3.72

Find the Norton equivalent circuit of the circuit in Fig. P3.71 after increasing the magnitude of the voltage source to $38\ V$.

✓ Answer ∨

With i_1 as the bottom left loop, i_2 as the top loop, i_3 as the center bottom loop, and i_4 is the encircling loop, and i_5 the short-loop when ab is shorted, all clockwise.

$$egin{bmatrix} 14 & -10 & -4 & 0 \ -10 & 35 & -20 & 5 \ -4 & -20 & 24 & 0 \ 0 & 5 & 0 & 13 \end{bmatrix} egin{bmatrix} i_1 \ i_2 \ -2i_1 + 2i_2 \ i_4 \end{bmatrix} = egin{bmatrix} 38 \ 0 \ v_3 \ 38 \end{bmatrix}$$

$$I = egin{bmatrix} -rac{19}{14} \ -rac{475}{126} \ -rac{304}{63} \ rac{551}{126} \end{bmatrix}$$
 $V = egin{bmatrix} 38 \ 0 \ -rac{2204}{63} \ 38 \end{bmatrix}$

This makes the voltage across a and b: $\frac{2204}{63}$ V

$$egin{bmatrix} 14 & -10 & -4 & 0 & 0 \ -10 & 35 & -20 & 5 & 0 \ -4 & -20 & 24 & 0 & 0 \ 0 & 5 & 0 & 13 & -8 \ 0 & 0 & 0 & -8 & 10 \end{bmatrix} egin{bmatrix} i_1 \ i_2 \ -2i_1 + 2i_2 \ i_4 \ i_5 \end{bmatrix} = egin{bmatrix} 38 \ 0 \ v_3 \ 38 \ 0 \end{bmatrix}$$

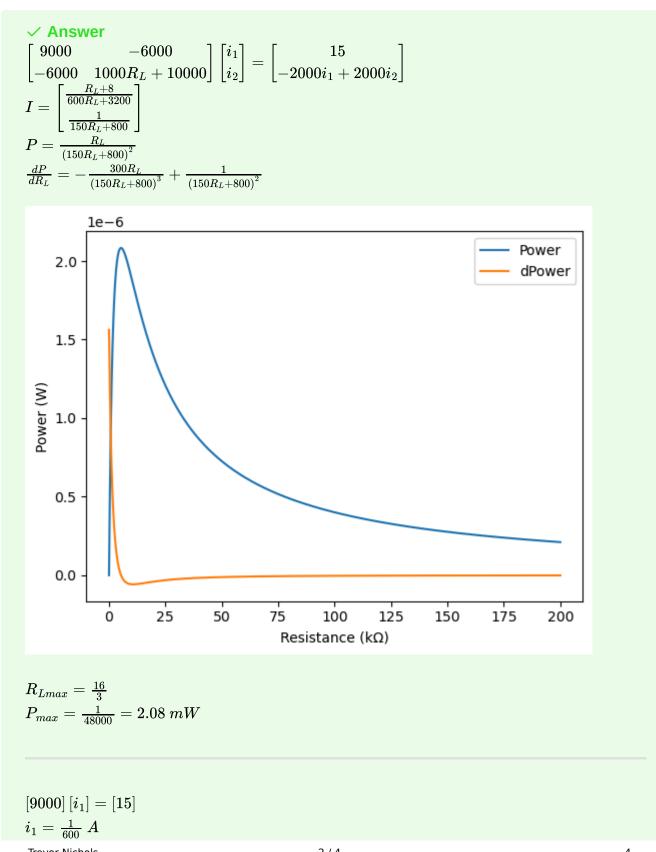
$$I = egin{bmatrix} -rac{703}{286} \ -rac{133}{26} \ -rac{760}{143} \ rac{2755}{286} \ rac{1102}{143} \end{bmatrix}$$
 $V = egin{bmatrix} 38 \ 0 \ -rac{2204}{143} \ 38 \ 0 \end{bmatrix}$

This makes our current across a and b: $\frac{1102}{143}$ A

We can then calculate our Norton equivalent: $R_N=rac{286}{63}~\Omega$ and $I_N=rac{1102}{143}~A$

3.83

Determine the maximum power that can be extracted by the load resistor from the circuit in Fig. P3.83.



$$egin{align} V_{Th} &= (6000-2000)i_1 = rac{20}{3} \ V \ &egin{align} 9000 & -6000 \ -6000 & 1000R_L + 10000 \end{bmatrix} egin{bmatrix} i_1 \ i_2 \end{bmatrix} = egin{bmatrix} 15 \ -2000i_1 + 2000i_2 \end{bmatrix} \ I_N &= i_2 = rac{1}{800} \ &rac{V_{Th}I_N}{4} = rac{1}{480} \ W &= 2.08 \ mW \end{aligned}$$

4.6

The inverting-amplifier circuit shown in Fig. P4.6 uses a resistor R_f to provide feedback from the output terminal to the inverting-input terminal.

b

Determine the value of G for $R_s=10\Omega$, $R_i=10~M\Omega$, $R_f=1~k\Omega$, $R_o=50\Omega$, $R_L=1k\Omega$, and $A=10^6$.

$$\begin{bmatrix} R_i + R_s & -R_s & 0 \\ -R_s & R_f + R_l + R_s & -R_l \\ 0 & -R_l & R_l + R_o \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \\ i_3 \end{bmatrix} = \begin{bmatrix} -V_s \\ V_s \\ -AR_i i_1 \end{bmatrix}$$

$$I = \begin{bmatrix} \frac{-R_f R_l V_s - R_f R_o V_s - R_l R_o V_s}{AR_i R_l R_s + R_f R_i R_l + R_f R_i R_o + R_f R_l R_s + R_f R_o R_s + R_l R_l R_o + R_i R_l R_s + R_l R_o R_s + R_l R_o R_s} \\ \frac{AR_i R_l V_s + R_i R_l V_s + R_i R_o V_s}{AR_i R_l R_s + R_f R_i R_o + R_f R_l R_s + R_f R_o R_s + R_l R_o R_s + R_l R_o R_s + R_l R_o R_s} \\ \frac{AR_f R_l V_s + AR_i R_l V_s + R_i R_l V_s}{AR_i R_l R_s + R_f R_i R_o + R_f R_l R_s + R_f R_o R_s + R_l R_o R_s + R_l R_o R_s + R_l R_o R_s} \end{bmatrix}$$

$$G = 1000 \frac{R_i R_o - AR_f R_i}{AR_i R_l R_s + R_f R_i R_l + R_f R_i R_o + R_f R_l R_s + R_f R_o R_s + R_l R_o$$

C

Simplify the expression for G obtained in (a) by letting $A \to \infty$, $R_i \to \infty$, and $R_o \to 0$ (ideal op-amp model).

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d

Evaluate the approximate expression obtained in (c) and compare the result with the value obtained in (b).

✓ Answer

They are very close, to the point of error.

3.93

Obtain an expression for V_{out} in terms of V_{in} for the common emitter-amplifier circuit in Fig. P3.93 . Assume $V_{in}\gg V_{BE}$.

✓ Answer

Current through the battery: I

$$I_{R_E} = (1+eta)I$$

$$I_{R_L} o eta I$$

We assume $\beta\gg 1$

Thus,
$$V_{R_s} pprox 0$$

Thus,
$$V_{R_E} = V_{in}$$

$$I_{R_E}pproxeta I=I_{R_L}$$

$$V_{R_E} = I_{R_L} R_E = V_{in}$$

$$V_{out} = V_{R_L} = I_{R_L} R_L = rac{V_{in} R_L}{R_E}$$

$$V_{out} = rac{V_{in}R_L}{R_E}$$

4.11

Determine the output voltage for the circuit in Fig. P4.11 and specify the linear range for v_s , given that $V_{cc}=15\ V$ and $V_0=0$.

✓ Answer

$$\frac{-V_s}{2k} + \frac{-V_o}{200k} =$$

$$V_o = -100V_s$$

$$G=-100~rac{V}{V}$$

$$V_{cc}=V_o$$

$$V_s = -rac{15}{100} = -0.15 \; V$$