosity of $10^{35} \text{ cm}^{-2} \text{s}^{-1}$. Under these conditions the production rate of protons, kaons, and pions studied using SIDIS Monte Carlo event-lists is such that, in most of the kinematic plane, the kaon rate is about one order of magnitude lower than the rate of pions and protons. Thus, successful kaon identification requires a rejection factor from pions around 1:500, i.e. a contamination in the kaon sample of a few percent. This corresponds to 4σ separation. In the momentum range between 3 and 8 GeV, neither gas nor liquid radiators provide sufficient angular separation to achieve the required pion rejection factor (see Fig. 2) and the only viable solution is silica aerogel, an amorphous solid network of SiO_2 nanocrystals with a very low macroscopic density and a refractive index in between gases and liquids. To detect the Cherenkov light emitted in the visible wavelength range, Hamamatsu Multi-Anode PhotoMultipliers Tubes (MaPMTs) were chosen for their high quantum efficiency in the visible and near ultraviolet (UV) regions, their fast response, and the required spatial resolution. Since the RICH detector must fit into the original CLAS12 Forward Carriage there were several constraints imposed upon its design. Each sector required a projective geometry, limited depth of 1.2 m, and $\sim 4.5 \text{ m}^2$ entrance windows. Simulation studies favored a hybrid imaging Cherenkov detector design incorporating aerogel radiators, visible light photon detectors, and a focusing mirror system. The focusing mirror system is used to reduce the detection area instrumented by photon detectors to $\sim 1 \text{ m}^2$ per sector, minimizing costs and influence on the Forward Time-of-Flight and electromagnetic calorimeter [5] systems. Depending upon the incident particle track angle, Cherenkov light is either imaged directly or after one or more reflections and passes through the aerogel. Figure 3 shows a schematic view of two examples of direct imaging and imaging after multiples reflections. Such peculiar hybrid-optics design is an innovative solution that has been successfully validated with a test-beam campaign [6].

3. Detector Design

The RICH detector replaces two sectors of the existing gas Low Threshold Cherenkov detector (LTCC), which is located at a 5 m distance from the interaction point. The first RICH module was designed while the CLAS12 spectrometer was already under construction and, as a consequence, it had to cover the same large area to match the trapezoidal shape of the LTCC sector. This resulted in several challenging requirements

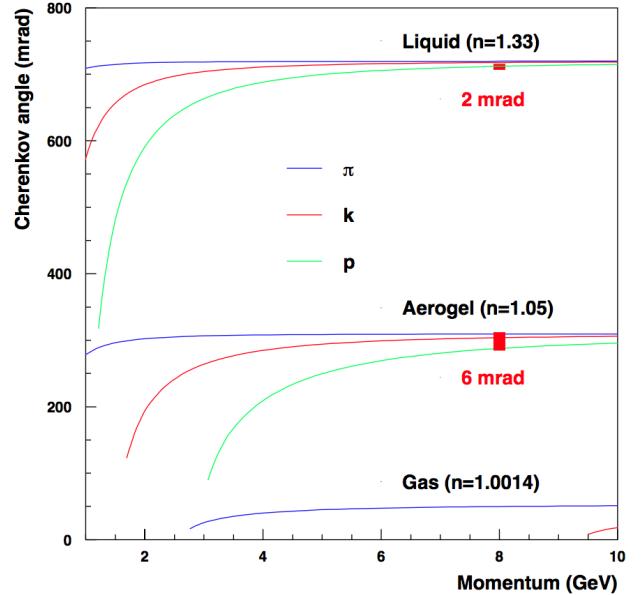


Figure 2: Cherenkov light opening angle as a function of the momentum for different particles using liquid, gas, or aerogel radiators. The angular separation between kaons and pions at the highest momenta is also indicated.

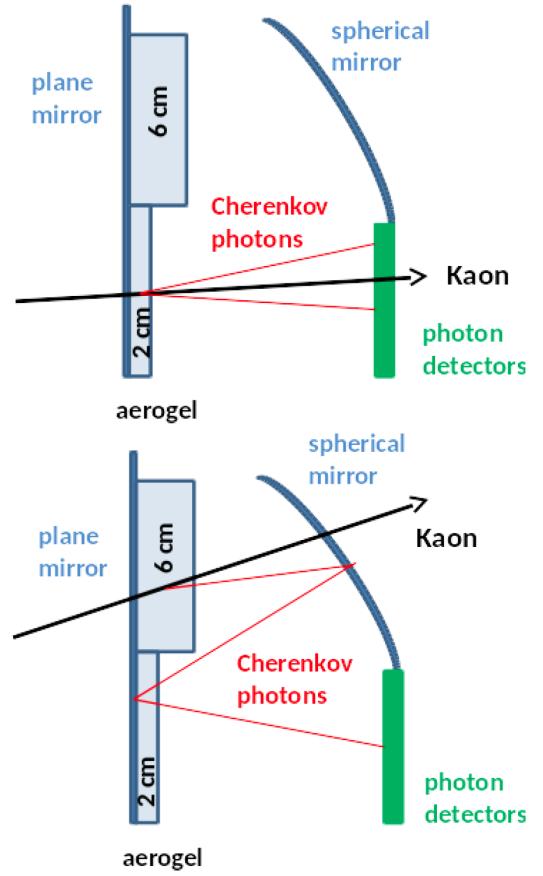


Figure 3: Examples of CLAS12 RICH imaging: direct detection of the Cherenkov cone produced in the thin aerogel layer (left plot); detection of the Cherenkov cone produced in the thick aerogel layer after multiple reflections and passes through the thin aerogel layer (right plot).

for the mechanical structure. The guiding principles were to minimize the material budget inside the acceptance and to limit the impact on the downstream detectors, ensuring at the same time the rigidity of the structure imposed by the optical requirements. Therefore, light materials, in particular carbon fiber, were largely utilized for all elements inside the CLAS12 acceptance. For all the parts with large dimensions, the sandwich technique, in which two thin solid skins are glued together on a thick honeycomb core, was also used. This technique indeed combines high stiffness with substantial weight reduction, resulting in a total weight of the detector of about 900 kg, ~30% lower than the LTCC.

A sketch of the detector is shown in Fig. 4. It is composed of a trapezoidal box (larger base of 4.2 m, smaller base of 0.3 m, height of 3.7 m, and depth of 1.2 m) in which all of the active elements are installed: the wall of aerogel tiles, the mirrors, the photomultiplier tubes, and the electronics. The main structural elements of the box are: the two lateral panels made of aluminum sandwich, the top panel made of carbon fiber sandwich, and the two upper angular elements and the bottom element made of aluminum. Each of the lateral panels supports two planar mirrors, while another planar mirror is installed on the bottom of the box. The box is closed on the front face (with respect to the beam direction) by two entrance panels made of a sandwich of two 1-mm-thick carbon fiber skins glued on a Nomex honeycomb core. Two planar mirrors with a wall of 2-cm-thick aerogel tiles are installed on the lower entrance panel, while a wall made of two layers of 3-cm-thick aerogel tiles is installed on the upper one. Therefore, the profile of the entrance panels was specifically designed not only to ensure the best light and gas tightness, but also to include stiffening ribs for the installation of the mirrors and the aerogel. The same sandwich structure was used for the electronics panel, located on the bottom part of the backward face of the box. It is composed of a main panel where all of the front-end electronics and the PMTs are installed, and a thin cover. The panel and the cover are screwed together on the mechanical structure, making a very rigid system. Finally, a very light exit panel made of a thin Tedlar sheet glued on an aluminum frame not supporting any active element, closes the back face of the trapezoidal box.

The total material budget of the detector is largely dominated by the electronics panel, which contributes to approximately 0.3 X_0 in the region from the beamline up to about 17°. A sizable contribution comes also from the aerogel (with a maximum contribution of 0.05 X_0 in the polar angles from 17° to 26°), while other active components like the spherical and planar mirrors contribute only to approximately 0.01 X_0 each. The total material budget of the passive elements is estimated to be, on average, below 0.05 X_0 .

The mechanical structures and all of the active elements (mirrors, aerogel, electronics, MaPMTs) define the RICH detector. The RICH is attached to the CLAS12 Forward Carriage by means of steel connections, attached to the angular and bottom elements. Detailed Finite Element Analysis (FEA) studies were performed in order to optimize the design of the detector with respect to the maximum deformation allowed by the required accuracy of the optical systems. These studies

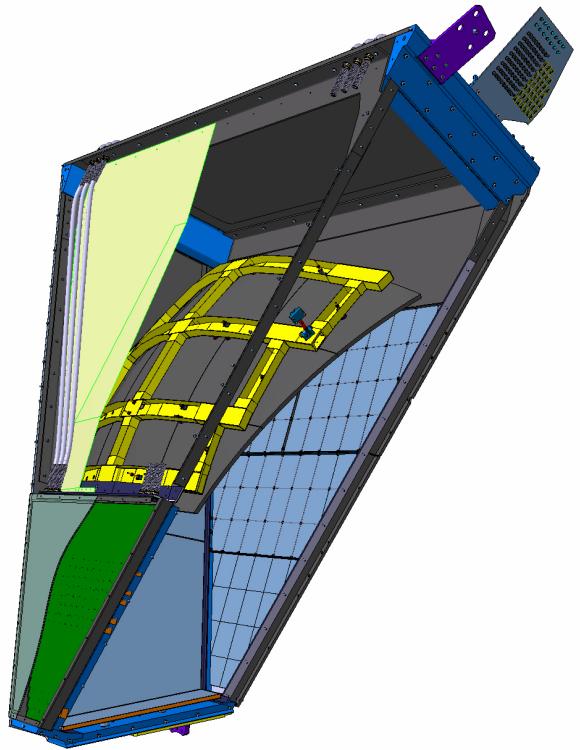


Figure 4: A schematic drawing of the CLAS12 RICH with the internal components highlighted. From left to right, the components of the upper half are exit panel, spherical mirror support and sub-mirrors, double 3-cm-thick aerogel layer, entrance panel. The components of the lower half are cover, electronics panel - mounting the front-end readout and the MaPMT sensors, 2-cm-thick aerogel layer, front planar mirrors, entrance panel.

included optimization of the ratio between skin and honeycomb thicknesses of the sandwich, and of the total thickness and profile of various stiffening and connection elements. Simulations of the load conditions during the assembly and installation of the detector and in the RICH final position in CLAS12 were also performed together with a seismic analysis¹. These simulations demonstrated that all stresses produced on the detector elements during the installation are well inside the elastic regime, and that the total deformations expected when the RICH is installed in CLAS12 never exceed a few mm.

4. The RICH Components

4.1. The Mirror System

The mirror system, composed of planar and spherical mirrors, was designed to minimize the photon loss and to direct as much of the Cherenkov radiation as possible toward the photodetectors. Simulations were performed to optimize the segmentation, the position and the radius of curvature of these mirrors, and to define the specifications of the optical performance. A drawing of the system is shown in Fig. 5.

¹According to US regulations, seismic analyses are performed by increasing the expected weight load by 10%.

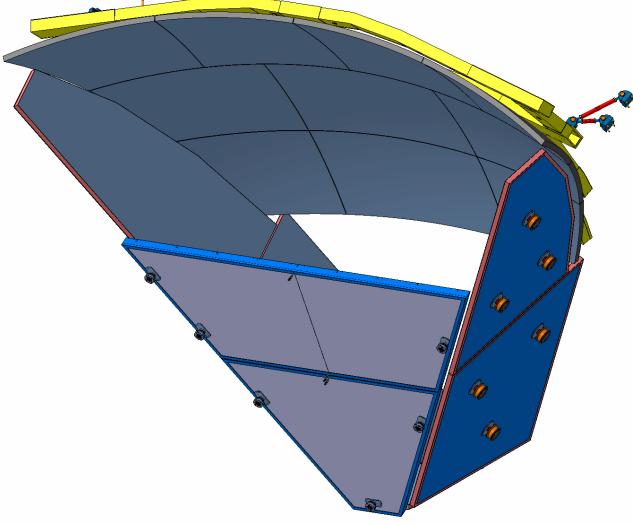


Figure 5: Drawing of the CLAS12 RICH mirror system with their mounting joints. The 10 sub-mirrors of the spherical mirror face the two front planar mirrors. An array of planar mirrors, two in each side and one (not visible) on the bottom completes the light containment system.

4.1.1. The Spherical Mirrors

The spherical mirror system, installed inside the box in front of the exit panel, has a total surface of about 3.6 m^2 , a radius of curvature $R = 2.7 \text{ m}$, and is segmented into 10 sub-mirrors. They were produced by the *Composite Mirror Applications* company [7], and are made of two layers of carbon fiber glued on a honeycomb core of small carbon fiber cylinders. The areal weight of these mirrors is $\approx 5 \text{ kg/m}^2$, with an improvement of about 10% with respect to the mirrors produced by the same company for the LHCb experiment [8]. Each mirror is positioned on a light carbon frame by means of three special joints equipped with a spring and a precision screw that allowed their relative alignment. The frame is then attached to the mechanical structure by means of three similar joints that allow the alignment of the full mirror system with respect to the other active elements of the detector.

The accuracy of the spherical surface of the sub-mirrors was quantified by means of the so-called spot size measurement, in which each mirror was illuminated with a point-like light source and the size of the reflected spot was measured by a XIMEA camera with a 1-cm-wide CMOS sensor. The size of the spot is quantified by D_0 , which is defined as the minimum diameter containing 90% of the total reflected light, and is related to the angular resolution on the reflected photons by the relation

$$\sigma_\theta = \frac{D_0}{8R}. \quad (1)$$

The smaller D_0 is, the closer the mirror surface is to a perfect sphere. The measurements also allow for the extraction of the radius of curvature, which corresponds to the distance between the camera and the mirror where the spot size is minimal. The results of a typical measurement of one sub-mirror is shown

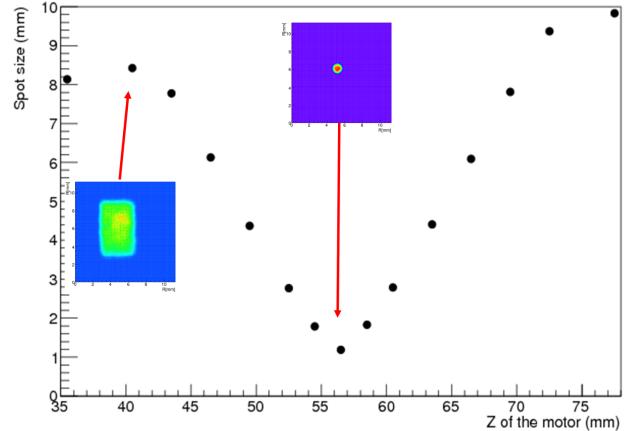


Figure 6: D_0 as function of the distance between the mirror and the camera for one of the spherical sub-mirrors. The two inserts show the shape of the reflected spot at the beginning of the distance scan and at the minimum.

in Fig. 6, where the D_0 as a function of the distance, and the shape of the spot at the beginning of the distance scan and at the minimum, are shown. All of the sub-mirrors exhibit a D_0 smaller than 1.5 mm, which means σ_θ significantly below 1 mrad, and a variation in the measured radii below 0.5%. All of these numbers are well within the specifications.

The sub-mirrors were coated with a reflecting layer by *Evaporated Coatings Inc* [9]. The quality of this coating was verified by measuring the reflectivity on several surface spots in the wavelength range from 300 to 650 nm. For all of the sub-mirrors, we obtained on average a reflectivity between 88% and 90%, relatively flat in the whole range.

4.1.2. The Planar Mirrors

The planar mirror system is composed of 7 mirrors: two installed on each of the lateral panels, two on the frontal panel, and one on the bottom, for a total surface area of about 6.5 m^2 . These mirrors were produced by the *Media Lario* company [10] and are made by two thin layers of glass glued on an aluminum honeycomb core. This is a standard technique widely used in telescopes for astrophysics studies but used for the first time in nuclear physics experiments, and allows for the production of mirrors as light as the carbon fiber ones but at much lower costs. Being in the acceptance of the detector, the frontal mirrors use very thin (0.7 mm) glass layers, allowing a reduction of the material budget down to about $0.01 X_0$, while for the lateral and the bottom mirrors thicker (1.6 mm) glass layers were used.

The planarity of the mirror was measured with a Coordinate Measuring Machine (CMM). Typically, the measured accuracy of the surface was few microns RMS. To better quantify the quality of the surface, the local slope profile was reconstructed from the spatial profile, as shown for one of the lateral mirrors in Fig. 7, where we see only a few spots with non-zero slope over a largely flat surface. All of the mirrors satisfy the requirement that only a few percent of the total surface should exceed a local slope of 0.3 mrad.

The characterization of the planar mirrors was completed by

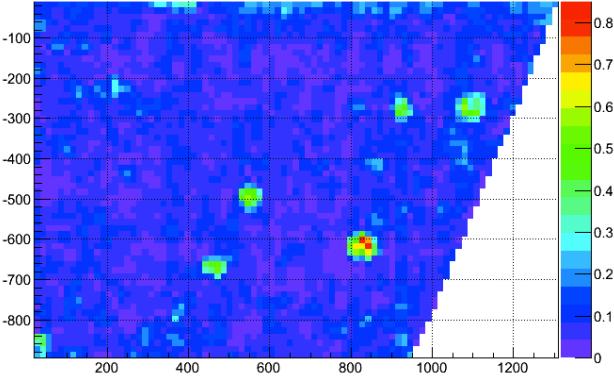


Figure 7: Profile of the local slope (indicated by the color scale in mrad) of the surface of one of the lateral planar mirror measured with a CMM.

measuring the reflectivity in a few random spots of the surface in the wavelength range from 300 to 650 nm. The measurements showed a maximum reflectivity of approximately 95% at 400 nm and a reflectivity higher than 90% in the whole range.

4.2. The Aerogel Radiator

The aerogel radiator was produced by the *Budker and Boreskov Institute of Nuclear Physics* (Russia), which was able to fabricate tiles of different shape and thickness, a critical requirement of the complex CLAS12 geometry. A total of 102 tiles with nominal refractive index 1.05, cut into squares 200×200 mm 2 , as well as pentagonal, trapezoidal, and triangular shapes, were assembled in two sections. The first section, covering the region between the beam pipe and the polar angle of 17.5° , was made of one layer of 2-cm-thick tiles. The second section, covering the polar angles between 17.5° and 26° , was made of two layers of 3-cm-thick tiles, the thickest aerogel tiles ever used in Cherenkov radiation applications at this high value of refractive index.

Each tile was tested to determine the geometric and optical parameters [11]. The measured geometric parameters are the side length and thickness, and the planarity of the tile surface. The measured optical parameters include the refractive index at the reference wavelength of 400 nm, and the light transmission as a function of the wavelength. The transparency parameter A_0 , the clarity parameter C , and the scattering length L_{scatt} at 400 nm are then extracted from the measured optical parameters using the Hunt parameterization [12]. Distributions of the measured values of the refractive index, A_0 (in percent) and L_{scatt} for the square 2 cm tiles are shown in Fig. 8. The average values obtained over all the tiles are $L_{scatt} = 50.5$ mm, $A_0 = 0.975$, and $C = 0.00512 \mu\text{m}^4/\text{cm}$. From these measurements, the expected photon yield for $\beta = 1$ particles is estimated to be about 19 photoelectrons (p.e.) in the 2 cm sector and about 25 in the 6 cm (3 cm + 3 cm) sector.

4.3. The Photon Detector

Due to the imaging aspects of the RICH, there are several requirements that the photon detector has to fulfill: it has to

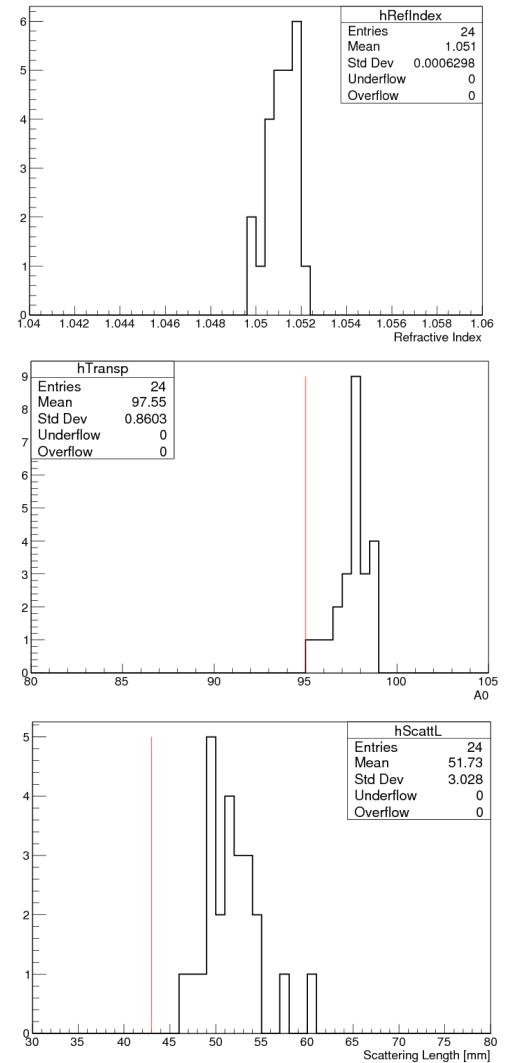


Figure 8: Distributions of the measured refractive index (top plot), A_0 (in percent, central plot), and L_{scatt} (bottom plot) for the square 2 cm tiles. The red lines indicate the specification limits.

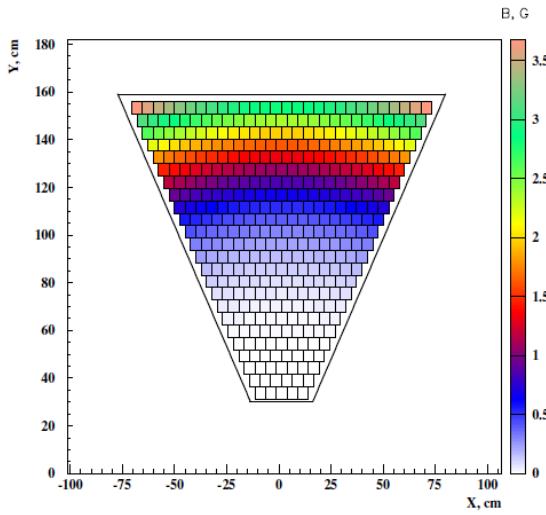


Figure 9: Calculated map of the Torus fringe field strength (in Gauss) in the RICH photodetector area.

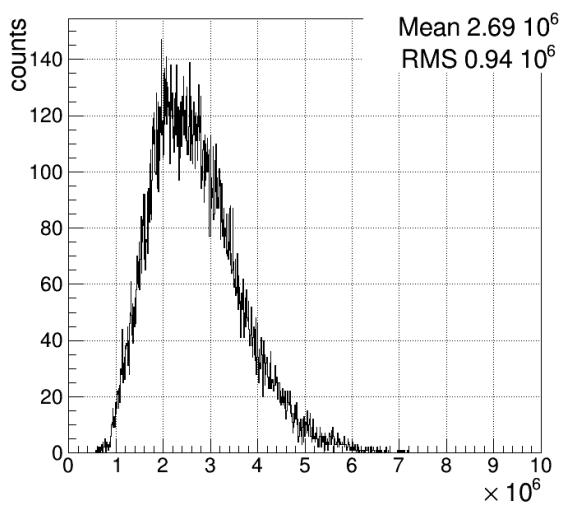


Figure 10: Distribution of the data-sheet gains of the 25000 RICH MaPMT channels.

efficiently detect single photoelectron (SPE) level signals, it must be sensitive in the visible light wavelengths (due to the aerogel radiator material), it must have the spatial resolution required to achieve the design angular resolution, and it has to provide an active area with minimal dead space. In addition, it has to be insensitive to the low torus fringe field where the RICH readout is located, which is estimated to be 3.5 G maximum, see Fig. 9. The Hamamatsu flat-panel H8500 Multi-Anode PhotoMultiplier Tube (MaPMT) [13] with an 8×8 array of $6 \times 6 \text{ mm}^2$ pixels over a compact active area of $5 \times 5 \text{ cm}^2$ and with high packing fractions (89%), was initially selected as a good candidate. Despite not advertised as the optimal choice in the SPE regime, such MaPMTs showed adequate performance in several laboratory tests [14] and beam tests [15]. Just after the RICH construction startup, the novel Hamamatsu H12700 became available, with the same layout as the H8500, but an optimized dynode structure for single photon detection [16].

Of the 391 MaPMTs that the CLAS12 RICH employs, 80 are of the H8500 type and the rest are of the H12700 type. This results in a total of 25024 individual pixels, covering the $\sim 1 \text{ m}^2$ trapezoidal active area of the first RICH module. The production specifications included requirements on the minimum gain of 1×10^6 and a maximum total dark current of 5 nA. Both were fully achieved. Figure 10 shows the distribution of the pixel gains, that has an average value of 2.7×10^6 , corresponding to about 400 fC generated charge per SPE.

4.4. The Readout Electronics

The RICH front-end electronics are designed to ensure 100% efficiency at 1/3 of the average photoelectron signal level, 1 to 4 gain spread compensation, time resolution of the order of 1 ns to distinguish direct from reflected photon hits, and a trigger rate up to 20 kHz with 8 μs trigger latency.

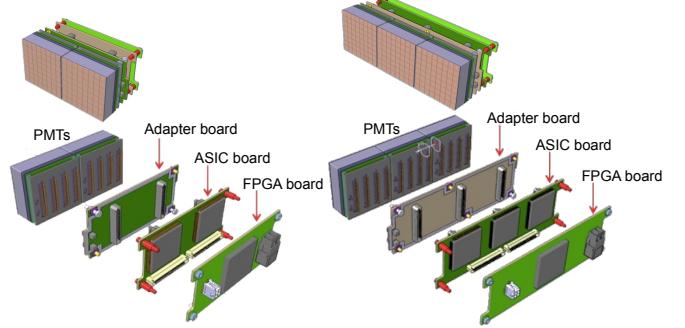


Figure 11: The CLAS12 RICH readout unit design (see text for details).

The front-end electronics are organized into compact units (tiles, see Fig. 11) mechanically designed to fit the MaPMT dimensions, each serving two or three MaPMTs, thus allowing the tessellation of large surfaces with minimum dead space and material budget. Each readout unit comprises three boards with complementary functions.

A feed-through adapter board provides the electrical connectivity of the sensors with the external readout system, while preserving the adequate light and gas tightness of the inner detector volume when mounted on the RICH carbon fiber supporting panel. It also distributes the sensor bias voltage (with -1000 V as nominal value).

The signal processing board is based on the MAROC3 chip [17], a 64-channel microcircuit dedicated to MaPMT pulse processing. Each channel comprises a low impedance adjustable gain preamplifier followed by two highly configurable shaping sections with independent processing. The first section embeds a slow shaper and a sample and hold structure to allow linear charge measurements up to 5 pC. Requiring short trigger delays and multiplexed access, this section can be used as a RICH calibration tool. The second section features a fast shaper and an adjustable threshold discriminator

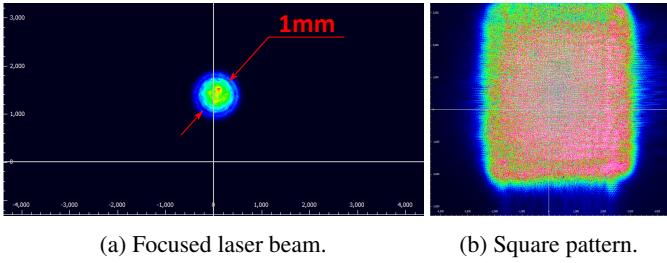


Figure 12: The laser output options.

to produce, for each input signal, a start and stop logic pulse. A constant-threshold binary readout requires good stability of the baseline (pedestal) and definition of the working point (gain and threshold). During the board production, quality assurance tests confirmed the excellent sensitivity of the logical readout, able to discriminate signals down to a few percent of a single photoelectron discharge, as will be extensively discussed in Sec. 6.

The third stage of the readout is made of the FPGA boards, hosting a Xilinx7 FPGA chip, responsible for configuring and reading the front-end MAROC3, distributing the trigger, and interfacing with the data acquisition system [18] via optical link. The FPGA provides a TDC functionality with a 1 ns time stamp for both start and stop times. The start time is used for timing purposes, while the difference between the stop and start times, the so-called Time-Over-Threshold (ToT), provides a non-linear estimate of the amplitude of the input signal and is used for the time walk correction, see Sec. 9. Finally, the FPGAs also embed a self-trigger scaler readout that is used as a calibration and monitor tool.

4.4.1. *MaPMT Characterization*

The characterization of hundreds of MaPMTs is a challenging problem. In order to test them efficiently within a reasonable time frame, a fully automated test stand was built to evaluate 6 MaPMTs at once. The test stand consists of a 470 nm diode laser system, 2 long travel motorized stands to drive a laser fiber in two-dimensional space for individual pixel illumination, and a motorized neutral density filter system. The laser light is directed through the fiber and attenuated to the single photon level using neutral density filters to mimic the conditions of the RICH detector. The motors are remotely controlled to move the focused laser 1 mm beam spot across the entire surface of the MaPMT entrance window and illuminate one by one the 64 pixels individually (see Fig. 12a). Alternatively, one can illuminate the whole surface of the MaPMT photocathode at once using an Engineered Diffuser to produce a square pattern with a non-Gaussian intensity distribution (see Fig. 12b). The latter configuration was used for the massive characterization of the RICH MaPMTs, bringing routine workloads to a minimum. The evaluation of 6 MaPMTs (corresponding to 384 individual channels) at 4 different high voltages and 6 different light intensities was completed in 6 hours with less than 15 minutes of human intervention.

The characteristics of the SPE spectrum were studied using

the charge measurement functionality of the slow shaper of the MAROC3 chip. A new computational model [19] for the description of the photomultiplier response functions of both the H8500 and H12700 MaPMTs was developed. Important features of the model include the ability to approximate the true single photoelectron spectra (SPE) from different photomultiplier tubes with a variety of parameterized spectral shapes. The predictive power of the model was tested by demonstrating that the SPE spectral parameters, obtained in the measurements, may describe well the amplitude distributions of the same photodetector measured at different levels of illumination and applied high voltage. Thus, the model allowed us to extract the characteristic parameters of the devices independently of the test measurement conditions.

The SPE spectrum is extracted by fitting with the model function the signal amplitude distribution measured as shown in Fig. 13 for the H8500 MaPMT and in Fig. 14 for the H12700. The x -axis is calibrated in terms of charge measured by the MAROC3 chip. To approximate the performance of the first amplification cascade of the MaPMTs, the probability function $T(n, m; \mathbf{t})$ was introduced in the model as a trinomial sum of three Poissonians with different average secondary multiplicities and the corresponding three relative probabilities for every photoelectron to generate secondary electrons. In the function m is the number of the electrons knocked out from the first dynode, n is the number of electrons emitted out of the second dynode, and \mathbf{t} is the vector of the model parameters (see Ref. [19] for more details).

In each fit, the quantum efficiency parameter μ corresponds to the average number of photoelectrons created at the photocathode by each laser pulse, $v_{average}$ is the average number of secondary electrons generated at the first dynode, and $scale$ is the average anode charge collected from one photoelectron.

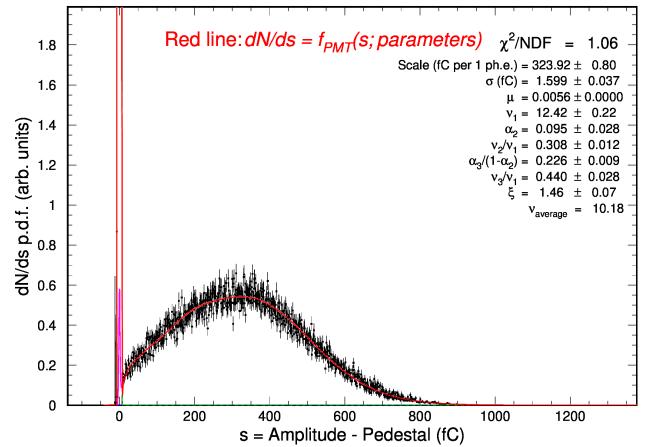


Figure 13: Sampled H8500 MaPMT single photoelectron spectrum from one of the pixels at 1000 V with a low-intensity laser light source. The fit function (see details in Ref. [19]) is shown as a solid line. The relevant parameters (see text) are $\mu = 0.0056$, $v_{average} = 10.18$ and $scale = 323.9$ fC. This corresponds to a PMT gain = 2.0×10^6 .

The data showed that the H12700 has, on average, a 10% better efficiency than the H8500, likely due to the improved photocathode performance and collection efficiency. An ex-

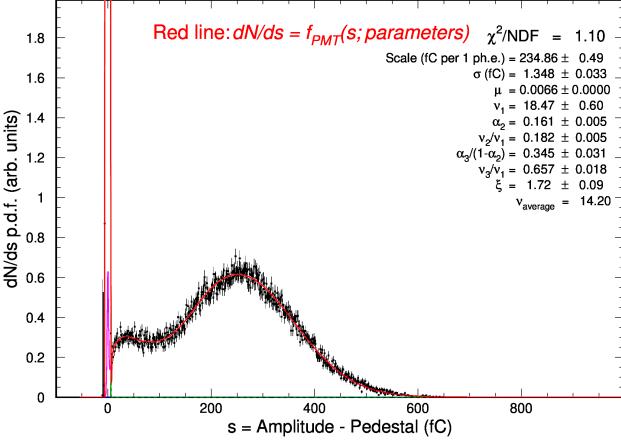


Figure 14: Sampled H12700 MaPMT single photoelectron spectrum from one of the pixels at 1000 V with a low-intensity laser light source. The fit function (see details in Ref. [19]) is shown as a solid line. The relevant parameters (see text) are $\mu = 0.0066$, $v_{\text{average}} = 14.18$ and $\text{scale} = 234.8 \text{ fC}$. This corresponds to a PMT gain $= 1.5 \times 10^6$.

ample of the results for one MaPMT is shown in Fig. 15. The parameter *scale* (top plot), characterizing the amplification (dynode) system, is virtually independent of the light radiation level while strongly dependent on the high voltage supply, the exact behavior one would expect from the characteristic internal dynode system of a MaPMT. On the contrary, the parameter v_{average} (center plot) that is related to the first dynode performance, is relatively independent of the bias voltage. The bottom plot shows the quantum efficiency parameter μ measured with different optical filters. It indicates that all of the channels respond in the same way as the light intensity increases.

The results of the characterization have been stored in the CLAS calibration database and are available for use in the Monte Carlo simulations. The extracted gain values have been used to perform the equalization of all 25024 readout channels.

The dark noise SPE spectra allow for the study of the efficiency dependence on the working parameters, i.e. MaPMT bias voltage, MAROC pre-amplification gain, and discriminator threshold² using the binary readout line. Data indicated that the efficiency reaches a plateau over a wide range of working parameter values [20]. The plateau corresponds to the region where all of the MaPMT discharges are digitized and the efficiency ultimately depends on the quality of the photocathode. The plateau is a consequence of the saturated mode employed in the MAROC binary readout and allows a flexible definition of the working point, a crucial feature when dealing with a large number of channels in the challenging single-photon regime.

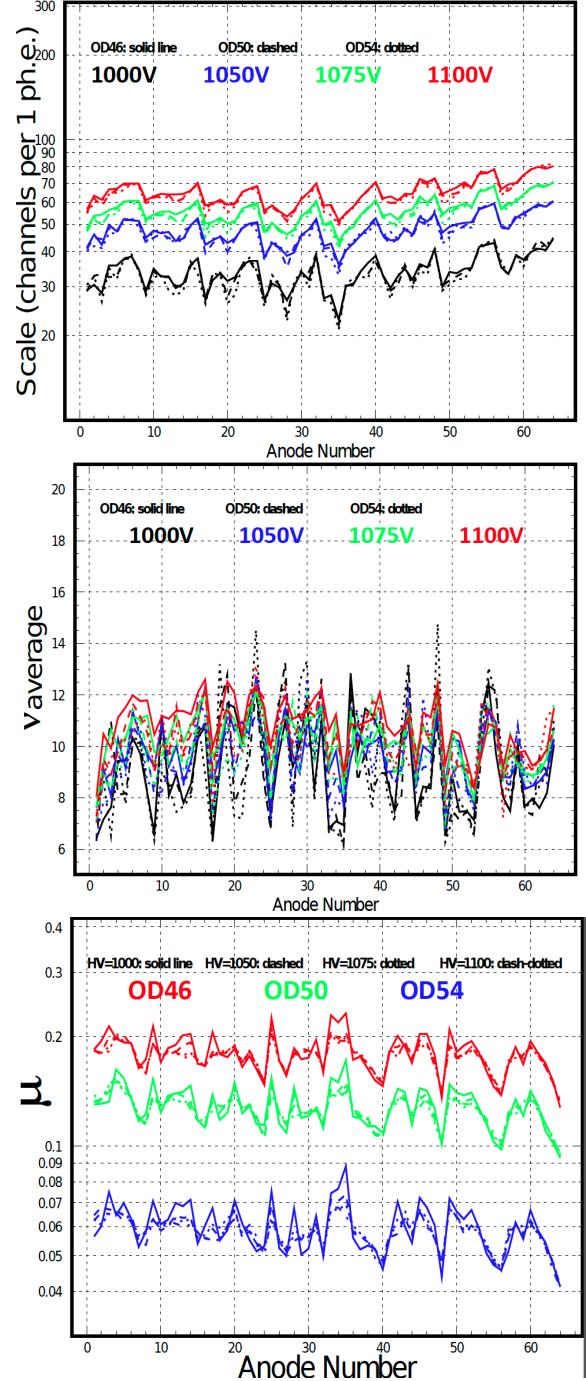


Figure 15: Distributions of fit parameters among the pixels of one MaPMT: the parameter *scale* characterizing the dynode amplification system (left) and the first dynode performance v (center) at 4 different high voltage supplies; the quantum efficiency parameter μ at 3 different light intensities (right).

²The programmed threshold levels are expressed in Digital-to-Analog Converter (DAC) units, 1 DAC unit corresponds to about 1 mV.

4.5. Services

The CLAS12 RICH requires various services, namely power, cooling, and gas purge whose number of lines has to be minimized and installed outside of the CLAS12 acceptance. A continuous nitrogen flow, supplied by the Hall B gas distribution system, is provided in order to keep the relative humidity inside the RICH vessel at the few percent level. The flow is set to about 60 l/m to ensure a complete inner volume exchange in a few hours. A backup system has been realized by a stack of nitrogen bottles to allow for up to 3 days of gas flow in case of failure of the primary distribution system.

The electronics power is controlled by a CAEN SY4527 power supply with five 8-channel A2518 LV boards and five 32-channel A1536 HV boards. Each LV channel powers 4 FPGA boards, while one HV channel drives one MaPMT. The electronic readout is connected to the back-end by three MTP trunks of 2.5 Gbps optical fibers. One trunk groups several multi-core fibers, each of them connecting one of the eight ports in the VME/SSP [18] back-end module to four FPGA boards.

The readout electronics dissipates about 3.5 W per unit, mainly due to the FPGA chip and the optical transceiver, as shown by the thermocamera image in Fig. 16. The total heat load, at the level of 500 W, is removed by a forced air flow. Since the electronics panel is not fully sealed due to the numerous holes for the readout and HV connectors, there is a diffusive exchange in the RICH vessel between the nitrogen gas used to keep the aerogel dry and the air in the electronics panel. As a consequence, dry and clean air is required to cool down the electronics. This is achieved with an Altas Copco multi-core oil free rotary scroll air compressor. The compressor fills a tank at 8 atm pressure, from where the cooling air is filtered and circulated towards two distributors located at the sides of the electronics panel and outside the acceptance. These are made of stainless steel tubes with several nozzles to direct the cooling air supersonic flow along the board surface. The exhaust is made of six corrugated tubes that run in the back of the RICH module behind the spherical mirror.

5. Assembly and Installation of the Detector

The assembly of the RICH detector was performed in a clean room and each element was installed after the completion of the relative characterization tests. The trapezoidal RICH vessel was attached to a large aluminum structure with a pivot to rotate the detector from the vertical to the horizontal position, as required by the various assembly phases.

The ten spherical sub-mirrors were mounted on a common frame inside the RICH vessel. To minimize the material budget, the frame is composed by a net of 1.5-mm-thick carbon-fiber U-profiles. Each element (frame and sub-mirrors) has three mounting points designed to allow precise alignment. The relative alignment of the sub-mirrors was performed with the same setup used to determine their surface accuracy. The full spherical mirror was illuminated by a point-like source and the position of each sub-mirror was adjusted until the ten spot images converged into the nominal center of curvature. In

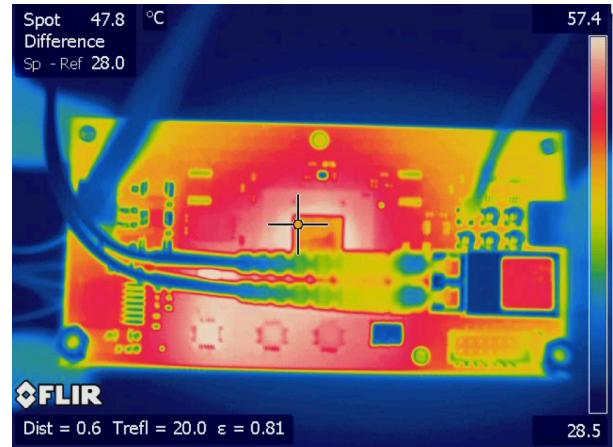


Figure 16: The CLAS12 RICH readout unit as imaged by a thermocamera. The hottest spots are the FPGA chip in the center and the optical transceiver on the right.

Fig. 17, the reflected images before the alignment (when each sub-mirror produces a spot at a different location) and after the alignment (when all the spots overlap within a few mm) are shown. The quality of the result is also visible in Fig. 18, where the spherical mirror system before (left) and after (right) the alignment is shown.

The lateral and bottom planar mirrors were attached to the RICH trapezoidal vessel structure, by means of joints allowing a precise alignment. The two frontal mirrors were mounted on the lower frontal panel made of carbon-fiber. The relative position of the mirrors was aligned with respect to the RICH vessel at the level of about 0.5 mrad by using a faro-arm. The fully installed mirror system as seen from the entrance panel is shown in Fig. 19.

The RICH photon detectors and readout electronics were installed on the electronics panel using an independent aluminum support structure to enable easy access and to allow rotations during the functionality tests. The photomultipliers with higher gain were placed closer to the beam pipe, where better detection performance is required. As the MaPMT in one readout unit share the same HV bias, they were selected of similar gain and same type (H8500 or H12700). The fully equipped electronics panel is shown in Fig. 20 from the MaPMTs side and in Fig. 21 from the readout electronics side.

After the electronics panel assembling was completed, particular care was devoted to minimize and stabilize the pedestal width values. The measured pedestal RMS was initially at the level of few DAC units, with relatively large variations not only from MaPMT to MaPMT but also among the channels of a single MaPMT, as is shown in the top plot of Fig. 22. As the readout uses a single threshold value per chip (or MaPMT), the channel by channel variation may effect the single channel efficiency in a way that would be complicated to correct for. Therefore, a grounding grid was realized by connecting all the boards with the detector chassis with a copper wire. In this way, all of the components of the readout system, powered by the floating 5V low-voltage lines, was properly referred to the same

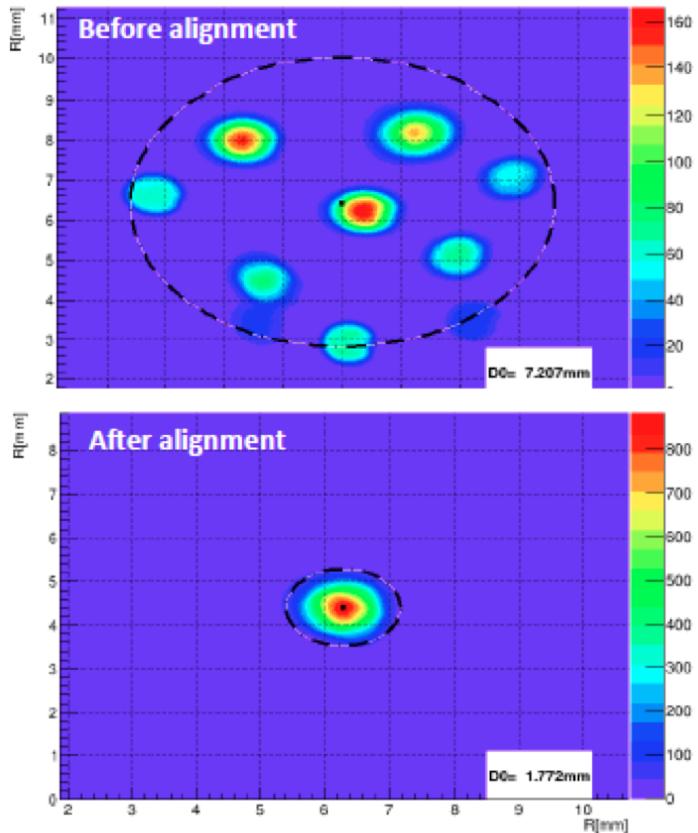


Figure 17: Reflected spot by the whole spherical mirror system: before the alignment (top plot), all sub-mirrors image the light source in different locations; after the alignment (bottom plot), all images overlap in the same position. The spot brightness depends on how close the sub-mirror center is to the sensor position.



Figure 18: The spherical mirror before (top plot) and after (bottom plot) alignment. As a result of the alignment, the image appears continuous along the whole mirror surface.

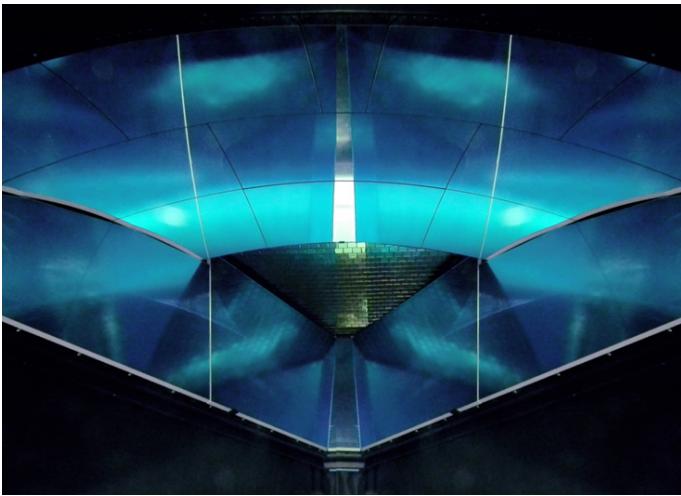


Figure 19: The mirror system as it is seen from the RICH entrance panel. Clockwise from the top, the ten spherical sub-mirrors, the two right lateral mirrors, the bottom mirror, and the two left lateral mirrors are visible. At the center, the MaPMT array is also visible.

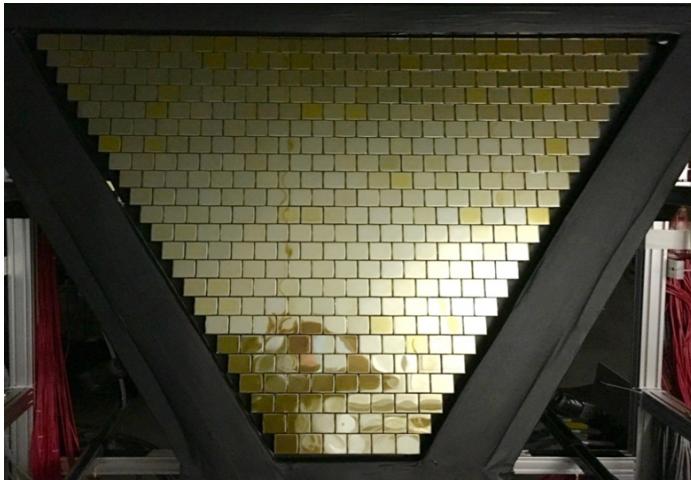


Figure 20: The fully assembled plane of MaPMTs.



Figure 21: The fully assembled and cabled front-end electronics. Visible are the gray 20 AWG LV cables, the red HTC-50-1-1 HV cables, and the cyan MTP optical fibers.

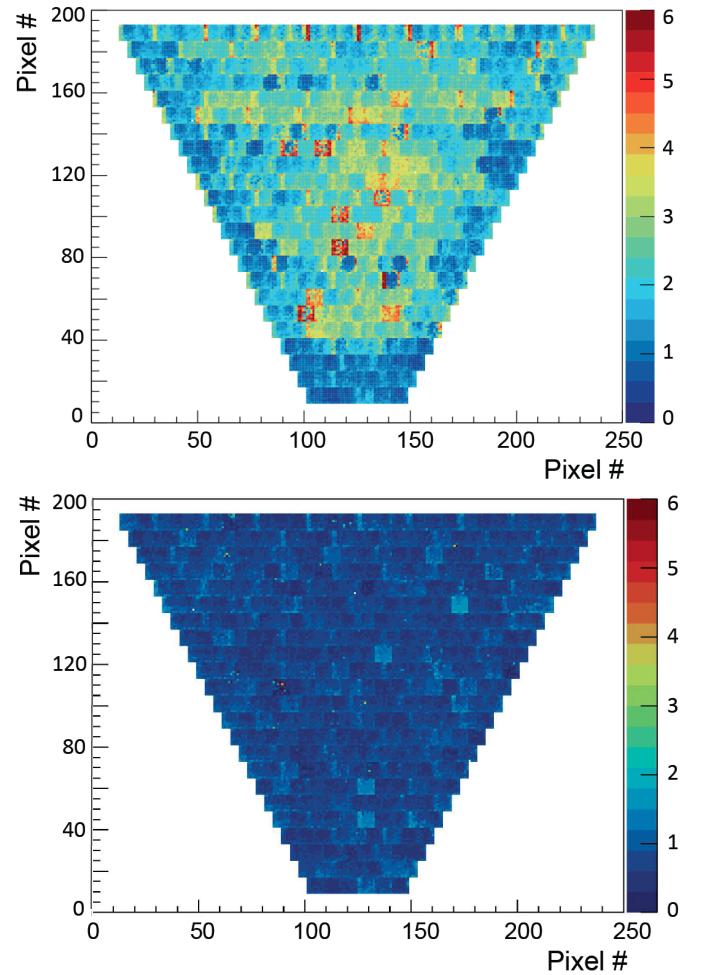


Figure 22: Map of the pedestal RMS values before (top) and after (bottom) the realization of a grounding grid connecting all the electronics units to the RICH chassis to provide a common ground reference for the floating power lines.

ground. This reduced the typical pedestal RMS down to about 1 DAC unit, a level comparable with the test bench results, as shown in the bottom plot of Fig. 22.

Several tests were performed at various stages of the electronics assembly, using cosmic rays. In the absence of a precise measure of the cosmic particle momentum, it was not possible to perform any study of the Cherenkov angle resolution. Nevertheless, cosmic runs allowed for the validation of the translation tables relating the electronics channels to the pixel positions, the development of the ring reconstruction software, the verification of the stability of the system, and the testing of the performance of the power supplies, cooling, readout, slow-controls, and interlock services. After all planned tests were completed, the complete readout system was eventually transferred into the mechanical structure.

The aerogel was the last element installed, being the most sensitive to the external conditions. For this reason, before its assembly, a test to verify the gas-tightness of the RICH vessel, temporarily completed with all of the closing panels, was performed. Each aerogel tile was inspected and mounted

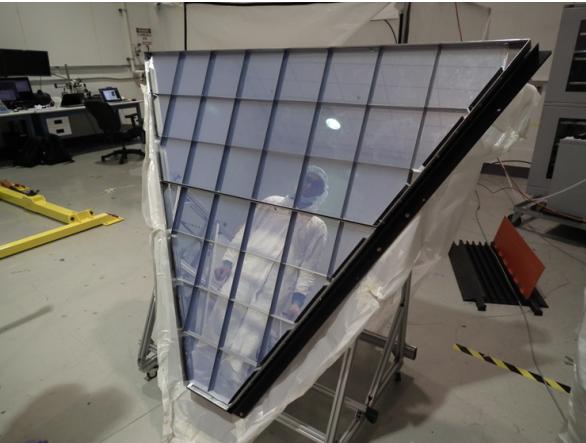


Figure 23: The 2-cm-thick section of the aerogel mounted on the two RICH frontal mirrors. Visible are the external aluminum frame and the black foam net that optically and mechanically isolates each tile from the others.

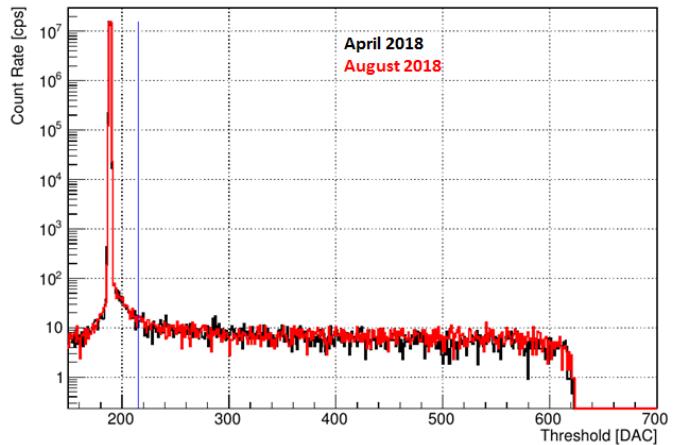


Figure 24: Example of a SPE spectrum from the dark rate measurement of one readout channel as a function of the threshold value. The two histograms were recorded in April and August 2018. The blue line indicates the threshold setting.

in a pre-selected location of the supporting structure, namely the frontal mirrors for the 2 cm tiles and the upper frontal panel for the 3 cm tiles. The location of each tile was determined in order to concentrate the tiles with the higher expected photon yield at forward polar angles where the particle identification requirements are most demanding. In addition, tiles with close optical properties were coupled in the same location of the double 3 cm layer. The tiles were secured in place by a net of nylon wires that ran along the edges and, on the side, by plastic bumpers covered by a thin foam layer to avoid damage to the aerogel. The tiles were also optically isolated each other by using a thin layer of foam stretched around each tile. In fact, photons produced in one tile and propagating through an adjacent one undergo surface effects that generally degrade the angular resolution. The foam is instrumental to avoid sharp edge contacts between the blocks that might originate cracks in the aerogel material. In addition, the foam net bonds together the tiles in forming a sole and stable layer. Figure 23 shows the frontal planar mirror system with the aerogel tiles fully installed.

During the assembly, the aerogel panels were maintained in a low-humidity atmosphere (around 20% relative humidity) to prevent moisture absorption. Once the assembly of all tiles was completed, the panels were quickly installed on the RICH vessel, the detector was sealed with all the closing panels and a flow of purged nitrogen was started to minimize the exposure to the external weather conditions.

Once the detector was sealed and before the transportation to the experimental hall, its functional parameters were tested for several weeks in the assembly room. The tests included the two gas systems serving the RICH: the nitrogen system that must keep the internal humidity at the few percent level to preserve the aerogel optical performance and the air cooling system of the readout electronics.

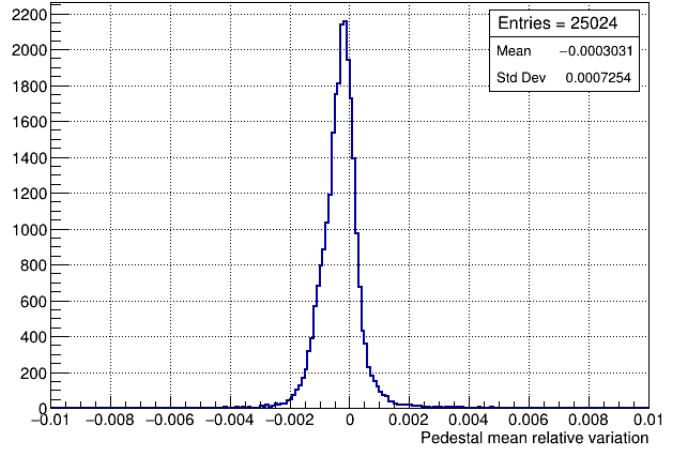


Figure 25: Relative variation of the mean pedestal position of the 25024 readout channels between April and August 2018.

6. Commissioning of the Detector

The RICH detector was installed in the CLAS12 spectrometer at the beginning of January 2018, in time with the start of the data taking in Hall B. In preparation for the data taking, a number of tests were routinely performed without and with beam to establish the running conditions and to verify the stability of the response.

The basic tool to monitor the RICH front-end electronics is provided by the measurement of the MaPMT dark noise counting rate using the self-triggered scaler readout provided by the FPGAs. The number of counts above a programmed threshold is recorded for a time on the order of a second. A fine scan of the threshold value allows for the reconstruction of the full SPE spectrum for each of the 25k channels. An example of one SPE spectrum is shown in Fig. 24. The main features of the data are: *a)* a very narrow pedestal where the

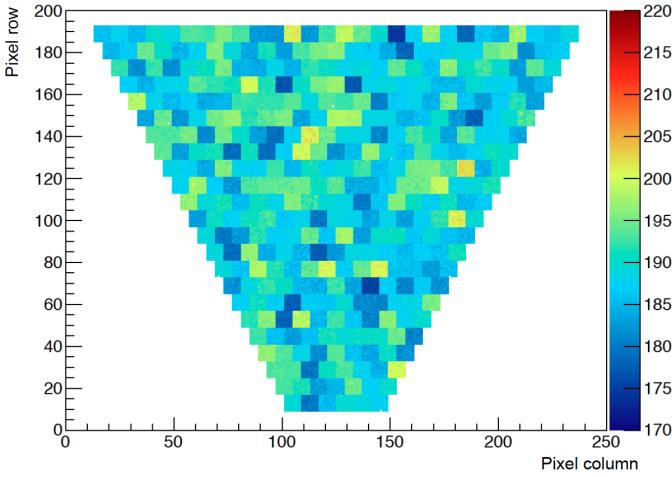


Figure 26: Map of the mean pedestal position in DAC units (color scale).

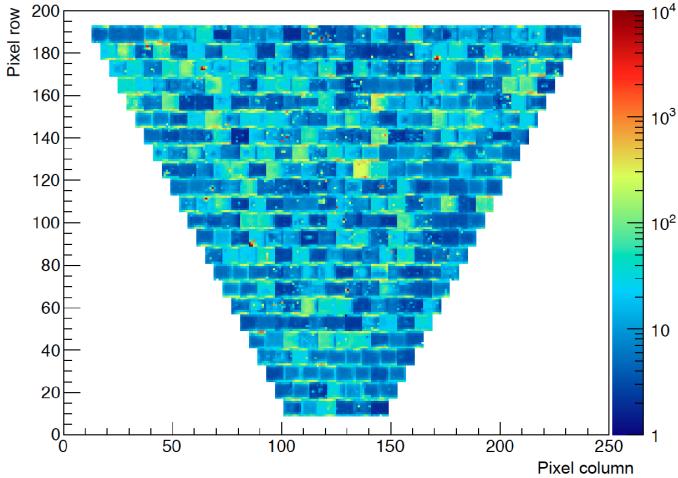


Figure 27: Map of the average dark count rate in the plateau region of threshold values (color scale).

threshold equals the baseline, *b*) a region close to the pedestal where the rate smoothly decreases as the threshold increases (corresponding to the almost linear regime of the MAROC), and *c*) a large plateau of the saturation regime, where the count rate is basically insensitive to the threshold setting almost up to the edge of the SPE region. The plateau is a crucial feature of the front-end electronics, because it allows a flexible definition of the working point without the need for extreme precision in the channel equalization. The spectra allow for the channel-by-channel extraction of the pedestal position and width, the dark count rate in the plateau region, and the amplitude of the SPE region. The black and red histograms in Fig. 24, taken in April and August 2018, respectively, demonstrate the stability of the readout system over several months of running. Moreover, in Fig. 25, the relative variation of the mean pedestal position in the same interval of time is shown. On average, the pedestals are stable at the level of 10^{-3} .

The pedestal level is different for each readout channel, but

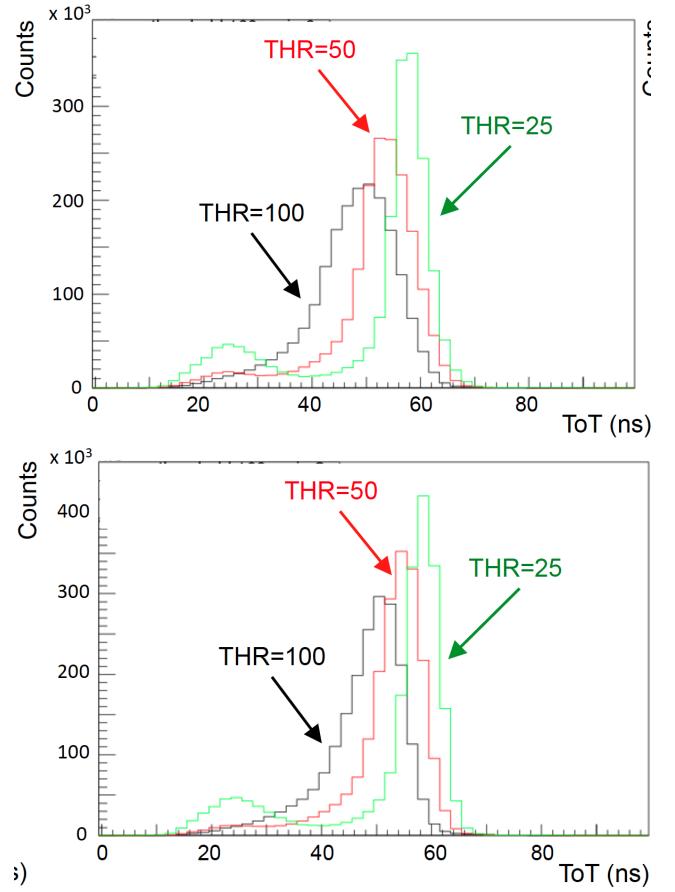


Figure 28: Time-over-Threshold (ToT) distributions of the RICH channels at three typical values of threshold (25, 50, and 100 DAC) without (left) and with (right) gain equalization. The saturated SPE signals generally yield ToT durations greater than 40 ns. When lowering the threshold weaker cross-talk signals are also recorded with ToT durations around 25 ns.

it is quite uniform within one MAROC chip, as can be seen from the map shown in Fig. 26. This result guarantees the effectiveness of the common threshold.

The average count rate in the plateau region provides a measurement of the dark count rate of the channel, as shown in the map of Fig. 27. The typical dark count rate is a few tens of Hz, with more than 99% of the channels below 100 Hz and only few channels above 10 kHz. It is also found that the highest dark count rates in the MaPMTs are located in the first and last row of pixels. Although measured with a completely different setup, these results are in good agreement with the values quoted in the Hamamatsu data sheets.

The MAROC preamplifier equalization gains are determined using the characterization measurements described in Sect. 4.4.1 by tuning the average MaPMT+MAROC gain to 2.7×10^6 in all channels. The equalization gains range from about 0.5 to 3, with an average value of 1.2. The effect of the channel-by-channel signal equalization was verified during the engineering run, by taking data at various thresholds for different MAROC gain configurations. Figure 28 shows the ToT distribution for three typical values of the threshold, on the left

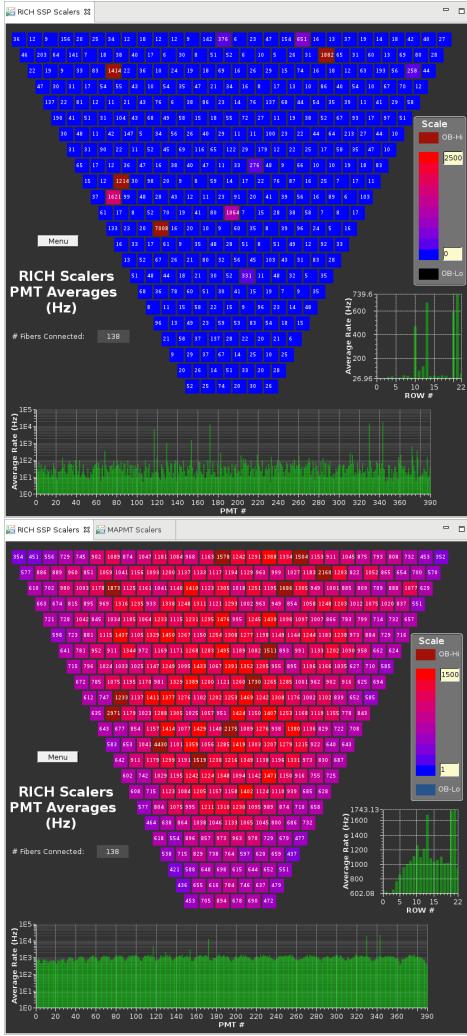


Figure 29: The average count rates (in Hz) over 64 pixels for each MaPMT during data taking. Top: without beam on target, Bottom: with beam.

for all channels without amplification (nominal MAROC gain of 1) and on the right after equalization. After equalization, the ToT distribution of saturated SPE signals is narrower than with unitary gains. With typical ToT values larger than 40 ns, the signal region is also clearly separated from the cross-talk signals whose ToT values are distributed around 25 ns.

After these tests, the common discrimination thresholds were set to +25 DAC units above the average MaPMT pedestal position, a level that corresponds to a small fraction of the average SPE amplitude.

7. RICH Slow Control and Interlocks

The RICH slow controls are based on Experimental Physics Industrial Control System (EPICS) [21]. It includes EPICS input-output controllers (IOCs) interfacing with different types of hardware via communication protocols and over 25k RICH process variables (PVs). The controls system monitors many aspects of the RICH detector, such as the scaler rates of all 25k

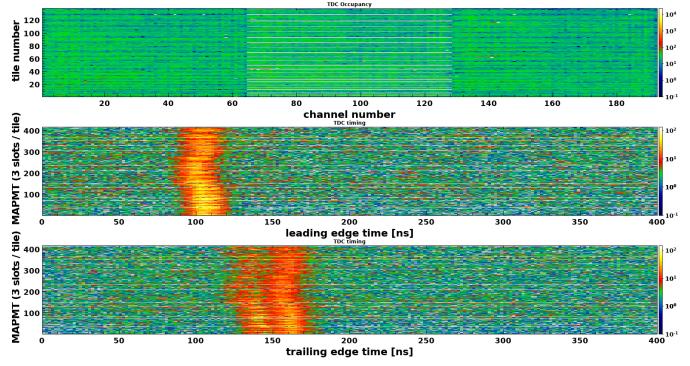


Figure 30: Online monitor plots of the TDC occupancy with beam on. From top to bottom: channel occupancy in terms of the tile vs. channel number; leading edge time distributions per MaPMT; trailing edge time distribution per MaPMT.

Hamamatsu MaPMT pixels, the FPGA temperatures of each readout board, the HV and LV power supplies, the LV and current consumption of each readout unit, the gas system, and the temperature and humidity of the electronics panel volume and detector volume. For the graphical user interface (GUI), the Control Systems Studio (CS-Studio), an Eclipse-based suite of tools for developing and monitoring large-scale control systems, is used.

The quality of the data is monitored by scaler and TDC plots. Figure 29 shows the average MaPMT rate measured by the scaler readout system when the beam is off (top plot) and when the beam is on (bottom plot). In the top plot, the few MaPMTs with hot pixels where the dark rate is substantially higher than the average can easily be seen. The bottom plot shows that when the beam is on the rate is always dominated by physics events. Figure 30 shows the occupancy plots from the TDC readout. The top plot shows the occupancy per channel, and the center and bottom plots show the distributions of the leading and trailing edge times per MaPMT, respectively. All of these plots are used during the data taking to identify possible malfunctioning channels and, eventually, restore them through a recovery procedure.

The slow controls and monitoring of the RICH detector is enforced by the hardware interlock system based on the National Instruments CompactRIO (cRIO) [22]. The cRIO system monitors the following parameters:

- Temperature and humidity in 16 locations of the detector volume;
- Temperature and humidity in 16 locations of the electronics panel;
- Air tank pressure;
- Air and nitrogen flow.

The locations of the temperature and humidity sensors, and the air and nitrogen flow meters inside the electronics panel and nitrogen volume are shown in Figs. 31 and 32, respectively. The inner temperature of the electronic panel ranges between

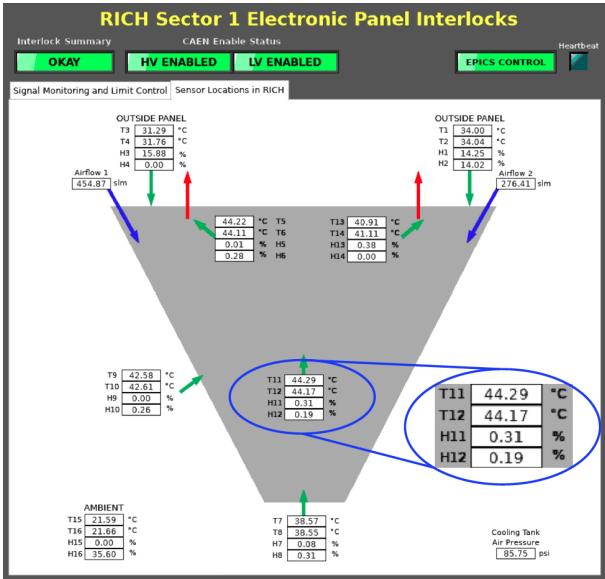


Figure 31: Location of the temperature, humidity, and gas flow meters in the electronics panel.

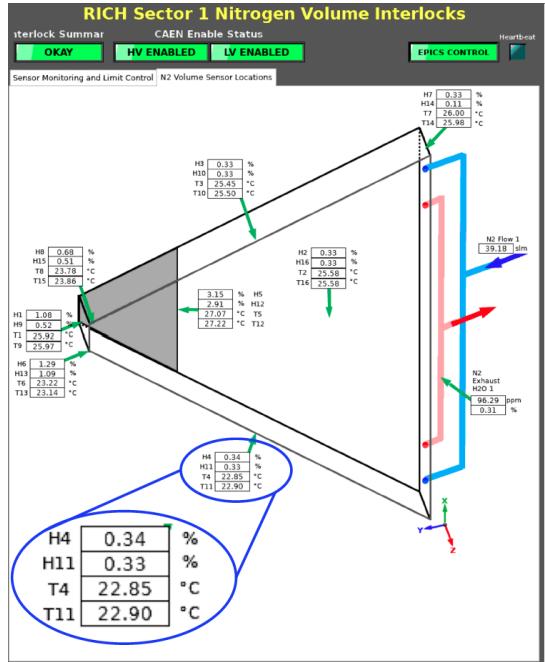


Figure 32: Location of the temperature, humidity, and gas flow meters in the nitrogen volume.

38.5° and 44.5° moving from the bottom towards the top of the module, whereas the external temperature stays below 34.5°, in accordance with the requirement to not drive the FTOF system above 40°. The relative humidity is below 0.5%. In the nitrogen volume, the temperature ranges between 23° and 27°. The relative humidity is below 1.3% except in the central point close to the spherical mirror pivot, where it reaches a 3% value.

The signal levels are controlled by setting limits. If the temperatures, air flow, or air pressure go out of limits, the HV and LV is powered off, i.e. interlocked. In case the humidity or the nitrogen flow are out of limits, an alarm signal is generated.

Important safety parameters of the RICH detector are: the temperature of the front-end electronics, the nitrogen flow, and the RICH internal relative humidity. Figure 33 presents the map of the temperatures of the front-end electronics. Typical temperature values are around 65°C on the FPGA chips and 40°C in the detector volume. The safety temperature limits are 85°C for the FPGAs, 80°C for the optical fiber cables, and 40°C for the temperature on the FTOF detector, which is about 10 cm away from the RICH. Therefore, the maximum allowed temperature was set to 75°C on the FPGA and to 45°C inside the electronics panel.

The nitrogen flow and the RICH internal relative humidity are measured by several probes installed inside the detector. An alarm is sent out in case the humidity exceeds 5% or in case the nitrogen flow drops below the normal value. In the latter case, the backup system starts working to restore the normal flow level and to ensure safe humidity conditions. During RICH operation, the humidity level has proven to be very stable with time.

8. RICH Event Reconstruction

The RICH reconstruction is organized in 4 steps. In the first step, the spatial and time information of each hit in the MaPMTs is corrected by the spatial misalignment and time calibration parameters. The hits are ordered as a function of their ToT value, as this reflects the corresponding amplitude (released charge). A 3×3 MaPMT pixel matrix centered around a local maximum, i.e. the hit with the highest local ToT, is called a nonet. If more than 3 hits are found in the same nonet they are grouped into a RICH cluster. A cluster is typically created by a charged particle producing Cherenkov light in the MaPMT window or ionization in the sensor dynode structure. If a sole hit is found close to a local maximum with a ToT lower than 80% of that maximum, the hit is flagged as possible cross-talk. Hits belonging to the same nonet of the local maximum are flagged as optical cross-talk, while hits readout by an electronics channel adjacent to the maximum hit in the MAROC chip are flagged as electrical cross-talk. Note that the readout circuit routing has been designed to connect anodes close in space to non-adjacent MAROC3 inputs. The above selection rejects about 87% of the cross-talk hits, as can be seen in Fig. 34. In the figure, the ToT distribution of the recorded RICH hits (black solid line) is shown together with the distributions of the hits identified as optical (magenta dash-dotted line) or electrical (green dashed line) cross-talk. The shoulders on the right of the cross-talk peaks are likely due to signal discharges wrongly identified as cross-talk. The hits selected for further analysis are highlighted by the dotted (blue) histogram. The excess at low ToT values indicates a residual contamination of unidentified cross-talk. The leftover

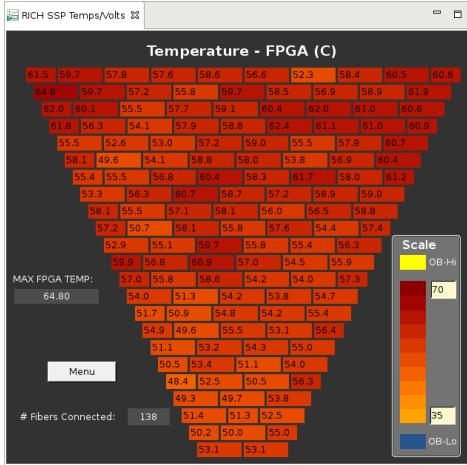


Figure 33: Slow controls display: Map of the temperatures measured on the FPGA chips.

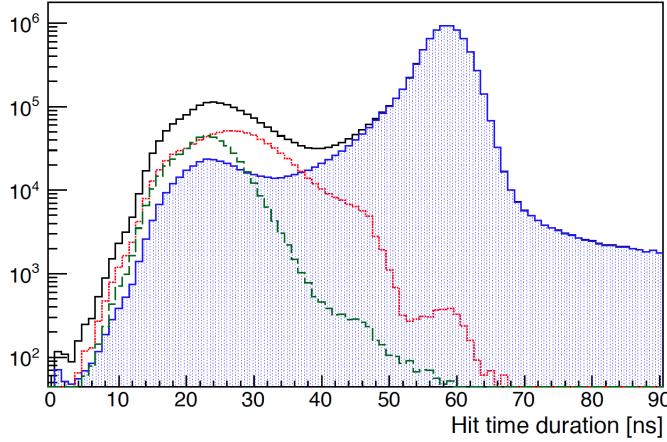


Figure 34: ToT distribution of the recorded RICH hits (black solid line) together with the optical (magenta dash-dotted line) and electrical (green dashed line) cross-talk distributions. The hits selected for further analysis are highlighted by the blue dotted histogram.

cross-talk contamination, at the level of 2.7% of the signal, can be further reduced only with a time versus amplitude analysis, see Sec 9. The cross-talk selection also removes a small (0.8% fraction) of true Cherenkov signals. Those correspond to MaPMT discharges that undergo incomplete dynode multiplication, while being by chance close in space to another Cherenkov signal. Hits flagged as cross-talk are not considered further in the RICH reconstruction.

The second step consists in finding the spatial match between the RICH clusters and the CLAS12 tracks. This requires that the extrapolated impact point of the track on the MaPMT plane is within 10 cm of the cluster center. The latter is calculated as a weighted average - with the ToT value as the weight - of the spatial coordinates of all the hits in the cluster. Matched clusters allow a precise study of the MaPMT detector position and orientation relative to the CLAS12 tracking system. This is shown in Fig. 35, where the distance between the RICH clusters

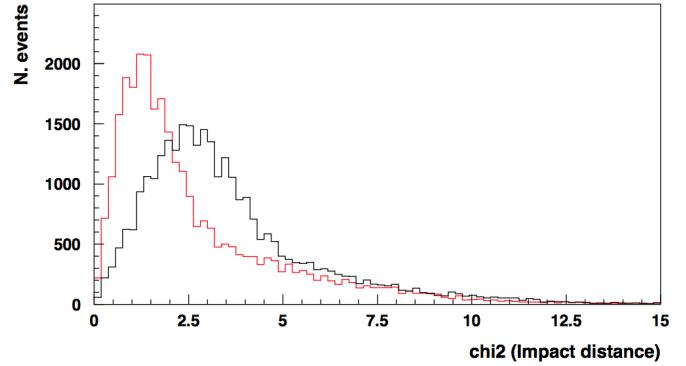


Figure 35: RICH matching χ^2 , defined as the distance between the RICH clusters and the matched drift-chamber tracks divided by the pixel spatial RMS. The black distribution is before and the red one after the alignment procedure.

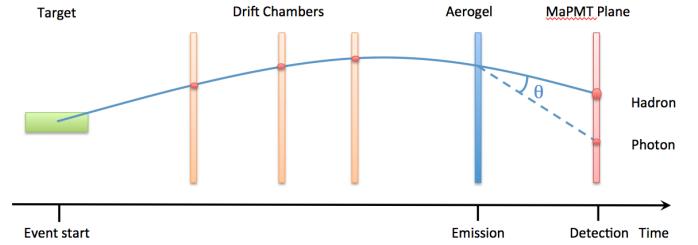


Figure 36: The RICH photon detection time as measured by the CLAS12 spectrometer. It is defined as the event start time plus the flight-times of the hadron from the interaction point to the radiator center, and of the ray-traced photon within the RICH volume.

and the matched drift-chamber tracks [23] divided by the pixel spatial RMS, (a sort of χ^2 distribution), is reported. The black distribution is before and the red one after the alignment procedure.

The third step is the core of the RICH reconstruction [24]. For each hit in the MaPMT plane, an estimate of the corresponding Cherenkov angle is derived by ray-tracing the photon path inside the RICH volume taking into account possible reflections. This is done in turn for each charged particle traced through the RICH, with the photon emission point assumed to be the middle point of the particle path inside the aerogel radiator. In the fourth step, a particle identification algorithm is applied using an event-based likelihood of the reconstructed Cherenkov angles and times.

9. Time Calibration and Resolution

The time information of the RICH hits is provided by the leading edge time T_1 measured by the TDC implemented into the FPGA board with a 1 ns precision. In-time photon hits are selected by comparing their T_1 with the time T_{calc} computed using the CLAS12 information (see Fig. 36). T_{calc} comprises the event start time, the charged track path and flight time provided by the tracking system, and the Cherenkov photon path reconstructed inside the RICH as explained in Ref. [24]. Being based on the precise Forward Time-of-Flight system and

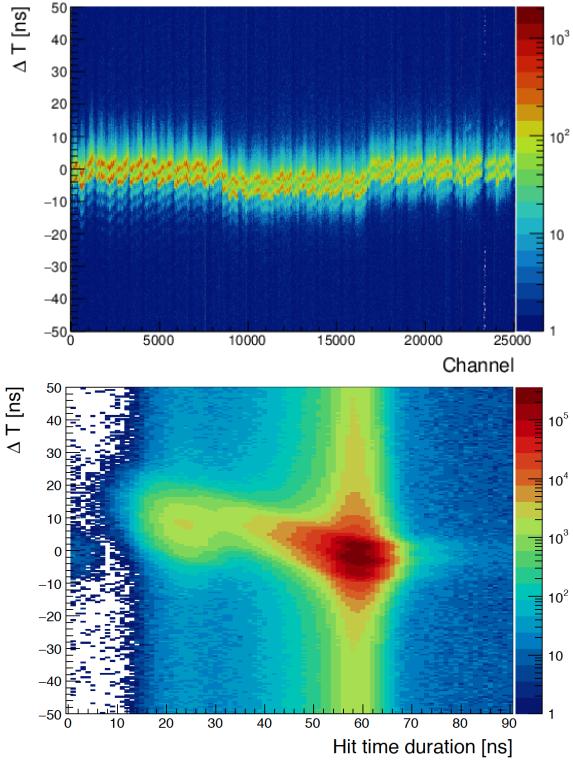


Figure 37: Top plot: distribution of the time difference ΔT between the measured RICH and calculated CLAS12 times as a function of the RICH readout channel. Bottom plot: cumulative distribution of the time difference ΔT as a function of the hit duration time (ToT).

the accelerator RF frequency, the CLAS computed time features a time resolution of the order of 100 ps, significantly better than RICH. The CLAS computed time can therefore be used as a reference for the RICH time calibration.

With respect to the expected time resolution, significant channel-by-channel variations are found in the difference between the measured and the calculated times as shown in the top plot of Fig. 37, where the distributions of $\Delta T = T_1 - T_{\text{calc}}$ as a function of the channel number is shown. These variations are introduced by the readout chain, with the biggest contribution coming from the average length of the 3 optical DAQ fiber trunks and from the specific length of the various fibers in each trunk. Smaller variations among the individual channels of one board can also occur due to the different circuit routing and components. An additional overall time constant is expected from the relative calibration of the RICH with respect to the rest of the CLAS12 detectors.

A broadening of the ΔT distributions is due to the time walk, i.e. the dependence of the trailing edge time on the amplitude of the input signal. Since the MAROC3 readout mostly works in the saturated regime already at the SPE level, this effect is expected to be relevant for small amplitude signals, as can be seen from the bottom plot of Fig. 37. Saturated signals have typical ToT values on the order of 60 ns, while small amplitude signals are expected to be discriminated up to several ns later. The vertical band at ToT ≈ 60 ns comprises a distribution of

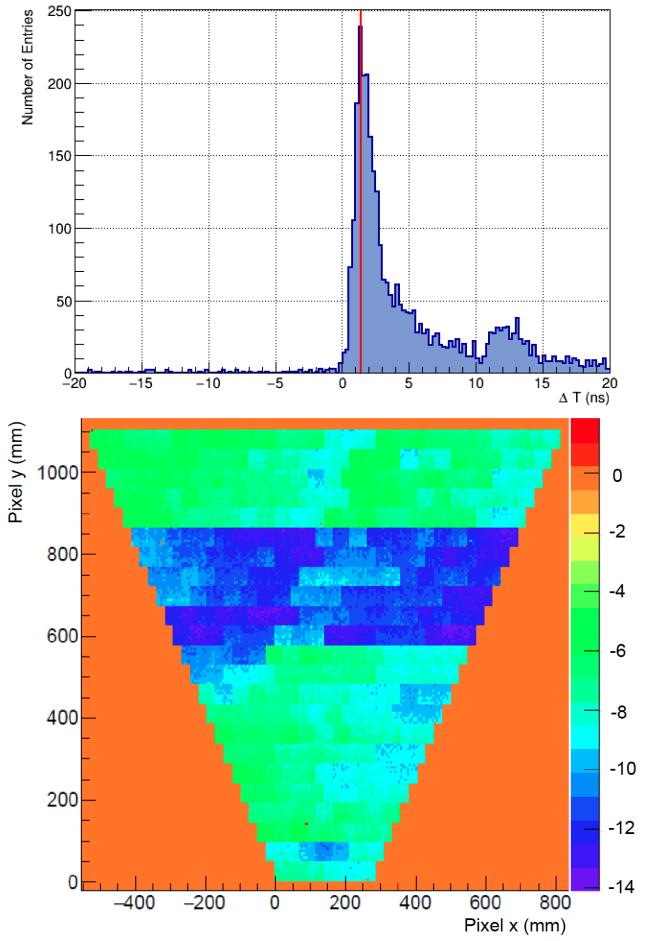


Figure 38: Top plot: ΔT distribution for one readout channel; the red line indicates the time offset value. Bottom plot: typical map of the time offsets.

random-time PMT dark counts and off-time beam bunches. The independent excess around $\text{ToT} \approx 25$ ns signals a residual contamination of cross-talk pulses anticipated in Sec. 8.

A two step calibration procedure was implemented in order to align the time measured by all RICH readout channels with the expected (calculated) one. The current version of the software uses electrons and charged pions identified in CLAS12 with momenta larger than 2.5 GeV and Cherenkov photons reconstructed in the RICH with no reflections on the mirrors.

The first step of the procedure consists in the evaluation of the 25024 time offset corrections. The values of ΔT are plotted for each channel and the position of the maximum is taken as the time offset for that channel. The top plot of Fig. 38 shows a typical ΔT distribution, with a pronounced peak, a broad tail due to the time walk, and a small enhancement above ≈ 10 ns most likely due to residual cross-talk hits. The vertical line indicates the adopted value for the time offset correction. The bottom plot of Fig. 38 shows a typical map of the time offsets. Three regions of comparable values are highlighted, corresponding to the tiles connected to the 3 optical fiber trunks, on top of smaller channel-by-channel variations.

Once the individual channels were corrected for the time

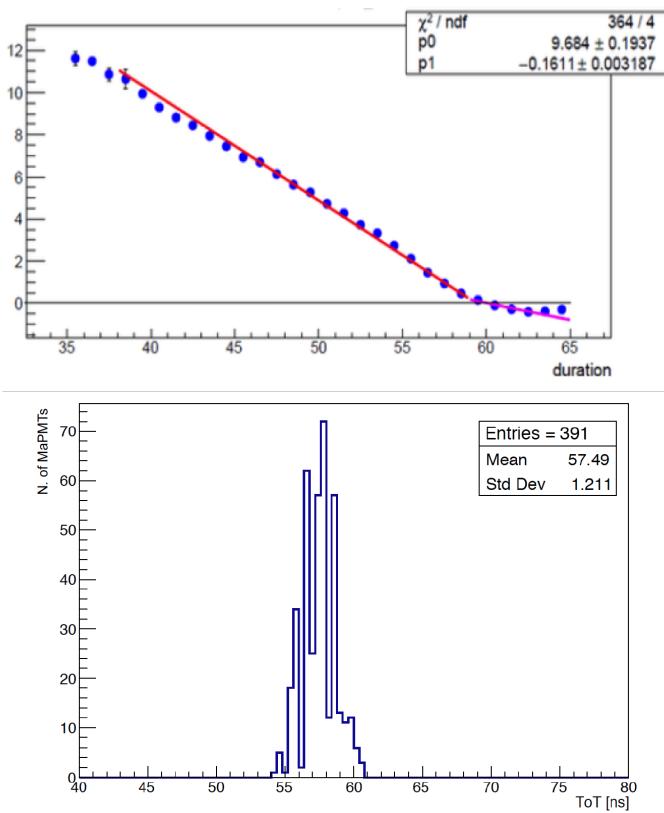


Figure 39: Top plot: fit of the time-walk correction for one MaPMT. Bottom plot: distribution of the ToT saturation values extracted from the time-walk correction.

offsets, the time-walk corrections were extracted from the ΔT distribution as a function of ToT. Since the threshold level is common to all channels of one MAROC3 chip, and the amplitude equalization has been performed, one expects that the same time-walk correction should work for all channels of one MaPMT. This was verified by comparing plots like the one shown in the bottom plot of Fig. 37 for all channels of the MaPMTs. A set of 391 time-walk correction functions, one per MaPMT, is therefore extracted by fitting the dependence of ΔT as a function of ToT, as shown in the top plot of the Fig. 39. The dependence is fit with two lines, one for the saturated regime and one for the linear region. The free parameters of the fit are the two slopes, the ToT value where the two lines cross, i.e. the saturation ToT, and the ΔT at zero ToT. The data show small deviations from the linear behavior, however such a simple functional form was adopted to minimize the probability of fit failure (having to deal with several hundreds of fits) and because it was proven to be enough to achieve time resolutions that meet the specifications. In the bottom plot of Fig. 39, a typical distribution of the saturation ToT values obtained from the fit is shown. The average value is around 57 ns with small variation from MaPMT to MaPMT.

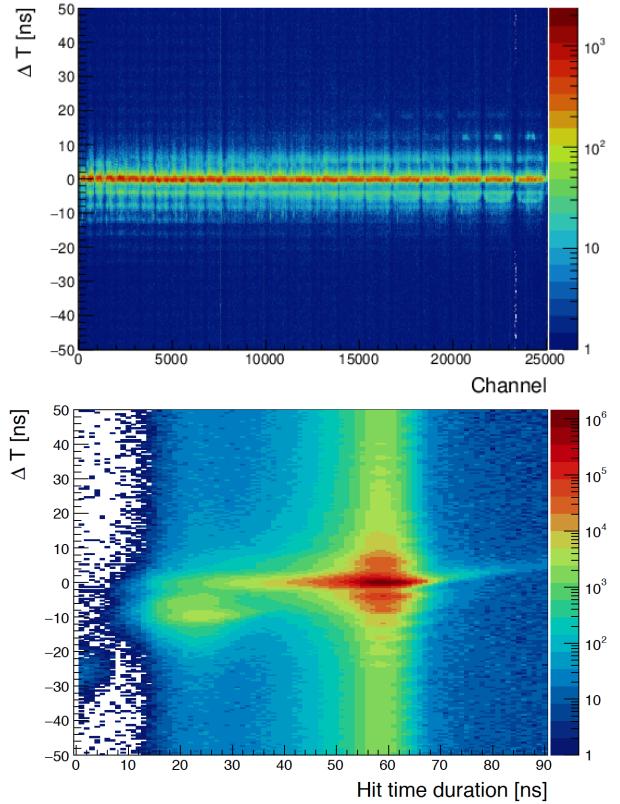


Figure 40: Distribution of the time difference ΔT between the measured RICH and extrapolated CLAS12 times after the time calibration. On the top as a function of the readout channel; on bottom as a function of the signal amplitude ToT.

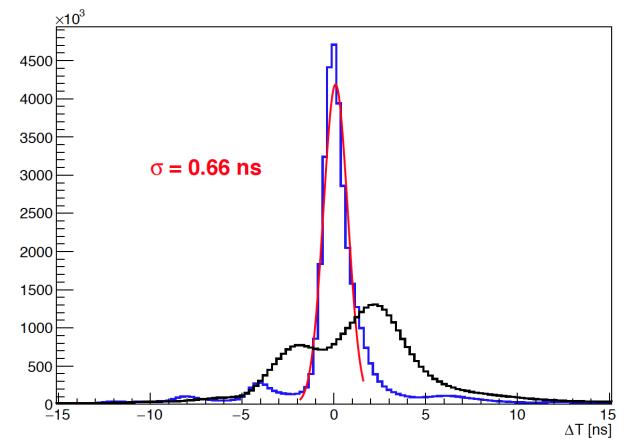


Figure 41: Typical ΔT distribution before (black) and after (blue) the time-walk correction for all the RICH pixels. The red line is a Gaussian fit of the corrected distribution, with a global 0.66 ns RMS.

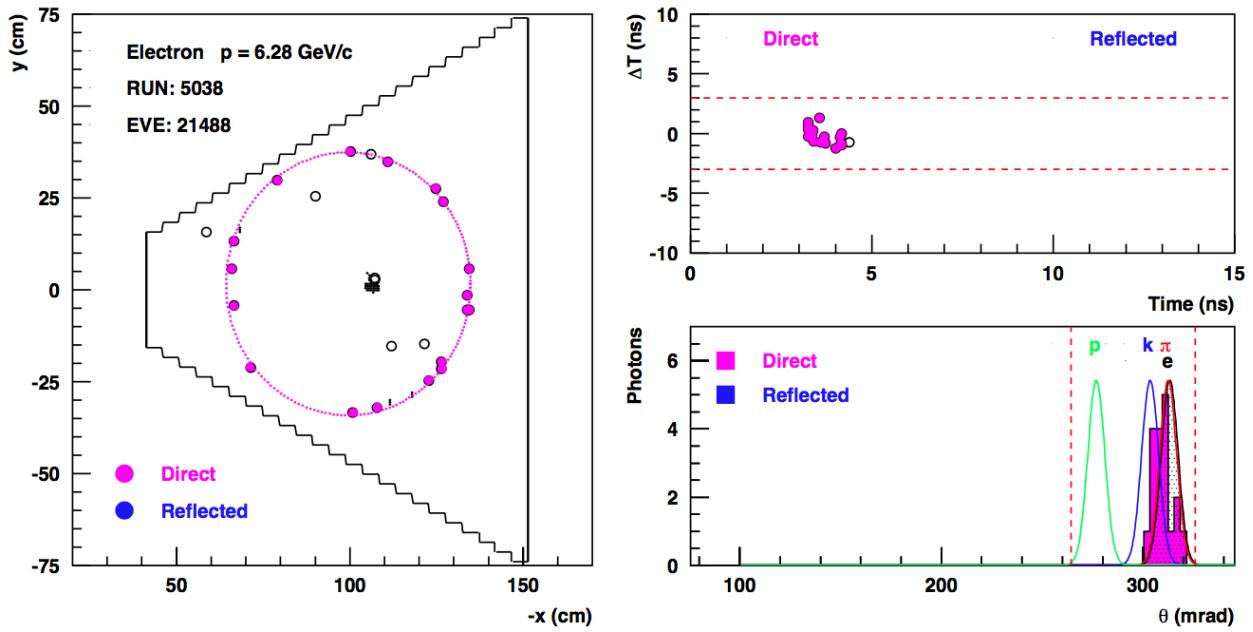


Figure 42: Example of a reconstructed RICH event with only direct photons.

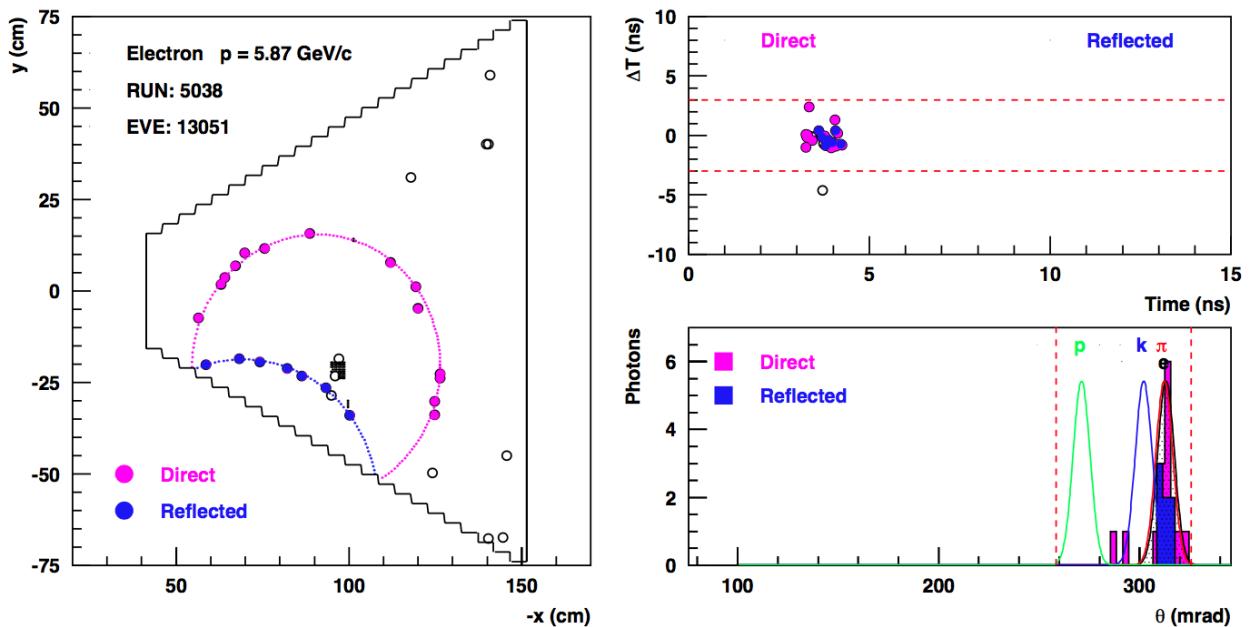


Figure 43: Example of a reconstructed RICH event with a partial ring reflected by the lateral flat mirror.

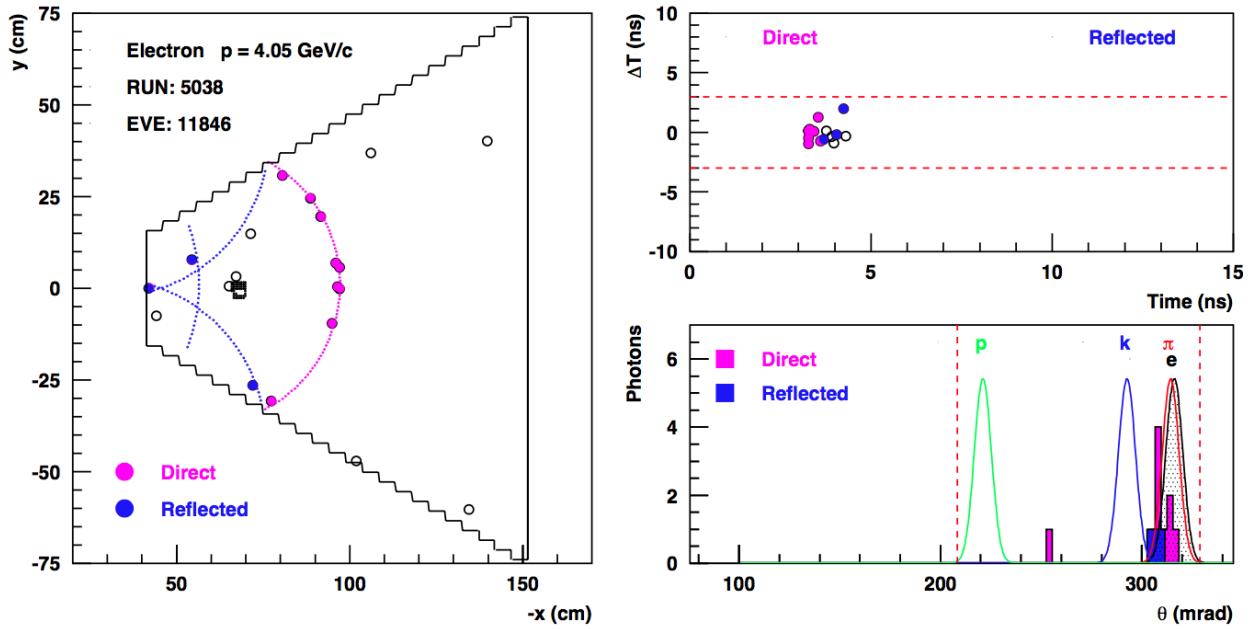


Figure 44: Example of a reconstructed RICH event with photons reflected by all the lateral mirrors.

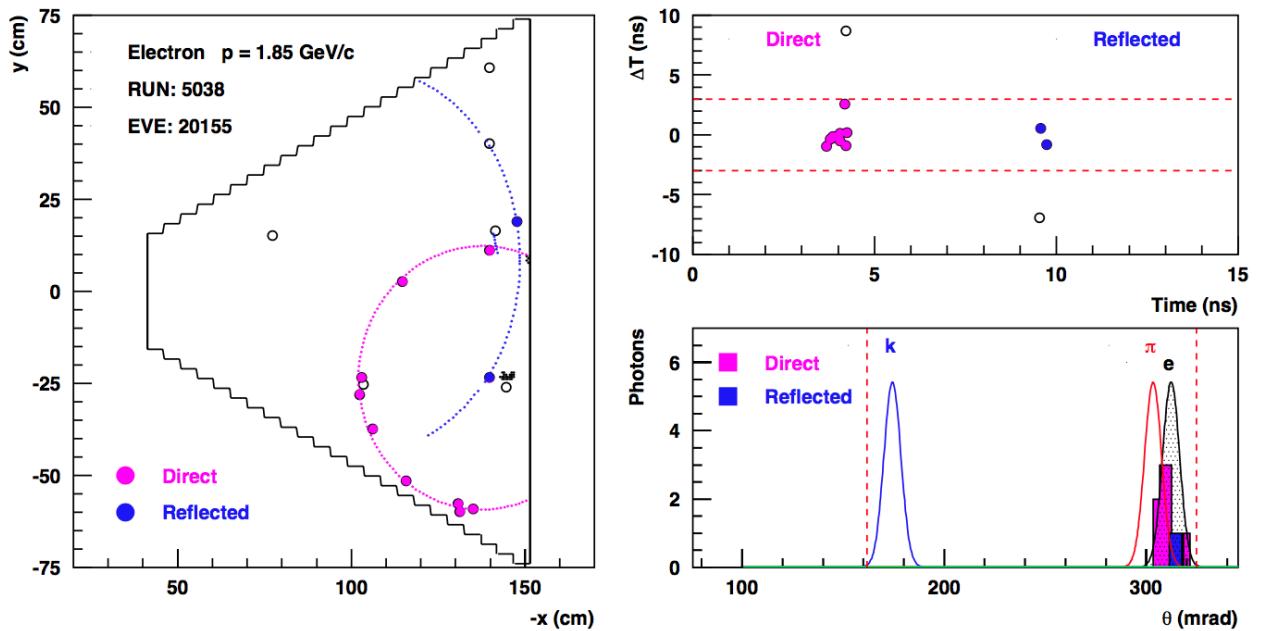


Figure 45: Example of a reconstructed RICH event with a partial ring reflected back by the spherical mirror and passing twice the aerogel layer.

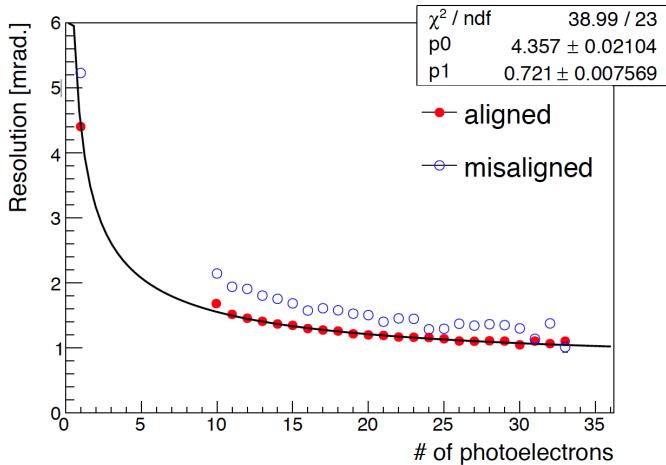


Figure 46: RICH Cherenkov resolution before (open points) and after (close points) a preliminary RICH alignment. The whole RICH detector is aligned minimizing the matching distance between RICH clusters and extrapolated DC tracks. No possible misalignment of the single RICH component is accounted for. The distribution is for particles passing through one aerogel tile of 2 cm thickness (tile 12 in layer 1) and for direct photons.

After calibration, the corrected ΔT distribution is centered at zero for all channels, see Fig. 40. As a consequence, a few ns time coincidence can be applied to remove the spurious hits. As shown in the bottom panel of Fig. 40, the cross-talk hits at $ToT \approx 25$ ns and the 4 ns sub-structure of the off-time beam bunches at $ToT \approx 60$ ns become clearly visible. A typical ΔT distribution is shown for one MaPMT in Fig. 41, where the red and black histograms show the ΔT values before and after the correction, respectively. The red curve is a Gaussian fit of the corrected distribution. On average, we obtained a time resolution $\langle \sigma \rangle \approx 0.7$ ns, well below the requirement of 1 ns.

10. RICH Hadron Separation

The RICH has been designed to provide hadron identification in the 3 - 8 GeV momentum range. The most challenging separation is between kaons and pions, as their Cherenkov angles become closer and closer with the increase of momentum until a minimum difference of 6 mrad at 8 GeV. In addition, in this momentum range the pion yield is more than an order of magnitude larger than for the other hadron species.

Various ring imaging topologies are possible due to the unconventional RICH geometry. These topologies are generated by direct photons in proximity focusing and by reflected photons in mirror focusing geometries. In the momentum range of interest (between 3 GeV and 8 GeV), electrons can be used for a detailed optimization of the RICH performance since, being in a saturated regime, their Cherenkov angles are indistinguishable from those of pions. The work is still ongoing to make use of the large recorded electron statistics.

Examples of reconstructed RICH events are shown in Figs. 42 to 45 for particles identified as electrons by CLAS12. In each figure, the reconstructed RICH event is displayed on the left. The ray-tracing approach allows, for each particle

hypothesis, to anticipate the expected photon pattern and the associated hits on the photodetectors, indicated by the small dots in the figures. The measured RICH hits are shown as open circles, whereas the reconstructed photon hits are shown as the full circles. Direct and reflected photons are indicated in magenta and blue, respectively. A remarkable feature of the RICH detector is the low level of spurious hits from accidentals, in-time background (i.e. Rayleigh scattering), and dark counts. This feature is crucial for the most challenging cases: particles with high momenta close to the 8 GeV limit that require the best resolution in Cherenkov angle, and particles pointing towards the spherical mirror whose number of detected photons is limited by the double reflection and a second passage through the radiator.

For each event, the details of the time and Cherenkov angle reconstruction are shown on the right. On the top panel, the time coincidence ΔT between the RICH measured hit and the CLAS12 calculated time is displayed as a function of the photon flight time within the RICH (photon transit time). The time coincidence ΔT should be close to zero for any true photon path. As a consequence, a valid photon reconstruction is initially selected by requiring $\Delta T < 3$ ns, indicated by the horizontal dashed lines. The path length is represented by the photon transit time inside the RICH, from the emission point within the aerogel to the detection point in the MaPMT plane after all possible reflections. Photons reflected by the spherical mirror and directed back to the aerogel travel twice the gap, with an expected significant increase of path length and a corresponding distinctive ≈ 6 ns longer transit time.

In the bottom panel, the measured angles are compared to the expected distributions for different particle hypotheses. The width of each distribution corresponds to the expected SPE angular resolution, while the average value depends on the particle type and momentum. An acceptance range is defined from the smallest angle expected for a proton to the largest angle expected for an electron, enlarged by three times the expected angular resolution. For the latter, a conservative value of 6 mrad is taken for the single photon case. These limits are indicated by the vertical dashed lines.

For each reconstructed photon path an estimate of the corresponding Cherenkov angle is obtained and histogrammed on the plot. In all cases studied, both reflected and direct photon information is consistent with the electron hypothesis. In particular, the reconstructed reflected and direct photon paths with ΔT close to zero provide Cherenkov angle values consistent with an electron, as expected. The narrow distribution of the measured angle values indicate that kaons can clearly be separated up to momenta greater than 6 GeV. Electrons can be distinguished from pions only at low momenta, below 2 GeV.

Each aerogel tile presents specific features because of the challenging production process, tuned to achieve the highest transparency over a large volume, is not fully industrialized. The most important quality parameters are the density, related to the average refractive index, homogeneity, related to the refractive index variations within the volume, and tile bending, originated by the inner material tension and related to the surface planarity. The effect of these features on the RICH

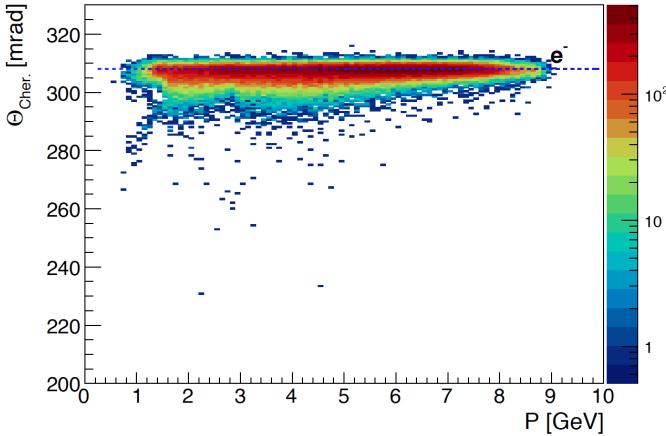


Figure 47: RICH response for electrons as identified by CLAS12. As expected, the measured Cherenkov angle is saturated over the whole momentum range, from 3 GeV up to 8 GeV. The distribution is for particles passing through one aerogel tile of 2 cm thickness (tile 12 in layer 1) and direct photons.

photon reconstruction can be studied in detail using the control sample of electrons identified by CLAS12. Given the large number of tiles and the broad range of particle directions after the CLAS12 bending magnets, such a study requires large statistics and is still ongoing. A similar approach is used for the alignment study. Also in this case, large statistics is needed due to the numerous involved components (aerogel layers, mirrors, and MaPMT plane) and photon path configurations.

As a general approach, the RICH performance is studied separately for each aerogel tile. The RICH global performance estimators are then defined by averaging the results over all the radiator tiles. Despite the fact that the above studies have not yet been finalized, and only partial corrections have been implemented so far, the preliminary SPE Cherenkov angle resolution yields typical values around 6 mrad. It is expected to improve towards the goal value of 4.5 mrad once the corrections for the detector misalignment are implemented and the realistic optical parameters of each aerogel tile are taken into account. As an example, the effect of a preliminary alignment of the whole RICH detector is shown for one aerogel tile in Fig. 46. After alignment, the resolution improve towards the TDR projected values, that are 4.5 mrad for single photon detection and 1.5 mrad for the average over all the photons associated with the hadron track. Such preliminary Cherenkov angle resolution is already sufficient for an effective hadron separation in the goal range of momenta, from 3 to 8 GeV, as shown by Figs. 47 to 49.

11. Conclusions

A RICH detector has been designed to enhance the hadron identification capability at CLAS12 in the 3 to 8 GeV momentum range. It substitutes the baseline gas threshold Cherenkov detector in two of the CLAS12 sectors, to create a symmetric left-right setup optimized for running with polarized targets. The first module was installed at the beginning of 2018, in

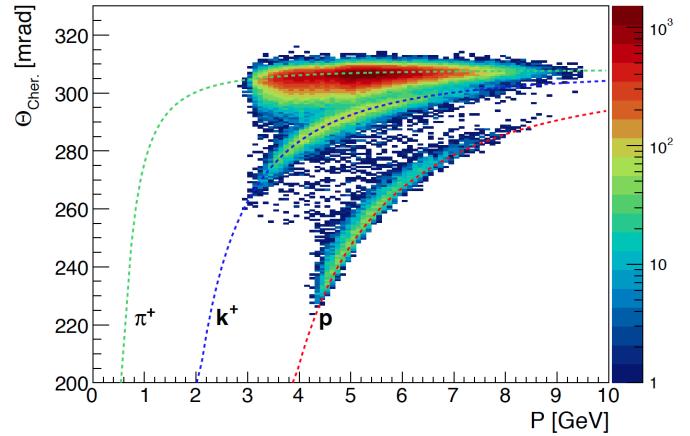


Figure 48: RICH response for non-electron particles as defined by CLAS12. The measured Cherenkov angles distribute around the expected values for pion, kaon, and proton hypotheses as a function of their momentum. The three hadron populations are separated over the whole momentum range, from 3 GeV up to 8 GeV. The distribution is for particles passing through one aerogel tile of 2 cm thickness (tile 12 in layer 1) and spanning the entire momentum range of interest for RICH.

time for the experiment data taking start. The second module is under construction and expected to be ready in the summer 2021, in time for the first run with polarized targets.

To efficiently cover the wanted few-GeV momentum range, the RICH employs innovative technological solutions. Among these, are composite aeronautic light-materials to ensure the needed mechanical structure rigidity, aerogel radiator of unprecedented large volume (up to $200 \times 200 \times 30$ mm³) and high transparency (≈ 50 mm scattering length), light (of the order of 1% of radiation length) mirrors made of carbon-fiber or, for the first time in a nuclear experiment, glass-skin technology, high-segmented and high-packed Hamamatsu H8500 and H12700 multi-anode photomultipliers. A compact and scalable readout electronics system has been realized for the detector, able to discriminate Cherenkov signals down to a as small as 1/32 fraction of the single photon amplitude, with excellent efficiency and stability, and a time resolution better than 1 ns.

The peculiar geometry of the CLAS12 sector suggested a innovative hybrid-optics solution to limit the active area to ≈ 1 square meter per sector, with part of the light directly imaged and part of the light focalized by mirrors. This and the bending into the torus field of the CLAS12 Forward Detector create a variety of possible topologies for the particle and photons paths. The RICH reconstruction exploits a ray-tracing algorithm to provide a Cherenkov angle estimation for each photon hit and hadron track in the event. This basic experimental information allows an independent development of higher-level PID algorithms with increasing sophistication.

Preliminary data analysis shows that the CLAS12 RICH is able to match the required time and Cherenkov angle resolutions. After calibration, each of the 25k channels features a time resolution of the order of 0.6 ns, better than the 1 ns specification. The high momentum particles define the most stringent requirements in performance. As the pion yield

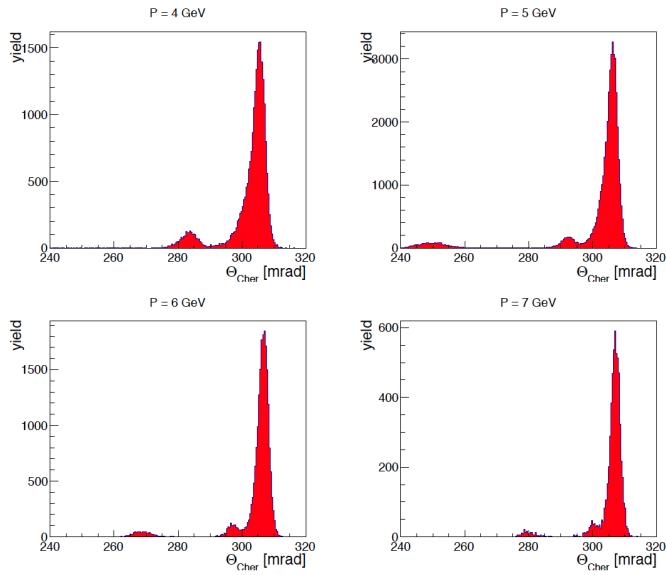


Figure 49: RICH response for non-electron particles in slices of momentum, from 4 GeV up to 7 GeV.

supersedes the other particles species by an order of magnitude, a 4σ angle separation is required to contain the contamination at the percent level. At 8 GeV, this implies an angle resolution of 1.5 mrad. Despite the detailed study of the alignment and optical performance of the various components is still ongoing, the detector has already demonstrated a single-photon angle resolution better than 5 mrad and an average number of 19 photons per charged particle in the forward high-momentum direction, in line with the TDR projections. This reflects in an angle resolution per charged particle close to the design value of 1.5 mrad and an effective hadron identification capability in the whole required momentum range.

12. Acknowledgments

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