□<u>PHYS115</u> □<u>PHYS121</u> □<u>PHYS123</u> □<u>PHYS116</u> □<u>PHYS122</u> □<u>PHYS124</u> <u>Lab Cover Letter</u>

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	ıch as #1: UNC) 4: RKE				
TA: _					
	GRADE (to be filled in by your TA) An 'x' next to a subcategory means you nee	See ed to	your impro	TA for detailed fove this aspect of	eedback. your work.
Paper	· Subtotals (points)	()	Discussion &	& Conclusions (6)
()	General (6) Sig. figs. Units Clarity of Presentation			Numerical comp Logical conclusion Discussion of po Suggestions to re	arison of results ons s. errors
	Format Abstract (4)	()	Paper Total (30 points fo	(60 points) or CME or EPF)
	Quantity or principle How measurement was made Numerical Results Conclusion	() —	Notebook (1 Format (proper	0 points) t style, following directions) t description of equipment,
() 	Intro & Theory (9) Basic principle Main equations to be used Apparatus What will be plotted	_		manually recor Experimental T	echnique (describing your ting & justifying uncerts.)
	Fitting parameters related Exp. Procedures (15)	(Re	_	Worksheet(s t (30 points) if)/Fill-in-the-Blank-
	Description Stating and justifying uncertainties Data Record Quality of Lab Work	()	•	s – late submissions, dures, etc. – or bonus points work.
()	Analysis & Error Analysis (20) Discussion Equations & Calculations	() Total (Grade
	Presentation inc. Graphs, Tables Results Reported & Reasonable Underlined items addressed	Gi	rade	ed by	(TA's initial)

1 Abstract

The purpose of this lab is to establish whether the formulas of inertia for point masses are consistent with both Monte-Carlo simulation data and experimental data.

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I_{Lpredicted} = 0.034~kgm^2 \ I_{L} = 0.02 \pm 0.01~kgm^2
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Our predicted values for inertia and the experimental values do line up fairly well, and thus is insufficient to reject the theoretical values of inertia for point masses.

Additional sources of error could be inaccuracy in measurement of the radius of the masses, additional friction in the system, inertia and drag of the flywheel, and the masses not truly being point masses.

2 Theory

2.1 Variables

2.1.1 Constants

```
egin{aligned} \Delta S &= 0.015 \ m \ R_{wheel} &= 0.200 \pm 0.002 \ m \ m_w &= 1.5 \ kg \ m_h &= 0.060 \ kg \ m_L &= 0.9223 \pm 0.0001 \ kg \ r &= 0.1845 \pm 0.0005 \ m \end{aligned}
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2.1.2 Measured Values

2.1.2.1 Simulated

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\delta_{\Delta T} = 0.0002 y_L(t): Position as a function of time
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2.1.2.2 Experimentally

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\delta_{\Delta T}=0.00005 y_W(t): Position as a function of time y_{W+L}(t): Position as a function of time
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2.2 Formulae

2.2.1 Calculation of velocity and position and expected inertia

$$egin{aligned} y &= i\Delta S \ v &= rac{\Delta S}{\Delta T} \ I &= mr^2 \ \delta_I &= \sqrt{\left(\delta_m r^2
ight)^2 + \left(\delta_r 2mr
ight)^2} \end{aligned}$$

2.2.2 Uncertainty in velocity squared

 $\delta_{v^2}=\delta_{v^2\Delta T}$ as ΔS has negligible variance $=2rac{\Delta S^2}{\Delta T^3}\delta_{\Delta T}$ from formula for velocity $=rac{2v^3}{\Delta S}\delta_{\Delta T}$

2.2.3 Measurement of Inertia

Separation of weights $\Delta U_W = \Delta U_{M_h} + \Delta U_{m_h}$ Conservation of energy $\Delta U_W + K_t + K_r - W_f = 0$ Cancellation of friction $\Delta U_{M_h} + K_t + K_r = 0$ $M_h gy = \frac{1}{2} M_h v^2 + \frac{1}{2} I \omega^2$ $M_h gy = \frac{1}{2} \left(M_h + \frac{I}{r^2} \right) v^2$ Measurable values vs. constants and Intertia $\frac{v^2}{y} = \frac{2g}{\left(1 + \frac{I}{M_h r^2}\right)}$ Intertia $I = M_h r^2 \left(\frac{2g}{\frac{v^2}{y}} - 1\right)$

2.2.4 Difference in Inertia for experimental setup

$$I = M_h r^2 \left(rac{2g}{rac{v^2}{y}} - 1
ight)$$
 Inertia of just the wheel $I_W = M_h r^2 \left(rac{2g}{rac{v_W^2}{y_W}} - 1
ight)$ Inertia of the wheel and weights $I_{W+L} = M_h r^2 \left(rac{2g}{rac{v_{W+L}^2}{y_{W+L}}} - 1
ight)$ Inertia of the weights $I_L = 2gM_h r^2 \left(rac{1}{rac{v_{W+L}^2}{y_{W+L}}} - rac{1}{rac{v_W^2}{y_W}}
ight)$

2.2.5 Uncertainty in Inertia of weights

$$\begin{array}{ll} \text{Initial Equation} & I_L = 2gM_h r^2 \left(\frac{1}{\frac{v_{W+L}^2}{y_{W+L}}} - \frac{1}{\frac{v_W^2}{y_W}} \right) \end{array} \\ \text{Combination of sources of variance} & \delta_{I_L} = \sqrt{\delta_{I_L r}^2 + \delta_{I_L \frac{v_{W+L}^2}{y_{W+L}}}^2 + \delta_{I_L \frac{v_W^2}{y_W}}^2} \\ \text{Let} & b_{W+L} = \frac{v_{W+L}^2}{y_{W+L}} \end{array} \\ \text{Let} & b_W = \frac{v_W^2}{y_W} \end{array}$$

Combination of sources of variance:

$$egin{split} \delta_{I_L} &= \sqrt{\left(\delta_r 4g M_h r \left(b_{W+L}^{-1} - b_W^{-1}
ight)
ight)^2 + \left(\delta_{b_{W+L}} 2g M_h r^2 b_{W+L}^{-2}
ight)^2 + \left(\delta_{b_W} 2g M_h r^2 b_W^{-2}
ight)^2} \ \delta_{I_L} &= 2g M_h r \sqrt{\left(2\delta_r \left(b_{W+L}^{-1} - b_W^{-1}
ight)
ight)^2 + \left(\delta_{b_{W+L}} r b_{W+L}^{-2}
ight)^2 + \left(\delta_{b_W} r b_W^{-2}
ight)^2} \end{split}$$

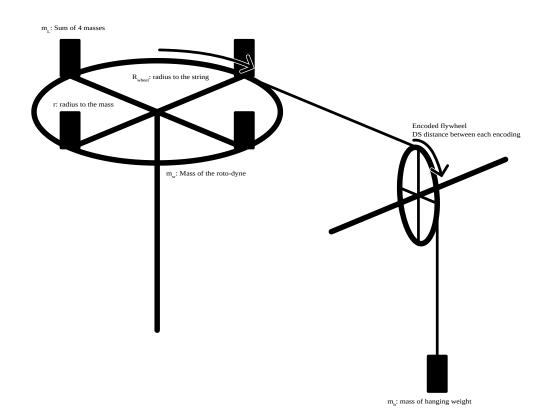
2.2.6 Uncertainty in Inertia of weights for MC

Let
$$b = \frac{v^2}{u}$$

Combination of sources of variance:

$$egin{aligned} \delta_{I_L} &= \sqrt{\left(\delta_r 4g M_h r \left(b^{-1}-1
ight)
ight)^2 + \left(\delta_b 2g M_h r^2 b^{-2}
ight)^2} \ \delta_{I_L} &= 2g M_h r \sqrt{\left(2\delta_r \left(b^{-1}-1
ight)
ight)^2 + \left(\delta_b r b^{-2}
ight)^2} \end{aligned}$$

3 Procedure



- 1. Set up the diagram above without the 4 masses on the roto-dyne or the hanging weight
- Add paperclips to the end of the string until the system is in equilibrium moving downward, this is to account for the friction in the system
- 3. Add the mass of m_h to the end of the string
- 4. Release the mass and record the data as it falls with the encoded flywheel
- 5. Reset the system and add the 4 masses to the roto-dyne
- 6. Release the mass and record the data as it falls with the encoded flywheel

4 Analysis

4.1 Monte Carlo Pre-setup

- 1. Estimate the inertia of the roto-dyne
- 2. Use seed data to generate the data

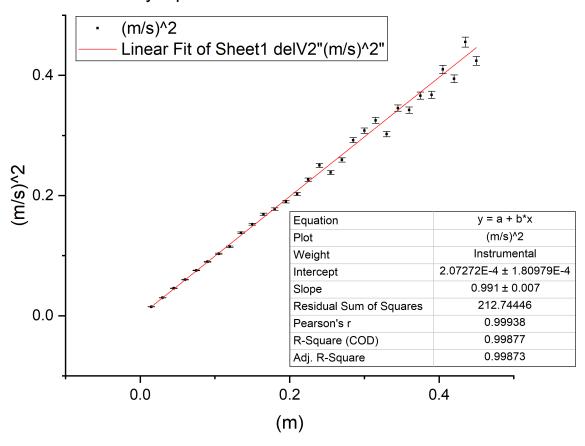
$$I_{predicted}=rac{3}{4}MR^2=0.045~kgm^2 \ {
m Seed}=0201$$

4.2 Analysis

- 1. After collecting all the data, we first derived the velocity and position through the formulae derived in section 2.2.1.
- 2. Then we calculated the variance in v^2 by the formulae given in section <u>2.2.2</u>.
- 3. We then graphed a position vs. velocity squared graph and used linear regression to obtain the slope with its uncertainty in *Origin*
- 4. From that, we obtained our estimated Inertia of the weights through the formulae given in sections <u>2.2.4</u> and <u>2.2.3</u> for the experimental and Monte-Carlo data respectively
- 5. We also calculate the variance in the Inertia value via the formulae in sections $\underline{2.2.5}$ and $\underline{2.2.6}$.
- 6. Then we compared our found inertia value with the expected value calculated by the formula given in section $\underline{2.2.1}$

4.3 Monte Carlo

MC velocity squared vs distance - Kat and Trevor

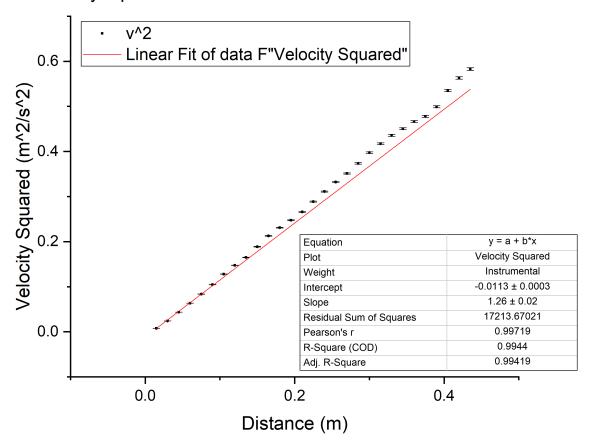


$$b = 0.991 \pm 0.007 \ rac{m}{s^2} \ I = 0.4512 \pm 0.0003 \ kgm^2$$

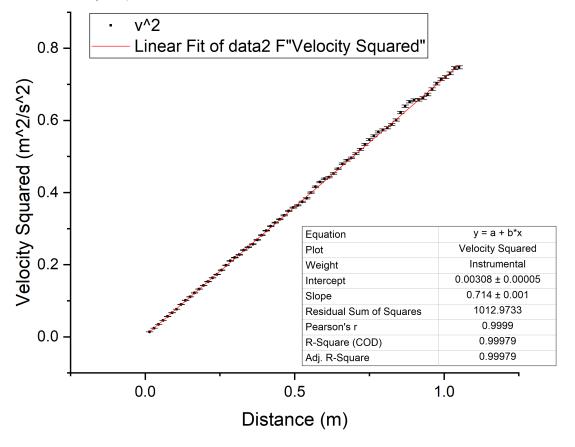
We found our experimental inertia to be within 3 SD of the predicted value. Additional variance is due to a large spread chosen for the random number generation.

4.4 Experimental

velocity squared vs distance without masses - Kat and Trevor



velocity squared vs distance with masses - Kat and Trevor



$$egin{aligned} b_W &= 1.26 \pm 0.02 \; rac{m}{s^2} \ b_{W+L} &= 0.714 \pm 0.001 \; rac{m}{s^2} \ I_L &= 0.02 \pm 0.01 \; kgm^2 \ I_{Lpredicted} &= 0.034 \; kgm^2 \end{aligned}$$

Our experimental finding is within 1.5 SD of the predicted value.

5 Conclusion

We concluded that our experimental data is consistent with the theoretical values of inertia for point masses. Our experimental values landed within 1.5 SD of the predicted value. Additional variance could be explained by inaccuracy in measurement of the radius of the masses, additional friction in the system, inertia and drag of the flywheel, and the masses not truly being point masses.

6 Acknowledgements and info

- Lab #5
- 27/03/2024
- Station 14 Rockefeller 404
- PHYS 121

Lab Partner: Katherine Chen

Lab Manual: Lab 5 RKE PHYS 121